PRELIMINARY HYDROLOGY STUDY

PREPARED FOR:

Pegasus Architects
Rabih Sater
4300 Edison Ave
Chino, CA 91710

FOR THE PROJECT:

Iris Ave and Oliver St Commercial Development
MORENO VALLEY, CA

PREPARED BY:

BLUE ENGINEERING AND CONSULTING, INC
9320 BASELINE RD., STE. D
RANCHO CUCAMONGA, CA 91702
(909) 248-6557

PREPARED UNDER THE SUPERVISION OF:

ANGEL CESAR, RCE 87222

December, 2022

INDEX:

INDEX 1

VICINITY MAP 2

INTRODUCTION 3

RESULTS 4-6

CONCLUSION 7

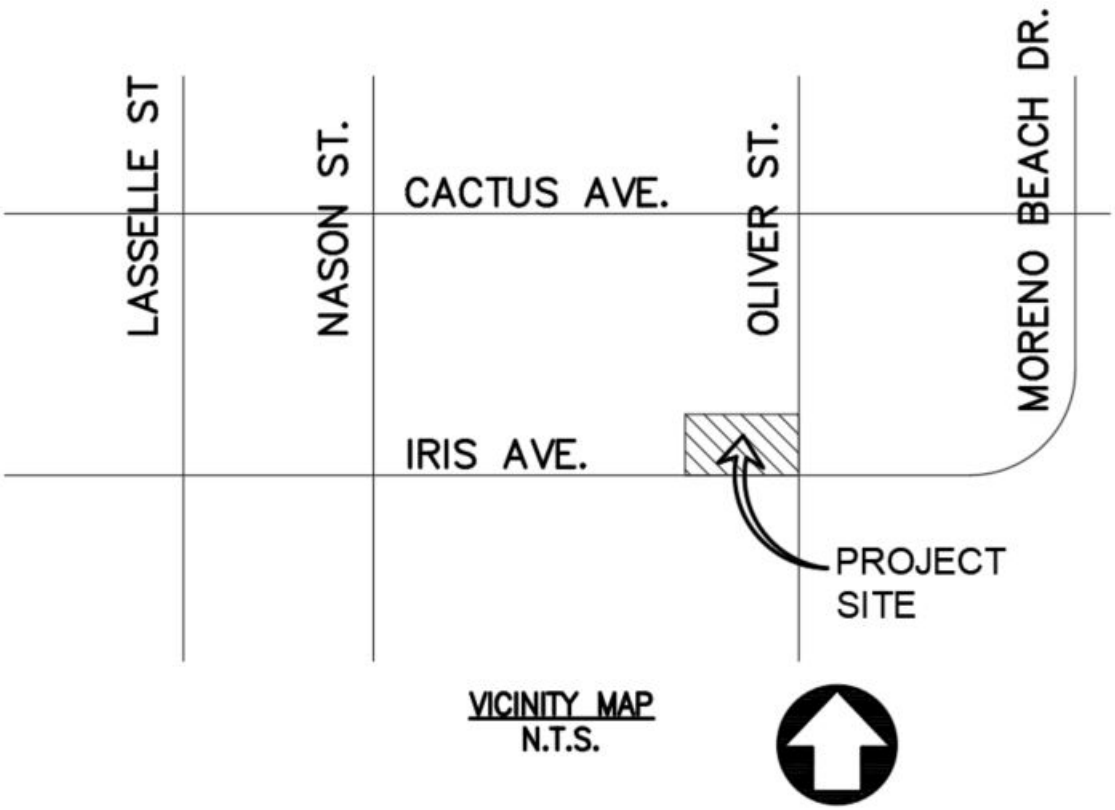
SOILS REPORT 8

HYDROLOGY MAP 9

- Pre-Development Exhibit
- Post Development Exhibit

Hydrology Calculations 10

- Precipitation Frequency Chart & Curves
- Rational Method Hydrology 10 yr. Pre-Development
- Rational Method Hydrology 10 yr. Pre-Development Off-site 1 & 2
- Rational Method Hydrology 100 yr. Pre-Development
- Rational Method Hydrology 100 yr. Pre-Development Off-site 1 & 2
- Rational Method Hydrology 10 yr. Post-Development
- Rational Method Hydrology 10 yr. Post-Development Off-site 1 & 2
- Rational Method Hydrology 100 yr. Post-Development
- Rational Method Hydrology 100 yr. Post-Development Off-site 1 & 2
- Synthetic Unit Hydrology 10 yr. 1 hr.
- Synthetic Unit Hydrology 10 yr. 3 hr.
- Synthetic Unit Hydrology 10 yr. 6 hr.
- Synthetic Unit Hydrology 10 yr. 24 hr.
- Synthetic Unit Hydrology 100 yr. 1 hr.
- Synthetic Unit Hydrology 100 yr. 3 hr.
- Synthetic Unit Hydrology 100 yr. 6 hr.
- Synthetic Unit Hydrology 100 yr. 24 hr.
- Flood Hydrograph Routing 10 yr. 1 hr.
- Flood Hydrograph Routing 10 yr. 3 hr.
- Flood Hydrograph Routing 10 yr. 6 hr.
- Flood Hydrograph Routing 10 yr. 24 hr.
- Flood Hydrograph Routing 100 yr. 1 hr.
- Flood Hydrograph Routing 100 yr. 3 hr.
- Flood Hydrograph Routing 100 yr. 6 hr.
- Flood Hydrograph Routing 100 yr. 24 hr.



VICINITY MAP
N.T.S.

I. INTRODUCTION

The project Iris Ave and Oliver St Commercial Development is an approximately 1.57 acres site located on the north side of Iris Avenue in the City of Moreno Valley, Riverside County, California (see attached vicinity map). The site is bordered to the south by Iris Ave, vacant lots to the west and north, and Oliver St to the east.

II. DESCRIPTION OF THE ONSITE CONDITIONS

The subject site consists of an almost square shaped parcel, approximately 1.57 acres in size. The site is currently undeveloped and appears to have been graded in the past. Ground surface cover consists of exposed soil and limited vegetation.

The site topography reveals a 4% slope from south to north. The highest point is along the southern property line closest to the southeast corner. The existing lowest point is along the northern property line, closest to the northwest corner. The existing site drains southeast to northwest towards the vacant lots next to the site.

The site will be developed into a commercial development. The site will contain two buildings footprint of approximately 7,344 square feet, as well as driveways, parking, and landscape areas. After the runoff is collected and treated in the proposed underground infiltration system located along the northwest property line and the maximum amount has been allowed to infiltrate, the remainder of runoff will be discharged to the adjacent development on the north. Once discharged, the flow will go West along Iris Avenue to Nancy St and then into a catch basin located at the cross-section of Iris Avenue and Grande Vista Dr, where they ultimately end up in the Perris Valley Storm Drain system.

III. OFFSITE HYDROLOGY

The project does not anticipate any off-site drainage draining onto the property. East and south property lines contain a fully developed road that carries water away from the project. On the north and west property lines, the project drains onto adjacent properties.

IV. ONSITE HYDROLOGY

The project is proposing to use one underground infiltration basin that will be located at the northwest corner of the project, to mitigate added flows generated by the additional impervious surface. No storm drain exists in Iris Avenue or Oliver St so to mitigate water will infiltrate into the ground any additional runoff will be discharged to the adjacent development on the north. Proposed storm drain laterals will collect water from the landscape swale. Proposed storm drain lines will run along the drive aisles and drain northwest toward the proposed underground chambers. Any remaining runoff will be discharge into the north development. The project will use minimal inlets and storm drainpipes where needed to

direct the flow to the basin. To calculate the flows that will be generated by the project site, CivilCADD/CivilDesign Engineering software, was used. The first step that was done was to run the Riverside County Rational Hydrology Program module for the existing and proposed drainage areas. The tables below summarize the calculations:

Table 1 Rational Method

Pre-Development Calculations					Post-Development Calculations				
Drainage area	Area (ac)	Frequency	Tc (m)	Q (cfs)	Drainage area	Area (ac)	Frequency	Tc (m)	Q (cfs)
DA-1	1.58	10 yr	10.448	2.094	DA-1	1.58	10 yr	6.514	3.351
		100 yr		3.739			100 yr		5.048

Table 2 Riverside County Synthetic Unit Hydrograph Analysis

Pre-Development Calculations								
Event	2 yr (cfs)	Flood Volume	5 yr (cfs)	Flood Volume	10 yr (cfs)	Flood Volume	100 yr (cfs)	Flood Volume
24 hr	0.044	1,175.80	0.06	1,605.60	0.173	2,139.1	0.831	12,977.5
6 hr	0.188	777.2	0.461	1,317.90	0.972	2,740.7	2.087	9,545.3
3 hr	0.248	642	0.574	1,219.30	1.13	2,530.40	2.353	8,507.8
1 hr	0.688	765.2	1.21	1,331.60	1.931	2,593.60	3.744	6,552.5

Post-Development Calculations								
Event	2 yr (cfs)	Flood Volume	5 yr (cfs)	Flood Volume	10 yr (cfs)	Flood Volume	100 yr (cfs)	Flood Volume
24 hr	0.362	9,641.2	0.495	13166.2	0.595	15,832.7	0.987	24,847.1
6 hr	0.871	5,737.7	1.155	7569.1	1.431	9,024.5	2.332	14,116.2
3 hr	0.966	4,086.9	1.322	5472.2	1.644	6,603.2	2.68	10,520.9
1 hr	2.224	3,401	2.224	3401	2.774	4211	4.607	7,141.6

Table 3 Basin Volumes*

Depth	Volume (ac.–ft)	Outfall (cfs)
10	0.350	1.43637
9.5	0.349	1.43637
9.25	0.348	0.55337
9	0.340	0.04537
8.5	0.326	0.04537
4.5	0.164	0.04537
1	0.024	0.04537
0	0	0

*Elevations per "Bioretention Area" detail on the Post Construction Hydrology Map

Table 4 Flood Hydrograph Routing

Post-Mitigation Calculations						
Event	2 yr Pre-Mitigation (cfs)	2 yr Post Mitigation (cfs)	Change	5 yr Pre Mitigation (cfs)	5 yr Post Mitigation (cfs)	Change
24 hr	0.362	0.045	0.317	0.495	0.045	0.450
6 hr	0.871	0.045	0.826	1.155	0.045	1.110
3 hr	0.966	0.045	0.921	1.322	0.045	1.277
1 hr	2.224	0.045	2.179	2.224	0.045	2.179

Post-Mitigation Calculations						
Event	10 yr Pre-Mitigation (cfs)	10 yr Post Mitigation (cfs)	Change	100 yr Pre Mitigation (cfs)	100 yr Post Mitigation (cfs)	Change
24 hr	0.595	0.045	0.550	0.987	0.751	0.236
6 hr	1.431	0.045	1.386	2.332	0.045	2.287
3 hr	1.644	0.045	1.599	2.68	0.045	2.635
1 hr	2.774	0.045	2.729	4.607	0.045	4.562

Table 5 Conclusion

100 yr

Event	Pre	Post Mitigated	Decrease	% Change
24 hr	0.831	0.751	0.080	-9.63%
6 hr	2.087	0.045	2.042	-97.84%
3 hr	2.353	0.045	2.308	-98.09%
1 hr	3.744	0.045	3.699	-98.80%

10 yr

Event	Pre	Post Mitigated	Decrease	% Change
24 hr	0.173	0.045	0.128	-73.99%
6 hr	0.972	0.045	0.927	-95.37%
3 hr	1.13	0.045	1.085	-96.02%
1 hr	1.931	0.045	1.886	-97.67%

5 yr

Event	Pre	Post Mitigated	Decrease	% Change
24 hr	0.06	0.045	0.015	-25.00%
6 hr	0.461	0.045	0.416	-90.24%
3 hr	0.574	0.045	0.529	-92.16%
1 hr	1.21	0.045	1.165	-96.28%

2 yr

Event	Pre	Post Mitigated	Decrease	% Change
24 hr	0.044	0.045*	0.001*	2.27%*
6 hr	0.188	0.045	0.143	-76.06%
3 hr	0.248	0.045	0.203	-81.85%
1 hr	0.688	0.045	0.643	-93.46%

*0.045 cfs accounts for the infiltration. Zero would be leaving the site. A 100% change.

V. CONCLUSION

The project will increase the post development Q amount compared to the predevelopment Q. To mitigate the increased flow coming from the project, an underground basin is being proposed to detain increased flows. The outlet of the basin will allow only predevelopment Q rates through. The underground basin volume is 15,237 cubic feet. After introducing the basin in the CivilD design software, the flow rates declined by 9.63%. During the 2-year 24-hour storm event, the mitigated flow equals 0.045 cfs (approximate flow that will be infiltrated) and will meet the predevelopment level by eliminating water leaving the project above ground. During standard storm events, any remaining runoff will outflow into the development to the north of the project.

SOILS REPORT

GEOTECHNICAL • ENVIRONMENTAL • GEOLOGY • MATERIALS TESTING & INSPECTION • FORENSIC • LABORATORY

SALEM
engineering group, inc.

PRELIMINARY GEOTECHNICAL ENGINESERING INVESTIGATION

PROPOSED ARCO STATION
NWC IRIS AVENUE AND OLIVER STREET
MORENO VALLEY, CALIFORNIA

SALEM PROJECT NO. 3-217-1265
NOVEMBER 30, 2017

PREPARED FOR:

MR. ERIC LEVAUGHN
SATER OIL INTERNATIONAL, LLC
683 CLIFFSIDE DRIVE
SAN DIMAS, CA 91773

PREPARED BY:

SALEM ENGINEERING GROUP, INC.
11650 MISSION PARK DR., #108
RANCHO CUCAMONGA, CA 91730
P: (909) 980-6455
F: (909) 980-6435
www.salemeng.com

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

SALEM engineering group, inc.

11650 Mission Park Dr., #108
Rancho Cucamonga, CA 91730
Phone (909) 980-6455
Fax (909) 980-6435

November 30, 2017 Project No. 3-217-1265

Mr. Eric LeVaughn
Sater Oil International, LLC
683 Cliffside Drive
San Dimas, CA 91773 85255

SUBJECT: PRELIMINARY GEOTECHNICAL ENGINEERING INVESTIGATION
PROPOSED ARCO STATION
NWC IRIS AVENUE AND OLIVER STREET
MORENO VALLEY, CALIFORNIA

Dear Mr. LeVaughn:

At your request and authorization, SALEM Engineering Group, Inc. (SALEM) has prepared this Preliminary Geotechnical Engineering Investigation report for the Proposed ARCO Station to be located at the subject site.

The accompanying report presents our findings, conclusions, and recommendations regarding the geotechnical aspects of designing and constructing the project as presently proposed. In our opinion, the proposed project is feasible from a geotechnical viewpoint provided our recommendations are incorporated into the design and construction of the project.

We appreciate the opportunity to assist you with this project. Should you have questions regarding this report or need additional information, please contact the undersigned at (909) 980-6455.

Respectfully Submitted,

SALEM ENGINEERING GROUP, INC.

Clarence Jiang, GE
Geotechnical Division Manager
RGE 2477

REGISTERED PROFESSIONAL ENGINEER
CLARENCE T. JIANG
No. 2477
Exp. 06/30/19
GEOTECHNICAL
STATE OF CALIFORNIA

R. Sammy Salem, MS, PE, GE
Principal Engineer
RCE 52762 / RGE 2549

REGISTERED PROFESSIONAL ENGINEER
R. SAMMY SALEM
GE 2549
Exp. Dec. 31, 2018
GEOTECHNICAL
STATE OF CALIFORNIA

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

TABLE OF CONTENTS

1. PURPOSE AND SCOPE 1
2. PROJECT DESCRIPTION 1
3. SITE LOCATION AND DESCRIPTION 2
4. FIELD EXPLORATION 2
5. LABORATORY TESTING 3
6. GEOLOGIC SETTING 3
7. GEOLOGIC HAZARDS 3
   - 7.1 Faulting and Seismicity 3
   - 7.2 Surface Fault Rupture 4
   - 7.3 Ground Shaking 4
   - 7.4 Liquefaction 4
   - 7.5 Lateral Spreading 5
   - 7.6 Landslides 5
   - 7.7 Tsunamis and Seiches 5
8. SOIL AND GROUNDWATER CONDITIONS 5
   - 8.1 Subsurface Conditions 5
   - 8.2 Groundwater 6
   - 8.3 Soil Corrosion Screening 6
   - 8.4 Percolation Testing 7
9. CONCLUSIONS AND RECOMMENDATIONS 8
   - 9.1 General 8
   - 9.2 Seismic Design Criteria 9
   - 9.3 Soil and Excavation Characteristics 10
   - 9.4 Materials for Fill 11
   - 9.5 Grading 12
   - 9.6 Shallow Foundations 14
   - 9.7 Concrete Slabs-on-Grade 15
   - 9.8 Caisson Foundations 17
   - 9.9 Lateral Earth Pressures and Frictional Resistance 18
   - 9.10 Retaining Walls 19
   - 9.11 Temporary Excavations 19
   - 9.12 Underground Utilities 20
   - 9.13 Surface Drainage 21
   - 9.14 Pavement Design 21
10. PLAN REVIEW, CONSTRUCTION OBSERVATION AND TESTING 22
    - 10.1 Plan and Specification Review 22
    - 10.2 Construction Observation and Testing Services 22
11. LIMITATIONS AND CHANGED CONDITIONS 23

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

TABLE OF CONTENTS (cont.)

FIGURES
Figure 1, Vicinity Map
Figure 2, Site Plan

APPENDIX A – FIELD INVESTIGATION
Figures A-1 through A-5, Logs of Exploratory Soil Borings B-1 through B-5
Percolation Testing Results, P-1 through P-4

APPENDIX B – LABORATORY TESTING
Consolidation Test Results
Direct Shear Test Results
Gradation Curves
Corrosivity Test Results
Maximum Density and Optimum Moisture Proctor Test Results

APPENDIX C – EARTHWORK AND PAVEMENT SPECIFICATIONS

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

SALEM engineering group, inc.

11650 Mission Park Drive, Suite 108
Rancho Cucamonga, CA 91730
Phone (909) 980-6455
Fax (909) 980-6435

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

PRELIMINARY GEOTECHNICAL ENGINEERING INVESTIGATION
PROPSOED ARCO STATION
NWC IRIS AVENUE AND OLIVER STREET
MORENO VALLEY, CALIFORNIA

1. PURPOSE AND SCOPE

This report presents the results of our Preliminary Geotechnical Engineering Investigation for the site of the Proposed ARCO Station to be located near the intersection of NWC Iris Avenue and Oliver Street in Moreno Valley, California (see Figure 1, Vicinity Map).

The purpose of our geotechnical engineering investigation was to observe and sample the subsurface conditions encountered at the site, and provide conclusions and recommendations relative to the geotechnical aspects of constructing the project as presently proposed.

The scope of this investigation included a field exploration, percolation testing, laboratory testing, engineering analysis and the preparation of this report. Our field exploration was performed on November 14, 2017 and included the drilling of five (5) small-diameter soil borings to a maximum depth of 50 feet at the site. Additionally, four (4) percolation tests were performed at depths of approximately 8 and 10 feet below existing grade for the determination of the infiltration rate. The locations of the soil borings and percolation tests are depicted on Figure 2, Site Plan. A detailed discussion of our field investigation, percolation tests, and exploratory boring logs are presented in Appendix A.

Laboratory tests were performed on selected soil samples obtained during the investigation to evaluate pertinent physical properties for engineering analyses. Appendix B presents the laboratory test results in tabular and graphic format.

The recommendations presented herein are based on analysis of the data obtained during the investigation and our experience with similar soil and geologic conditions.

If project details vary significantly from those described herein, SALEM should be contacted to determine the necessity for review and possible revision of this report. Earthwork and Pavement Specifications are presented in Appendix C. If text of the report conflict with the specifications in Appendix C, the recommendations in the text of the report have precedence.

2. PROJECT DESCRIPTION

Based on the Site Plan provided to us, we understand that the proposed development will include construction of an ARCO station with an approximately 3,800 square-foot AM/PM convenience store, an 8-MPD's fuel canopy, a 24 feet by 100 feet car wash, and underground storage tanks. On-site parking and landscaping are planned to be associated with the development. Maximum wall load is expected to

be on the order of 3 kips per linear foot. Maximum column load is expected to be on the order of 70 kips. Floor slab soil bearing pressure is expected to be on the order of 150 psf.

A site grading plan was not available at the time of preparation of this report. As the existing project area is essentially level, we anticipate that cuts and fills during earthwork will be minimal and limited to providing a level pad and positive site drainage. In the event that changes occur in the nature or design of the project, the conclusions and recommendations contained in this report will not be considered valid unless the changes are reviewed and the conclusions of our report are modified. The site configuration and locations of proposed improvements are shown on the Site Plan, Figure 2.

3. SITE LOCATION AND DESCRIPTION

The subject site is located at the northwest corner of the intersection of Iris Avenue and Oliver Street, in the City of Moreno Valley, CA (see Vicinity Map, Figure 1). The subject site is rectangular in shape and encompasses approximately 1.31 acres.

At the time of SALEM's field exploration, the site was a vacant lot with sparse shrubs. The site is bounded by vacant lands to the north and west, Oliver Street to the east, and Iris Avenue to the south. The site area is gently sloping to the north with elevations ranging from approximately 1,566 to 1,555 feet above mean sea level based on google earth imagery.

4. FIELD EXPLORATION

Our field exploration consisted of site surface reconnaissance and subsurface exploration. The exploratory test borings (B-1 through B-5) were drilled on November 14, 2017 in the area shown on the Site Plan, Figure 2. The test borings were advanced with a 6-inch diameter hollow stem auger and a 4 inch diameter solid flight auger rotated by a truck-mounted CME 45C drill rig. The test borings were extended to a maximum depth of 50 feet below existing grade.

The materials encountered in the test borings were visually classified in the field, and logs were recorded by a field engineer and stratification lines were approximated on the basis of observations made at the time of drilling. Visual classification of the materials encountered in the test borings were generally made in accordance with the Unified Soil Classification System (ASTM D2487). A soil classification chart and key to sampling is presented on the Unified Soil Classification Chart, in Appendix "A." The logs of the test borings are presented in Appendix "A." The Boring Logs include the soil type, color, moisture content, dry density, and the applicable Unified Soil Classification System symbol.

The location of the test borings were determined by measuring from features shown on the Site Plan, provided to us. Hence, accuracy can be implied only to the degree that this method warrants. The actual boundaries between different soil types may be gradual and soil conditions may vary. For a more detailed description of the materials encountered, the Boring Logs in Appendix "A" should be consulted.

Soil samples were obtained from the test borings at the depths shown on the logs of borings. The MCS samples were recovered and capped at both ends to preserve the samples at their natural moisture content; SPT samples were recovered and placed in a sealed bag to preserve their natural moisture content. The borings were backfilled with soil cuttings after completion of the drilling.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

5. LABORATORY TESTING

Laboratory tests were performed on selected soil samples to evaluate their physical characteristics and engineering properties. The laboratory-testing program was formulated with emphasis on the evaluation of natural moisture, in-situ density, shear strength, consolidation potential, maximum density and optimum moisture determination, and gradation of the materials encountered.

In addition, chemical tests were performed to evaluate the corrosivity of the soils to buried concrete and metal. Details of the laboratory test program and the results of laboratory test are summarized in Appendix "B." This information, along with the field observations, was used to prepare the final boring logs in Appendix "A."

6. GEOLOGIC SETTING

The subject site is located within the Peninsular Range Geomorphic Province, an area characterized by active northeast trending strike slip faults, including the San Jacinto to the northwest, and the Elsinore to the southwest. The project site is situated between the Santa Rosa Mountains and the San Jacinto Mountains to the east; and Santa Ana Mountains to the west and south. The near-surface deposits in the vicinity of the subject site are comprised of recent alluvium consisting of unconsolidated sands, silt, and clays derived from erosion of local mountain ranges. Deposits encountered on the subject site during exploratory drilling are discussed in detail in this report.

7. GEOLOGIC HAZARDS

7.1 Faulting and Seismicity

The Peninsular Range has historically been a province of relatively high seismic activity. The nearest faults to the project site are associated with the San Jacinto Fault system located approximately 4.1 miles from the site. There are no known active fault traces in the project vicinity. Based on mapping and historical seismicity, the seismicity of the Peninsular Range has been generally considered high by the scientific community.

The project area is not within an Alquist-Priolo Earthquake Fault (Special Studies) Zone and will not require a special site investigation by an Engineering Geologist. Soils on site are classified as Site Class D in accordance with Chapter 16 of the California Building Code. The proposed structures are determined to be in Seismic Design Category D.

To determine the distance of known active faults within 100 miles of the site, we used the United States Geological Survey (USGS) web-based application *2008 National Seismic Hazard Maps - Fault Parameters*. Site latitude is 33.8958° North; site longitude is 117.1833° West. The ten closest active faults are summarized below in Table 7.1.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

TABLE 7.1
REGIONAL FAULT SUMMARY

Fault Name	Distance to Site (miles)	Max. Earthquake Magnitude, M_w
San Jacinto; SBV+SJV+A+CC+B+SM	4.1	7.9
San Jacinto; A+CC+B+SM	4.3	7.6
San Jacinto; SBV	8.9	7.1
S. San Andreas; PK+CH+CC+BB+NM+SM+NSB+SSB+BG+CO	15.1	8.2
S. San Andreas; PK+CH+CC+BB+NM+SM+NSB	17.7	8.0
Elsinore; W+GI+T+J+CM	18.2	7.9
S. San Andreas; BG+CO	22.3	7.4
Chino, alt 2	22.6	6.8
Elsinore; W	23.9	7.0

The faults tabulated above and numerous other faults in the region are sources of potential ground motion. However, earthquakes that might occur on other faults throughout California are also potential generators of significant ground motion and could subject the site to intense ground shaking.

7.2 Surface Fault Rupture

The site is not within a currently established State of California Earthquake Fault Zone for surface fault rupture hazards. No active faults with the potential for surface fault rupture are known to pass directly beneath the site. Therefore, the potential for surface rupture due to faulting occurring beneath the site during the design life of the proposed development is considered low.

7.3 Ground Shaking

We used the USGS web-based application *US Seismic Design Maps* to estimate the peak ground acceleration adjusted for site class effects (PGA_M). Because of the proximity to the subject site and the maximum probable events for these faults, it appears that a maximum probable event along the fault zones could produce a peak horizontal acceleration of approximately 0.871g (2% probability of being exceeded in 50 years). While listing PGA is useful for comparison of potential effects of fault activity in a region, other considerations are important in seismic design, including frequency and duration of motion and soil conditions underlying the site.

7.4 Liquefaction

Soil liquefaction is a state of soil particles suspension caused by a complete loss of strength when the effective stress drops to zero. Liquefaction normally occurs under saturated conditions in soils such as sand in which the strength is purely frictional. Primary factors that trigger liquefaction are: moderate to strong ground shaking (seismic source), relatively clean, loose granular soils (primarily poorly graded sands and silty sands), and saturated soil conditions (shallow groundwater). Due to the increasing overburden pressure with depth, liquefaction of granular soils is generally limited to the upper 50 feet of a soil profile. However, liquefaction has occurred in soils other than clean sand.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

The soils encountered within the depth of 50 feet on the project site consisted predominately of very loose to dense silty sand with various amounts of clay and gravel, and dense to very dense silty clayey sand. Low to very low cohesion strength is associated with the sandy soil. A seismic hazard, which could cause damage to the proposed development during seismic shaking, is the post-liquefaction settlement of the liquefied sands.

The site was evaluated for liquefaction potential. The liquefaction analysis indicated that the soils had a low potential for liquefaction under seismic conditions. Therefore, no mitigation measures are warranted. Detailed geotechnical engineering recommendations are presented in the remaining portions of the text. The recommendations are based on the properties of the materials identified during our investigation.

7.5 Lateral Spreading

Lateral spreading is a phenomenon in which soils move laterally during seismic shaking and is often associated with liquefaction. The amount of movement depends on the soil strength, duration and intensity of seismic shaking, topography, and free face geometry. Due to the relatively flat site topography and low liquefaction potential, we judge the likelihood of lateral spreading to be low.

7.6 Landslides

There are no known landslides at the site, nor is the site in the path of any known or potential landslides. We do not consider the potential for a landslide to be a hazard to this project.

7.7 Tsunamis and Seiches

The site is not located within a coastal area. Therefore, tsunamis (seismic sea waves) are not considered a significant hazard at the site. Seiches are large waves generated in enclosed bodies of water in response to ground shaking. No major water-retaining structures are located immediately up gradient from the project site. Flooding from a seismically-induced seiche is considered unlikely.

8. SOIL AND GROUNDWATER CONDITIONS

8.1 Subsurface Conditions

The subsurface conditions encountered appear typical of those found in the geologic region of the site. In general, the soils within the depth of exploration consisted of alluvium deposits of very loose to dense silty sand with various amounts of clay and gravel, and dense to very dense silty clayey sand.

Fill soils maybe present on-site between our test boring locations. Verification of the extent of fill should be determined during site grading. Field and laboratory tests suggest that the deeper native soils are moderately strong and slightly compressible.

The soils were classified in the field during the drilling and sampling operations. The stratification lines were approximated by the field engineer on the basis of observations made at the time of drilling. The actual boundaries between different soil types may be gradual and soil conditions may vary. For a more detailed description of the materials encountered, the Boring Logs in Appendix "A" should be consulted.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

The Boring Logs include the soil type, color, moisture content, dry density, and the applicable Unified Soil Classification System symbol. The locations of the test borings were determined by measuring from feature shown on the Site Plan, provided to us. Hence, accuracy can be implied only to the degree that this method warrants.

8.2 Groundwater

The test boring locations were checked for the presence of groundwater during and after the drilling operations. Free groundwater was not encountered during this investigation.

It should be recognized that water table elevations may fluctuate with time, being dependent upon seasonal precipitation, irrigation, land use, localized pumping, and climatic conditions as well as other factors. Therefore, water level observations at the time of the field investigation may vary from those encountered during the construction phase of the project. The evaluation of such factors is beyond the scope of this report.

8.3 Soil Corrosion Screening

Excessive sulfate in either the soil or native water may result in an adverse reaction between the cement in concrete and the soil. The 2011 Edition of ACI 318 (ACI 318) has established criteria for evaluation of sulfate and chloride levels and how they relate to cement reactivity with soil and/or water.

A soil sample was obtained from the project site and was tested for the evaluation of the potential for concrete deterioration or steel corrosion due to attack by soil-borne soluble salts and soluble chloride. The water-soluble sulfate concentration in the saturation extract from the soil sample was detected to be 50 mg/kg. ACI 318 Tables 4.2.1 and 4.3.1 outline exposure categories, classes, and concrete requirements by exposure class. ACI 318 requirements for site concrete based upon soluble sulfate are summarized in Table 8.3 below.

TABLE 8.3
WATER SOLUBLE SULFATE EXPOSURE REQUIREMENTS

Water Soluble Sulfate (SO_4) in Soil, Percentage by Weight	Exposure Severity	Exposure Class	Maximum w/cm Ratio	Minimum Concrete Compressive Strength	Cementitious Materials Type
0.005	Not Applicable	S0	N/A	2,500 psi	No Restriction

The water-soluble chloride concentration detected in saturation extract from the soil samples was 21 mg/kg. This level of chloride concentration is not considered to be severely corrosive.

It is recommended that a qualified corrosion engineer be consulted regarding protection of buried steel or ductile iron piping and conduit or, at a minimum, applicable manufacturer's recommendations for corrosion protection of buried metal pipe be closely followed.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

8.4 Percolation Testing

Four percolation tests (P-1 through P-4) were performed within assumed infiltration areas and were conducted in accordance with in accordance with the guidelines established by the County of Riverside. The approximate locations of the percolation tests are shown on the attached Site Plan, Figure 2.

Four (4) 8-inch diameter boreholes were advanced to the depths shown on the percolation test worksheets. The holes were pre-saturated before percolation testing commenced. Percolation rates were measured by filling the test holes with clean water and measuring the water drops at a certain time interval.

The percolation rate data are presented in tabular format at the end of this Report. The difference in the percolation rates are reflected by the varied type of soil materials at the bottom of the test holes. The percolation rates were converted to infiltration rates using the "Porchet Method" according to County Design handbook. The test results are shown on the table below.

PERCOLATION TEST RESULTS

Test No.	Depth (feet)	Measured Percolation Rate (min/inch)	Infiltration Rate* (inch/hour)	Soil Type
P-1	8	7.6	**1.43**	Silty SAND (SM)
P-2	10	25.0	**0.55**	Silty SAND (SM)
P-3	8	25.0	**0.51**	Silty SAND (SM)
P-4	10	7.6	**1.27**	Silty SAND (SM)

*** Tested infiltration Rate = (ΔH 60 r) / (Δt(r + 2H_{avg}))**

The soil infiltration or percolation rates are based on tests conducted with clear water. The infiltration/percolation rates may vary with time as a result of soil clogging from water impurities. The infiltration/percolation rates will deteriorate over time due to the soil conditions.

The soils may also become less permeable to impermeable if the soil is compacted. Thus, periodic maintenance consisting of clearing the bottom of the drainage system of clogged soils should be expected. The infiltration/percolation rate may become slower if the surrounding soil is wet or saturated due to prolonged rainfalls. Additional percolation tests may be conducted at bottom of the drainage system during construction to verify the infiltration/percolation rate. Groundwater, if closer to the bottom of the drainage system, will also reduce the infiltration/percolation rate.

The scope of our services did not include a groundwater study and was limited to the performance of percolation testing and soil profile description, and the submitted data only. Our services did not include those associated with septic system design. Neither did services include an Environmental Site Assessment for the presence or absence of hazardous and/or toxic materials in the soil, groundwater, or atmosphere; or the presence of wetlands.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

Any statements, or absence of statements, in this report or on any boring logs regarding odors, unusual or suspicious items, or conditions observed, are strictly for descriptive purposes and are not intended to convey engineering judgment regarding potential hazardous and/or toxic assessment.

The geotechnical engineering information presented herein is based upon professional interpretation utilizing standard engineering practices. The work conducted through the course of this investigation, including the preparation of this report, has been performed in accordance with the generally accepted standards of geotechnical engineering practice, which existed in the geographic area at the time the report was written. No other warranty, express or implied, is made.

Please be advised that when performing percolation testing services in relatively small diameter borings, that the testing may not fully model the actual full scale long term performance of a given site. This is particularly true where percolation test data is to be used in the design of large infiltration system such as may be proposed for the site. The measured percolation rate includes dispersion of the water at the sidewalls of the boring as well as into the underlying soils. Subsurface conditions, including percolation rates, can change over time as fine-grained soils migrate. It is not warranted that such information and interpretation cannot be superseded by future geotechnical engineering developments. We emphasize that this report is valid for the project outlined above and should not be used for any other sites.

9. CONCLUSIONS AND RECOMMENDATIONS

9.1 General

9.1.1 Based upon the data collected during this investigation, and from a geotechnical engineering standpoint, it is our opinion that the site is suitable for the proposed construction of improvements at the site as planned, provided the recommendations contained in this report are incorporated into the project design and construction. Conclusions and recommendations provided in this report are based on our review of available literature, analysis of data obtained from our field exploration and laboratory testing program, and our understanding of the proposed development at this time.

9.1.2 The primary geotechnical constraints identified in our investigation is the presence of loose and potentially compressible material at the site. Recommendations to mitigate the effects of these soils are provided in this report.

9.1.3 Fill soils may be present on-site between our test boring locations. Undocumented fill materials are not suitable to support any future structures and should be replaced with Engineered Fill. Prior to fill placement, Salem Engineering Group, Inc. should inspect the bottom of the excavation to verify the fill condition.

9.1.4 Site demolition activities shall include removal of all surface obstructions not intended to be incorporated into final site design. In addition, underground buried structures and/or utility lines encountered during demolition and construction should be properly removed and the resulting excavations backfilled with Engineered Fill. It is suspected that possible demolition activities of the existing structures may disturb the upper soils. After demolition activities, it is recommended that disturbed soils be removed and/or recompacted.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

9.1.5 The near-surface onsite soils are moisture-sensitive and are moderately to highly compressible (collapsible soil) under saturated conditions. Structures within the project vicinity have experienced excessive post-construction settlement, when the foundation soils become near saturated. The collapsible or weak soils should be removed and recompacted according to the recommendations in the Grading section of this report (Section 9.5).

9.1.6 Based on the subsurface conditions at the site and the anticipated structural loading, we anticipate that the proposed building may be supported using conventional shallow foundations provided that the recommendations presented herein are incorporated in the design and construction of the project.

9.1.7 Provided the site is graded in accordance with the recommendations of this report and foundations constructed as described herein, we estimate that total settlement due to static loads utilizing conventional shallow foundations for the proposed building will be within 1 inch and corresponding differential settlement will be less than ½ inch.

9.1.8 All references to relative compaction and optimum moisture content in this report are based on ASTM D 1557 (latest edition).

9.1.9 SALEM shall review the project grading and foundation plans prior to final design submittal to assess whether our recommendations have been properly implemented and evaluate if additional analysis and/or recommendations are required. If SALEM is not provided plans and specifications for review, we cannot assume any responsibility for the future performance of the project.

9.1.10 SALEM shall be present at the site during site demolition and preparation to observe site clearing/demolition, preparation of exposed surfaces after clearing, and placement, treatment and compaction of fill material.

9.1.11 SALEM's observations should be supplemented with periodic compaction tests to establish substantial conformance with these recommendations. Moisture content of footings and slab subgrade should be tested immediately prior to concrete placement. SALEM should observe foundation excavations prior to placement of reinforcing steel or concrete to assess whether the actual bearing conditions are compatible with the conditions anticipated during the preparation of this report.

9.2 Seismic Design Criteria

9.2.1 For seismic design of the structures, and in accordance with the seismic provisions of the 2016 CBC, our recommended parameters are shown below. These parameters are based on Probabilistic Ground Motion of 2% Probability of Exceedance in 50 years. The Site Class was determined based on the results of our field exploration.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

TABLE 9.2.1
SEISMIC DESIGN PARAMETERS

Seismic Item	Symbol	Value	2016 CBC Reference
Site Coordinates (Datum = NAD 83)		33.8958 Lat -117.1833 Lon	
Site Class	--	D	ASCE 7 Table 20.3
Soil Profile Name	--	Stiff Soil	ASCE 7 Table 20.3
Risk Category	--	II	CBC Table 1604.5
Site Coefficient for PGA	F_{PGA}	1.200	ASCE 7 Table 11.8-1
Peak Ground Acceleration (adjusted for Site Class effects)	PGA_M	0.871 g	ASCE 7 Equation 11.8-1
Seismic Design Category	SDC	D	ASCE 7 Table 11.6-1 & 2
Mapped Spectral Acceleration (Short period - 0.2 sec)	S_S	1.715 g	CBC Figure 1613.3.1(1-6)
Mapped Spectral Acceleration (1.0 sec. period)	S_1	0.670 g	CBC Figure 1613.3.1(1-6)
Site Class Modified Site Coefficient	F_a	1.200	CBC Table 1613.3.3(1)
Site Class Modified Site Coefficient	F_v	1.700	CBC Table 1613.3.3(2)
MCE Spectral Response Acceleration (Short period - 0.2 sec) $S_{MS} = F_a S_S$	S_{MS}	2.058 g	CBC Equation 16-37
MCE Spectral Response Acceleration (1.0 sec. period) $S_{M1} = F_v S_1$	S_{M1}	1.139 g	CBC Equation 16-38
Design Spectral Response Acceleration $S_{DS}=⅔S_{MS}$ (short period - 0.2 sec)	S_{DS}	1.372 g	CBC Equation 16-39
Design Spectral Response Acceleration $S_{D1}=⅔S_{M1}$ (1.0 sec. period)	S_{D1}	0.759 g	CBC Equation 16-40

9.2.2 Conformance to the criteria in the above table for seismic design does not constitute any kind of guarantee or assurance that significant structural damage or ground failure will not occur if a large earthquake occurs. The primary goal of seismic design is to protect life, not to avoid all damage, since such design may be economically prohibitive.

9.3 Soil and Excavation Characteristics

9.3.1 Based on the soil conditions encountered in our soil borings, the onsite soils can be excavated with moderate to laborious effort using conventional heavy-duty or special excavation and earthmoving equipment.

9.3.2 It is the responsibility of the contractor to ensure that all excavations and trenches are properly shored and maintained in accordance with applicable Occupational Safety and Health Administration (OSHA) rules and regulations to maintain safety and maintain the stability of adjacent existing improvements. Temporary excavations are further discussed in a later Section of this report.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

9.3.3 The upper soils within the project site are identified primarily as silty sands and clayey sands. The sandy soils are moisture-sensitive and moderately collapsible under saturated conditions. These soils, in their present condition, possess moderate risk to construction in terms of possible post-construction movement of the foundations and floor systems if no mitigation measures are employed. Accordingly, measures are considered necessary to reduce anticipated expansion and collapse potential.

As recommended in Section 9.5, the collapsible soils should be removed and replaced with properly moisture conditioned and compacted Engineered Fill. Mitigation measures will not eliminate post-construction soil movement, but will reduce the soil movement. Success of the mitigation measures will depend on the thoroughness of the contractor in dealing with the soil conditions.

9.3.4 The near surface soils identified as part of our investigation are, generally, slightly moist to moist due to the absorption characteristics of the soil. Earthwork operations may encounter very moist unstable soils which may require removal to a stable bottom. Exposed native soils exposed as part of site grading operations shall not be allowed to dry out and should be kept continuously moist prior to placement of subsequent fill.

9.4 Materials for Fill

9.4.1 Excavated soils generated from cut operations at the site are suitable for use as general Engineered Fill in structural areas, provided they do not contain deleterious matter, organic material, or rock material larger than 3 inches in maximum dimension.

9.4.2 The preferred materials specified for Engineered Fill are suitable for most applications with the exception of exposure to erosion. Project site winterization and protection of exposed soils during the construction phase should be the sole responsibility of the Contractor, since they have complete control of the project site.

9.4.3 Import soil shall be well-graded, slightly cohesive silty fine sand or sandy silt, with relatively impervious characteristics when compacted. A clean sand or very sandy soil is not acceptable for this purpose. This material should be approved by the Engineer prior to use and should typically possess the soil characteristics summarized below in Table 9.4.3.

TABLE 9.4.3
IMPORT FILL REQUIREMENTS

Minimum Percent Passing No. 200 Sieve	20
Maximum Percent Passing No. 200 Sieve	50
Minimum Percent Passing No. 4 Sieve	80
Maximum Particle Size	3"
Maximum Plasticity Index	10
Maximum CBC Expansion Index	15

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

9.4.4 Environmental characteristics and corrosion potential of import soil materials should also be considered.

9.4.5 Proposed import materials should be sampled, tested, and approved by SALEM prior to its transportation to the site.

9.5 Grading

9.5.1 A representative of our firm should be present during all site clearing and grading operations to test and observe earthwork construction. This testing and observation is an integral part of our service as acceptance of earthwork construction is dependent upon compaction of the material and the stability of the material. The Geotechnical Engineer may reject any material that does not meet compaction and stability requirements. Further recommendations of this report are predicated upon the assumption that earthwork construction will conform to recommendations set forth in this section as well as other portions of this report.

9.5.2 A preconstruction conference should be held at the site prior to the beginning of grading operations with the owner, contractor, civil engineer and geotechnical engineer in attendance.

9.5.3 Site preparation should begin with removal of existing surface/subsurface structures, underground utilities (as required), any existing uncertified fill, and debris. Excavations or depressions resulting from site clearing operations, or other existing excavations or depressions, should be restored with Engineered Fill in accordance with the recommendations of this report.

9.5.4 Surface vegetation consisting of grasses and other similar vegetation should be removed by stripping to a sufficient depth to remove organic-rich topsoil. The upper 2 to 4 inches of the soils containing, vegetation, roots and other objectionable organic matter encountered at the time of grading should be stripped and removed from the surface. Deeper stripping may be required in localized areas. In addition, existing concrete and asphalt materials shall be removed from areas of proposed improvements and stockpiled separately from excavated soil material. The stripped vegetation, asphalt and concrete materials will not be suitable for use as Engineered Fill or within 5 feet of building pads or within pavement areas. However, stripped topsoil may be stockpiled and reused in landscape or non-structural areas or exported from the site.

9.5.5 Structural building pad areas should be considered as areas extending a minimum of 5 feet horizontally beyond the outside dimensions of building, including footings and non-cantilevered overhangs carrying structural loads.

9.5.6 To minimize post-construction soil movement and provide uniform support for the proposed building, overexcavation and recompaction within the proposed building areas should be performed to a minimum depth of **five (5) feet** below existing grade or **three (3) feet** below proposed footing bottom, whichever is deeper. The overexcavation and recompaction should also extend laterally to a minimum of 5 feet beyond the outer edges of the proposed footings.

9.5.7 Within pavement areas, it is recommended that overexcavation and recompaction be performed to a minimum depth of **1.5 feet** below existing grade or proposed grade, whichever is deeper. Deeper overexcavation may be required in some local areas to removal all unsuitable materials.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

The overexcavation and recompaction should also extend laterally to a minimum of 2 feet beyond the outer edges of the proposed pavement.

9.5.8 Any fill or disturbed soils encountered during grading should be removed and replaced with engineered fill. The actual depth of the overexcavation and recompaction should be determined by our field representative during construction.

9.5.9 Prior to placement of fill soils, the upper 8 to 10 inches of native subgrade soils should be scarified, moisture-conditioned to no less than the optimum moisture content and recompacted to a minimum of 95 percent of the maximum dry density based on ASTM D1557 Test Method latest edition.

9.5.10 All Engineered Fill (including scarified ground surfaces and backfill) should be placed in thin lifts which will allow for adequate bonding and compaction (typically 6 to 8 inches in loose thickness).

9.5.11 Engineered Fill soils should be placed, moisture conditioned to near optimum moisture content, and compacted to at least 95% relative compaction.

9.5.12 An integral part of satisfactory fill placement is the stability of the placed lift of soil. If placed materials exhibit excessive instability as determined by a SALEM field representative, the lift will be considered unacceptable and shall be remedied prior to placement of additional fill material. Additional lifts should not be placed if the previous lift did not meet the required dry density or if soil conditions are not stable.

9.5.13 Final pavement subgrade should be finished to a smooth, unyielding surface. We further recommend proof-rolling the subgrade with a loaded water truck (or similar equipment with high contact pressure) to verify the stability of the subgrade prior to placing aggregate base.

9.5.14 The most effective site preparation alternatives will depend on site conditions prior to grading. We should evaluate site conditions and provide supplemental recommendations immediately prior to grading, if necessary.

9.5.15 We do not anticipate groundwater or seepage to adversely affect construction if conducted during the drier moths of the year (typically summer and fall). However, groundwater and soil moisture conditions could be significantly different during the wet season (typically winter and spring) as surface soil becomes wet; perched groundwater conditions may develop. Grading during this time period will likely encounter wet materials resulting in possible excavation and fill placement difficulties. Project site winterization consisting of placement of aggregate base and protecting exposed soils during construction should be performed. If the construction schedule requires grading operations during the wet season, we can provide additional recommendations as conditions warrant.

9.5.16 Typical remedial measures include: discing and aerating the soil during dry weather; mixing the soil with dryer materials; removing and replacing the soil with an approved fill material or placement of crushed rocks or aggregate base material; or mixing the soil with an approved lime or cement product.

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

The most common remedial measure of stabilizing the bottom of the excavation due to wet soil condition is to reduce the moisture of the soil to near the optimum moisture content by having the subgrade soils scarified and aerated or mixed with drier soils prior to compacting. However, the drying process may require an extended period of time and delay the construction operation.

To expedite the stabilizing process, crushed rock may be utilized for stabilization provided this method is approved by the owner for the cost purpose.

If the use of crushed rock is considered, it is recommended that the upper soft and wet soils be replaced by 6 to 24 inches of ¾-inch to 1-inch crushed rocks. The thickness of the rock layer depends on the severity of the soil instability. The recommended 6 to 24 inches of crushed rock material will provide a stable platform. It is further recommended that lighter compaction equipment be utilized for compacting the crushed rock. A layer of geofabric is recommended to be placed on top of the compacted crushed rock to minimize migration of soil particles into the voids of the crushed rock, resulting in soil movement.

Although it is not required, the use of geogrid (e.g. Tensar TX 140) below the crushed rock will enhance stability and reduce the required thickness of crushed rock necessary for stabilization. Our firm should be consulted prior to implementing remedial measures to provide appropriate recommendations.

9.6 Shallow Foundations

9.6.1 The site is suitable for use of conventional shallow foundations consisting of continuous footings and isolated pad footings bearing in properly compacted Engineered Fill.

9.6.2 The bearing wall footings considered for the structure should be continuous with a minimum width of 15 inches and extend to a minimum depth of 18 inches below the lowest adjacent grade. Isolated column footings should have a minimum width of 24 inches and extend a minimum depth of 18 inches below the lowest adjacent grade.

9.6.3 The bottom of footing excavations should be maintained free of loose and disturbed soil. Footing concrete should be placed into a neat excavation.

9.6.4 For design purposes, total settlement due to static loading on the order of 1 inch may be assumed for shallow footings. Differential settlement due to static loading, along a 20-foot exterior wall footing or between adjoining column footings, should be ½ inch, producing an angular distortion of 0.002. Most of the settlement is expected to occur during construction as the loads are applied. However, additional post-construction settlement may occur if the foundation soils are flooded or saturated. The footing excavations should not be allowed to dry out any time prior to pouring concrete.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

9.6.5 Footings proportioned as recommended above may be designed for the maximum allowable soil bearing pressures shown in the table below.

Loading Condition	Allowable Bearing
Dead Load Only	2,000 psf
Dead-Plus-Live Load	2,500 psf
Total Load, Including Wind or Seismic Loads	3,325 psf

9.6.6 Resistance to lateral footing displacement can be computed using an allowable coefficient of friction factor of 0.40 acting between the base of foundations and the supporting subgrade.

9.6.7 Lateral resistance for footings can alternatively be developed using an allowable equivalent fluid passive pressure of 400 pounds per cubic foot acting against the appropriate vertical native footing faces. The frictional and passive resistance of the soil may be combined without reduction in determining the total lateral resistance. An increase of one-third is permitted when using the alternate load combination in Section 1605.3.2 of the 2015 IBC/2016 CBC that includes wind or earthquake loads.

9.6.8 Underground utilities running parallel to footings should not be constructed in the zone of influence of footings. The zone of influence may be taken to be the area beneath the footing and within a 1:1 plane extending out and down from the bottom edge of the footing.

9.6.9 The foundation subgrade should be sprinkled as necessary to maintain a moist condition without significant shrinkage cracks as would be expected in any concrete placement. Prior to placing rebar reinforcement, foundation excavations should be evaluated by a representative of SALEM for appropriate support characteristics and moisture content. Moisture conditioning may be required for the materials exposed at footing bottom, particularly if foundation excavations are left open for an extended period.

9.7 Concrete Slabs-on-Grade

9.7.1 Slab thickness and reinforcement should be determined by the structural engineer based on the anticipated loading. We recommend that non-structural slabs-on-grade be at least 4 inches thick and underlain by six (6) inches of compacted granular aggregate subbase material compacted to at least 95% relative compaction.

9.7.2 Granular aggregate subbase material shall conform to ASTM D-2940, Latest Edition (Table 1, bases) with at least 95 percent passing a 1½-inch sieve and not more than 8% passing a No. 200 sieve or its approved equivalent to prevent capillary moisture rise.

9.7.3 We recommend reinforcing slabs, at a minimum, with No. 3 reinforcing bars placed 18 inches on center, each way.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

9.7.4 Slabs subject to structural loading may be designed utilizing a modulus of subgrade reaction K of 180 pounds per square inch per inch. The K value was approximated based on inter-relationship of soil classification and bearing values (Portland Cement Association, Rocky Mountain Northwest).

9.7.5 The spacing of crack control joints should be designed by the project structural engineer. In order to regulate cracking of the slabs, we recommend that full depth construction joints or control joints be provided at a maximum spacing of 15 feet in each direction for 5-inch thick slabs and 12 feet for 4-inch thick slabs.

9.7.6 Crack control joints should extend a minimum depth of one-fourth the slab thickness and should be constructed using saw-cuts or other methods as soon as practical after concrete placement. The exterior floors should be poured separately in order to act independently of the walls and foundation system.

9.7.7 It is recommended that the utility trenches within the structure be compacted, as specified in our report, to minimize the transmission of moisture through the utility trench backfill. Special attention to the immediate drainage and irrigation around the structures is recommended.

9.7.8 Moisture within the structure may be derived from water vapors, which were transformed from the moisture within the soils. This moisture vapor penetration can affect floor coverings and produce mold and mildew in the structure. To minimize moisture vapor intrusion, it is recommended that a vapor retarder be installed in accordance with manufacturer's recommendations and/or ASTM guidelines, whichever is more stringent. In addition, ventilation of the structure is recommended to reduce the accumulation of interior moisture.

9.7.9 In areas where it is desired to reduce floor dampness where moisture-sensitive coverings are anticipated, construction should have a suitable waterproof vapor retarder (a minimum of 15 mils thick polyethylene vapor retarder sheeting, Raven Industries "VaporBlock 15, Stego Industries 15 mil "StegoWrap" or W.R. Meadows Sealtight 15 mil "Perminator") incorporated into the floor slab design. The water vapor retarder should be decay resistant material complying with ASTM E96 not exceeding 0.04 perms, ASTM E154 and ASTM E1745 Class A. The vapor barrier should be placed between the concrete slab and the compacted granular aggregate subbase material. The water vapor retarder (vapor barrier) should be installed in accordance with ASTM Specification E 1643-94.

9.7.10 The concrete maybe placed directly on vapor retarder. The vapor retarder should be inspected prior to concrete placement. Cut or punctured retarder should be repaired using vapor retarder material lapped 6 inches beyond damaged areas and taped.

9.7.11 The recommendations of this report are intended to reduce the potential for cracking of slabs due to soil movement. However, even with the incorporation of the recommendations presented herein, foundations, stucco walls, and slabs-on-grade may exhibit some cracking due to soil movement. This is common for project areas that contain expansive soils since designing to eliminate potential soil movement is cost prohibitive. The occurrence of concrete shrinkage cracks is independent of the supporting soil characteristics. Their occurrence may be reduced and/or controlled by limiting the slump of the concrete, proper concrete placement and curing,

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

and by the placement of crack control joints at periodic intervals, in particular, where re-entrant slab corners occur.

9.7.12 Proper finishing and curing should be performed in accordance with the latest guidelines provided by the American Concrete Institute, Portland Cement Association, and ASTM.

9.8 Caisson Foundations

9.8.1 It is recommended that the caisson foundation should have a minimum depth of 12 feet below the lowest adjacent grade.

9.8.2 The caissons may be designed using an allowable sidewall friction of 160 psf. This value is for dead-plus-live loads. An allowable end bearing capacity of 3,000 psf may be used provided that the bottom of the caisson is cleaned with the use of a clean-out bucket or equivalent and inspected by our representative prior to placement of reinforcement and concrete. An increase of one-third is permitted when using the alternate load combination in Section 1605.3.2 of the CBC that includes wind or earthquake loads.

9.8.3 Uplift loads can be resisted by caissons using an allowable sidewall friction of 120 psf of the surface area and the weight of the caisson.

9.8.4 The total static settlement of the caisson footing is not expected to exceed 1 inches. Differential settlement should be less than ½ inch. Most of the settlement is expected to occur during construction as the loads are applied.

9.8.5 Lateral loads for caissons may be designed utilizing the Isolated Pole Formula and Specifications shown on Table 1804.2, Sections 1804.3.1 and 1808.2.2 of the California Building Code. The drilled caissons may be designed for a lateral capacity of 400 pounds per square foot per foot of depth below the lowest adjacent grade to a maximum of 6,000 psf.

9.8.6 The top one-foot of adjacent subgrade should be deleted from the passive pressure computation.

9.8.7 These values may be increased by one-third when using the alternative load combinations in Section 1605.3.2 of the IBC that include wind or earthquake loads. These values should not be doubled since the values given herein are higher than the tabular values shown on the Table 1804.2. The lateral loading criteria is based on the assumption that the load application is applied at the ground level, flexible cap connections applied and a minimum embedment depth of 10 feet.

9.8.8 Sandy soils were encountered at the site. Casing will be required during drilling of the caisson footings.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

9.9 Lateral Earth Pressures and Frictional Resistance

9.9.1 Active, at-rest and passive unit lateral earth pressures against footings and walls are summarized in the table below:

Lateral Pressure Level Backfill and Drained Conditions	Equivalent Fluid Pressure, pcf
Active Pressure	35
At-Rest Pressure	55
Passive Pressure	400
Related Parameters	
Allowable Coefficient of Friction	0.40
In-Place Soil Density (lbs/ft^3)	120

9.9.2 Active pressure applies to walls, which are free to rotate. At-rest pressure applies to walls, which are restrained against rotation. The preceding lateral earth pressures assume sufficient drainage behind retaining walls to prevent the build-up of hydrostatic pressure.

9.9.3 The top one-foot of adjacent subgrade should be deleted from the passive pressure computation.

9.9.4 A safety factor consistent with the design conditions should be included when using the values in the above table.

9.9.5 For stability against lateral sliding, which is resisted solely by the passive pressure, we recommend a minimum safety factor of 1.5.

9.9.6 For stability against lateral sliding, which is resisted by the combined passive and frictional resistance, a minimum safety factor of 2.0 is recommended.

9.9.7 For lateral stability against seismic loading conditions, we recommend a minimum safety factor of 1.1.

9.9.8 For dynamic seismic lateral loading the following equation shall be used:

Dynamic Seismic Lateral Loading Equation
Dynamic Seismic Lateral Load = $\frac{3}{8}\gamma K_h H^2$
Where: γ = In-Place Soil Density
K_h = Horizontal Acceleration = $\frac{2}{3}PGA_M$
H = Wall Height

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

9.10 Retaining Walls

9.10.1 Retaining and/or below grade walls should be drained with either perforated pipe encased in free-draining gravel or a prefabricated drainage system. The gravel zone should have a minimum width of 12 inches wide and should extend upward to within 12 inches of the top of the wall. The upper 12 inches of backfill should consist of native soils, concrete, asphaltic-concrete or other suitable backfill to minimize surface drainage into the wall drain system. The gravel should conform to Class II permeable materials graded in accordance with the current CalTrans Standard Specifications.

9.10.2 Prefabricated drainage systems, such as Miradrain®, Enkadrain®, or an equivalent substitute, are acceptable alternatives in lieu of gravel provided they are installed in accordance with the manufacturer's recommendations. If a prefabricated drainage system is proposed, our firm should review the system for final acceptance prior to installation.

9.10.3 Drainage pipes should be placed with perforations down and should discharge in a non-erosive manner away from foundations and other improvements. The top of the perforated pipe should be placed at or below the bottom of the adjacent floor slab or pavements. The pipe should be placed in the center line of the drainage blanket and should have a minimum diameter of 4 inches. Slots should be no wider than 1/8-inch in diameter, while perforations should be no more than ¼-inch in diameter.

9.10.4 If retaining walls are less than 5 feet in height, the perforated pipe may be omitted in lieu of weep holes on 4 feet maximum spacing. The weep holes should consist of 2-inch minimum diameter holes (concrete walls) or unmortared head joints (masonry walls) and placed no higher than 18 inches above the lowest adjacent grade. Two 8-inch square overlapping patches of geotextile fabric (conforming to the CalTrans Standard Specifications for "edge drains") should be affixed to the rear wall opening of each weep hole to retard soil piping.

9.10.5 During grading and backfilling operations adjacent to any walls, heavy equipment should not be allowed to operate within a lateral distance of 5 feet from the wall, or within a lateral distance equal to the wall height, whichever is greater, to avoid developing excessive lateral pressures. Within this zone, only hand operated equipment ("whackers," vibratory plates, or pneumatic compactors) should be used to compact the backfill soils.

9.11 Temporary Excavations

9.11.1 We anticipate that the majority of the sandy site soils will be classified as Cal-OSHA "Type C" soil when encountered in excavations during site development and construction. Excavation sloping, benching, the use of trench shields, and the placement of trench spoils should conform to the latest applicable Cal-OSHA standards. The contractor should have a Cal-OSHA-approved "competent person" onsite during excavation to evaluate trench conditions and make appropriate recommendations where necessary.

9.11.2 It is the contractor's responsibility to provide sufficient and safe excavation support as well as protecting nearby utilities, structures, and other improvements which may be damaged by earth movements. All onsite excavations must be conducted in such a manner that potential surcharges

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

from existing structures, construction equipment, and vehicle loads are resisted. The surcharge area may be defined by a 1:1 projection down and away from the bottom of an existing foundation or vehicle load.

9.11.3 Temporary excavations and slope faces should be protected from rainfall and erosion. Surface runoff should be directed away from excavations and slopes.

9.11.4 Open, unbraced excavations in undisturbed soils should be made according to the slopes presented in the following table:

RECOMMENDED EXCAVATION SLOPES

Depth of Excavation (ft)	Slope (Horizontal : Vertical)
0-5	1:1
5-10	2:1

9.11.5 If, due to space limitation, excavations near property lines or existing structures are performed in a vertical position, slot cuts, braced shorings or shields may be used for supporting vertical excavations. Therefore, in order to comply with the local and state safety regulations, a properly designed and installed shoring system would be required to accomplish planned excavations and installation. A Specialty Shoring Contractor should be responsible for the design and installation of such a shoring system during construction.

9.11.6 Braced shorings should be designed for a maximum pressure distribution of 30H, (where H is the depth of the excavation in feet). The foregoing does not include excess hydrostatic pressure or surcharge loading. Fifty percent of any surcharge load, such as construction equipment weight, should be added to the lateral load given herein. Equipment traffic should concurrently be limited to an area at least 3 feet from the shoring face or edge of the slope.

9.11.7 The excavation and shoring recommendations provided herein are based on soil characteristics derived from the borings within the area. Variations in soil conditions will likely be encountered during the excavations. SALEM Engineering Group, Inc. should be afforded the opportunity to provide field review to evaluate the actual conditions and account for field condition variations not otherwise anticipated in the preparation of this recommendation. Slope height, slope inclination, or excavation depth should in no case exceed those specified in local, state, or federal safety regulation, (e.g. OSHA) standards for excavations, 29 CFR part 1926, or Assessor's regulations.

9.12 Underground Utilities

9.12.1 Underground utility trenches should be backfilled with properly compacted material. The material excavated from the trenches should be adequate for use as backfill provided it does not contain deleterious matter, vegetation or rock larger than 3 inches in maximum dimension. Trench backfill should be placed in loose lifts not exceeding 8 inches and compacted to at least 95% relative compaction at or above optimum moisture content.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

9.12.2 Bedding and pipe zone backfill typically extends from the bottom of the trench excavations to approximately 6 to 12 inches above the crown of the pipe. Pipe bedding and backfill material should conform to the requirements of the governing utility agency.

9.12.3 It is suggested that underground utilities crossing beneath new or existing structures be plugged at entry and exit locations to the buildings or structures to prevent water migration. Trench plugs can consist of on-site clay soils, if available, or sand cement slurry. The trench plugs should extend 2 feet beyond each side of individual perimeter foundations.

9.12.4 The contractor is responsible for removing all water-sensitive soils from the trench regardless of the backfill location and compaction requirements. The contractor should use appropriate equipment and methods to avoid damage to the utilities and/or structures during fill placement and compaction.

9.13 Surface Drainage

9.13.1 Proper surface drainage is critical to the future performance of the project. Uncontrolled infiltration of irrigation excess and storm runoff into the soils can adversely affect the performance of the planned improvements. Saturation of a soil can cause it to lose internal shear strength and increase its compressibility, resulting in a change to important engineering properties. Proper drainage should be maintained at all times.

9.13.2 The ground immediately adjacent to the foundation shall be sloped away from the building at a slope of not less than 5 percent for a minimum distance of 10 feet.

9.13.3 Impervious surfaces within 10 feet of the building foundation shall be sloped a minimum of 2 percent away from the building and drainage gradients maintained to carry all surface water to collection facilities and off site. These grades should be maintained for the life of the project. Ponding of water should not be allowed adjacent to the structure. Over-irrigation within landscaped areas adjacent to the structure should not be performed.

9.13.4 Roof drains should be installed with appropriate downspout extensions out-falling on splash blocks so as to direct water a minimum of 5 feet away from the structures or be connected to the storm drain system for the development.

9.14 Pavement Design

9.14.1 Based on site soil conditions, an R-value of 40 was used for the preliminary flexible asphaltic concrete pavement design. The R-value may be verified during grading of the pavement areas.

9.14.2 The pavement design recommendations provided herein are based on the State of California Department of Transportation (CALTRANS) design manual. The asphaltic concrete (flexible pavement) is based on a 20-year pavement life utilizing 1200 passenger vehicles, 10 single unit trucks, and 2 multi-unit trucks. The following table shows the recommended pavement sections for various traffic indices.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

TABLE 9.14.2
ASPHALT CONCRETE PAVEMENT THICKNESSES

Traffic Index	Asphaltic Concrete	Class II Aggregate Base*	Compacted Subgrade*
5.0 (Parking and Vehicle Drive Areas)	2.5"	5.0"	18.0"
6.0 (Heavy Truck Areas)	3.0"	6.0"	18.0"

95% compaction based on ASTM D1557-07 Test Method or Cal 216

9.14.3 The following recommendations are for light-duty and heavy-duty Portland Cement Concrete pavement sections.

TABLE 9.14.3
PORTLAND CEMENT CONCRETE PAVEMENT THICKNESSES

Traffic Index	Portland Cement Concrete*	Class II Aggregate Base**	Compacted Subgrade**
5.0 (Light Duty)	5.0"	5.0"	18.0"
6.0 (Heavy Duty)	6.0"	5.0"	18.0"

**** Minimum Compressive Strength of 4,000 psi***
***** 95% compaction based on ASTM D1557-07 Test Method or Cal 216***

10. PLAN REVIEW, CONSTRUCTION OBSERVATION AND TESTING

10.1 Plan and Specification Review

10.1.1 SALEM should review the project plans and specifications prior to final design submittal to assess whether our recommendations have been properly implemented and evaluate if additional analysis and/or recommendations are required.

10.2 Construction Observation and Testing Services

10.2.1 The recommendations provided in this report are based on the assumption that we will continue as Geotechnical Engineer of Record throughout the construction phase. It is important to maintain continuity of geotechnical interpretation and confirm that field conditions encountered are similar to those anticipated during design. If we are not retained for these services, we cannot assume any responsibility for others interpretation of our recommendations, and therefore the future performance of the project.

10.2.2 SALEM should be present at the site during site preparation to observe site clearing, preparation of exposed surfaces after clearing, and placement, treatment and compaction of fill material.

10.2.3 SALEM's observations should be supplemented with periodic compaction tests to establish substantial conformance with these recommendations. Moisture content of footings and slab

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

subgrade should be tested immediately prior to concrete placement. SALEM should observe foundation excavations prior to placement of reinforcing steel or concrete to assess whether the actual bearing conditions are compatible with the conditions anticipated during the preparation of this report.

11. LIMITATIONS AND CHANGED CONDITIONS

The analyses and recommendations submitted in this report are based upon the data obtained from the test borings drilled at the approximate locations shown on the Site Plan, Figure 2. The report does not reflect variations which may occur between borings. The nature and extent of such variations may not become evident until construction is initiated.

If variations then appear, a re-evaluation of the recommendations of this report will be necessary after performing on-site observations during the excavation period and noting the characteristics of such variations. The findings and recommendations presented in this report are valid as of the present and for the proposed construction. If site conditions change due to natural processes or human intervention on the property or adjacent to the site, or changes occur in the nature or design of the project, or if there is a substantial time lapse between the submission of this report and the start of the work at the site, the conclusions and recommendations contained in our report will not be considered valid unless the changes are reviewed by SALEM and the conclusions of our report are modified or verified in writing.

The validity of the recommendations contained in this report is also dependent upon an adequate testing and observations program during the construction phase. Our firm assumes no responsibility for construction compliance with the design concepts or recommendations unless we have been retained to perform the on-site testing and review during construction. SALEM has prepared this report for the exclusive use of the owner and project design consultants.

SALEM does not practice in the field of corrosion engineering. It is recommended that a qualified corrosion engineer be consulted regarding protection of buried steel or ductile iron piping and conduit or, at a minimum, that manufacturer's recommendations for corrosion protection be closely followed. Further, a corrosion engineer may be needed to incorporate the necessary precautions to avoid premature corrosion of concrete slabs and foundations in direct contact with native soil.

The importation of soil and or aggregate materials to the site should be screened to determine the potential for corrosion to concrete and buried metal piping. The report has been prepared in accordance with generally accepted geotechnical engineering practices in the area. No other warranties, either express or implied, are made as to the professional advice provided under the terms of our agreement and included in this report.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

If you have any questions, or if we may be of further assistance, please do not hesitate to contact our office at (909) 980-6455.

Respectfully Submitted,

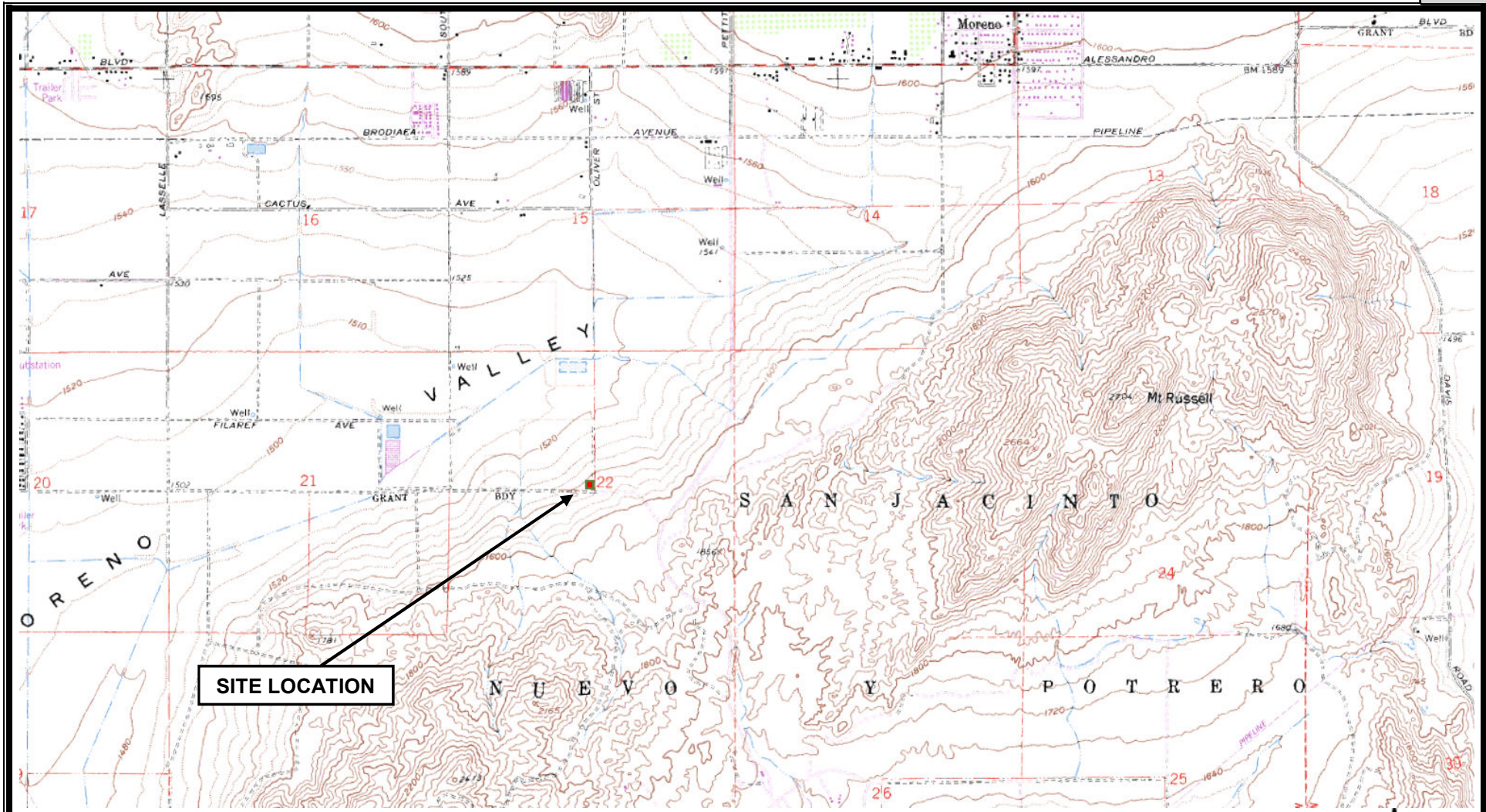
SALEM ENGINEERING GROUP, INC.

Ibrahim Ibrahim, MS, PE
Geotechnical Staff Engineer
RCE 86724

Clarence Jiang, GE
Senior Geotechnical Engineer
RGE 2477

R. Sammy Salem, MS, PE, GE
Principal Engineer
RCE 52762 / RGE 2549

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)



Source Image: U.S. Geological Survey, Sunnymead, Calif. 7.5' Quadrangle, 1967 (Photo Revised 1980)

N

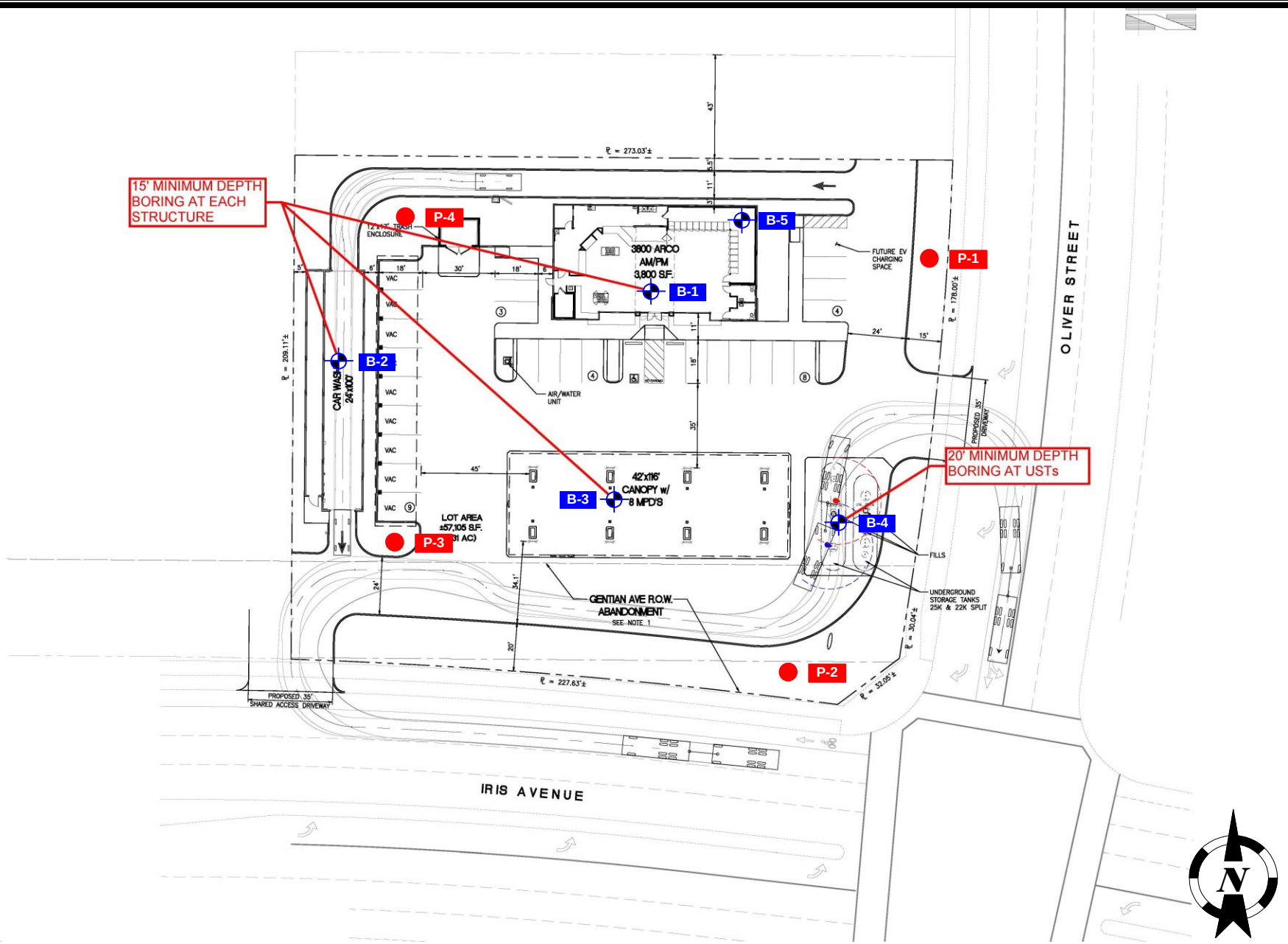
VICINITY MAP

GEOTECHNICAL ENGINEERING INVESTIGATION
Proposed Arco Station
NWC Iris Avenue & Oliver Street
Moreno Valley, California

SCALE:	DATE:
NOT TO SCALE	11/2017
DRAWN BY:	APPROVED BY:
II	CJ
PROJECT NO.	FIGURE NO.
3-217-1265	1

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A



SITE PLAN

GEOTECHNICAL ENGINEERING INVESTIGATION
Proposed Arco Station
NWC Iris Avenue & Oliver Street
Moreno Valley, California

SCALE:	DATE:
NOT TO SCALE	11/2017
DRAWN BY:	APPROVED BY:
II	CJ
PROJECT NO.	FIGURE NO.
3-217-1265	2

LEGEND:
- B-1 Soil Boring Location
- P-1 Percolation Location

All Locations Approximate

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

APPENDIX

A

APPENDIX A
FIELD EXPLORATION

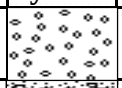
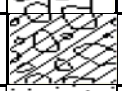
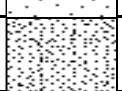
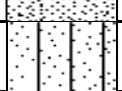
Fieldwork for our investigation (drilling) was conducted on November 14, 2017 and included a site visit, subsurface exploration, and soil sampling. Percolation tests were performed on November 15, 2017. The locations of the exploratory borings and percolation tests are shown on the Site Plan, Figure 2. Boring logs for our exploration are presented in figures following the text in this appendix. Borings were located in the field using existing reference points. Therefore, actual boring locations may deviate slightly.

In general, our borings were performed using a truck-mounted CME 45C drill rig equipped with an 8-inch and a 6-inch hollow-stem augers and a 4-inch diameter solid flight auger. Sampling in the borings was accomplished using a hydraulic 140-pound hammer with a 30-inch drop. Samples were obtained with a 3-inch outside-diameter (OD), split spoon (California Modified) sampler, and a 2-inch OD, Standard Penetration Test (SPT) sampler. The number of blows required to drive the sampler the last 12 inches (or fraction thereof) of the 18-inch sampling interval were recorded on the boring logs. The blow counts shown on the boring logs should not be interpreted as standard SPT "N" values; corrections have not been applied. Upon completion, the borings were backfilled with soil cuttings.

Subsurface conditions encountered in the exploratory borings were visually examined, classified and logged in general accordance with the American Society for Testing and Materials (ASTM) Practice for Description and Identification of Soils (Visual-Manual Procedure D2488). This system uses the Unified Soil Classification System (USCS) for soil designations. The logs depict soil and geologic conditions encountered and depths at which samples were obtained. The logs also include our interpretation of the conditions between sampling intervals. Therefore, the logs contain both observed and interpreted data. We determined the lines designating the interface between soil materials on the logs using visual observations, drill rig penetration rates, excavation characteristics and other factors. The transition between materials may be abrupt or gradual. Where applicable, the field logs were revised based on subsequent laboratory testing.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

Unified Soil Classification System

Major Divisions			Letter	Symbol	Description
Coarse-grained Soils More than ½ retained on the No. 200 Sieve	**Gravels** More than ½ coarse fraction retained on the No. 4 sieve	Clean Gravels	GW		Well-graded gravels and gravel-sand mixtures, little or no fines.
			GP		Poorly-graded gravels and gravel-sand mixtures, little or no fines.
		Gravels With Fines	GM		Silty gravels, gravel-sand-silt mixtures.
			GC		Clayey gravels, gravel-sand-clay mixtures.
	Sands More than ½ passing through the No. 200 sieve	Clean Sands	SW		Well-graded sands and gravelly sands, little or no fines.
			SP		Poorly-graded sands and gravelly sands, little or no fines.
		Sands With Fines	SM		Silty sands, sand-silt mixtures
			SC		Clayey sands, sandy-clay mixtures.
Fine-grained Soils More than ½ passing through the No. 200 Sieve	**Silts and Clays** Liquid Limit less than 50%		ML		Inorganic silts, very fine sands, rock flour, silty or clayey fine sands.
			CL		Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays.
			OL		Organic clays of medium to high plasticity.
	Silts and Clays Liquid Limit greater than 50%		MH		Inorganic silts, micaceous or diatomaceous fines sands or silts, elastic silts.
			CH		Inorganic clays of high plasticity, fat clays.
			OH		Organic clays of medium to high plasticity.
Highly Organic Soils			PT		Peat, muck, and other highly organic soils.

Consistency Classification

Granular Soils			*Cohesive Soils*		
Description - Blows Per Foot (Corrected)			Description - Blows Per Foot (Corrected)		
	MCS	SPT		MCS	SPT
Very loose	<5	<4	Very soft	<3	<2
Loose	5 - 15	4 - 10	Soft	3 - 5	2 - 4
Medium dense	16 - 40	11 - 30	Firm	6 - 10	5 - 8
Dense	41 - 65	31 - 50	Stiff	11 - 20	9 - 15
Very dense	>65	>50	Very Stiff	21 - 40	16 - 30
			Hard	>40	>30

MCS = Modified California Sampler SPT = Standard Penetration Test Sampler

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

Boring No. B-1

Project: Proposed Arco Station
Client: Sater Oil International, LLC
Location: NWC Iris Avenue & Oliver Street, Moreno Valley, CA
Grnd. Surf. Elev. (Ft. MSL) N/A

Project No: 3-217-1265
Figure No.: A-1
Logged By: JH
Initial: None
At Completion: None
Depth to Water>

Depth (ft)	Symbol	Description	Dry Density (pcf)	Moisture Content (%)	Sampler Type	Penetration	Blow Count	Penetration Test (20 40 60 80)	Water Level
0		Ground Surface							
		Silty SAND (SM) Loose; brown; moist; fine to medium-grained.	82.4	10.5	MCS		6		
5		Grades as above.	111.2	3.1	MCS		11		
10		Grades as above; medium dense.	109.1	4.6	MCS		22		
15		**Silty Clayey SAND (SC)** Dense; brown-orange; moist; fine to medium-grained; low plasticity.	--	9.6	SPT		48		
20		**Silty SAND (SM)** Medium dense; brown; moist; fine to medium-grained.	--	4.2	SPT		23		
25		Grades as above.	--	4.9	SPT		28		

Drill Method: Hollow Stem Auger
Drill Rig: CME 45C
Driller: Salem Engineering Group, Inc.
Sheet: 1 of 2

Drill Date: 11/14/2017
Borehole Size: 6 Inches
Hammer Type: Auto Trip
Weight & Drop: 140 lbs./30 in.

SALEM

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

Boring No. B-1

Project: Proposed Arco Station
Client: Sater Oil International, LLC
Location: NWC Iris Avenue & Oliver Street, Moreno Valley, CA
Grnd. Surf. Elev. (Ft. MSL) N/A

Project No: 3-217-1265
Figure No.: A-1
Logged By: JH
Initial: None
Depth to Water>
At Completion: None

SUBSURFACE PROFILE			SAMPLE						
Depth (ft)	Symbol	Description	Dry Density (pcf)	Moisture Content (%)	Sampler Type	Penetration	Blow Count	Penetration Test (20 40 60 80)	Water Level
30		Grades as above; dense.	--	5.6	SPT		37		
35		Grades as above; medium dense.	--	4.9	SPT		25		
40		Grades as above; with trace of clay.	--	5.9	SPT		29		
45		Grades as above.	--	5.9	SPT		25		
50		Grades as above.							
		End of Borehole							

Drill Method: Hollow Stem Auger
Drill Rig: CME 45C
Driller: Salem Engineering Group, Inc.
Sheet: 2 of 2

Drill Date: 11/14/2017
Borehole Size: 6 Inches
Hammer Type: Auto Trip
Weight & Drop: 140 lbs./30 in.

SALEM

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

Boring No. B-2

Project: Proposed Arco Station
Client: Sater Oil International, LLC
Location: NWC Iris Avenue & Oliver Street, Moreno Valley, CA
Grnd. Surf. Elev. (Ft. MSL) N/A

Project No: 3-217-1265
Figure No.: A-2
Logged By: JH
Initial: None
At Completion: None
Depth to Water>

Depth (ft)	Symbol	Description	Dry Density (pcf)	Moisture Content (%)	Sampler Type	Penetration	Blow Count	Penetration Test (20 40 60 80)	Water Level
0		Ground Surface							
		Silty SAND (SM) with trace of Gravel Very loose; brown; moist; fine to coarse-grained.	104.0	4.8	MCS		3		
5		**Silty SAND (SM)** Loose; brown; moist; fine to medium-grained.	108.8	5.4	MCS		9		
10		Grades as above; medium dense.	109.8	4.1	MCS		32		
		Silty Clayey SAND (SC) Very dense; brown; moist; fine to medium-grained.							
15			--	8.4	SPT		50		
		End of Borehole							
20									
25									

Drill Method: Solid Flight Auger
Drill Rig: CME 45C
Driller: Salem Engineering Group, Inc.
Sheet: 1 of 1

Drill Date: 11/14/2017
Borehole Size: 4 Inches
Hammer Type: Auto Trip
Weight & Drop: 140 lbs/30 in.

SALEM

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

Boring No. B-3

Project: Proposed Arco Station
Client: Sater Oil International, LLC
Location: NWC Iris Avenue & Oliver Street, Moreno Valley, CA
Grnd. Surf. Elev. (Ft. MSL) N/A

Project No: 3-217-1265
Figure No.: A-3
Logged By: JH
Initial: None
At Completion: None
Depth to Water>

Depth (ft)	Symbol	Description	Dry Density (pcf)	Moisture Content (%)	Sampler Type	Penetration	Blow Count	Penetration Test (20 40 60 80)	Water Level
0		Ground Surface							
		Silty SAND (SM) Medium dense; brown; moist; fine to medium-grained.	107.2	2.2	MCS		19		
5		Grades as above; loose.	104.4	2.0	MCS		11		
10		Grades as above; medium dense.	108.9	4.5	MCS		17		
		Silty Clayey SAND (SC) Dense; brown; moist; fine to medium-grained.	--	8.6	SPT		48		
15		End of Borehole							
20									
25									

Drill Method: Solid Flight Auger
Drill Rig: CME 45C
Driller: Salem Engineering Group, Inc.
Sheet: 1 of 1

Drill Date: 11/14/2017
Borehole Size: 4 Inches
Hammer Type: Auto Trip
Weight & Drop: 140 lbs/30 in.

SALEM

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

Boring No. B-4

Project: Proposed Arco Station
Client: Sater Oil International, LLC
Location: NWC Iris Avenue & Oliver Street, Moreno Valley, CA
Grnd. Surf. Elev. (Ft. MSL) N/A

Project No: 3-217-1265
Figure No.: A-4
Logged By: JH
Initial: None
At Completion: None
Depth to Water>

Depth (ft)	Symbol	Description	Dry Density (pcf)	Moisture Content (%)	Sampler Type	Penetration	Blow Count
0		Ground Surface					
		Silty SAND (SM) Loose; brown; moist; fine to medium-grained.	111.7	4.0	MCS		7
5		Grades as above.	106.3	5.2	MCS		7
10		Grades as above; medium dense.	112.5	2.5	MCS		22
15		**Silty Clayey SAND (SC)** Dense; brown; moist; fine to medium-grained.	--	9.2	SPT		32
20		**Silty SAND (SM)** Dense; brown; moist; fine to medium-grained.	--	6.4	SPT		36
25		Grades as above.	--	5.4	SPT		39
		End of Borehole					

Penetration Test: 20 40 60 80

Water Level

Drill Method: Solid Flight Auger
Drill Rig: CME 45C
Driller: Salem Engineering Group, Inc.
Sheet: 1 of 1

Drill Date: 11/14/2017
Borehole Size: 4 Inches
Hammer Type: Auto Trip
Weight & Drop: 140 lbs/30 in.

SALEM

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

Boring No. B-5

Project: Proposed Arco Station
Client: Sater Oil International, LLC
Location: NWC Iris Avenue & Oliver Street, Moreno Valley, CA
Grnd. Surf. Elev. (Ft. MSL) N/A

Project No: 3-217-1265
Figure No.: A-5
Logged By: JH
Initial: None
Depth to Water>
At Completion: None

Depth (ft)	Symbol	Description	Dry Density (pcf)	Moisture Content (%)	Sampler Type	Penetration	Blow Count	Penetration Test (20 40 60 80)	Water Level
0		Ground Surface							
		Silty SAND (SM) Loose; brown; moist; fine to medium-grained.	105.7	2.0	MCS		11		
5		Grades as above.	105.8	2.0	MCS		12		
10		Grades as above; medium dense.	114.6	4.4	MCS		23		
15		Grades as above; with clay.	--	7.9	SPT		19		
		End of Borehole							
20									
25									

Drill Method: Solid Flight Auger
Drill Rig: CME 45C
Driller: Salem Engineering Group, Inc.
Sheet: 1 of 1

Drill Date: 11/14/2017
Borehole Size: 4 Inches
Hammer Type: Auto Trip
Weight & Drop: 140 lbs/30 in.

SALEM

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

Percolation Test Worksheet

Project: Proposed Arco Station
NWC Iris Ave & Oliver Street
Moreno Valley, CA

Job No.: 3-217-1265
Date Drilled: 11/14/2017
Soil Classification: Silty SAND (SM)

Hole Radius: 4 in.
Pipe Dia.: 3 in.
Total Depth of Hole: 96 in.

Test Hole No.: P-1
Tested by: JH
Drilled Hole Depth: 8 ft.

Presoaking Date: 11/14/2017
Test Date: 11/15/2017

Stick Up 0 ft

Time Start	Time Finish	Depth of Test Hole (ft)#	Refill-Yes or No	Elapsed Time (hrs:min)	Initial Water Level# (ft)	Final Water Level# (ft)	Δ Water Level (in.)	Δ Min.	Meas. Perc Rate (min/in)	Initial Height of Water (in)	Final Height of Water (in)	Average Height of Water (in)	Infiltration Rate, It (in/hr)
11:21	11:46	8.0	Y	0:25	6.15	6.75	7.20	25	3.5	22.2	15.0	18.6	1.68
11:47	12:12	8.0	Y	0:25	6.22	6.77	6.60	25	3.8	21.4	14.8	18.1	1.58
12:14	12:24	8.0	Y	0:10	6.41	6.62	2.52	10	4.0	19.1	16.6	17.8	1.53
12:24	12:34	8.0	N	0:10	6.62	6.80	2.16	10	4.6	16.6	14.4	15.5	1.48
12:34	12:44	8.0	N	0:10	6.80	6.96	1.92	10	5.2	14.4	12.5	13.4	1.49
12:44	12:54	8.0	N	0:10	6.96	7.10	1.68	10	6.0	12.5	10.8	11.6	1.48
12:54	13:04	8.0	N	0:10	7.10	7.22	1.44	10	6.9	10.8	9.4	10.1	1.43
13:04	13:14	8.0	N	0:10	7.22	7.33	1.32	10	7.6	9.4	8.0	8.7	1.48

Recommended for Design: **Infiltration Rate** **1.43**

SALEM engineering group, Inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

Percolation Test Worksheet

Project: Proposed Arco Station
NWC Iris Ave & Oliver Street
Moreno Valley, CA

Job No.: 3-217-1265
Date Drilled: 11/14/2017
Soil Classification: Silty SAND (SM)

Hole Radius: 4 in.
Pipe Dia.: 3 in.
Total Depth of Hole: 120 in.

Test Hole No.: P-2
Tested by: JH
Drilled Hole Depth: 10 ft.

Presoaking Date: 11/14/2017
Test Date: 11/15/2017

Stick Up 0 ft

Time Start	Time Finish	Depth of Test Hole (ft)#	Refill-Yes or No	Elapsed Time (hrs:min)	Initial Water Level# (ft)	Final Water Level# (ft)	Δ Water Level (in.)	Δ Min.	Meas. Perc Rate (min/in)	Initial Height of Water (in)	Final Height of Water (in)	Average Height of Water (in)	Infiltration Rate, It (in/hr)
11:13	11:43	10.0	Y	0:30	6.25	6.91	7.92	30	3.8	45.0	37.1	41.0	0.74
11:43	12:13	10.0	N	0:30	6.91	7.41	6.00	30	5.0	37.1	31.1	34.1	0.67
12:13	12:43	10.0	N	0:30	7.41	7.82	4.92	30	6.1	31.1	26.2	28.6	0.64
12:43	13:13	10.0	N	0:30	7.82	8.15	3.96	30	7.6	26.2	22.2	24.2	0.61
13:13	13:43	10.0	N	0:30	8.15	8.42	3.24	30	9.3	22.2	19.0	20.6	0.57
13:43	14:13	10.0	N	0:30	8.42	8.65	2.76	30	10.9	19.0	16.2	17.6	0.56
14:13	14:43	10.0	N	0:30	8.65	8.85	2.40	30	12.5	16.2	13.8	15.0	0.56
14:43	15:13	10.0	N	0:30	8.85	9.02	2.04	30	14.7	13.8	11.8	12.8	0.55
15:13	15:43	10.0	N	0:30	9.02	9.17	1.80	30	16.7	11.8	10.0	10.9	0.56
15:43	16:13	10.0	N	0:30	9.17	9.30	1.56	30	19.2	10.0	8.4	9.2	0.56
16:13	16:43	10.0	N	0:30	9.30	9.42	1.44	30	20.8	8.4	7.0	7.7	0.60
16:43	17:13	10.0	N	0:30	9.42	9.52	1.20	30	25.0	7.0	5.8	6.4	0.57
Recommended for Design:										**Infiltration Rate**			**0.55**

SALEM engineering group

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

Percolation Test Worksheet

Project: Proposed Arco Station
NWC Iris Ave & Oliver Street
Moreno Valley, CA

Job No.: 3-217-1265
Date Drilled: 11/14/2017
Soil Classification: Silty SAND (SM)

Hole Radius: 4 in.
Pipe Dia.: 3 in.
Total Depth of Hole: 96 in.

Test Hole No.: P-3
Tested by: JH
Drilled Hole Depth: 8 ft.

Presoaking Date: 11/14/2017
Test Date: 11/15/2017

Stick Up 0 ft

Time Start	Time Finish	Depth of Test Hole (ft)#	Refill-Yes or No	Elapsed Time (hrs:min)	Initial Water Level# (ft)	Final Water Level# (ft)	Δ Water Level (in.)	Δ Min.	Meas. Perc Rate (min/in)	Initial Height of Water (in)	Final Height of Water (in)	Average Height of Water (in)	Infiltration Rate, It (in/hr)
11:15	11:45	8.0	Y	0:30	4.52	5.11	7.08	30	4.2	41.8	34.7	38.2	0.70
11:45	12:15	8.0	N	0:30	5.11	5.54	5.16	30	5.8	34.7	29.5	32.1	0.61
12:15	12:45	8.0	N	0:30	5.54	5.88	4.08	30	7.4	29.5	25.4	27.5	0.55
12:45	13:15	8.0	N	0:30	5.88	6.16	3.36	30	8.9	25.4	22.1	23.8	0.52
13:15	13:45	8.0	N	0:30	6.16	6.40	2.88	30	10.4	22.1	19.2	20.6	0.51
13:45	14:15	8.0	N	0:30	6.40	6.61	2.52	30	11.9	19.2	16.7	17.9	0.51
14:15	14:45	8.0	N	0:30	6.61	6.80	2.28	30	13.2	16.7	14.4	15.5	0.52
14:45	15:15	8.0	N	0:30	6.80	6.97	2.04	30	14.7	14.4	12.4	13.4	0.53
15:15	15:45	8.0	N	0:30	6.97	7.12	1.80	30	16.7	12.4	10.6	11.5	0.53
15:45	16:15	8.0	N	0:30	7.12	7.25	1.56	30	19.2	10.6	9.0	9.8	0.53
16:15	16:45	8.0	N	0:30	7.25	7.36	1.32	30	22.7	9.0	7.7	8.3	0.51
16:45	17:15	8.0	N	0:30	7.36	7.46	1.20	30	25.0	7.7	6.5	7.1	0.53
Recommended for Design:										**Infiltration Rate**			**0.51**

SALEM engineering group

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

Percolation Test Worksheet

Project: Proposed Arco Station
NWC Iris Ave & Oliver Street
Moreno Valley, CA

Job No.: 3-217-1265
Date Drilled: 11/14/2017
Soil Classification: Silty SAND (SM)

Hole Radius: 4 in.
Pipe Dia.: 3 in.
Total Depth of Hole: 120 in.

Test Hole No.: P-4
Tested by: JH
Drilled Hole Depth: 10 ft.

Presoaking Date: 11/14/2017
Test Date: 11/15/2017

Stick Up 0 ft

Time Start	Time Finish	Depth of Test Hole (ft)#	Refill-Yes or No	Elapsed Time (hrs:min)	Initial Water Level# (ft)	Final Water Level# (ft)	Δ Water Level (in.)	Δ Min.	Meas. Perc Rate (min/in)	Initial Height of Water (in)	Final Height of Water (in)	Average Height of Water (in)	Infiltration Rate, It (in/hr)
11:23	11:48	10.0	Y	0:25	8.00	8.57	6.84	25	3.7	24.0	17.2	20.6	1.45
11:49	12:14	10.0	Y	0:25	8.11	8.62	6.12	25	4.1	22.7	16.6	19.6	1.36
12:16	12:26	10.0	Y	0:10	8.36	8.55	2.28	10	4.4	19.7	17.4	18.5	1.33
12:26	12:36	10.0	N	0:10	8.55	8.72	2.04	10	4.9	17.4	15.4	16.4	1.33
12:36	12:46	10.0	N	0:10	8.72	8.87	1.80	10	5.6	15.4	13.6	14.5	1.31
12:46	12:56	10.0	N	0:10	8.87	9.00	1.56	10	6.4	13.6	12.0	12.8	1.27
12:56	13:06	10.0	N	0:10	9.00	9.12	1.44	10	6.9	12.0	10.6	11.3	1.30
13:06	13:16	10.0	N	0:10	9.12	9.23	1.32	10	7.6	10.6	9.2	9.9	1.33

Recommended for Design: **Infiltration Rate** **1.27**

SALEM engineering group, Inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

APPENDIX

B

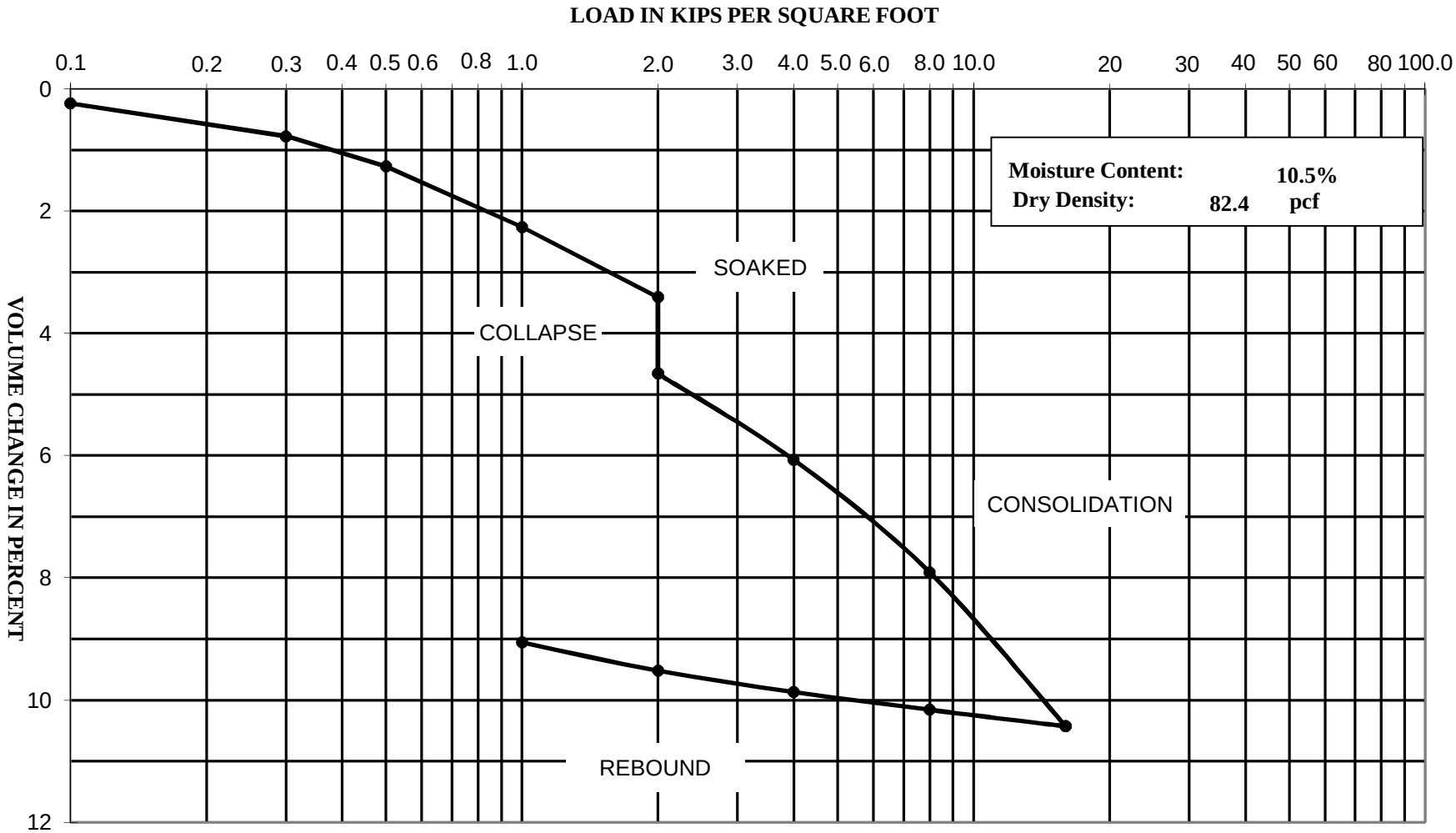
APPENDIX B
LABORATORY TESTING

Laboratory tests were performed in accordance with generally accepted test methods of the American Society for Testing and Materials (ASTM), Caltrans, or other suggested procedures. Selected samples were tested for in-situ dry density and moisture content, corrosivity, consolidation, shear strength, maximum density and optimum moisture content, and grain size distribution. The results of the laboratory tests are summarized in the following figures.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

CONSOLIDATION - PRESSURE TEST DATA

ASTM D 2435



Prop. Arco Station - Moreno Valley, CA

Project Number: 3-217-1265

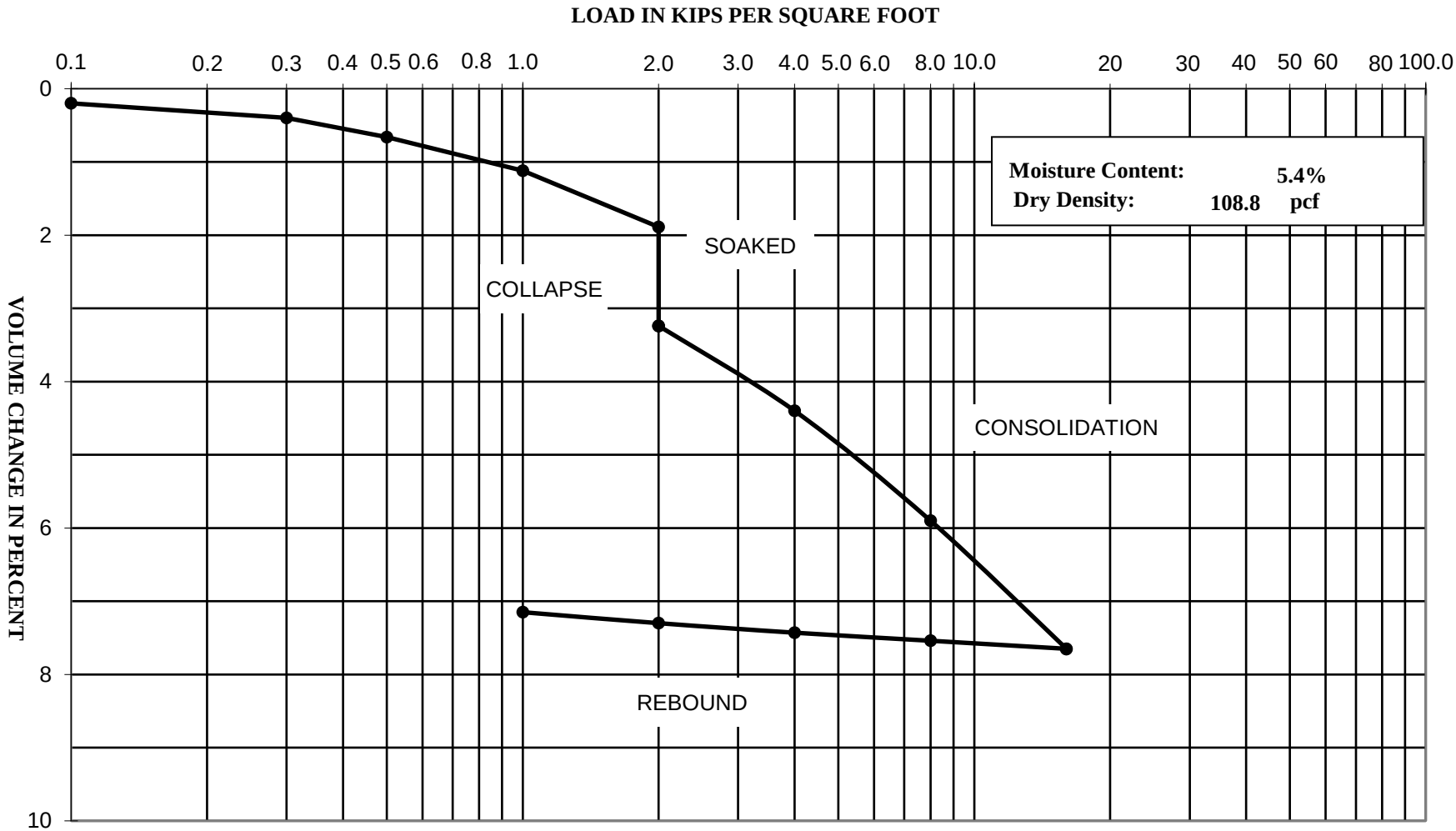
Boring: B-1 @ 2'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

CONSOLIDATION - PRESSURE TEST DATA

ASTM D 2435



Prop. Arco Station - Moreno Valley, CA

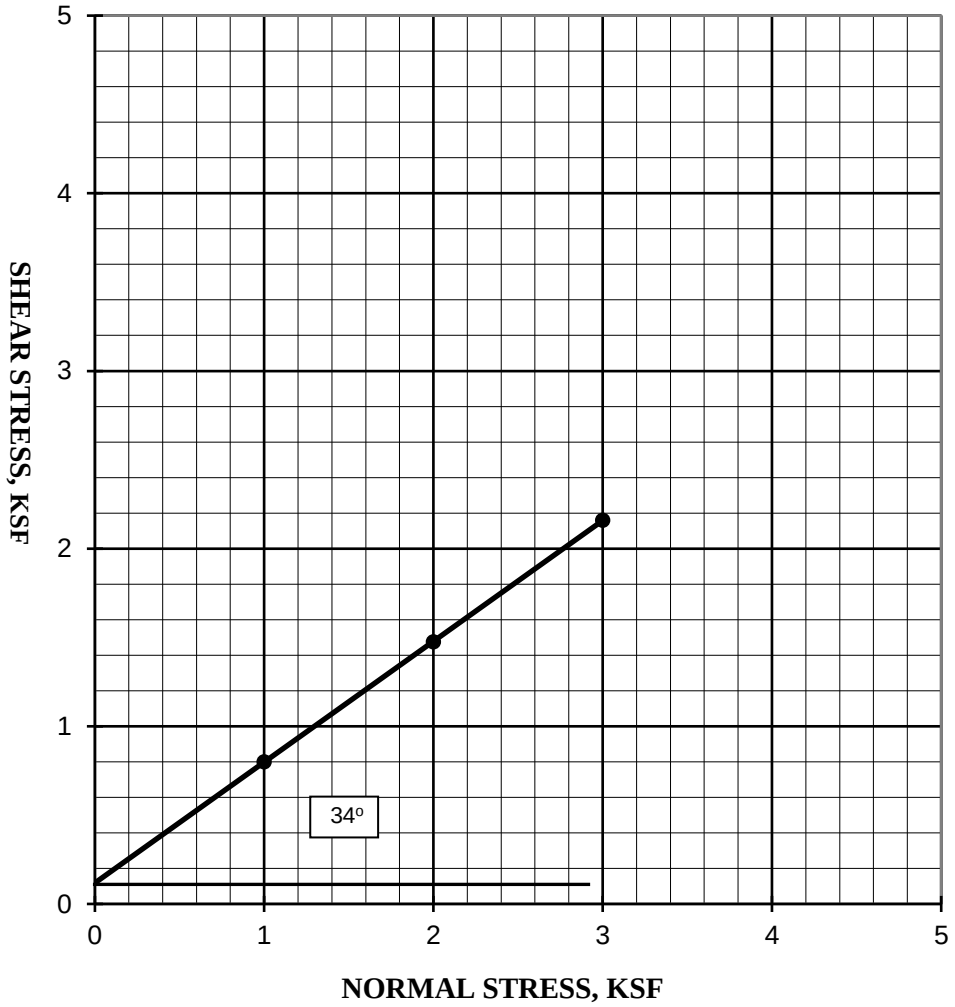
Project Number: 3-217-1265

Boring: B-2 @ 5'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

SHEAR STRENGTH DIAGRAM
(DIRECT SHEAR)
ASTM D - 3080



Prop. Arco Station - Moreno Valley, CA

Project Number: 3-217-1265

Boring: B-1 @ 5'
Soil Type: Silty SAND (SM)

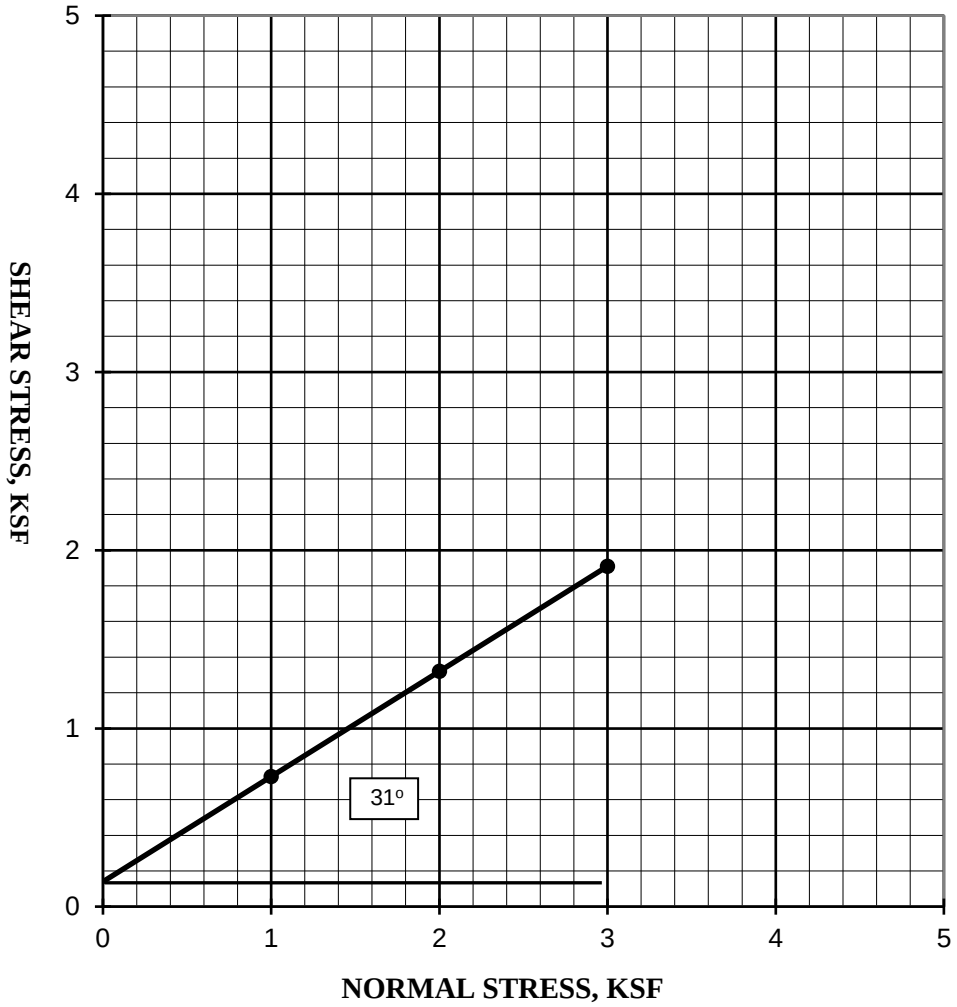
Friction Angle:	**34**	**degrees**
Cohesion:	**120**	**psf**

Moisture Content	**3.1%**
Dry Density	**111.2 pcf**

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

SHEAR STRENGTH DIAGRAM
(DIRECT SHEAR)
ASTM D - 3080



Prop. Arco Station - Moreno Valley, CA

Project Number: 3-217-1265

Boring: B-2 @ 2'
Soil Type: Silty SAND (SM)

Friction Angle:	**31**	**degrees**
Cohesion:	**140**	**psf**

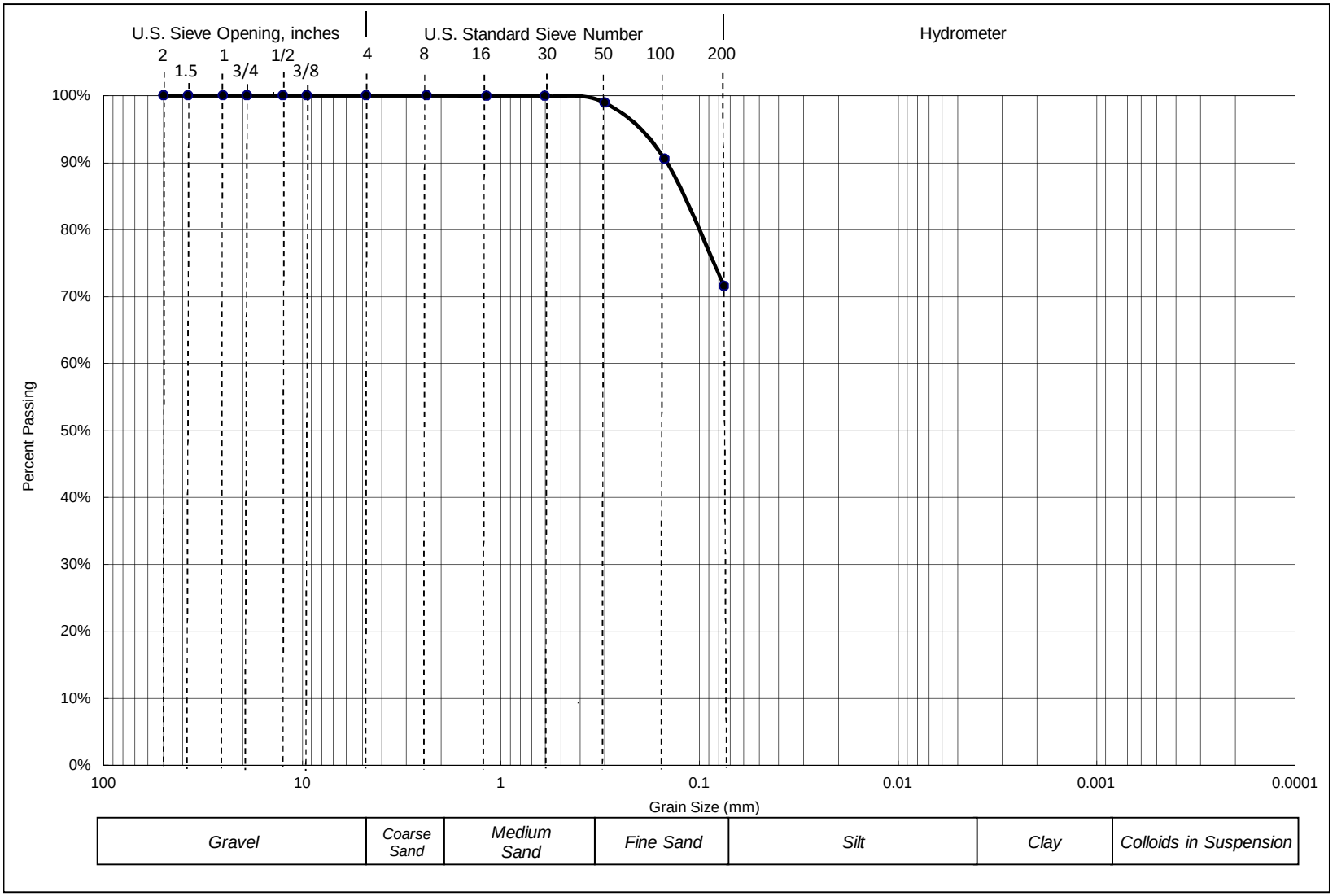
Moisture Content	**4.8%**
Dry Density	**104.0 pcf**

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

PARTICLE SIZE DISTRIBUTION DIAGRAM

GRADATION TEST - ASTM C136



Prop. Arco Station - Moreno Valley, CA

Project Number: 3-217-1265

Boring: B-1 @ 2'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

DRY SIEVE ANALYSIS

ASTM C136 (without Hydrometer)

Sieve Size	Particle Size, mm	Percent Passing
1 1/2-in.	37.5	100.0%
1-in.	25	100.0%
3/4-in.	19	100.0%
1/2-in.	12.5	100.0%
3/8-in.	9.5	100.0%
No. 4	4.75	100.0%
No. 8	2.36	100.0%
No. 16	1.18	100.0%
No. 30	0.6	100.0%
No. 50	0.3	99.0%
No. 100	0.15	90.6%
No. 200	0.075	71.59%

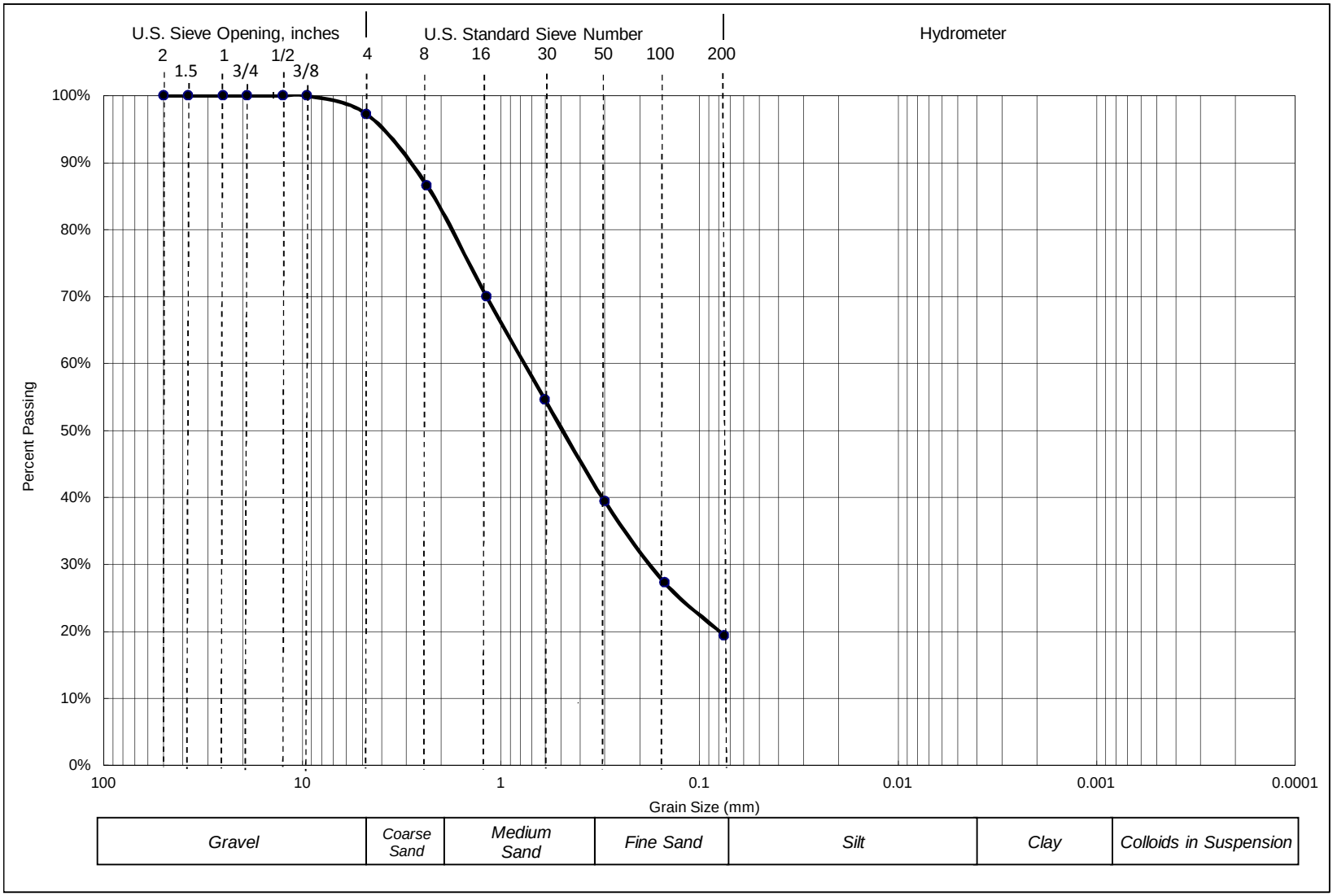
Prop. Arco Station - Moreno Valley, CA
Project Number: 3-217-1265
Boring: B-1 @ 2'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

PARTICLE SIZE DISTRIBUTION DIAGRAM

GRADATION TEST - ASTM C136



Prop. Arco Station - Moreno Valley, CA

Project Number: 3-217-1265

Boring: B-1 @ 5'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

DRY SIEVE ANALYSIS

ASTM C136 (without Hydrometer)

Sieve Size	Particle Size, mm	Percent Passing
1 1/2-in.	37.5	100.0%
1-in.	25	100.0%
3/4-in.	19	100.0%
1/2-in.	12.5	100.0%
3/8-in.	9.5	100.0%
No. 4	4.75	97.2%
No. 8	2.36	86.6%
No. 16	1.18	70.0%
No. 30	0.6	54.6%
No. 50	0.3	39.4%
No. 100	0.15	27.3%
No. 200	0.075	19.36%

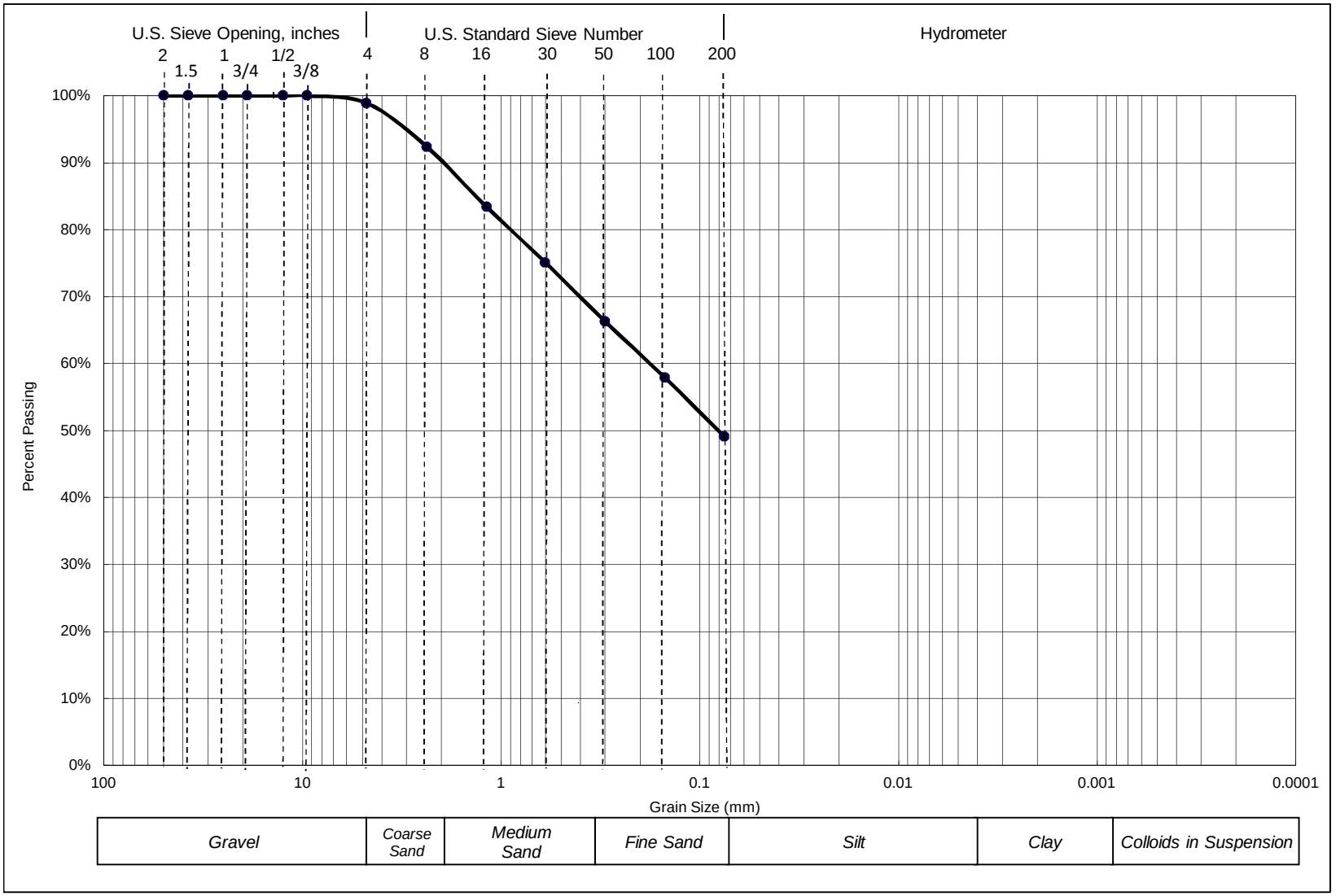
Prop. Arco Station - Moreno Valley, CA
Project Number: 3-217-1265
Boring: B-1 @ 5'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

PARTICLE SIZE DISTRIBUTION DIAGRAM

GRADATION TEST - ASTM C136



Prop. Arco Station - Moreno Valley, CA

Project Number: 3-217-1265

Boring: B-1 @ 15'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

DRY SIEVE ANALYSIS

ASTM C136 (without Hydrometer)

Sieve Size	Particle Size, mm	Percent Passing
1 1/2-in.	37.5	100.0%
1-in.	25	100.0%
3/4-in.	19	100.0%
1/2-in.	12.5	100.0%
3/8-in.	9.5	100.0%
No. 4	4.75	98.9%
No. 8	2.36	92.3%
No. 16	1.18	83.4%
No. 30	0.6	75.1%
No. 50	0.3	66.3%
No. 100	0.15	57.9%
No. 200	0.075	49.05%

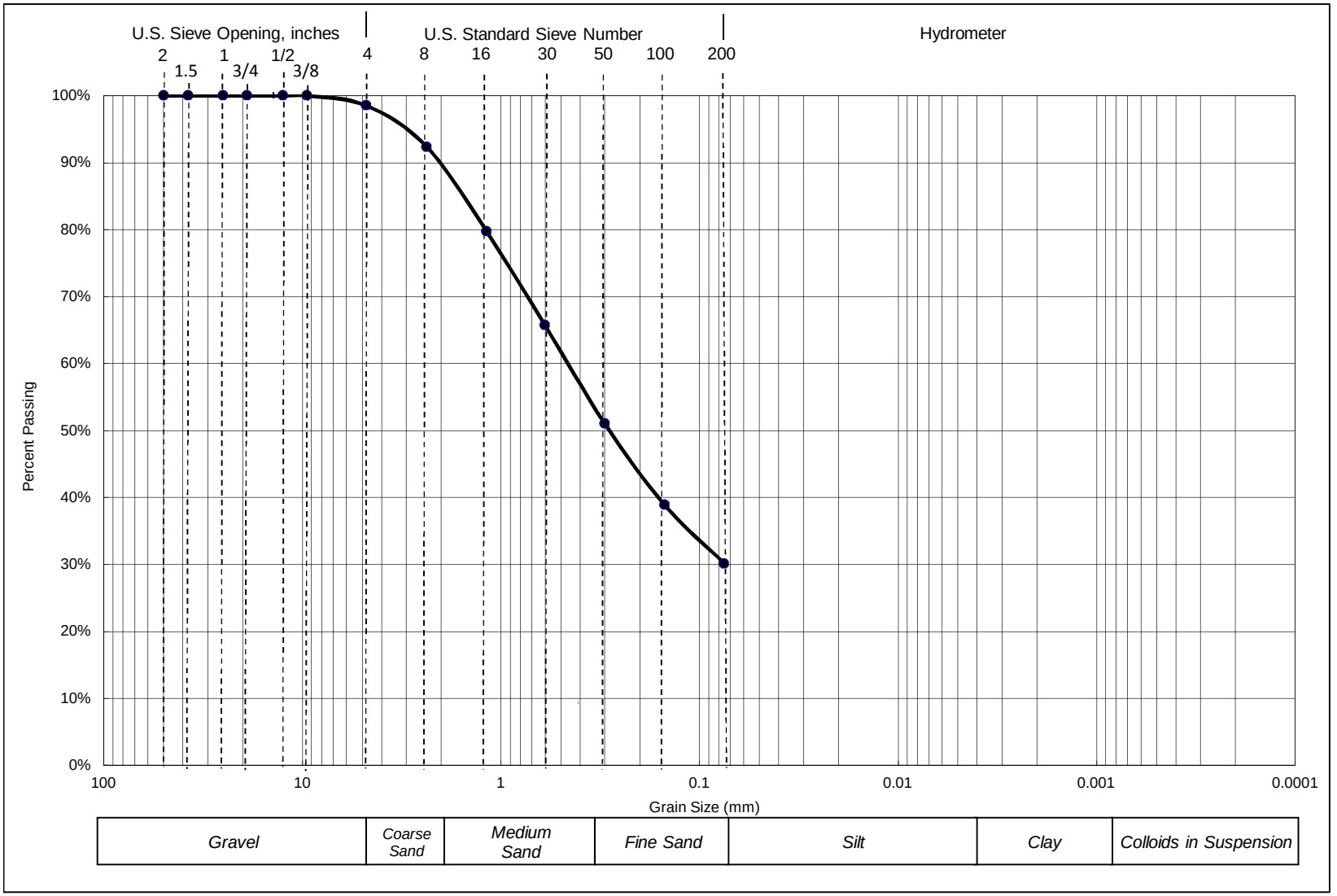
Prop. Arco Station - Moreno Valley, CA
Project Number: 3-217-1265
Boring: B-1 @ 15'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

PARTICLE SIZE DISTRIBUTION DIAGRAM

GRADATION TEST - ASTM C136



Prop. Arco Station - Moreno Valley, CA

Project Number: 3-217-1265

Boring: B-1 @ 30'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

DRY SIEVE ANALYSIS

ASTM C136 (without Hydrometer)

Sieve Size	Particle Size, mm	Percent Passing
1 1/2-in.	37.5	100.0%
1-in.	25	100.0%
3/4-in.	19	100.0%
1/2-in.	12.5	100.0%
3/8-in.	9.5	100.0%
No. 4	4.75	98.5%
No. 8	2.36	92.3%
No. 16	1.18	79.7%
No. 30	0.6	65.7%
No. 50	0.3	51.0%
No. 100	0.15	38.9%
No. 200	0.075	30.13%

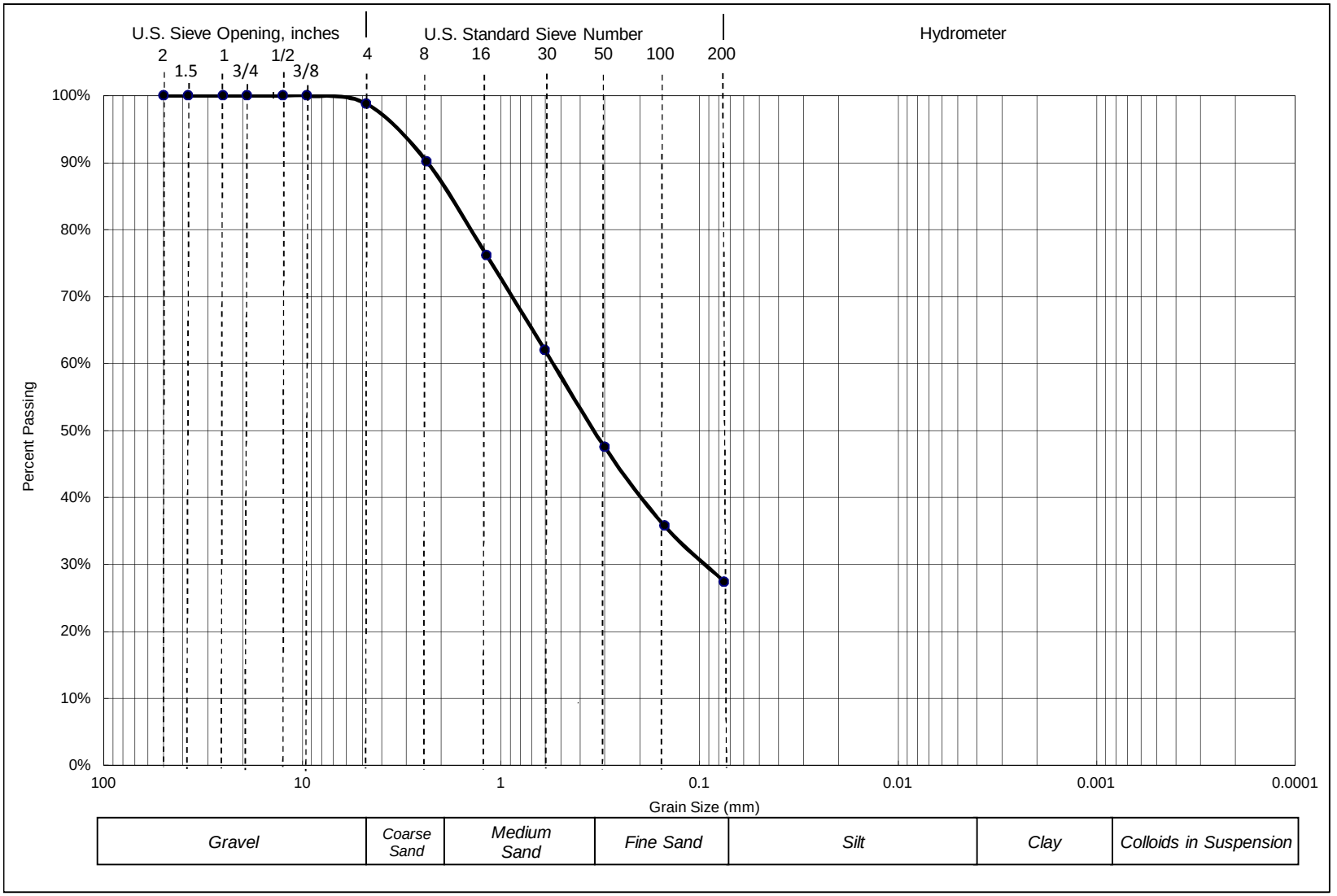
Prop. Arco Station - Moreno Valley, CA
Project Number: 3-217-1265
Boring: B-1 @ 30'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

PARTICLE SIZE DISTRIBUTION DIAGRAM

GRADATION TEST - ASTM C136



Prop. Arco Station - Moreno Valley, CA

Project Number: 3-217-1265

Boring: B-1 @ 40'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

DRY SIEVE ANALYSIS

ASTM C136 (without Hydrometer)

Sieve Size	Particle Size, mm	Percent Passing
1 1/2-in.	37.5	100.0%
1-in.	25	100.0%
3/4-in.	19	100.0%
1/2-in.	12.5	100.0%
3/8-in.	9.5	100.0%
No. 4	4.75	98.8%
No. 8	2.36	90.1%
No. 16	1.18	76.1%
No. 30	0.6	62.0%
No. 50	0.3	47.5%
No. 100	0.15	35.7%
No. 200	0.075	27.40%

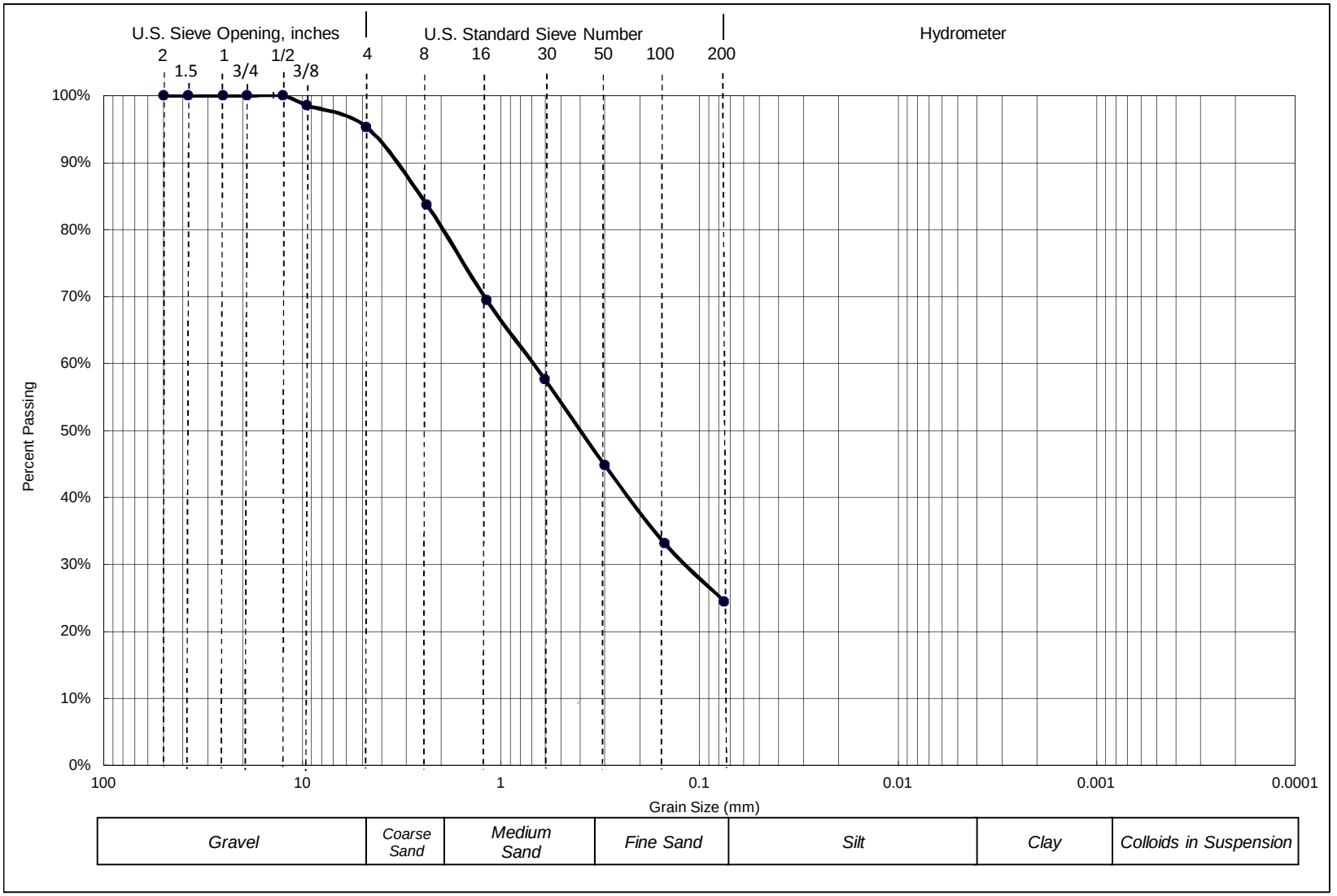
Prop. Arco Station - Moreno Valley, CA
Project Number: 3-217-1265
Boring: B-1 @ 40'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

PARTICLE SIZE DISTRIBUTION DIAGRAM

GRADATION TEST - ASTM C136



Prop. Arco Station - Moreno Valley, CA

Project Number: 3-217-1265

Boring: B-2 @ 2'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

DRY SIEVE ANALYSIS

ASTM C136 (without Hydrometer)

Sieve Size	Particle Size, mm	Percent Passing
1 1/2-in.	37.5	100.0%
1-in.	25	100.0%
3/4-in.	19	100.0%
1/2-in.	12.5	100.0%
3/8-in.	9.5	98.6%
No. 4	4.75	95.3%
No. 8	2.36	83.7%
No. 16	1.18	69.5%
No. 30	0.6	57.6%
No. 50	0.3	44.8%
No. 100	0.15	33.2%
No. 200	0.075	24.46%

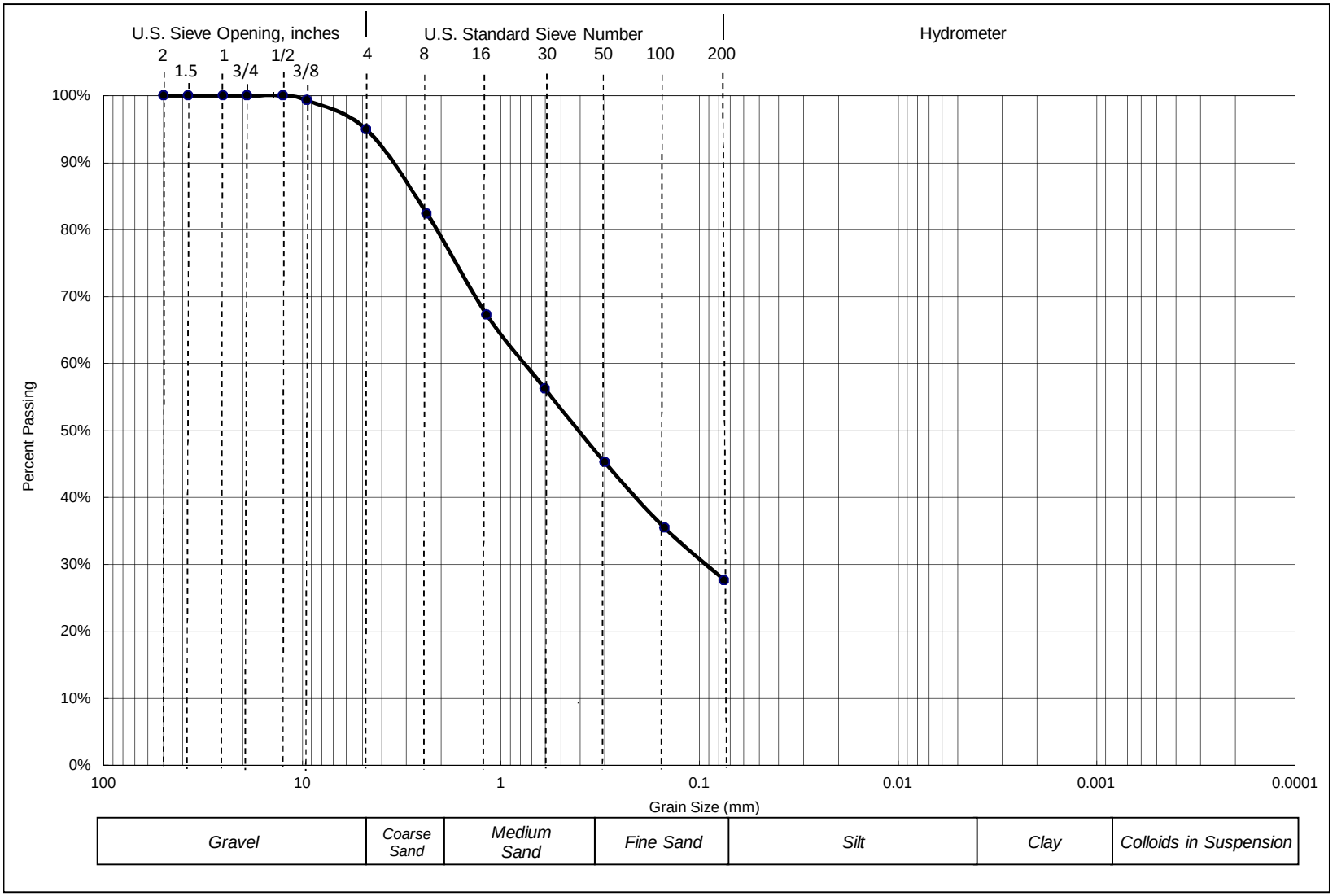
Prop. Arco Station - Moreno Valley, CA
Project Number: 3-217-1265
Boring: B-2 @ 2'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

PARTICLE SIZE DISTRIBUTION DIAGRAM

GRADATION TEST - ASTM C136



Prop. Arco Station - Moreno Valley, CA

Project Number: 3-217-1265

Boring: B-2 @ 5'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A

DRY SIEVE ANALYSIS

ASTM C136 (without Hydrometer)

Sieve Size	Particle Size, mm	Percent Passing
1 1/2-in.	37.5	100.0%
1-in.	25	100.0%
3/4-in.	19	100.0%
1/2-in.	12.5	100.0%
3/8-in.	9.5	99.3%
No. 4	4.75	95.0%
No. 8	2.36	82.4%
No. 16	1.18	67.3%
No. 30	0.6	56.2%
No. 50	0.3	45.2%
No. 100	0.15	35.5%
No. 200	0.075	27.65%

Prop. Arco Station - Moreno Valley, CA
Project Number: 3-217-1265
Boring: B-2 @ 5'

SALEM engineering group, inc.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

CHEMICAL ANALYSIS

SO_4 - Modified Caltrans 417 & Cl - Modified Caltrans 417/422

Prop. Arco Station - Moreno Valley, CA
Project Number: 3-217-1265
Date: 11/17/17
Soil Classification: Silty SAND (SM)

Sample Number	Sample Location	Soluble Sulfate SO_4-S	Soluble Chloride Cl	pH
1a.	B-1 @ 0 - 3'	50 mg/kg	21 mg/kg	7.0
1b.	B-1 @ 0 - 3'	50 mg/kg	20 mg/kg	7.0
1c.	B-1 @ 0 - 3'	50 mg/kg	21 mg/kg	7.0
Average:		**50 mg/kg**	**21 mg/kg**	**7.0**

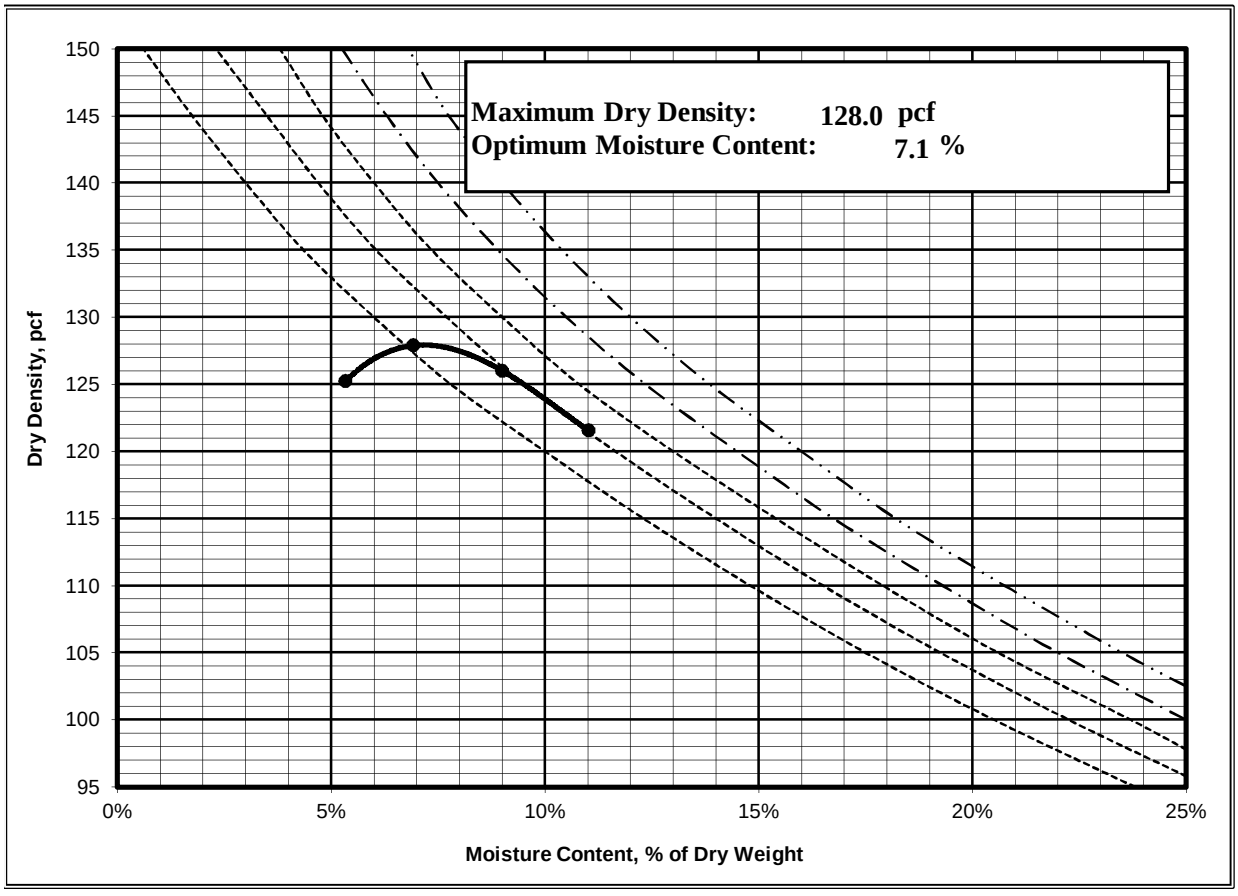
Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

SALEM engineering group, inc.

Laboratory Compaction Curve
ASTM D1557

Prop. Arco Station - Moreno Valley, CA
Project Number: 3-217-1265
Date Tested: 11/17/17
Sample Location: B-1 @ 0 - 3'
Soil Classification: Silty Sand, Brown, Non-Cohesive
Sample/Curve Number: 1
Test Method: 1557 A

	1	2	3	4
Weight of Moist Specimen & Mold, (g)	3991.6	4064.2	4073.2	4037.0
Weight of Compaction Mold, (g)	1998.9	1998.9	1998.9	1998.9
Weight of Moist Specimen, (g)	1992.7	2065.3	2074.3	2038.1
Volume of mold, (ft^2)	0.0333	0.0333	0.0333	0.0333
Wet Density, (pcf)	131.9	136.7	137.3	134.9
Weight of Wet (Moisture) Sample, (g)	341.2	341.2	341.2	341.2
Weight of Dry (Moisture) Sample, (g)	323.9	319.1	313.0	307.3
Moisture Content, (%)	5.3%	6.9%	9.0%	11.0%
Dry Density, (pcf)	125.2	127.9	126.0	121.5



Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

SALEM engineering group, inc.

APPENDIX

C

APPENDIX C
GENERAL EARTHWORK AND PAVEMENT SPECIFICATIONS

When the text of the report conflicts with the general specifications in this appendix, the recommendations in the report have precedence.

1.0 SCOPE OF WORK: These specifications and applicable plans pertain to and include all earthwork associated with the site rough grading, including, but not limited to, the furnishing of all labor, tools and equipment necessary for site clearing and grubbing, stripping, preparation of foundation materials for receiving fill, excavation, processing, placement and compaction of fill and backfill materials to the lines and grades shown on the project grading plans and disposal of excess materials.

2.0 PERFORMANCE: The Contractor shall be responsible for the satisfactory completion of all earthwork in accordance with the project plans and specifications. This work shall be inspected and tested by a representative of SALEM Engineering Group, Incorporated, hereinafter referred to as the Soils Engineer and/or Testing Agency. Attainment of design grades, when achieved, shall be certified by the project Civil Engineer. Both the Soils Engineer and the Civil Engineer are the Owner's representatives. If the Contractor should fail to meet the technical or design requirements embodied in this document and on the applicable plans, he shall make the necessary adjustments until all work is deemed satisfactory as determined by both the Soils Engineer and the Civil Engineer. No deviation from these specifications shall be made except upon written approval of the Soils Engineer, Civil Engineer, or project Architect.

No earthwork shall be performed without the physical presence or approval of the Soils Engineer. The Contractor shall notify the Soils Engineer at least 2 working days prior to the commencement of any aspect of the site earthwork.

The Contractor shall assume sole and complete responsibility for job site conditions during the course of construction of this project, including safety of all persons and property; that this requirement shall apply continuously and not be limited to normal working hours; and that the Contractor shall defend, indemnify and hold the Owner and the Engineers harmless from any and all liability, real or alleged, in connection with the performance of work on this project, except for liability arising from the sole negligence of the Owner or the Engineers.

3.0 TECHNICAL REQUIREMENTS: All compacted materials shall be densified to no less that 95 percent of relative compaction (90 percent for cohesive soils) based on ASTM D1557 Test Method (latest edition), UBC or CAL-216, or as specified in the technical portion of the Soil Engineer's report. The location and frequency of field density tests shall be determined by the Soils Engineer. The results of these tests and compliance with these specifications shall be the basis upon which satisfactory completion of work will be judged by the Soils Engineer.

4.0 SOILS AND FOUNDATION CONDITIONS: The Contractor is presumed to have visited the site and to have familiarized himself with existing site conditions and the contents of the data presented in the Geotechnical Engineering Report. The Contractor shall make his own interpretation of the data contained in the Geotechnical Engineering Report and the Contractor shall not be relieved of liability for any loss sustained as a result of any variance between conditions indicated by or deduced from said report and the actual conditions encountered during the progress of the work.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

5.0 DUST CONTROL: The work includes dust control as required for the alleviation or prevention of any dust nuisance on or about the site or the borrow area, or off-site if caused by the Contractor's operation either during the performance of the earthwork or resulting from the conditions in which the Contractor leaves the site. The Contractor shall assume all liability, including court costs of codefendants, for all claims related to dust or wind-blown materials attributable to his work. Site preparation shall consist of site clearing and grubbing and preparation of foundation materials for receiving fill.

6.0 CLEARING AND GRUBBING: The Contractor shall accept the site in this present condition and shall demolish and/or remove from the area of designated project earthwork all structures, both surface and subsurface, trees, brush, roots, debris, organic matter and all other matter determined by the Soils Engineer to be deleterious. Such materials shall become the property of the Contractor and shall be removed from the site.

Tree root systems in proposed improvement areas should be removed to a minimum depth of 3 feet and to such an extent which would permit removal of all roots greater than 1 inch in diameter. Tree roots removed in parking areas may be limited to the upper 1½ feet of the ground surface. Backfill of tree root excavations is not permitted until all exposed surfaces have been inspected and the Soils Engineer is present for the proper control of backfill placement and compaction. Burning in areas which are to receive fill materials shall not be permitted.

7.0 SUBGRADE PREPARATION: Surfaces to receive Engineered Fill and/or building or slab loads shall be prepared as outlined above, scarified to a minimum of 12 inches, moisture-conditioned as necessary, and recompacted to 95 percent relative compaction (90 percent for cohesive soils).

Loose soil areas and/or areas of disturbed soil shall be moisture-conditioned as necessary and recompacted to 95 percent relative compaction (90 percent for cohesive soils). All ruts, hummocks, or other uneven surface features shall be removed by surface grading prior to placement of any fill materials. All areas which are to receive fill materials shall be approved by the Soils Engineer prior to the placement of any fill material.

8.0 EXCAVATION: All excavation shall be accomplished to the tolerance normally defined by the Civil Engineer as shown on the project grading plans. All over-excavation below the grades specified shall be backfilled at the Contractor's expense and shall be compacted in accordance with the applicable technical requirements.

9.0 FILL AND BACKFILL MATERIAL: No material shall be moved or compacted without the presence or approval of the Soils Engineer. Material from the required site excavation may be utilized for construction site fills, provided prior approval is given by the Soils Engineer. All materials utilized for constructing site fills shall be free from vegetation or other deleterious matter as determined by the Soils Engineer.

10.0 PLACEMENT, SPREADING AND COMPACTION: The placement and spreading of approved fill materials and the processing and compaction of approved fill and native materials shall be the responsibility of the Contractor. Compaction of fill materials by flooding, ponding, or jetting shall not be permitted unless specifically approved by local code, as well as the Soils Engineer. Both cut and fill shall be surface-compacted to the satisfaction of the Soils Engineer prior to final acceptance.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

11.0 SEASONAL LIMITS: No fill material shall be placed, spread, or rolled while it is frozen or thawing, or during unfavorable wet weather conditions. When the work is interrupted by heavy rains, fill operations shall not be resumed until the Soils Engineer indicates that the moisture content and density of previously placed fill is as specified.

12.0 DEFINITIONS - The term "pavement" shall include asphaltic concrete surfacing, untreated aggregate base, and aggregate subbase. The term "subgrade" is that portion of the area on which surfacing, base, or subbase is to be placed.

The term "Standard Specifications": hereinafter referred to, is the most recent edition of the Standard Specifications of the State of California, Department of Transportation. The term "relative compaction" refers to the field density expressed as a percentage of the maximum laboratory density as determined by ASTM D1557 Test Method (latest edition) or California Test Method 216 (CAL-216), as applicable.

13.0 PREPARATION OF THE SUBGRADE - The Contractor shall prepare the surface of the various subgrades receiving subsequent pavement courses to the lines, grades, and dimensions given on the plans. The upper 12 inches of the soil subgrade beneath the pavement section shall be compacted to a minimum relative compaction of 95 percent based upon ASTM D1557. The finished subgrades shall be tested and approved by the Soils Engineer prior to the placement of additional pavement courses.

14.0 AGGREGATE BASE - The aggregate base material shall be spread and compacted on the prepared subgrade in conformity with the lines, grades, and dimensions shown on the plans. The aggregate base material shall conform to the requirements of Section 26 of the Standard Specifications for Class II material, ¾-inch or 1½-inches maximum size. The aggregate base material shall be compacted to a minimum relative compaction of 95 percent based upon CAL-216. The aggregate base material shall be spread in layers not exceeding 6 inches and each layer of aggregate material course shall be tested and approved by the Soils Engineer prior to the placement of successive layers.

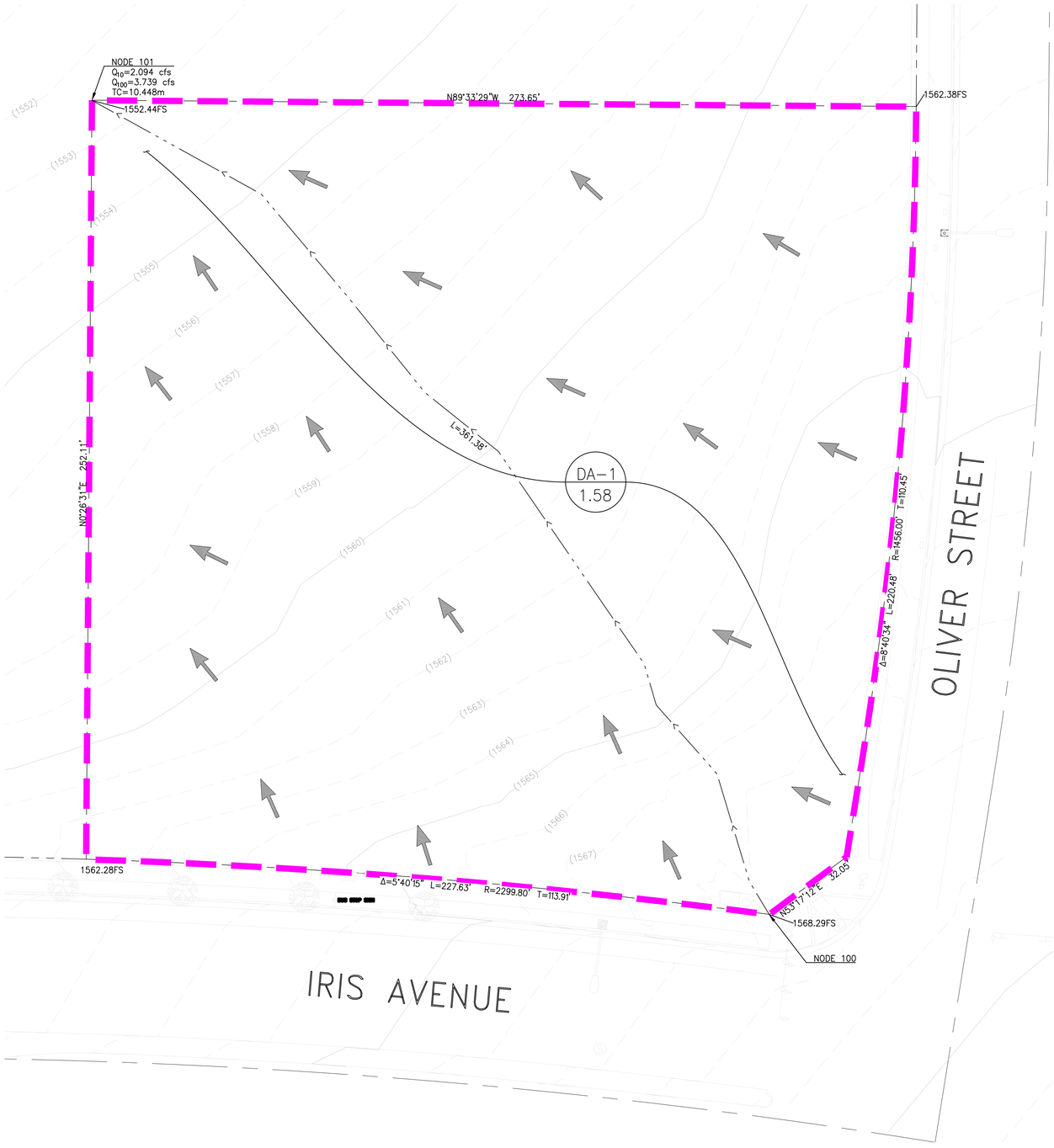
15.0 AGGREGATE SUBBASE - The aggregate subbase shall be spread and compacted on the prepared subgrade in conformity with the lines, grades, and dimensions shown on the plans. The aggregate subbase material shall conform to the requirements of Section 25 of the Standard Specifications for Class II Subbase material. The aggregate subbase material shall be compacted to a minimum relative compaction of 95 percent based upon CAL-216, and it shall be spread and compacted in accordance with the Standard Specifications. Each layer of aggregate subbase shall be tested and approved by the Soils Engineer prior to the placement of successive layers.

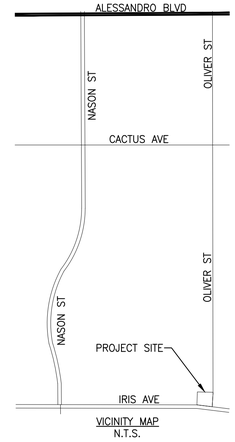
16.0 ASPHALTIC CONCRETE SURFACING - Asphaltic concrete surfacing shall consist of a mixture of mineral aggregate and paving grade asphalt, mixed at a central mixing plant and spread and compacted on a prepared base in conformity with the lines, grades, and dimensions shown on the plans. The viscosity grade of the asphalt shall be PG 64-10, unless otherwise stipulated or local conditions warrant more stringent grade. The mineral aggregate shall be Type A or B, ½ inch maximum size, medium grading, and shall conform to the requirements set forth in Section 39 of the Standard Specifications. The drying, proportioning, and mixing of the materials shall conform to Section 39. The prime coat, spreading and compacting equipment, and spreading and compacting the mixture shall conform to the applicable chapters of Section 39, with the exception that no surface course shall be placed when the atmospheric temperature is below 50 degrees F. The surfacing shall be rolled with a combination steel-wheel and pneumatic rollers, as described in the Standard Specifications. The surface course shall be placed with an approved self-propelled mechanical spreading and finishing machine.

Attachment: Appendix G - Water Quality Management Plan (3309 : CONDITIONAL USE PERMIT FOR A GAS STATION)

HYDROLOGY MAP

Pre-Development Exhibit
Post Development Exhibit





VICINITY MAP
N.T.S.

LEGEND

- FLOW LINE
- FLOW DIRECTION
- DRAINAGE AREA BOUNDARY
- # / X.XX — DRAINAGE AREA DESIGNATION / DRAINAGE AREA

SCALE
20 0 10 20 40
(FEET)
1 INCH = 20 FT.

NO WORK SHALL BE DONE ON THIS SITE UNTIL BELOW AGENCY IS NOTIFIED OF INTENTION TO GRADE OR EXCAVATE.

DIGALERT

CALL
811 or
1-800-422-4133
2 Working Days Before You Dig
WWW.CALL811.COM

REVIEW BY CITY STAFF	BENCHMARK	BASIS OF BEARING
		XXXX

MARK	DATE	INITIAL	DESCRIPTION	REC.	APPR	DATE
		E.O.R.	REVISION			

CITY OF MORENO VALLEY APPROVALS

ENGINEER OF RECORD'S SEAL

REGISTERED PROFESSIONAL ENGINEER
ANGEL CESAR
No. 87222
CIVIL
STATE OF CALIFORNIA

BLUE
Engineering & Consulting, Inc

UNDER THE SUPERVISION OF:

ANGEL CESAR
RCE 87222

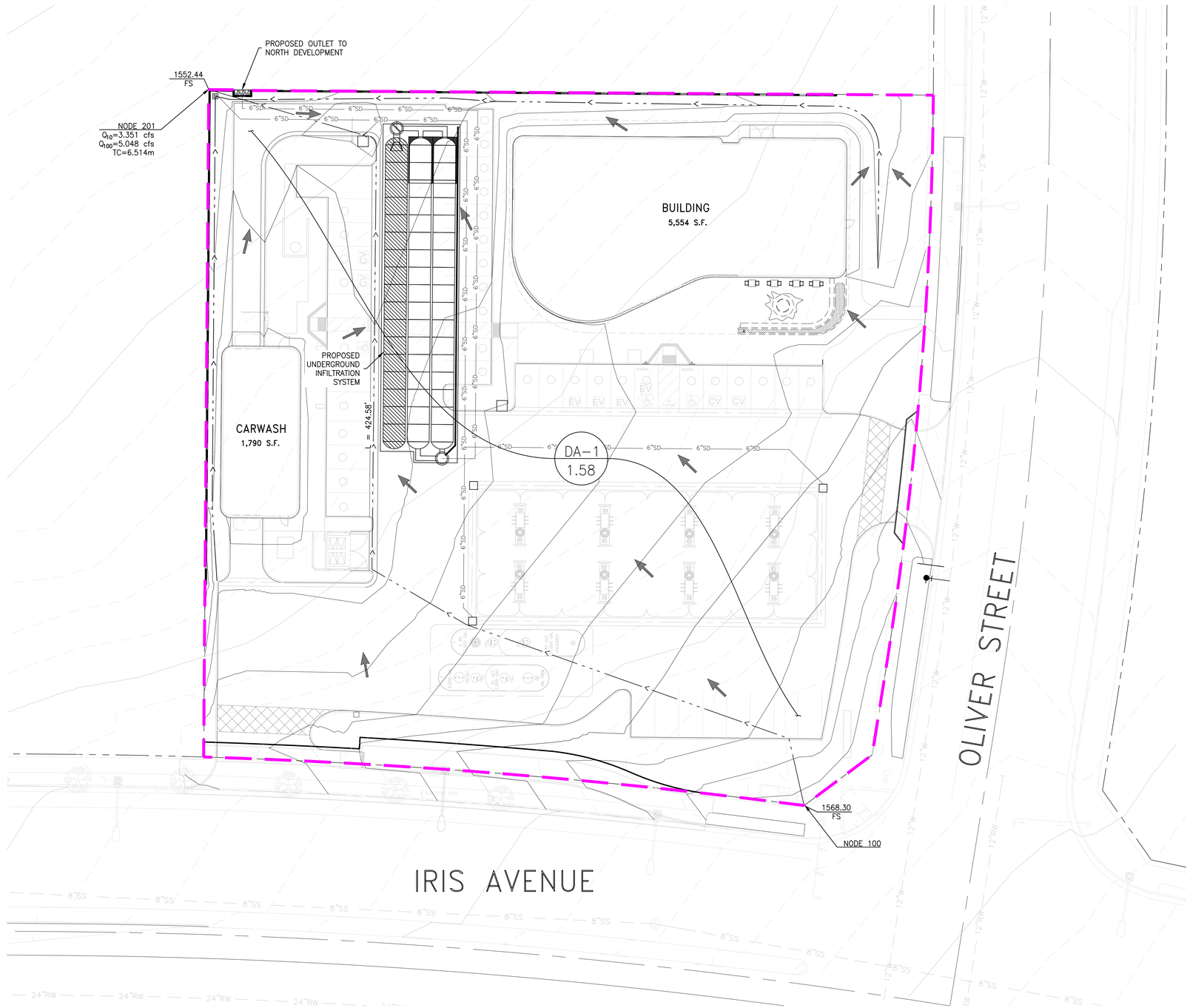
DATE

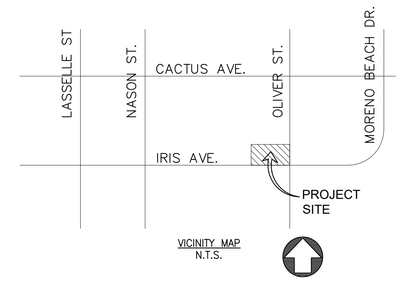
CITY OF MORENO VALLEY

PRE HYDROLOGY EXHIBIT

APN. 486-310-038
IRIS AVE AND OLIVER ST, MORENO VALLEY
PRELIMINARY GRADING PLAN

SHEET ___ OF ___
CITY ID No





VICINITY MAP
N.T.S.

LEGEND

- FLOW LINE
- FLOW DIRECTION
- DRAINAGE AREA BOUNDARY
- # / X.XX — DRAINAGE AREA DESIGNATION / DRAINAGE AREA

SCALE
20 0 10 20 40
(FEET)
1 INCH = 20 FT.

NO WORK SHALL BE DONE ON THIS SITE UNTIL BELOW AGENCY IS NOTIFIED OF INTENTION TO GRADE OR EXCAVATE.

DIGALERT

CALL 811 or 1-800-422-4133
2 Working Days Before You Dig
WWW.CALL811.COM

PEN22-0176

REVIEW BY CITY STAFF

BENCHMARK

THE BENCHMARK FOR THIS SURVEY IS CORS STATION "PPBF", ELEV = 1511.70' PER NGS DATA SHEET DH7168 DESIGNATED "PPBF ARD"

BASIS OF BEARING

THE BEARINGS SHOWN HEREON ARE BASED ON THE CENTERLINE OF OLIVER STREET SHOWN AS N 00°25'52" E ON THIS MAP ANS PARCEL MAP NO. 33361, PMB 239/30-32 AS N 00°26'04" E

MARK	DATE	INITIAL	DESCRIPTION	REC.	APPR	DATE
		E.O.R.	REVISION			

CITY OF MORENO VALLEY APPROVALS

ENGINEER OF RECORD'S SEAL

REGISTERED PROFESSIONAL ENGINEER — ANGEL CESAR — No. 87222 — CIVIL — STATE OF CALIFORNIA

BLUE Engineering & Consulting, Inc

UNDER THE SUPERVISION OF:

ANGEL CESAR
RCE 87222

DATE

CITY OF MORENO VALLEY

POST HYDROLOGY EXHIBIT

APN. 486-310-038
IRIS AVE AND OLIVER ST, MORENO VALLEY
PRELIMINARY GRADING PLAN

SHEET 2 OF 2

CITY ID No

Hydrology Calculations

Precipitation Frequency Chart & Curves
Rational Method Hydrology 10 yr. Pre-Development
Rational Method Hydrology 100 yr. Pre-Development
Rational Method Hydrology 10 yr. Post-Development
Rational Method Hydrology 100 yr. Post-Development
Pre-Synthetic Unit Hydrology 2yr. 1 hr. 3 hr, 6 hr, and 24 hr.
Pre-Synthetic Unit Hydrology 5 yr. 1 hr. 3 hr, 6 hr, and 24 hr.
Pre-Synthetic Unit Hydrology 10 yr. 1 hr. 3 hr, 6 hr, and 24 hr.
Pre-Synthetic Unit Hydrology 100 yr. 1 hr. 3 hr, 6 hr, and 24 hr.
Post Synthetic Unit Hydrology 2yr. 1 hr. 3 hr, 6 hr, and 24 hr.
Post Synthetic Unit Hydrology 5 yr. 1 hr. 3 hr, 6 hr, and 24 hr.
Post Synthetic Unit Hydrology 10 yr. 1 hr. 3 hr, 6 hr, and 24 hr.
Post Synthetic Unit Hydrology 100 yr. 1 hr. 3 hr, 6 hr, and 24 hr.
Flood Hydrograph Routing 2 yr. 1 hr, 3 hr, 6 hr, and 24 hr.
Flood Hydrograph Routing 5 yr. 1 hr, 3 hr, 6 hr, and 24 hr.
Flood Hydrograph Routing 10 yr. 1 hr, 3 hr, 6 hr, and 24 hr.
Flood Hydrograph Routing 100 yr. 1 hr, 3 hr, 6 hr, and 24 hr.

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2018 Version 9.0
Rational Hydrology Study Date: 08/06/22 File:Iris.out

Iris and Oliver
Pre Development
10 yr

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6481

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 10.00 Antecedent Moisture Condition = 2

Standard intensity-duration curves data (Plate D-4.1)
For the [Sunnymead-Moreno] area used.
10 year storm 10 minute intensity = 2.010(In/Hr)
10 year storm 60 minute intensity = 0.820(In/Hr)
100 year storm 10 minute intensity = 2.940(In/Hr)
100 year storm 60 minute intensity = 1.200(In/Hr)

Storm event year = 10.0
Calculated rainfall intensity data:
1 hour intensity = 0.820(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 100.000 to Point/Station 101.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 361.380(Ft.)
Top (of initial area) elevation = 1568.290(Ft.)

```
Bottom (of initial area) elevation =  1552.440(Ft.)
Difference in elevation =    15.850(Ft.)
Slope =    0.04386  s(percent)=       4.39
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.448 min.
Rainfall intensity =      1.965(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.675
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  67.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      2.094(CFS)
Total initial stream area =        1.580(Ac.)
Pervious area fraction = 1.000
End of computations, total study area =            1.58 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number =  67.0
```

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2018 Version 9.0
Rational Hydrology Study Date: 08/06/22 File:Iris.out

Iris and Oliver
Pre Development
100 YR

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6481

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 3

Standard intensity-duration curves data (Plate D-4.1)
For the [Sunnymead-Moreno] area used.
10 year storm 10 minute intensity = 2.010(In/Hr)
10 year storm 60 minute intensity = 0.820(In/Hr)
100 year storm 10 minute intensity = 2.940(In/Hr)
100 year storm 60 minute intensity = 1.200(In/Hr)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.200(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 100.000 to Point/Station 101.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 361.380(Ft.)
Top (of initial area) elevation = 1568.290(Ft.)

Bottom (of initial area) elevation = 1552.440(Ft.)
Difference in elevation =   15.850(Ft.)
Slope =   0.04386 s(percent)=   4.39
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.448 min.
Rainfall intensity =   2.876(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.823
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 3) = 83.20
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff =   3.739(CFS)
Total initial stream area =   1.580(Ac.)
Pervious area fraction = 1.000
End of computations, total study area =   1.58 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number = 67.0

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2018 Version 9.0
Rational Hydrology Study Date: 08/06/22 File:IrisP.out

Iris and Oliver
Post Development
10 yr

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6481

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 10.00 Antecedent Moisture Condition = 2

Standard intensity-duration curves data (Plate D-4.1)
For the [Sunnymead-Moreno] area used.
10 year storm 10 minute intensity = 2.010(In/Hr)
10 year storm 60 minute intensity = 0.820(In/Hr)
100 year storm 10 minute intensity = 2.940(In/Hr)
100 year storm 60 minute intensity = 1.200(In/Hr)

Storm event year = 10.0
Calculated rainfall intensity data:
1 hour intensity = 0.820(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 200.000 to Point/Station 201.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 424.580(Ft.)
Top (of initial area) elevation = 1568.300(Ft.)

Bottom (of initial area) elevation = 1552.440(Ft.)
Difference in elevation =   15.860(Ft.)
Slope =   0.03735 s(percent)=   3.74
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   6.514 min.
Rainfall intensity =   2.489(In/Hr) for a   10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.852
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 32.00
Pervious area fraction = 0.100; Impervious fraction = 0.900
Initial subarea runoff =   3.351(CFS)
Total initial stream area =   1.580(Ac.)
Pervious area fraction = 0.100
End of computations, total study area =   1.58 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.100
Area averaged RI index number = 32.0

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2018 Version 9.0
Rational Hydrology Study Date: 08/06/22 File:IrisP.out

Iris and Oliver
Post Development
100 yr

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6481

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 3

Standard intensity-duration curves data (Plate D-4.1)
For the [Sunnymead-Moreno] area used.
10 year storm 10 minute intensity = 2.010(In/Hr)
10 year storm 60 minute intensity = 0.820(In/Hr)
100 year storm 10 minute intensity = 2.940(In/Hr)
100 year storm 60 minute intensity = 1.200(In/Hr)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.200(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 200.000 to Point/Station 201.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 424.580(Ft.)
Top (of initial area) elevation = 1568.300(Ft.)

```
Bottom (of initial area) elevation =  1552.440(Ft.)
Difference in elevation =    15.860(Ft.)
Slope =    0.03735  s(percent)=       3.74
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    6.514 min.
Rainfall intensity =      3.642(In/Hr) for a   100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.877
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 3)  =  52.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      5.048(CFS)
Total initial stream area =        1.580(Ac.)
Pervious area fraction = 0.100
End of computations, total study area =            1.58 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.100
Area averaged RI index number =  32.0
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris12.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
2 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.49	0.78

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	1.35	2.13

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.493(In)
Area Averaged 100-Year Rainfall = 1.350(In)

Point rain (area averaged) = 0.493(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.493(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.580	67.00	0.000

Total Area Entered = 1.58(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
67.0	47.4	0.597	0.000	0.597	1.000	0.597
					Sum (F) =	0.597

Area averaged mean soil loss (F) (In/Hr) = 0.597
Minimum soil loss rate ((In/Hr)) = 0.299
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

Slope of intensity-duration curve for a 1 hour storm =0.5000

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	59.952	8.204	0.131
2	0.167	119.904	33.934	0.540
3	0.250	179.856	26.599	0.424
4	0.333	239.808	10.311	0.164
5	0.417	299.760	6.100	0.097
6	0.500	359.712	4.123	0.066
7	0.583	419.664	2.936	0.047
8	0.667	479.616	2.066	0.033
9	0.750	539.568	1.709	0.027
10	0.833	599.520	1.265	0.020
11	0.917	659.472	0.962	0.015

12	1.000	719.424	0.685	0.011
13	1.083	779.376	0.600	0.010
14	1.167	839.329	0.506	0.008
		Sum = 100.000	Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.20	0.248	(0.597)	0.224	0.025
2	0.17	4.30	0.254	(0.597)	0.229	0.025
3	0.25	5.00	0.296	(0.597)	0.266	0.030
4	0.33	5.00	0.296	(0.597)	0.266	0.030
5	0.42	5.80	0.343	(0.597)	0.309	0.034
6	0.50	6.50	0.385	(0.597)	0.346	0.038
7	0.58	7.40	0.438	(0.597)	0.394	0.044
8	0.67	8.60	0.509	(0.597)	0.458	0.051
9	0.75	12.30	0.728	0.597	(0.655)	0.130
10	0.83	29.10	1.722	0.597	(1.549)	1.124
11	0.92	6.80	0.402	(0.597)	0.362	0.040
12	1.00	5.00	0.296	(0.597)	0.266	0.030
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	1.6

Flood volume = Effective rainfall 0.13(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.36(In)
Total soil loss = 0.047(Ac.Ft)
Total rainfall = 0.49(In)
Flood volume = 765.2 Cubic Feet
Total soil loss = 2062.4 Cubic Feet

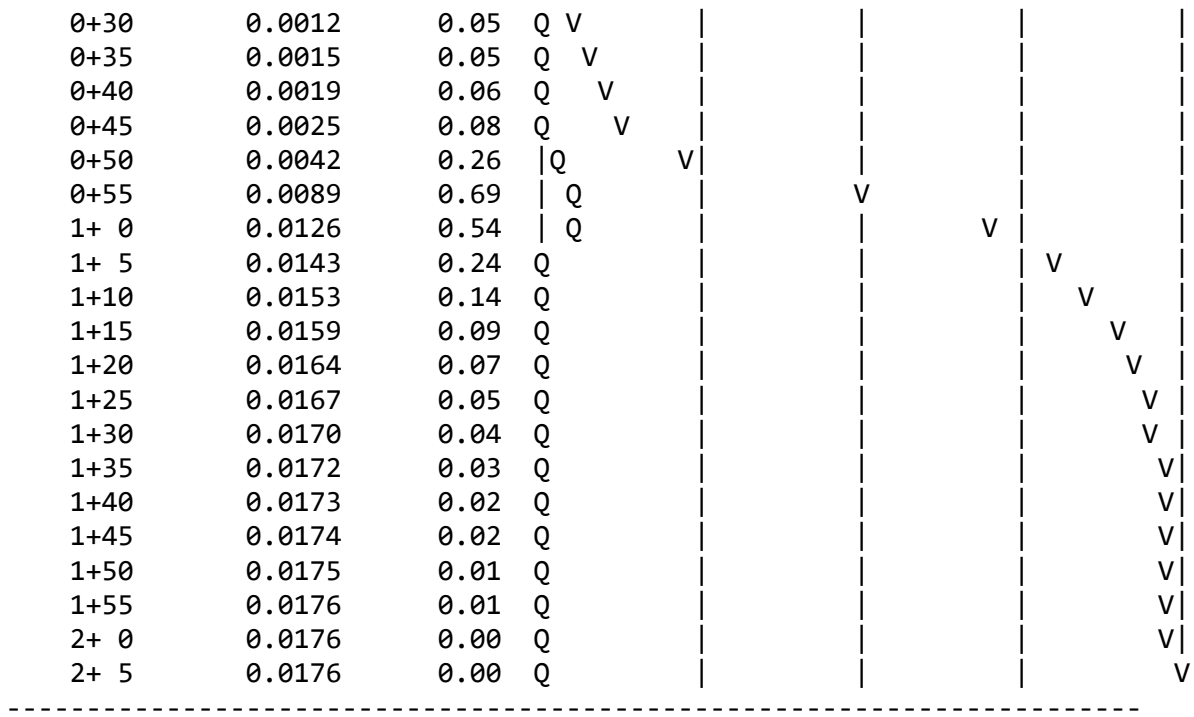
Peak flow rate of this hydrograph = 0.688(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.00	Q	|	|	|	|
0+10	0.0001	0.02	Q	|	|	|	|
0+15	0.0003	0.03	Q	|	|	|	|
0+20	0.0006	0.03	QV	|	|	|	|
0+25	0.0008	0.04	QV	|	|	|	|


0+30 0.0012 0.05 Q V
0+35 0.0015 0.05 Q V
0+40 0.0019 0.06 Q V
0+45 0.0025 0.08 Q V
0+50 0.0042 0.26 Q V
0+55 0.0089 0.69 Q V
1+ 0 0.0126 0.54 Q V
1+ 5 0.0143 0.24 Q V
1+10 0.0153 0.14 Q V
1+15 0.0159 0.09 Q V
1+20 0.0164 0.07 Q V
1+25 0.0167 0.05 Q V
1+30 0.0170 0.04 Q V
1+35 0.0172 0.03 Q V
1+40 0.0173 0.02 Q V
1+45 0.0174 0.02 Q V
1+50 0.0175 0.01 Q V
1+55 0.0176 0.01 Q V
2+ 0 0.0176 0.00 Q V
2+ 5 0.0176 0.00 Q V

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris32.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
2 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.87	1.37

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            2.10                   3.32

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    0.869(In)
Area Averaged 100-Year Rainfall =    2.100(In)

Point rain (area averaged) =    0.869(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    0.869(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           67.00         0.000
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
67.0  47.4      0.597     0.000        0.597       1.000      0.597
                                                 Sum (F) =   0.597
Area averaged mean soil loss (F) (In/Hr) =  0.597
Minimum soil loss rate ((In/Hr)) =  0.299
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
------------------------------------------------------------------------
    1   0.083         59.952          8.204             0.131
    2   0.167        119.904         33.934             0.540
    3   0.250        179.856         26.599             0.424
    4   0.333        239.808         10.311             0.164
    5   0.417        299.760          6.100             0.097
    6   0.500        359.712          4.123             0.066
    7   0.583        419.664          2.936             0.047
    8   0.667        479.616          2.066             0.033
    9   0.750        539.568          1.709             0.027
   10   0.833        599.520          1.265             0.020
   11   0.917        659.472          0.962             0.015
   12   1.000        719.424          0.685             0.011
   13   1.083        779.376          0.600             0.010
```

14	1.167	839.329	0.506		0.008
			Sum = 100.000	Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.136	(0.597)	0.122	0.014
2	0.17	1.30	0.136	(0.597)	0.122	0.014
3	0.25	1.10	0.115	(0.597)	0.103	0.011
4	0.33	1.50	0.156	(0.597)	0.141	0.016
5	0.42	1.50	0.156	(0.597)	0.141	0.016
6	0.50	1.80	0.188	(0.597)	0.169	0.019
7	0.58	1.50	0.156	(0.597)	0.141	0.016
8	0.67	1.80	0.188	(0.597)	0.169	0.019
9	0.75	1.80	0.188	(0.597)	0.169	0.019
10	0.83	1.50	0.156	(0.597)	0.141	0.016
11	0.92	1.60	0.167	(0.597)	0.150	0.017
12	1.00	1.80	0.188	(0.597)	0.169	0.019
13	1.08	2.20	0.229	(0.597)	0.206	0.023
14	1.17	2.20	0.229	(0.597)	0.206	0.023
15	1.25	2.20	0.229	(0.597)	0.206	0.023
16	1.33	2.00	0.209	(0.597)	0.188	0.021
17	1.42	2.60	0.271	(0.597)	0.244	0.027
18	1.50	2.70	0.282	(0.597)	0.253	0.028
19	1.58	2.40	0.250	(0.597)	0.225	0.025
20	1.67	2.70	0.282	(0.597)	0.253	0.028
21	1.75	3.30	0.344	(0.597)	0.310	0.034
22	1.83	3.10	0.323	(0.597)	0.291	0.032
23	1.92	2.90	0.302	(0.597)	0.272	0.030
24	2.00	3.00	0.313	(0.597)	0.282	0.031
25	2.08	3.10	0.323	(0.597)	0.291	0.032
26	2.17	4.20	0.438	(0.597)	0.394	0.044
27	2.25	5.00	0.521	(0.597)	0.469	0.052
28	2.33	3.50	0.365	(0.597)	0.328	0.036
29	2.42	6.80	0.709	0.597	(0.638)	0.112
30	2.50	7.30	0.761	0.597	(0.685)	0.164
31	2.58	8.20	0.855	0.597	(0.770)	0.258
32	2.67	5.90	0.615	(0.597)	0.554	0.062
33	2.75	2.00	0.209	(0.597)	0.188	0.021
34	2.83	1.80	0.188	(0.597)	0.169	0.019
35	2.92	1.80	0.188	(0.597)	0.169	0.019
36	3.00	0.60	0.063	(0.597)	0.056	0.006
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	1.3

Flood volume = Effective rainfall 0.11(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)

```
      Total soil loss =      0.76(In)
      Total soil loss =     0.100(Ac.Ft)
      Total rainfall =      0.87(In)
      Flood volume =         642.0 Cubic Feet
      Total soil loss =        4342.0 Cubic Feet
      ------------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.248(CFS)
      ------------------------------------------------------------------------
      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          3 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ------------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ------------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0000      0.00  Q         |         |         |         |
  0+10       0.0001      0.01  Q         |         |         |         |
  0+15       0.0002      0.01  Q         |         |         |         |
  0+20       0.0003      0.02  Q         |         |         |         |
  0+25       0.0004      0.02  QV        |         |         |         |
  0+30       0.0006      0.02  QV        |         |         |         |
  0+35       0.0007      0.02  QV        |         |         |         |
  0+40       0.0009      0.02  Q V       |         |         |         |
  0+45       0.0011      0.03  Q V       |         |         |         |
  0+50       0.0013      0.03  Q  V      |         |         |         |
  0+55       0.0015      0.03  Q  V      |         |         |         |
  1+ 0       0.0016      0.03  Q   V     |         |         |         |
  1+ 5       0.0018      0.03  Q   V     |         |         |         |
  1+10       0.0020      0.03  Q    V    |         |         |         |
  1+15       0.0023      0.03  Q     V   |         |         |         |
  1+20       0.0025      0.03  Q     V   |         |         |         |
  1+25       0.0028      0.03  Q      V  |         |         |         |
  1+30       0.0030      0.04  Q       V |         |         |         |
  1+35       0.0033      0.04  Q       V |         |         |         |
  1+40       0.0036      0.04  Q        V|         |         |         |
  1+45       0.0039      0.04  Q         V         |         |         |
  1+50       0.0042      0.05  Q         |V        |         |         |
  1+55       0.0045      0.05  Q         | V       |         |         |
  2+ 0       0.0049      0.05  Q         |  V      |         |         |
  2+ 5       0.0052      0.05  Q         |   V     |         |         |
  2+10       0.0055      0.05  Q         |    V    |         |         |
  2+15       0.0060      0.06  Q         |     V   |         |         |
  2+20       0.0064      0.07  Q         |      V  |         |         |
  2+25       0.0069      0.07  Q         |       V |         |         |
  2+30       0.0077      0.12  Q         |         V         |         |
  2+35       0.0090      0.19  Q         |         |   V     |         |
  2+40       0.0107      0.25  Q         |         |        V|         |
  2+45       0.0121      0.19  Q         |         |         | V       |
```

```
    2+50       0.0128      0.11  Q         |          |          |   V      |
    2+55       0.0134      0.08  Q         |          |          |     V    |
    3+ 0       0.0138      0.06  Q         |          |          |      V   |
    3+ 5       0.0141      0.04  Q         |          |          |       V  |
    3+10       0.0143      0.03  Q         |          |          |       V  |
    3+15       0.0144      0.02  Q         |          |          |        V |
    3+20       0.0145      0.01  Q         |          |          |        V |
    3+25       0.0146      0.01  Q         |          |          |        V |
    3+30       0.0147      0.01  Q         |          |          |        V |
    3+35       0.0147      0.01  Q         |          |          |        V |
    3+40       0.0147      0.00  Q         |          |          |        V |
    3+45       0.0147      0.00  Q         |          |          |        V |
    3+50       0.0147      0.00  Q         |          |          |        V |
    3+55       0.0147      0.00  Q         |          |          |        V |
    4+ 0       0.0147      0.00  Q         |          |          |        V |
    4+ 5       0.0147      0.00  Q         |          |          |         V
---------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris62.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
2 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	1.22	1.93

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.87	4.53

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.220(In)
Area Averaged 100-Year Rainfall = 2.870(In)

Point rain (area averaged) = 1.220(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.220(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.580	67.00	0.000

Total Area Entered = 1.58(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
67.0	47.4	0.597	0.000	0.597	1.000	0.597
					Sum (F) =	0.597

Area averaged mean soil loss (F) (In/Hr) = 0.597
Minimum soil loss rate ((In/Hr)) = 0.299
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	59.952	8.204	0.131
2	0.167	119.904	33.934	0.540
3	0.250	179.856	26.599	0.424
4	0.333	239.808	10.311	0.164
5	0.417	299.760	6.100	0.097
6	0.500	359.712	4.123	0.066
7	0.583	419.664	2.936	0.047
8	0.667	479.616	2.066	0.033
9	0.750	539.568	1.709	0.027
10	0.833	599.520	1.265	0.020
11	0.917	659.472	0.962	0.015
12	1.000	719.424	0.685	0.011
13	1.083	779.376	0.600	0.010

14	1.167	839.329	0.506			0.008
			Sum = 100.000		Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.073	(0.597)	0.066	0.007
2	0.17	0.60	0.088	(0.597)	0.079	0.009
3	0.25	0.60	0.088	(0.597)	0.079	0.009
4	0.33	0.60	0.088	(0.597)	0.079	0.009
5	0.42	0.60	0.088	(0.597)	0.079	0.009
6	0.50	0.70	0.102	(0.597)	0.092	0.010
7	0.58	0.70	0.102	(0.597)	0.092	0.010
8	0.67	0.70	0.102	(0.597)	0.092	0.010
9	0.75	0.70	0.102	(0.597)	0.092	0.010
10	0.83	0.70	0.102	(0.597)	0.092	0.010
11	0.92	0.70	0.102	(0.597)	0.092	0.010
12	1.00	0.80	0.117	(0.597)	0.105	0.012
13	1.08	0.80	0.117	(0.597)	0.105	0.012
14	1.17	0.80	0.117	(0.597)	0.105	0.012
15	1.25	0.80	0.117	(0.597)	0.105	0.012
16	1.33	0.80	0.117	(0.597)	0.105	0.012
17	1.42	0.80	0.117	(0.597)	0.105	0.012
18	1.50	0.80	0.117	(0.597)	0.105	0.012
19	1.58	0.80	0.117	(0.597)	0.105	0.012
20	1.67	0.80	0.117	(0.597)	0.105	0.012
21	1.75	0.80	0.117	(0.597)	0.105	0.012
22	1.83	0.80	0.117	(0.597)	0.105	0.012
23	1.92	0.80	0.117	(0.597)	0.105	0.012
24	2.00	0.90	0.132	(0.597)	0.119	0.013
25	2.08	0.80	0.117	(0.597)	0.105	0.012
26	2.17	0.90	0.132	(0.597)	0.119	0.013
27	2.25	0.90	0.132	(0.597)	0.119	0.013
28	2.33	0.90	0.132	(0.597)	0.119	0.013
29	2.42	0.90	0.132	(0.597)	0.119	0.013
30	2.50	0.90	0.132	(0.597)	0.119	0.013
31	2.58	0.90	0.132	(0.597)	0.119	0.013
32	2.67	0.90	0.132	(0.597)	0.119	0.013
33	2.75	1.00	0.146	(0.597)	0.132	0.015
34	2.83	1.00	0.146	(0.597)	0.132	0.015
35	2.92	1.00	0.146	(0.597)	0.132	0.015
36	3.00	1.00	0.146	(0.597)	0.132	0.015
37	3.08	1.00	0.146	(0.597)	0.132	0.015
38	3.17	1.10	0.161	(0.597)	0.145	0.016
39	3.25	1.10	0.161	(0.597)	0.145	0.016
40	3.33	1.10	0.161	(0.597)	0.145	0.016

41	3.42	1.20	0.176	(0.597)	0.158	0.018
42	3.50	1.30	0.190	(0.597)	0.171	0.019
43	3.58	1.40	0.205	(0.597)	0.184	0.020
44	3.67	1.40	0.205	(0.597)	0.184	0.020
45	3.75	1.50	0.220	(0.597)	0.198	0.022
46	3.83	1.50	0.220	(0.597)	0.198	0.022
47	3.92	1.60	0.234	(0.597)	0.211	0.023
48	4.00	1.60	0.234	(0.597)	0.211	0.023
49	4.08	1.70	0.249	(0.597)	0.224	0.025
50	4.17	1.80	0.264	(0.597)	0.237	0.026
51	4.25	1.90	0.278	(0.597)	0.250	0.028
52	4.33	2.00	0.293	(0.597)	0.264	0.029
53	4.42	2.10	0.307	(0.597)	0.277	0.031
54	4.50	2.10	0.307	(0.597)	0.277	0.031
55	4.58	2.20	0.322	(0.597)	0.290	0.032
56	4.67	2.30	0.337	(0.597)	0.303	0.034
57	4.75	2.40	0.351	(0.597)	0.316	0.035
58	4.83	2.40	0.351	(0.597)	0.316	0.035
59	4.92	2.50	0.366	(0.597)	0.329	0.037
60	5.00	2.60	0.381	(0.597)	0.343	0.038
61	5.08	3.10	0.454	(0.597)	0.408	0.045
62	5.17	3.60	0.527	(0.597)	0.474	0.053
63	5.25	3.90	0.571	(0.597)	0.514	0.057
64	5.33	4.20	0.615	(0.597)	0.553	0.061
65	5.42	4.70	0.688	0.597	(0.619)	0.091
66	5.50	5.60	0.820	0.597	(0.738)	0.222
67	5.58	1.90	0.278	(0.597)	0.250	0.028
68	5.67	0.90	0.132	(0.597)	0.119	0.013
69	5.75	0.60	0.088	(0.597)	0.079	0.009
70	5.83	0.50	0.073	(0.597)	0.066	0.007
71	5.92	0.30	0.044	(0.597)	0.040	0.004
72	6.00	0.20	0.029	(0.597)	0.026	0.003

(Loss Rate Not Used)

Sum = 100.0 Sum = 1.6

Flood volume = Effective rainfall 0.14(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 1.08(In)
Total soil loss = 0.143(Ac.Ft)
Total rainfall = 1.22(In)
Flood volume = 777.2 Cubic Feet
Total soil loss = 6219.9 Cubic Feet

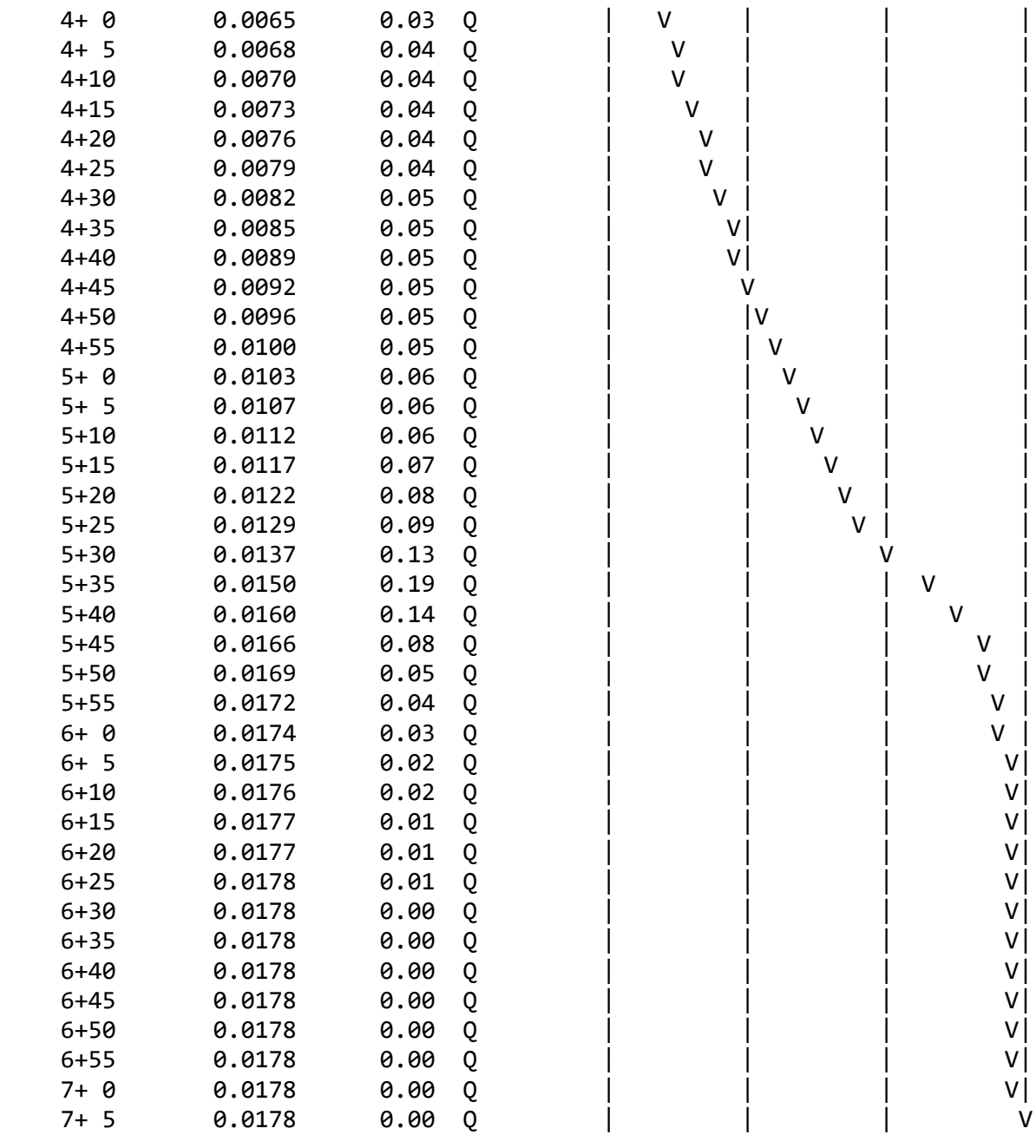
Peak flow rate of this hydrograph = 0.188(CFS)

++

6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.00	Q	|	|	|	|
0+10	0.0000	0.01	Q	|	|	|	|
0+15	0.0001	0.01	Q	|	|	|	|
0+20	0.0002	0.01	Q	|	|	|	|
0+25	0.0003	0.01	Q	|	|	|	|
0+30	0.0003	0.01	Q	|	|	|	|
0+35	0.0004	0.01	Q	|	|	|	|
0+40	0.0005	0.01	QV	|	|	|	|
0+45	0.0006	0.02	QV	|	|	|	|
0+50	0.0008	0.02	QV	|	|	|	|
0+55	0.0009	0.02	QV	|	|	|	|
1+ 0	0.0010	0.02	Q V	|	|	|	|
1+ 5	0.0011	0.02	Q V	|	|	|	|
1+10	0.0012	0.02	Q V	|	|	|	|
1+15	0.0013	0.02	Q V	|	|	|	|
1+20	0.0015	0.02	Q V	|	|	|	|
1+25	0.0016	0.02	Q V	|	|	|	|
1+30	0.0017	0.02	Q V	|	|	|	|
1+35	0.0018	0.02	Q V	|	|	|	|
1+40	0.0020	0.02	Q V	|	|	|	|
1+45	0.0021	0.02	Q V	|	|	|	|
1+50	0.0022	0.02	Q V	|	|	|	|
1+55	0.0024	0.02	Q V	|	|	|	|
2+ 0	0.0025	0.02	Q V	|	|	|	|
2+ 5	0.0026	0.02	Q V	|	|	|	|
2+10	0.0028	0.02	Q V	|	|	|	|
2+15	0.0029	0.02	Q V	|	|	|	|
2+20	0.0030	0.02	Q V	|	|	|	|
2+25	0.0032	0.02	Q V	|	|	|	|
2+30	0.0033	0.02	Q V	|	|	|	|
2+35	0.0035	0.02	Q V	|	|	|	|
2+40	0.0036	0.02	Q V	|	|	|	|
2+45	0.0038	0.02	Q V	|	|	|	|
2+50	0.0039	0.02	Q V	|	|	|	|
2+55	0.0041	0.02	Q V	|	|	|	|
3+ 0	0.0042	0.02	Q V	|	|	|	|
3+ 5	0.0044	0.02	Q V	|	|	|	|
3+10	0.0045	0.02	Q V	|	|	|	|
3+15	0.0047	0.02	Q V	|	|	|	|
3+20	0.0049	0.02	Q V	|	|	|	|
3+25	0.0050	0.03	Q V	|	|	|	|
3+30	0.0052	0.03	Q V	|	|	|	|
3+35	0.0054	0.03	Q V	|	|	|	|
3+40	0.0056	0.03	Q V	|	|	|	|
3+45	0.0058	0.03	Q V	|	|	|	|
3+50	0.0061	0.03	Q V	|	|	|	|
3+55	0.0063	0.03	Q V	|	|	|	|


4+ 0 0.0065 0.03 Q
4+ 5 0.0068 0.04 Q
4+10 0.0070 0.04 Q
4+15 0.0073 0.04 Q
4+20 0.0076 0.04 Q
4+25 0.0079 0.04 Q
4+30 0.0082 0.05 Q
4+35 0.0085 0.05 Q
4+40 0.0089 0.05 Q
4+45 0.0092 0.05 Q
4+50 0.0096 0.05 Q
4+55 0.0100 0.05 Q
5+ 0 0.0103 0.06 Q
5+ 5 0.0107 0.06 Q
5+10 0.0112 0.06 Q
5+15 0.0117 0.07 Q
5+20 0.0122 0.08 Q
5+25 0.0129 0.09 Q
5+30 0.0137 0.13 Q
5+35 0.0150 0.19 Q
5+40 0.0160 0.14 Q
5+45 0.0166 0.08 Q
5+50 0.0169 0.05 Q
5+55 0.0172 0.04 Q
6+ 0 0.0174 0.03 Q
6+ 5 0.0175 0.02 Q
6+10 0.0176 0.02 Q
6+15 0.0177 0.01 Q
6+20 0.0177 0.01 Q
6+25 0.0178 0.01 Q
6+30 0.0178 0.00 Q
6+35 0.0178 0.00 Q
6+40 0.0178 0.00 Q
6+45 0.0178 0.00 Q
6+50 0.0178 0.00 Q
6+55 0.0178 0.00 Q
7+ 0 0.0178 0.00 Q
7+ 5 0.0178 0.00 Q

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris242.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
2 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.05	3.24

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            5.25                   8.29

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    2.050(In)
Area Averaged 100-Year Rainfall =    5.250(In)

Point rain (area averaged) =    2.050(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    2.050(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           67.00         0.000
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
67.0  47.4      0.597     0.000        0.597       1.000      0.597
                                                 Sum (F) =   0.597
Area averaged mean soil loss (F) (In/Hr) =  0.597
Minimum soil loss rate ((In/Hr)) =  0.299
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         59.952          8.204              0.131
    2   0.167        119.904         33.934              0.540
    3   0.250        179.856         26.599              0.424
    4   0.333        239.808         10.311              0.164
    5   0.417        299.760          6.100              0.097
    6   0.500        359.712          4.123              0.066
    7   0.583        419.664          2.936              0.047
    8   0.667        479.616          2.066              0.033
    9   0.750        539.568          1.709              0.027
   10   0.833        599.520          1.265              0.020
   11   0.917        659.472          0.962              0.015
   12   1.000        719.424          0.685              0.011
   13   1.083        779.376          0.600              0.010
```

	14	1.167	839.329	0.506		0.008
				Sum = 100.000	Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.016	(1.059)	0.015	0.002
2	0.17	0.07	0.016	(1.055)	0.015	0.002
3	0.25	0.07	0.016	(1.051)	0.015	0.002
4	0.33	0.10	0.025	(1.047)	0.022	0.002
5	0.42	0.10	0.025	(1.043)	0.022	0.002
6	0.50	0.10	0.025	(1.039)	0.022	0.002
7	0.58	0.10	0.025	(1.035)	0.022	0.002
8	0.67	0.10	0.025	(1.031)	0.022	0.002
9	0.75	0.10	0.025	(1.027)	0.022	0.002
10	0.83	0.13	0.033	(1.023)	0.030	0.003
11	0.92	0.13	0.033	(1.019)	0.030	0.003
12	1.00	0.13	0.033	(1.015)	0.030	0.003
13	1.08	0.10	0.025	(1.011)	0.022	0.002
14	1.17	0.10	0.025	(1.007)	0.022	0.002
15	1.25	0.10	0.025	(1.003)	0.022	0.002
16	1.33	0.10	0.025	(0.999)	0.022	0.002
17	1.42	0.10	0.025	(0.995)	0.022	0.002
18	1.50	0.10	0.025	(0.991)	0.022	0.002
19	1.58	0.10	0.025	(0.987)	0.022	0.002
20	1.67	0.10	0.025	(0.983)	0.022	0.002
21	1.75	0.10	0.025	(0.979)	0.022	0.002
22	1.83	0.13	0.033	(0.975)	0.030	0.003
23	1.92	0.13	0.033	(0.971)	0.030	0.003
24	2.00	0.13	0.033	(0.967)	0.030	0.003
25	2.08	0.13	0.033	(0.963)	0.030	0.003
26	2.17	0.13	0.033	(0.959)	0.030	0.003
27	2.25	0.13	0.033	(0.955)	0.030	0.003
28	2.33	0.13	0.033	(0.951)	0.030	0.003
29	2.42	0.13	0.033	(0.947)	0.030	0.003
30	2.50	0.13	0.033	(0.944)	0.030	0.003
31	2.58	0.17	0.041	(0.940)	0.037	0.004
32	2.67	0.17	0.041	(0.936)	0.037	0.004
33	2.75	0.17	0.041	(0.932)	0.037	0.004
34	2.83	0.17	0.041	(0.928)	0.037	0.004
35	2.92	0.17	0.041	(0.924)	0.037	0.004
36	3.00	0.17	0.041	(0.921)	0.037	0.004
37	3.08	0.17	0.041	(0.917)	0.037	0.004
38	3.17	0.17	0.041	(0.913)	0.037	0.004
39	3.25	0.17	0.041	(0.909)	0.037	0.004
40	3.33	0.17	0.041	(0.905)	0.037	0.004

41	3.42	0.17	0.041	(0.902)	0.037	0.004
42	3.50	0.17	0.041	(0.898)	0.037	0.004
43	3.58	0.17	0.041	(0.894)	0.037	0.004
44	3.67	0.17	0.041	(0.890)	0.037	0.004
45	3.75	0.17	0.041	(0.887)	0.037	0.004
46	3.83	0.20	0.049	(0.883)	0.044	0.005
47	3.92	0.20	0.049	(0.879)	0.044	0.005
48	4.00	0.20	0.049	(0.875)	0.044	0.005
49	4.08	0.20	0.049	(0.872)	0.044	0.005
50	4.17	0.20	0.049	(0.868)	0.044	0.005
51	4.25	0.20	0.049	(0.864)	0.044	0.005
52	4.33	0.23	0.057	(0.861)	0.052	0.006
53	4.42	0.23	0.057	(0.857)	0.052	0.006
54	4.50	0.23	0.057	(0.853)	0.052	0.006
55	4.58	0.23	0.057	(0.850)	0.052	0.006
56	4.67	0.23	0.057	(0.846)	0.052	0.006
57	4.75	0.23	0.057	(0.842)	0.052	0.006
58	4.83	0.27	0.066	(0.839)	0.059	0.007
59	4.92	0.27	0.066	(0.835)	0.059	0.007
60	5.00	0.27	0.066	(0.831)	0.059	0.007
61	5.08	0.20	0.049	(0.828)	0.044	0.005
62	5.17	0.20	0.049	(0.824)	0.044	0.005
63	5.25	0.20	0.049	(0.821)	0.044	0.005
64	5.33	0.23	0.057	(0.817)	0.052	0.006
65	5.42	0.23	0.057	(0.813)	0.052	0.006
66	5.50	0.23	0.057	(0.810)	0.052	0.006
67	5.58	0.27	0.066	(0.806)	0.059	0.007
68	5.67	0.27	0.066	(0.803)	0.059	0.007
69	5.75	0.27	0.066	(0.799)	0.059	0.007
70	5.83	0.27	0.066	(0.796)	0.059	0.007
71	5.92	0.27	0.066	(0.792)	0.059	0.007
72	6.00	0.27	0.066	(0.789)	0.059	0.007
73	6.08	0.30	0.074	(0.785)	0.066	0.007
74	6.17	0.30	0.074	(0.782)	0.066	0.007
75	6.25	0.30	0.074	(0.778)	0.066	0.007
76	6.33	0.30	0.074	(0.775)	0.066	0.007
77	6.42	0.30	0.074	(0.771)	0.066	0.007
78	6.50	0.30	0.074	(0.768)	0.066	0.007
79	6.58	0.33	0.082	(0.764)	0.074	0.008
80	6.67	0.33	0.082	(0.761)	0.074	0.008
81	6.75	0.33	0.082	(0.757)	0.074	0.008
82	6.83	0.33	0.082	(0.754)	0.074	0.008
83	6.92	0.33	0.082	(0.751)	0.074	0.008
84	7.00	0.33	0.082	(0.747)	0.074	0.008
85	7.08	0.33	0.082	(0.744)	0.074	0.008
86	7.17	0.33	0.082	(0.740)	0.074	0.008
87	7.25	0.33	0.082	(0.737)	0.074	0.008
88	7.33	0.37	0.090	(0.734)	0.081	0.009
89	7.42	0.37	0.090	(0.730)	0.081	0.009
90	7.50	0.37	0.090	(0.727)	0.081	0.009

91	7.58	0.40	0.098	(0.724)	0.089	0.010
92	7.67	0.40	0.098	(0.720)	0.089	0.010
93	7.75	0.40	0.098	(0.717)	0.089	0.010
94	7.83	0.43	0.107	(0.714)	0.096	0.011
95	7.92	0.43	0.107	(0.710)	0.096	0.011
96	8.00	0.43	0.107	(0.707)	0.096	0.011
97	8.08	0.50	0.123	(0.704)	0.111	0.012
98	8.17	0.50	0.123	(0.701)	0.111	0.012
99	8.25	0.50	0.123	(0.697)	0.111	0.012
100	8.33	0.50	0.123	(0.694)	0.111	0.012
101	8.42	0.50	0.123	(0.691)	0.111	0.012
102	8.50	0.50	0.123	(0.688)	0.111	0.012
103	8.58	0.53	0.131	(0.684)	0.118	0.013
104	8.67	0.53	0.131	(0.681)	0.118	0.013
105	8.75	0.53	0.131	(0.678)	0.118	0.013
106	8.83	0.57	0.139	(0.675)	0.125	0.014
107	8.92	0.57	0.139	(0.671)	0.125	0.014
108	9.00	0.57	0.139	(0.668)	0.125	0.014
109	9.08	0.63	0.156	(0.665)	0.140	0.016
110	9.17	0.63	0.156	(0.662)	0.140	0.016
111	9.25	0.63	0.156	(0.659)	0.140	0.016
112	9.33	0.67	0.164	(0.656)	0.148	0.016
113	9.42	0.67	0.164	(0.653)	0.148	0.016
114	9.50	0.67	0.164	(0.649)	0.148	0.016
115	9.58	0.70	0.172	(0.646)	0.155	0.017
116	9.67	0.70	0.172	(0.643)	0.155	0.017
117	9.75	0.70	0.172	(0.640)	0.155	0.017
118	9.83	0.73	0.180	(0.637)	0.162	0.018
119	9.92	0.73	0.180	(0.634)	0.162	0.018
120	10.00	0.73	0.180	(0.631)	0.162	0.018
121	10.08	0.50	0.123	(0.628)	0.111	0.012
122	10.17	0.50	0.123	(0.625)	0.111	0.012
123	10.25	0.50	0.123	(0.622)	0.111	0.012
124	10.33	0.50	0.123	(0.619)	0.111	0.012
125	10.42	0.50	0.123	(0.616)	0.111	0.012
126	10.50	0.50	0.123	(0.613)	0.111	0.012
127	10.58	0.67	0.164	(0.610)	0.148	0.016
128	10.67	0.67	0.164	(0.607)	0.148	0.016
129	10.75	0.67	0.164	(0.604)	0.148	0.016
130	10.83	0.67	0.164	(0.601)	0.148	0.016
131	10.92	0.67	0.164	(0.598)	0.148	0.016
132	11.00	0.67	0.164	(0.595)	0.148	0.016
133	11.08	0.63	0.156	(0.592)	0.140	0.016
134	11.17	0.63	0.156	(0.589)	0.140	0.016
135	11.25	0.63	0.156	(0.586)	0.140	0.016
136	11.33	0.63	0.156	(0.583)	0.140	0.016
137	11.42	0.63	0.156	(0.580)	0.140	0.016
138	11.50	0.63	0.156	(0.578)	0.140	0.016
139	11.58	0.57	0.139	(0.575)	0.125	0.014
140	11.67	0.57	0.139	(0.572)	0.125	0.014

141	11.75	0.57	0.139	(0.569)	0.125	0.014
142	11.83	0.60	0.148	(0.566)	0.133	0.015
143	11.92	0.60	0.148	(0.563)	0.133	0.015
144	12.00	0.60	0.148	(0.561)	0.133	0.015
145	12.08	0.83	0.205	(0.558)	0.184	0.020
146	12.17	0.83	0.205	(0.555)	0.184	0.020
147	12.25	0.83	0.205	(0.552)	0.184	0.020
148	12.33	0.87	0.213	(0.549)	0.192	0.021
149	12.42	0.87	0.213	(0.547)	0.192	0.021
150	12.50	0.87	0.213	(0.544)	0.192	0.021
151	12.58	0.93	0.230	(0.541)	0.207	0.023
152	12.67	0.93	0.230	(0.538)	0.207	0.023
153	12.75	0.93	0.230	(0.536)	0.207	0.023
154	12.83	0.97	0.238	(0.533)	0.214	0.024
155	12.92	0.97	0.238	(0.530)	0.214	0.024
156	13.00	0.97	0.238	(0.528)	0.214	0.024
157	13.08	1.13	0.279	(0.525)	0.251	0.028
158	13.17	1.13	0.279	(0.522)	0.251	0.028
159	13.25	1.13	0.279	(0.520)	0.251	0.028
160	13.33	1.13	0.279	(0.517)	0.251	0.028
161	13.42	1.13	0.279	(0.514)	0.251	0.028
162	13.50	1.13	0.279	(0.512)	0.251	0.028
163	13.58	0.77	0.189	(0.509)	0.170	0.019
164	13.67	0.77	0.189	(0.507)	0.170	0.019
165	13.75	0.77	0.189	(0.504)	0.170	0.019
166	13.83	0.77	0.189	(0.501)	0.170	0.019
167	13.92	0.77	0.189	(0.499)	0.170	0.019
168	14.00	0.77	0.189	(0.496)	0.170	0.019
169	14.08	0.90	0.221	(0.494)	0.199	0.022
170	14.17	0.90	0.221	(0.491)	0.199	0.022
171	14.25	0.90	0.221	(0.489)	0.199	0.022
172	14.33	0.87	0.213	(0.486)	0.192	0.021
173	14.42	0.87	0.213	(0.484)	0.192	0.021
174	14.50	0.87	0.213	(0.481)	0.192	0.021
175	14.58	0.87	0.213	(0.479)	0.192	0.021
176	14.67	0.87	0.213	(0.476)	0.192	0.021
177	14.75	0.87	0.213	(0.474)	0.192	0.021
178	14.83	0.83	0.205	(0.471)	0.184	0.020
179	14.92	0.83	0.205	(0.469)	0.184	0.020
180	15.00	0.83	0.205	(0.467)	0.184	0.020
181	15.08	0.80	0.197	(0.464)	0.177	0.020
182	15.17	0.80	0.197	(0.462)	0.177	0.020
183	15.25	0.80	0.197	(0.460)	0.177	0.020
184	15.33	0.77	0.189	(0.457)	0.170	0.019
185	15.42	0.77	0.189	(0.455)	0.170	0.019
186	15.50	0.77	0.189	(0.452)	0.170	0.019
187	15.58	0.63	0.156	(0.450)	0.140	0.016
188	15.67	0.63	0.156	(0.448)	0.140	0.016
189	15.75	0.63	0.156	(0.446)	0.140	0.016
190	15.83	0.63	0.156	(0.443)	0.140	0.016

191	15.92	0.63	0.156	(0.441)	0.140	0.016
192	16.00	0.63	0.156	(0.439)	0.140	0.016
193	16.08	0.13	0.033	(0.437)	0.030	0.003
194	16.17	0.13	0.033	(0.434)	0.030	0.003
195	16.25	0.13	0.033	(0.432)	0.030	0.003
196	16.33	0.13	0.033	(0.430)	0.030	0.003
197	16.42	0.13	0.033	(0.428)	0.030	0.003
198	16.50	0.13	0.033	(0.425)	0.030	0.003
199	16.58	0.10	0.025	(0.423)	0.022	0.002
200	16.67	0.10	0.025	(0.421)	0.022	0.002
201	16.75	0.10	0.025	(0.419)	0.022	0.002
202	16.83	0.10	0.025	(0.417)	0.022	0.002
203	16.92	0.10	0.025	(0.415)	0.022	0.002
204	17.00	0.10	0.025	(0.413)	0.022	0.002
205	17.08	0.17	0.041	(0.411)	0.037	0.004
206	17.17	0.17	0.041	(0.409)	0.037	0.004
207	17.25	0.17	0.041	(0.407)	0.037	0.004
208	17.33	0.17	0.041	(0.404)	0.037	0.004
209	17.42	0.17	0.041	(0.402)	0.037	0.004
210	17.50	0.17	0.041	(0.400)	0.037	0.004
211	17.58	0.17	0.041	(0.398)	0.037	0.004
212	17.67	0.17	0.041	(0.396)	0.037	0.004
213	17.75	0.17	0.041	(0.394)	0.037	0.004
214	17.83	0.13	0.033	(0.392)	0.030	0.003
215	17.92	0.13	0.033	(0.391)	0.030	0.003
216	18.00	0.13	0.033	(0.389)	0.030	0.003
217	18.08	0.13	0.033	(0.387)	0.030	0.003
218	18.17	0.13	0.033	(0.385)	0.030	0.003
219	18.25	0.13	0.033	(0.383)	0.030	0.003
220	18.33	0.13	0.033	(0.381)	0.030	0.003
221	18.42	0.13	0.033	(0.379)	0.030	0.003
222	18.50	0.13	0.033	(0.377)	0.030	0.003
223	18.58	0.10	0.025	(0.376)	0.022	0.002
224	18.67	0.10	0.025	(0.374)	0.022	0.002
225	18.75	0.10	0.025	(0.372)	0.022	0.002
226	18.83	0.07	0.016	(0.370)	0.015	0.002
227	18.92	0.07	0.016	(0.368)	0.015	0.002
228	19.00	0.07	0.016	(0.367)	0.015	0.002
229	19.08	0.10	0.025	(0.365)	0.022	0.002
230	19.17	0.10	0.025	(0.363)	0.022	0.002
231	19.25	0.10	0.025	(0.361)	0.022	0.002
232	19.33	0.13	0.033	(0.360)	0.030	0.003
233	19.42	0.13	0.033	(0.358)	0.030	0.003
234	19.50	0.13	0.033	(0.356)	0.030	0.003
235	19.58	0.10	0.025	(0.355)	0.022	0.002
236	19.67	0.10	0.025	(0.353)	0.022	0.002
237	19.75	0.10	0.025	(0.352)	0.022	0.002
238	19.83	0.07	0.016	(0.350)	0.015	0.002
239	19.92	0.07	0.016	(0.348)	0.015	0.002
240	20.00	0.07	0.016	(0.347)	0.015	0.002

241	20.08	0.10	0.025	(0.345)	0.022	0.002
242	20.17	0.10	0.025	(0.344)	0.022	0.002
243	20.25	0.10	0.025	(0.342)	0.022	0.002
244	20.33	0.10	0.025	(0.341)	0.022	0.002
245	20.42	0.10	0.025	(0.339)	0.022	0.002
246	20.50	0.10	0.025	(0.338)	0.022	0.002
247	20.58	0.10	0.025	(0.337)	0.022	0.002
248	20.67	0.10	0.025	(0.335)	0.022	0.002
249	20.75	0.10	0.025	(0.334)	0.022	0.002
250	20.83	0.07	0.016	(0.332)	0.015	0.002
251	20.92	0.07	0.016	(0.331)	0.015	0.002
252	21.00	0.07	0.016	(0.330)	0.015	0.002
253	21.08	0.10	0.025	(0.328)	0.022	0.002
254	21.17	0.10	0.025	(0.327)	0.022	0.002
255	21.25	0.10	0.025	(0.326)	0.022	0.002
256	21.33	0.07	0.016	(0.325)	0.015	0.002
257	21.42	0.07	0.016	(0.323)	0.015	0.002
258	21.50	0.07	0.016	(0.322)	0.015	0.002
259	21.58	0.10	0.025	(0.321)	0.022	0.002
260	21.67	0.10	0.025	(0.320)	0.022	0.002
261	21.75	0.10	0.025	(0.319)	0.022	0.002
262	21.83	0.07	0.016	(0.318)	0.015	0.002
263	21.92	0.07	0.016	(0.317)	0.015	0.002
264	22.00	0.07	0.016	(0.315)	0.015	0.002
265	22.08	0.10	0.025	(0.314)	0.022	0.002
266	22.17	0.10	0.025	(0.313)	0.022	0.002
267	22.25	0.10	0.025	(0.312)	0.022	0.002
268	22.33	0.07	0.016	(0.311)	0.015	0.002
269	22.42	0.07	0.016	(0.310)	0.015	0.002
270	22.50	0.07	0.016	(0.310)	0.015	0.002
271	22.58	0.07	0.016	(0.309)	0.015	0.002
272	22.67	0.07	0.016	(0.308)	0.015	0.002
273	22.75	0.07	0.016	(0.307)	0.015	0.002
274	22.83	0.07	0.016	(0.306)	0.015	0.002
275	22.92	0.07	0.016	(0.305)	0.015	0.002
276	23.00	0.07	0.016	(0.305)	0.015	0.002
277	23.08	0.07	0.016	(0.304)	0.015	0.002
278	23.17	0.07	0.016	(0.303)	0.015	0.002
279	23.25	0.07	0.016	(0.303)	0.015	0.002
280	23.33	0.07	0.016	(0.302)	0.015	0.002
281	23.42	0.07	0.016	(0.301)	0.015	0.002
282	23.50	0.07	0.016	(0.301)	0.015	0.002
283	23.58	0.07	0.016	(0.300)	0.015	0.002
284	23.67	0.07	0.016	(0.300)	0.015	0.002
285	23.75	0.07	0.016	(0.300)	0.015	0.002
286	23.83	0.07	0.016	(0.299)	0.015	0.002
287	23.92	0.07	0.016	(0.299)	0.015	0.002
288	24.00	0.07	0.016	(0.299)	0.015	0.002
		(Loss Rate Not Used)				
	Sum =	100.0			Sum =	2.5

```
      Flood volume = Effective rainfall      0.20(In)
       times area       1.6(Ac.)/[(In)/(Ft.)] =       0.0(Ac.Ft)
      Total soil loss =      1.84(In)
      Total soil loss =     0.243(Ac.Ft)
      Total rainfall =      2.05(In)
      Flood volume =        1175.8 Cubic Feet
      Total soil loss =       10581.8 Cubic Feet
      ----------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.044(CFS)
      ----------------------------------------------------------------------
      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ----------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ----------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
----------------------------------------------------------------------
  0+ 5       0.0000      0.00  Q         |         |         |         |
  0+10       0.0000      0.00  Q         |         |         |         |
  0+15       0.0000      0.00  Q         |         |         |         |
  0+20       0.0000      0.00  Q         |         |         |         |
  0+25       0.0001      0.00  Q         |         |         |         |
  0+30       0.0001      0.00  Q         |         |         |         |
  0+35       0.0001      0.00  Q         |         |         |         |
  0+40       0.0001      0.00  Q         |         |         |         |
  0+45       0.0002      0.00  Q         |         |         |         |
  0+50       0.0002      0.00  Q         |         |         |         |
  0+55       0.0002      0.00  Q         |         |         |         |
  1+ 0       0.0002      0.00  Q         |         |         |         |
  1+ 5       0.0003      0.00  Q         |         |         |         |
  1+10       0.0003      0.00  Q         |         |         |         |
  1+15       0.0003      0.00  Q         |         |         |         |
  1+20       0.0004      0.00  Q         |         |         |         |
  1+25       0.0004      0.00  Q         |         |         |         |
  1+30       0.0004      0.00  Q         |         |         |         |
  1+35       0.0004      0.00  Q         |         |         |         |
  1+40       0.0005      0.00  Q         |         |         |         |
  1+45       0.0005      0.00  Q         |         |         |         |
  1+50       0.0005      0.00  Q         |         |         |         |
  1+55       0.0006      0.00  Q         |         |         |         |
  2+ 0       0.0006      0.00  Q         |         |         |         |
  2+ 5       0.0006      0.00  Q         |         |         |         |
  2+10       0.0007      0.01  Q         |         |         |         |
  2+15       0.0007      0.01  QV        |         |         |         |
  2+20       0.0007      0.01  QV        |         |         |         |
  2+25       0.0008      0.01  QV        |         |         |         |
  2+30       0.0008      0.01  QV        |         |         |         |
  2+35       0.0008      0.01  QV        |         |         |         |
```

2+40	0.0009	0.01	QV	|	|	|	|
2+45	0.0009	0.01	QV	|	|	|	|
2+50	0.0010	0.01	QV	|	|	|	|
2+55	0.0010	0.01	QV	|	|	|	|
3+ 0	0.0010	0.01	QV	|	|	|	|
3+ 5	0.0011	0.01	QV	|	|	|	|
3+10	0.0011	0.01	QV	|	|	|	|
3+15	0.0012	0.01	QV	|	|	|	|
3+20	0.0012	0.01	QV	|	|	|	|
3+25	0.0013	0.01	QV	|	|	|	|
3+30	0.0013	0.01	QV	|	|	|	|
3+35	0.0014	0.01	Q V	|	|	|	|
3+40	0.0014	0.01	Q V	|	|	|	|
3+45	0.0015	0.01	Q V	|	|	|	|
3+50	0.0015	0.01	Q V	|	|	|	|
3+55	0.0015	0.01	Q V	|	|	|	|
4+ 0	0.0016	0.01	Q V	|	|	|	|
4+ 5	0.0017	0.01	Q V	|	|	|	|
4+10	0.0017	0.01	Q V	|	|	|	|
4+15	0.0018	0.01	Q V	|	|	|	|
4+20	0.0018	0.01	Q V	|	|	|	|
4+25	0.0019	0.01	Q V	|	|	|	|
4+30	0.0019	0.01	Q V	|	|	|	|
4+35	0.0020	0.01	Q V	|	|	|	|
4+40	0.0020	0.01	Q V	|	|	|	|
4+45	0.0021	0.01	Q V	|	|	|	|
4+50	0.0022	0.01	Q V	|	|	|	|
4+55	0.0022	0.01	Q V	|	|	|	|
5+ 0	0.0023	0.01	Q V	|	|	|	|
5+ 5	0.0024	0.01	Q V	|	|	|	|
5+10	0.0024	0.01	Q V	|	|	|	|
5+15	0.0025	0.01	Q V	|	|	|	|
5+20	0.0026	0.01	Q V	|	|	|	|
5+25	0.0026	0.01	Q V	|	|	|	|
5+30	0.0027	0.01	Q V	|	|	|	|
5+35	0.0027	0.01	Q V	|	|	|	|
5+40	0.0028	0.01	Q V	|	|	|	|
5+45	0.0029	0.01	Q V	|	|	|	|
5+50	0.0029	0.01	Q V	|	|	|	|
5+55	0.0030	0.01	Q V	|	|	|	|
6+ 0	0.0031	0.01	Q V	|	|	|	|
6+ 5	0.0032	0.01	Q V	|	|	|	|
6+10	0.0032	0.01	Q V	|	|	|	|
6+15	0.0033	0.01	Q V	|	|	|	|
6+20	0.0034	0.01	Q V	|	|	|	|
6+25	0.0035	0.01	Q V	|	|	|	|
6+30	0.0036	0.01	Q V	|	|	|	|
6+35	0.0036	0.01	Q V	|	|	|	|
6+40	0.0037	0.01	Q V	|	|	|	|
6+45	0.0038	0.01	Q V	|	|	|	|

```
 6+50       0.0039      0.01  Q    V    |          |          |          |
 6+55       0.0040      0.01  Q    V    |          |          |          |
 7+ 0       0.0041      0.01  Q     V   |          |          |          |
 7+ 5       0.0042      0.01  Q     V   |          |          |          |
 7+10       0.0042      0.01  Q     V   |          |          |          |
 7+15       0.0043      0.01  Q     V   |          |          |          |
 7+20       0.0044      0.01  Q     V   |          |          |          |
 7+25       0.0045      0.01  Q     V   |          |          |          |
 7+30       0.0046      0.01  Q     V   |          |          |          |
 7+35       0.0047      0.01  Q     V   |          |          |          |
 7+40       0.0048      0.01  Q      V  |          |          |          |
 7+45       0.0049      0.02  Q      V  |          |          |          |
 7+50       0.0050      0.02  Q      V  |          |          |          |
 7+55       0.0051      0.02  Q      V  |          |          |          |
 8+ 0       0.0052      0.02  Q      V  |          |          |          |
 8+ 5       0.0054      0.02  Q      V  |          |          |          |
 8+10       0.0055      0.02  Q       V |          |          |          |
 8+15       0.0056      0.02  Q       V |          |          |          |
 8+20       0.0057      0.02  Q       V |          |          |          |
 8+25       0.0059      0.02  Q       V |          |          |          |
 8+30       0.0060      0.02  Q       V |          |          |          |
 8+35       0.0061      0.02  Q        V|          |          |          |
 8+40       0.0063      0.02  Q        V|          |          |          |
 8+45       0.0064      0.02  Q        V|          |          |          |
 8+50       0.0066      0.02  Q        V|          |          |          |
 8+55       0.0067      0.02  Q        V|          |          |          |
 9+ 0       0.0069      0.02  Q         V          |          |          |
 9+ 5       0.0070      0.02  Q         V          |          |          |
 9+10       0.0072      0.02  Q         V          |          |          |
 9+15       0.0073      0.02  Q         V          |          |          |
 9+20       0.0075      0.02  Q         |V         |          |          |
 9+25       0.0077      0.02  Q         |V         |          |          |
 9+30       0.0078      0.03  Q         |V         |          |          |
 9+35       0.0080      0.03  Q         |V         |          |          |
 9+40       0.0082      0.03  Q         | V        |          |          |
 9+45       0.0084      0.03  Q         | V        |          |          |
 9+50       0.0086      0.03  Q         | V        |          |          |
 9+55       0.0088      0.03  Q         | V        |          |          |
10+ 0       0.0090      0.03  Q         |  V       |          |          |
10+ 5       0.0091      0.03  Q         |  V       |          |          |
10+10       0.0093      0.02  Q         |  V       |          |          |
10+15       0.0095      0.02  Q         |   V      |          |          |
10+20       0.0096      0.02  Q         |   V      |          |          |
10+25       0.0098      0.02  Q         |   V      |          |          |
10+30       0.0099      0.02  Q         |   V      |          |          |
10+35       0.0100      0.02  Q         |   V      |          |          |
10+40       0.0102      0.02  Q         |    V     |          |          |
10+45       0.0104      0.02  Q         |    V     |          |          |
10+50       0.0105      0.03  Q         |    V     |          |          |
10+55       0.0107      0.03  Q         |    V     |          |          |
```

```
11+ 0       0.0109      0.03  Q         |     V   |         |         |
11+ 5       0.0111      0.03  Q         |     V   |         |         |
11+10       0.0112      0.03  Q         |     V   |         |         |
11+15       0.0114      0.02  Q         |     V   |         |         |
11+20       0.0116      0.02  Q         |      V  |         |         |
11+25       0.0118      0.02  Q         |      V  |         |         |
11+30       0.0119      0.02  Q         |      V  |         |         |
11+35       0.0121      0.02  Q         |      V  |         |         |
11+40       0.0123      0.02  Q         |       V |         |         |
11+45       0.0124      0.02  Q         |       V |         |         |
11+50       0.0126      0.02  Q         |       V |         |         |
11+55       0.0127      0.02  Q         |       V |         |         |
12+ 0       0.0129      0.02  Q         |        V|         |         |
12+ 5       0.0131      0.02  Q         |        V|         |         |
12+10       0.0133      0.03  Q         |        V|         |         |
12+15       0.0135      0.03  Q         |        V|         |         |
12+20       0.0137      0.03  Q         |         V         |         |
12+25       0.0139      0.03  Q         |         V         |         |
12+30       0.0141      0.03  Q         |         V         |         |
12+35       0.0143      0.03  Q         |         |V        |         |
12+40       0.0146      0.03  Q         |         |V        |         |
12+45       0.0148      0.04  Q         |         |V        |         |
12+50       0.0151      0.04  Q         |         | V       |         |
12+55       0.0153      0.04  Q         |         | V       |         |
13+ 0       0.0156      0.04  Q         |         |  V      |         |
13+ 5       0.0158      0.04  Q         |         |  V      |         |
13+10       0.0161      0.04  Q         |         |  V      |         |
13+15       0.0164      0.04  Q         |         |   V     |         |
13+20       0.0167      0.04  Q         |         |   V     |         |
13+25       0.0170      0.04  Q         |         |    V    |         |
13+30       0.0173      0.04  Q         |         |    V    |         |
13+35       0.0176      0.04  Q         |         |     V   |         |
13+40       0.0179      0.04  Q         |         |     V   |         |
13+45       0.0181      0.03  Q         |         |     V   |         |
13+50       0.0183      0.03  Q         |         |      V  |         |
13+55       0.0185      0.03  Q         |         |      V  |         |
14+ 0       0.0188      0.03  Q         |         |      V  |         |
14+ 5       0.0190      0.03  Q         |         |       V |         |
14+10       0.0192      0.03  Q         |         |       V |         |
14+15       0.0194      0.03  Q         |         |       V |         |
14+20       0.0197      0.03  Q         |         |        V|         |
14+25       0.0199      0.03  Q         |         |        V|         |
14+30       0.0201      0.03  Q         |         |        V|         |
14+35       0.0204      0.03  Q         |         |         V         |
14+40       0.0206      0.03  Q         |         |         V         |
14+45       0.0208      0.03  Q         |         |         V         |
14+50       0.0211      0.03  Q         |         |         |V        |
14+55       0.0213      0.03  Q         |         |         |V        |
15+ 0       0.0215      0.03  Q         |         |         |V        |
15+ 5       0.0218      0.03  Q         |         |         | V       |
```

```
15+10       0.0220      0.03  Q        |          |          | V        |
15+15       0.0222      0.03  Q        |          |          | V        |
15+20       0.0224      0.03  Q        |          |          |  V       |
15+25       0.0226      0.03  Q        |          |          |  V       |
15+30       0.0228      0.03  Q        |          |          |  V       |
15+35       0.0231      0.03  Q        |          |          |   V      |
15+40       0.0232      0.03  Q        |          |          |   V      |
15+45       0.0234      0.03  Q        |          |          |   V      |
15+50       0.0236      0.03  Q        |          |          |   V      |
15+55       0.0238      0.03  Q        |          |          |    V     |
16+ 0       0.0240      0.03  Q        |          |          |    V     |
16+ 5       0.0241      0.02  Q        |          |          |    V     |
16+10       0.0242      0.02  Q        |          |          |    V     |
16+15       0.0243      0.01  Q        |          |          |     V    |
16+20       0.0244      0.01  Q        |          |          |     V    |
16+25       0.0244      0.01  Q        |          |          |     V    |
16+30       0.0245      0.01  Q        |          |          |     V    |
16+35       0.0245      0.01  Q        |          |          |     V    |
16+40       0.0246      0.01  Q        |          |          |     V    |
16+45       0.0246      0.01  Q        |          |          |     V    |
16+50       0.0246      0.00  Q        |          |          |     V    |
16+55       0.0247      0.00  Q        |          |          |     V    |
17+ 0       0.0247      0.00  Q        |          |          |     V    |
17+ 5       0.0247      0.00  Q        |          |          |     V    |
17+10       0.0248      0.01  Q        |          |          |     V    |
17+15       0.0248      0.01  Q        |          |          |     V    |
17+20       0.0249      0.01  Q        |          |          |     V    |
17+25       0.0249      0.01  Q        |          |          |     V    |
17+30       0.0249      0.01  Q        |          |          |     V    |
17+35       0.0250      0.01  Q        |          |          |      V   |
17+40       0.0250      0.01  Q        |          |          |      V   |
17+45       0.0251      0.01  Q        |          |          |      V   |
17+50       0.0251      0.01  Q        |          |          |      V   |
17+55       0.0252      0.01  Q        |          |          |      V   |
18+ 0       0.0252      0.01  Q        |          |          |      V   |
18+ 5       0.0252      0.01  Q        |          |          |      V   |
18+10       0.0253      0.01  Q        |          |          |      V   |
18+15       0.0253      0.01  Q        |          |          |      V   |
18+20       0.0253      0.01  Q        |          |          |      V   |
18+25       0.0254      0.01  Q        |          |          |      V   |
18+30       0.0254      0.01  Q        |          |          |      V   |
18+35       0.0255      0.01  Q        |          |          |      V   |
18+40       0.0255      0.00  Q        |          |          |      V   |
18+45       0.0255      0.00  Q        |          |          |      V   |
18+50       0.0255      0.00  Q        |          |          |      V   |
18+55       0.0256      0.00  Q        |          |          |      V   |
19+ 0       0.0256      0.00  Q        |          |          |      V   |
19+ 5       0.0256      0.00  Q        |          |          |      V   |
19+10       0.0256      0.00  Q        |          |          |      V   |
19+15       0.0257      0.00  Q        |          |          |       V  |
```

19+20	0.0257	0.00	Q	|	|	|	V |
19+25	0.0257	0.00	Q	|	|	|	V |
19+30	0.0257	0.00	Q	|	|	|	V |
19+35	0.0258	0.00	Q	|	|	|	V |
19+40	0.0258	0.00	Q	|	|	|	V |
19+45	0.0258	0.00	Q	|	|	|	V |
19+50	0.0259	0.00	Q	|	|	|	V |
19+55	0.0259	0.00	Q	|	|	|	V |
20+ 0	0.0259	0.00	Q	|	|	|	V |
20+ 5	0.0259	0.00	Q	|	|	|	V |
20+10	0.0260	0.00	Q	|	|	|	V |
20+15	0.0260	0.00	Q	|	|	|	V |
20+20	0.0260	0.00	Q	|	|	|	V |
20+25	0.0260	0.00	Q	|	|	|	V |
20+30	0.0261	0.00	Q	|	|	|	V |
20+35	0.0261	0.00	Q	|	|	|	V |
20+40	0.0261	0.00	Q	|	|	|	V |
20+45	0.0261	0.00	Q	|	|	|	V |
20+50	0.0262	0.00	Q	|	|	|	V |
20+55	0.0262	0.00	Q	|	|	|	V |
21+ 0	0.0262	0.00	Q	|	|	|	V |
21+ 5	0.0262	0.00	Q	|	|	|	V |
21+10	0.0263	0.00	Q	|	|	|	V |
21+15	0.0263	0.00	Q	|	|	|	V |
21+20	0.0263	0.00	Q	|	|	|	V |
21+25	0.0263	0.00	Q	|	|	|	V|
21+30	0.0263	0.00	Q	|	|	|	V|
21+35	0.0264	0.00	Q	|	|	|	V|
21+40	0.0264	0.00	Q	|	|	|	V|
21+45	0.0264	0.00	Q	|	|	|	V|
21+50	0.0264	0.00	Q	|	|	|	V|
21+55	0.0265	0.00	Q	|	|	|	V|
22+ 0	0.0265	0.00	Q	|	|	|	V|
22+ 5	0.0265	0.00	Q	|	|	|	V|
22+10	0.0265	0.00	Q	|	|	|	V|
22+15	0.0266	0.00	Q	|	|	|	V|
22+20	0.0266	0.00	Q	|	|	|	V|
22+25	0.0266	0.00	Q	|	|	|	V|
22+30	0.0266	0.00	Q	|	|	|	V|
22+35	0.0266	0.00	Q	|	|	|	V|
22+40	0.0267	0.00	Q	|	|	|	V|
22+45	0.0267	0.00	Q	|	|	|	V|
22+50	0.0267	0.00	Q	|	|	|	V|
22+55	0.0267	0.00	Q	|	|	|	V|
23+ 0	0.0267	0.00	Q	|	|	|	V|
23+ 5	0.0267	0.00	Q	|	|	|	V|
23+10	0.0268	0.00	Q	|	|	|	V|
23+15	0.0268	0.00	Q	|	|	|	V|
23+20	0.0268	0.00	Q	|	|	|	V|
23+25	0.0268	0.00	Q	|	|	|	V|

23+30	0.0268	0.00	Q	|	|	|	V|
23+35	0.0269	0.00	Q	|	|	|	V|
23+40	0.0269	0.00	Q	|	|	|	V|
23+45	0.0269	0.00	Q	|	|	|	V|
23+50	0.0269	0.00	Q	|	|	|	V|
23+55	0.0269	0.00	Q	|	|	|	V|
24+ 0	0.0269	0.00	Q	|	|	|	V|
24+ 5	0.0270	0.00	Q	|	|	|	V|
24+10	0.0270	0.00	Q	|	|	|	V|
24+15	0.0270	0.00	Q	|	|	|	V|
24+20	0.0270	0.00	Q	|	|	|	V|
24+25	0.0270	0.00	Q	|	|	|	V|
24+30	0.0270	0.00	Q	|	|	|	V|
24+35	0.0270	0.00	Q	|	|	|	V|
24+40	0.0270	0.00	Q	|	|	|	V|
24+45	0.0270	0.00	Q	|	|	|	V|
24+50	0.0270	0.00	Q	|	|	|	V|
24+55	0.0270	0.00	Q	|	|	|	V|
25+ 0	0.0270	0.00	Q	|	|	|	V|
25+ 5	0.0270	0.00	Q	|	|	|	V|

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris15.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
5 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.49	0.78

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            1.35                   2.13

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.493(In)
Area Averaged 100-Year Rainfall =    1.350(In)

Point rain (area averaged) =    0.694(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    0.694(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           67.00         0.000
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
67.0  47.4      0.597     0.000        0.597       1.000      0.597
                                                 Sum (F) =   0.597
Area averaged mean soil loss (F) (In/Hr) =  0.597
Minimum soil loss rate ((In/Hr)) =  0.299
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5000
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
-----------------------------------------------------------------
               Unit Hydrograph Data
-----------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
-----------------------------------------------------------------
    1   0.083         59.952          8.204              0.131
    2   0.167        119.904         33.934              0.540
    3   0.250        179.856         26.599              0.424
    4   0.333        239.808         10.311              0.164
    5   0.417        299.760          6.100              0.097
    6   0.500        359.712          4.123              0.066
    7   0.583        419.664          2.936              0.047
    8   0.667        479.616          2.066              0.033
    9   0.750        539.568          1.709              0.027
   10   0.833        599.520          1.265              0.020
   11   0.917        659.472          0.962              0.015
```

12	1.000	719.424	0.685	0.011
13	1.083	779.376	0.600	0.010
14	1.167	839.329	0.506	0.008
		Sum = 100.000	Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.20	0.350	(0.597)	0.315	0.035
2	0.17	4.30	0.358	(0.597)	0.322	0.036
3	0.25	5.00	0.416	(0.597)	0.375	0.042
4	0.33	5.00	0.416	(0.597)	0.375	0.042
5	0.42	5.80	0.483	(0.597)	0.435	0.048
6	0.50	6.50	0.541	(0.597)	0.487	0.054
7	0.58	7.40	0.616	(0.597)	0.554	0.062
8	0.67	8.60	0.716	0.597	(0.644)	0.118
9	0.75	12.30	1.024	0.597	(0.922)	0.426
10	0.83	29.10	2.422	0.597	(2.180)	1.825
11	0.92	6.80	0.566	(0.597)	0.509	0.057
12	1.00	5.00	0.416	(0.597)	0.375	0.042
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	2.8

Flood volume = Effective rainfall 0.23(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 0.46(In)
Total soil loss = 0.061(Ac.Ft)
Total rainfall = 0.69(In)
Flood volume = 1331.6 Cubic Feet
Total soil loss = 2647.1 Cubic Feet

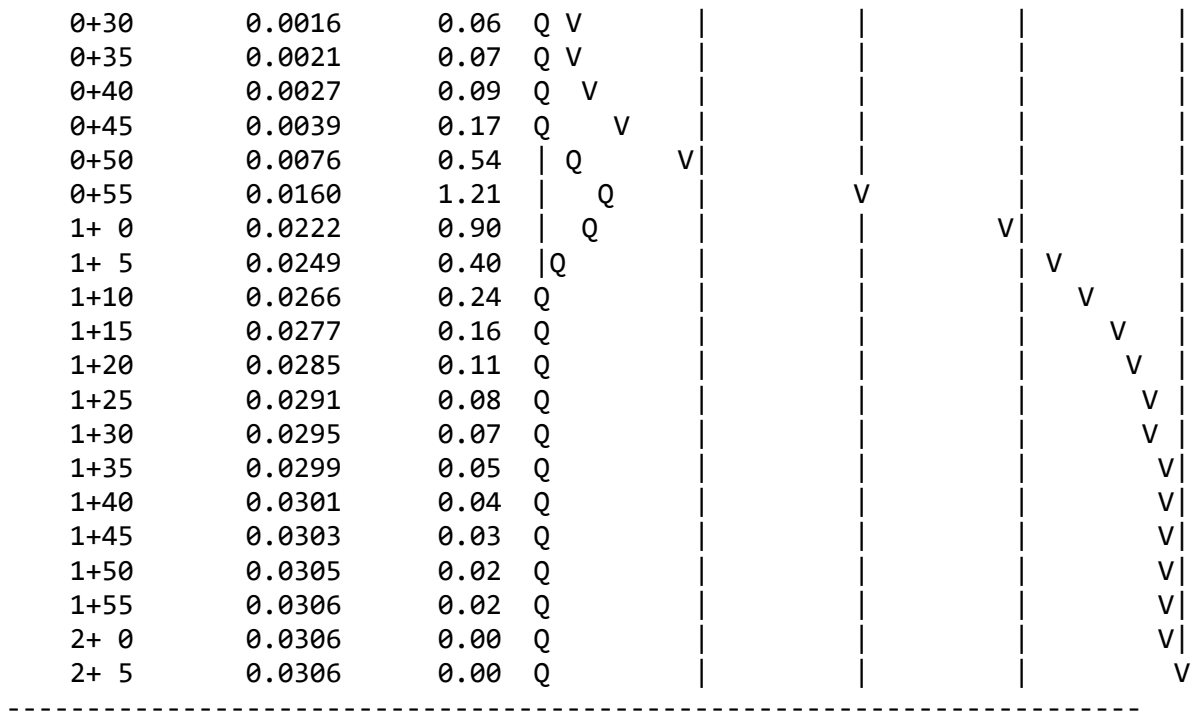
Peak flow rate of this hydrograph = 1.210(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.00	Q	|	|	|	|
0+10	0.0002	0.02	Q	|	|	|	|
0+15	0.0005	0.04	Q	|	|	|	|
0+20	0.0008	0.05	QV	|	|	|	|
0+25	0.0012	0.06	QV	|	|	|	|


0+30 0.0016 0.06
0+35 0.0021 0.07
0+40 0.0027 0.09
0+45 0.0039 0.17
0+50 0.0076 0.54
0+55 0.0160 1.21
1+ 0 0.0222 0.90
1+ 5 0.0249 0.40
1+10 0.0266 0.24
1+15 0.0277 0.16
1+20 0.0285 0.11
1+25 0.0291 0.08
1+30 0.0295 0.07
1+35 0.0299 0.05
1+40 0.0301 0.04
1+45 0.0303 0.03
1+50 0.0305 0.02
1+55 0.0306 0.02
2+ 0 0.0306 0.00
2+ 5 0.0306 0.00

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris35.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
5 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.87	1.37

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.10	3.32

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.869(In)
Area Averaged 100-Year Rainfall = 2.100(In)

Point rain (area averaged) = 1.157(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.157(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.580	67.00	0.000

Total Area Entered = 1.58(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
67.0	47.4	0.597	0.000	0.597	1.000	0.597
					Sum (F) =	0.597

Area averaged mean soil loss (F) (In/Hr) = 0.597
Minimum soil loss rate ((In/Hr)) = 0.299
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	59.952	8.204	0.131
2	0.167	119.904	33.934	0.540
3	0.250	179.856	26.599	0.424
4	0.333	239.808	10.311	0.164
5	0.417	299.760	6.100	0.097
6	0.500	359.712	4.123	0.066
7	0.583	419.664	2.936	0.047
8	0.667	479.616	2.066	0.033
9	0.750	539.568	1.709	0.027
10	0.833	599.520	1.265	0.020
11	0.917	659.472	0.962	0.015
12	1.000	719.424	0.685	0.011
13	1.083	779.376	0.600	0.010

14	1.167	839.329	0.506		0.008
			Sum = 100.000	Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.181	(0.597)	0.162	0.018
2	0.17	1.30	0.181	(0.597)	0.162	0.018
3	0.25	1.10	0.153	(0.597)	0.137	0.015
4	0.33	1.50	0.208	(0.597)	0.187	0.021
5	0.42	1.50	0.208	(0.597)	0.187	0.021
6	0.50	1.80	0.250	(0.597)	0.225	0.025
7	0.58	1.50	0.208	(0.597)	0.187	0.021
8	0.67	1.80	0.250	(0.597)	0.225	0.025
9	0.75	1.80	0.250	(0.597)	0.225	0.025
10	0.83	1.50	0.208	(0.597)	0.187	0.021
11	0.92	1.60	0.222	(0.597)	0.200	0.022
12	1.00	1.80	0.250	(0.597)	0.225	0.025
13	1.08	2.20	0.306	(0.597)	0.275	0.031
14	1.17	2.20	0.306	(0.597)	0.275	0.031
15	1.25	2.20	0.306	(0.597)	0.275	0.031
16	1.33	2.00	0.278	(0.597)	0.250	0.028
17	1.42	2.60	0.361	(0.597)	0.325	0.036
18	1.50	2.70	0.375	(0.597)	0.337	0.037
19	1.58	2.40	0.333	(0.597)	0.300	0.033
20	1.67	2.70	0.375	(0.597)	0.337	0.037
21	1.75	3.30	0.458	(0.597)	0.412	0.046
22	1.83	3.10	0.431	(0.597)	0.387	0.043
23	1.92	2.90	0.403	(0.597)	0.362	0.040
24	2.00	3.00	0.417	(0.597)	0.375	0.042
25	2.08	3.10	0.431	(0.597)	0.387	0.043
26	2.17	4.20	0.583	(0.597)	0.525	0.058
27	2.25	5.00	0.694	0.597	(0.625)	0.097
28	2.33	3.50	0.486	(0.597)	0.437	0.049
29	2.42	6.80	0.944	0.597	(0.850)	0.347
30	2.50	7.30	1.014	0.597	(0.912)	0.416
31	2.58	8.20	1.139	0.597	(1.025)	0.541
32	2.67	5.90	0.819	0.597	(0.737)	0.222
33	2.75	2.00	0.278	(0.597)	0.250	0.028
34	2.83	1.80	0.250	(0.597)	0.225	0.025
35	2.92	1.80	0.250	(0.597)	0.225	0.025
36	3.00	0.60	0.083	(0.597)	0.075	0.008
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	2.6

Flood volume = Effective rainfall 0.21(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)

```
      Total soil loss =      0.94(In)
      Total soil loss =     0.124(Ac.Ft)
      Total rainfall =      1.16(In)
      Flood volume =        1219.3 Cubic Feet
      Total soil loss =        5418.4 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.574(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          3 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0000      0.00  Q         |         |         |         |
  0+10       0.0001      0.01  Q         |         |         |         |
  0+15       0.0002      0.02  Q         |         |         |         |
  0+20       0.0004      0.02  Q         |         |         |         |
  0+25       0.0006      0.03  Q         |         |         |         |
  0+30       0.0008      0.03  QV        |         |         |         |
  0+35       0.0010      0.03  QV        |         |         |         |
  0+40       0.0012      0.03  QV        |         |         |         |
  0+45       0.0014      0.03  Q V       |         |         |         |
  0+50       0.0017      0.04  Q V       |         |         |         |
  0+55       0.0019      0.04  Q V       |         |         |         |
  1+ 0       0.0022      0.04  Q  V      |         |         |         |
  1+ 5       0.0024      0.04  Q  V      |         |         |         |
  1+10       0.0027      0.04  Q  V      |         |         |         |
  1+15       0.0030      0.04  Q   V     |         |         |         |
  1+20       0.0034      0.05  Q   V     |         |         |         |
  1+25       0.0037      0.05  Q    V    |         |         |         |
  1+30       0.0040      0.05  Q    V    |         |         |         |
  1+35       0.0044      0.05  Q     V   |         |         |         |
  1+40       0.0048      0.05  Q     V   |         |         |         |
  1+45       0.0052      0.06  Q      V  |         |         |         |
  1+50       0.0056      0.06  Q      V  |         |         |         |
  1+55       0.0060      0.06  Q       V |         |         |         |
  2+ 0       0.0065      0.06  Q        V|         |         |         |
  2+ 5       0.0069      0.06  Q        V|         |         |         |
  2+10       0.0074      0.07  Q         V         |         |         |
  2+15       0.0080      0.08  Q         |V        |         |         |
  2+20       0.0087      0.10  Q         | V       |         |         |
  2+25       0.0096      0.14  Q         |  V      |         |         |
  2+30       0.0116      0.29  |Q        |     V   |         |         |
  2+35       0.0149      0.47  |Q        |         |V        |         |
  2+40       0.0188      0.57  | Q       |         |     V   |         |
  2+45       0.0221      0.47  |Q        |         |         |V        |
```

```
    2+50       0.0239      0.27  |Q        |          |          |   V      |
    2+55       0.0251      0.17  Q         |          |          |    V     |
    3+ 0       0.0260      0.12  Q         |          |          |      V   |
    3+ 5       0.0266      0.09  Q         |          |          |      V   |
    3+10       0.0270      0.06  Q         |          |          |       V  |
    3+15       0.0273      0.04  Q         |          |          |        V|
    3+20       0.0275      0.03  Q         |          |          |        V|
    3+25       0.0277      0.02  Q         |          |          |        V|
    3+30       0.0278      0.02  Q         |          |          |        V|
    3+35       0.0279      0.01  Q         |          |          |        V|
    3+40       0.0280      0.01  Q         |          |          |        V|
    3+45       0.0280      0.00  Q         |          |          |        V|
    3+50       0.0280      0.00  Q         |          |          |        V|
    3+55       0.0280      0.00  Q         |          |          |        V|
    4+ 0       0.0280      0.00  Q         |          |          |        V|
    4+ 5       0.0280      0.00  Q         |          |          |         V
---------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris65.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
5 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	1.22	1.93

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.87	4.53

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.220(In)
Area Averaged 100-Year Rainfall = 2.870(In)

Point rain (area averaged) = 1.606(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.606(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.580	67.00	0.000

Total Area Entered = 1.58(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
67.0	47.4	0.597	0.000	0.597	1.000	0.597
					Sum (F) =	0.597

Area averaged mean soil loss (F) (In/Hr) = 0.597
Minimum soil loss rate ((In/Hr)) = 0.299
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	59.952	8.204	0.131
2	0.167	119.904	33.934	0.540
3	0.250	179.856	26.599	0.424
4	0.333	239.808	10.311	0.164
5	0.417	299.760	6.100	0.097
6	0.500	359.712	4.123	0.066
7	0.583	419.664	2.936	0.047
8	0.667	479.616	2.066	0.033
9	0.750	539.568	1.709	0.027
10	0.833	599.520	1.265	0.020
11	0.917	659.472	0.962	0.015
12	1.000	719.424	0.685	0.011
13	1.083	779.376	0.600	0.010

14	1.167	839.329	0.506			0.008
			Sum = 100.000		Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.096	(0.597)	0.087	0.010
2	0.17	0.60	0.116	(0.597)	0.104	0.012
3	0.25	0.60	0.116	(0.597)	0.104	0.012
4	0.33	0.60	0.116	(0.597)	0.104	0.012
5	0.42	0.60	0.116	(0.597)	0.104	0.012
6	0.50	0.70	0.135	(0.597)	0.121	0.013
7	0.58	0.70	0.135	(0.597)	0.121	0.013
8	0.67	0.70	0.135	(0.597)	0.121	0.013
9	0.75	0.70	0.135	(0.597)	0.121	0.013
10	0.83	0.70	0.135	(0.597)	0.121	0.013
11	0.92	0.70	0.135	(0.597)	0.121	0.013
12	1.00	0.80	0.154	(0.597)	0.139	0.015
13	1.08	0.80	0.154	(0.597)	0.139	0.015
14	1.17	0.80	0.154	(0.597)	0.139	0.015
15	1.25	0.80	0.154	(0.597)	0.139	0.015
16	1.33	0.80	0.154	(0.597)	0.139	0.015
17	1.42	0.80	0.154	(0.597)	0.139	0.015
18	1.50	0.80	0.154	(0.597)	0.139	0.015
19	1.58	0.80	0.154	(0.597)	0.139	0.015
20	1.67	0.80	0.154	(0.597)	0.139	0.015
21	1.75	0.80	0.154	(0.597)	0.139	0.015
22	1.83	0.80	0.154	(0.597)	0.139	0.015
23	1.92	0.80	0.154	(0.597)	0.139	0.015
24	2.00	0.90	0.173	(0.597)	0.156	0.017
25	2.08	0.80	0.154	(0.597)	0.139	0.015
26	2.17	0.90	0.173	(0.597)	0.156	0.017
27	2.25	0.90	0.173	(0.597)	0.156	0.017
28	2.33	0.90	0.173	(0.597)	0.156	0.017
29	2.42	0.90	0.173	(0.597)	0.156	0.017
30	2.50	0.90	0.173	(0.597)	0.156	0.017
31	2.58	0.90	0.173	(0.597)	0.156	0.017
32	2.67	0.90	0.173	(0.597)	0.156	0.017
33	2.75	1.00	0.193	(0.597)	0.173	0.019
34	2.83	1.00	0.193	(0.597)	0.173	0.019
35	2.92	1.00	0.193	(0.597)	0.173	0.019
36	3.00	1.00	0.193	(0.597)	0.173	0.019
37	3.08	1.00	0.193	(0.597)	0.173	0.019
38	3.17	1.10	0.212	(0.597)	0.191	0.021
39	3.25	1.10	0.212	(0.597)	0.191	0.021
40	3.33	1.10	0.212	(0.597)	0.191	0.021

41	3.42	1.20	0.231	(0.597)	0.208	0.023	
42	3.50	1.30	0.251	(0.597)	0.226	0.025	
43	3.58	1.40	0.270	(0.597)	0.243	0.027	
44	3.67	1.40	0.270	(0.597)	0.243	0.027	
45	3.75	1.50	0.289	(0.597)	0.260	0.029	
46	3.83	1.50	0.289	(0.597)	0.260	0.029	
47	3.92	1.60	0.308	(0.597)	0.278	0.031	
48	4.00	1.60	0.308	(0.597)	0.278	0.031	
49	4.08	1.70	0.328	(0.597)	0.295	0.033	
50	4.17	1.80	0.347	(0.597)	0.312	0.035	
51	4.25	1.90	0.366	(0.597)	0.330	0.037	
52	4.33	2.00	0.386	(0.597)	0.347	0.039	
53	4.42	2.10	0.405	(0.597)	0.364	0.040	
54	4.50	2.10	0.405	(0.597)	0.364	0.040	
55	4.58	2.20	0.424	(0.597)	0.382	0.042	
56	4.67	2.30	0.443	(0.597)	0.399	0.044	
57	4.75	2.40	0.463	(0.597)	0.416	0.046	
58	4.83	2.40	0.463	(0.597)	0.416	0.046	
59	4.92	2.50	0.482	(0.597)	0.434	0.048	
60	5.00	2.60	0.501	(0.597)	0.451	0.050	
61	5.08	3.10	0.598	(0.597)	0.538	0.060	
62	5.17	3.60	0.694	0.597	(0.625)	0.097	
63	5.25	3.90	0.752	0.597	(0.677)	0.154	
64	5.33	4.20	0.810	0.597	(0.729)	0.212	
65	5.42	4.70	0.906	0.597	(0.815)	0.309	
66	5.50	5.60	1.080	0.597	(0.972)	0.482	
67	5.58	1.90	0.366	(0.597)	0.330	0.037	
68	5.67	0.90	0.173	(0.597)	0.156	0.017	
69	5.75	0.60	0.116	(0.597)	0.104	0.012	
70	5.83	0.50	0.096	(0.597)	0.087	0.010	
71	5.92	0.30	0.058	(0.597)	0.052	0.006	
72	6.00	0.20	0.039	(0.597)	0.035	0.004	

(Loss Rate Not Used)

Sum = 100.0 Sum = 2.8

Flood volume = Effective rainfall 0.23(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.0(Ac.Ft)
Total soil loss = 1.38(In)
Total soil loss = 0.181(Ac.Ft)
Total rainfall = 1.61(In)
Flood volume = 1317.9 Cubic Feet
Total soil loss = 7895.8 Cubic Feet

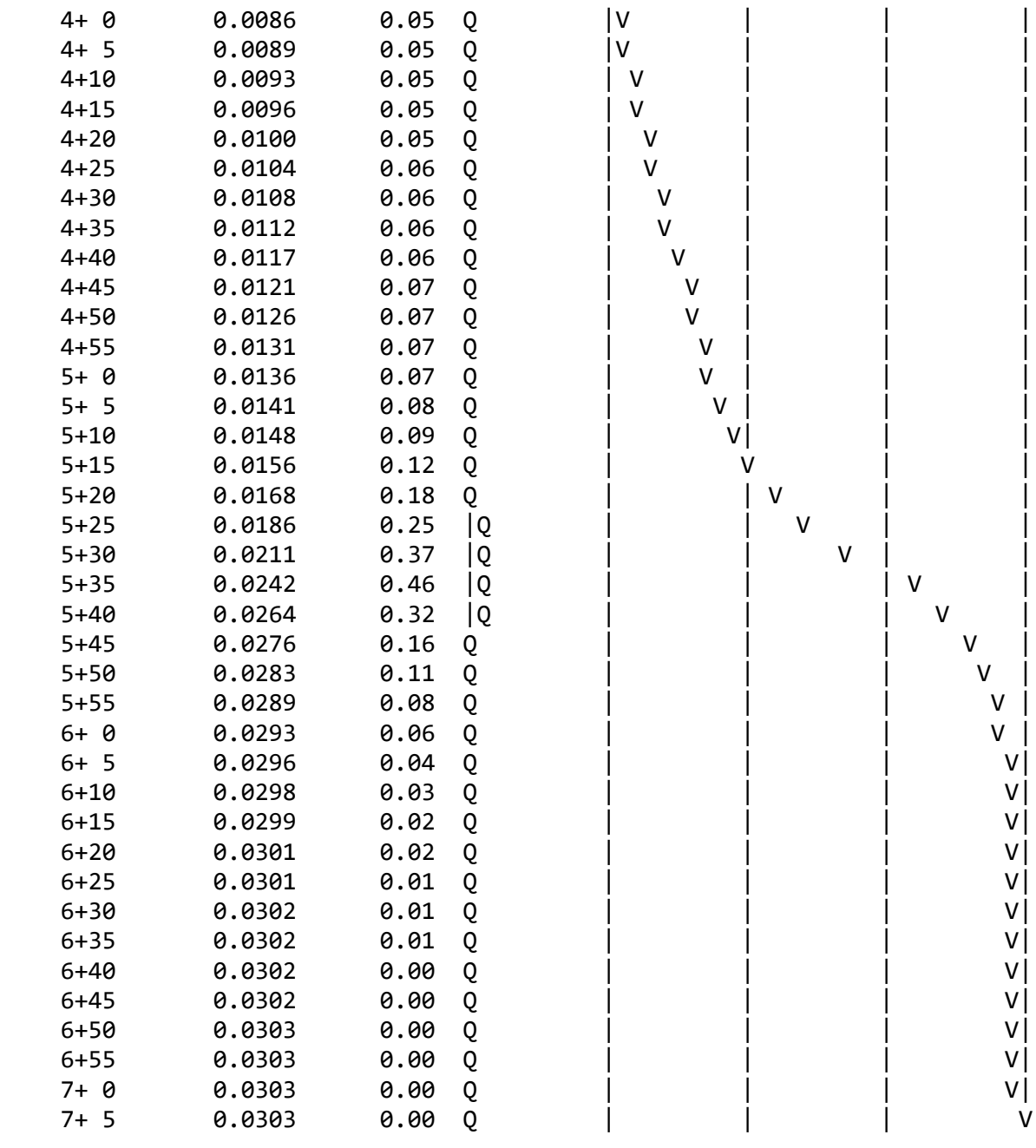
Peak flow rate of this hydrograph = 0.461(CFS)

++

6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.00	Q				
0+10	0.0001	0.01	Q				
0+15	0.0001	0.01	Q				
0+20	0.0002	0.01	Q				
0+25	0.0003	0.02	Q				
0+30	0.0005	0.02	Q				
0+35	0.0006	0.02	Q				
0+40	0.0007	0.02	Q				
0+45	0.0009	0.02	QV				
0+50	0.0010	0.02	QV				
0+55	0.0011	0.02	QV				
1+ 0	0.0013	0.02	QV				
1+ 5	0.0014	0.02	QV				
1+10	0.0016	0.02	Q V				
1+15	0.0018	0.02	Q V				
1+20	0.0019	0.02	Q V				
1+25	0.0021	0.02	Q V				
1+30	0.0023	0.02	Q V				
1+35	0.0024	0.02	Q V				
1+40	0.0026	0.02	Q V				
1+45	0.0028	0.02	Q V				
1+50	0.0029	0.02	Q V				
1+55	0.0031	0.02	Q V				
2+ 0	0.0033	0.02	Q V				
2+ 5	0.0035	0.03	Q V				
2+10	0.0036	0.03	Q V				
2+15	0.0038	0.03	Q V				
2+20	0.0040	0.03	Q V				
2+25	0.0042	0.03	Q V				
2+30	0.0044	0.03	Q V				
2+35	0.0046	0.03	Q V				
2+40	0.0047	0.03	Q V				
2+45	0.0049	0.03	Q V				
2+50	0.0051	0.03	Q V				
2+55	0.0053	0.03	Q V				
3+ 0	0.0055	0.03	Q V				
3+ 5	0.0058	0.03	Q V				
3+10	0.0060	0.03	Q V				
3+15	0.0062	0.03	Q V				
3+20	0.0064	0.03	Q V				
3+25	0.0066	0.03	Q V				
3+30	0.0069	0.03	Q V				
3+35	0.0071	0.04	Q V				
3+40	0.0074	0.04	Q V				
3+45	0.0077	0.04	Q V				
3+50	0.0080	0.04	Q V				
3+55	0.0083	0.04	Q V				


4+ 0 0.0086 0.05 Q
4+ 5 0.0089 0.05 Q
4+10 0.0093 0.05 Q
4+15 0.0096 0.05 Q
4+20 0.0100 0.05 Q
4+25 0.0104 0.06 Q
4+30 0.0108 0.06 Q
4+35 0.0112 0.06 Q
4+40 0.0117 0.06 Q
4+45 0.0121 0.07 Q
4+50 0.0126 0.07 Q
4+55 0.0131 0.07 Q
5+ 0 0.0136 0.07 Q
5+ 5 0.0141 0.08 Q
5+10 0.0148 0.09 Q
5+15 0.0156 0.12 Q
5+20 0.0168 0.18 Q
5+25 0.0186 0.25 Q
5+30 0.0211 0.37 Q
5+35 0.0242 0.46 Q
5+40 0.0264 0.32 Q
5+45 0.0276 0.16 Q
5+50 0.0283 0.11 Q
5+55 0.0289 0.08 Q
6+ 0 0.0293 0.06 Q
6+ 5 0.0296 0.04 Q
6+10 0.0298 0.03 Q
6+15 0.0299 0.02 Q
6+20 0.0301 0.02 Q
6+25 0.0301 0.01 Q
6+30 0.0302 0.01 Q
6+35 0.0302 0.01 Q
6+40 0.0302 0.00 Q
6+45 0.0302 0.00 Q
6+50 0.0303 0.00 Q
6+55 0.0303 0.00 Q
7+ 0 0.0303 0.00 Q
7+ 5 0.0303 0.00 Q

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris245.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
5 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.05	3.24

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            5.25                   8.29

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    2.050(In)
Area Averaged 100-Year Rainfall =    5.250(In)

Point rain (area averaged) =    2.800(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    2.800(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           67.00         0.000
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
67.0  47.4      0.597     0.000        0.597       1.000      0.597
                                                 Sum (F) =   0.597
Area averaged mean soil loss (F) (In/Hr) =  0.597
Minimum soil loss rate ((In/Hr)) =  0.299
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
------------------------------------------------------------------------
    1   0.083         59.952          8.204             0.131
    2   0.167        119.904         33.934             0.540
    3   0.250        179.856         26.599             0.424
    4   0.333        239.808         10.311             0.164
    5   0.417        299.760          6.100             0.097
    6   0.500        359.712          4.123             0.066
    7   0.583        419.664          2.936             0.047
    8   0.667        479.616          2.066             0.033
    9   0.750        539.568          1.709             0.027
   10   0.833        599.520          1.265             0.020
   11   0.917        659.472          0.962             0.015
   12   1.000        719.424          0.685             0.011
   13   1.083        779.376          0.600             0.010
```

14	1.167	839.329	0.506			0.008
			Sum = 100.000		Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.022	(1.059)	0.020	0.002
2	0.17	0.07	0.022	(1.055)	0.020	0.002
3	0.25	0.07	0.022	(1.051)	0.020	0.002
4	0.33	0.10	0.034	(1.047)	0.030	0.003
5	0.42	0.10	0.034	(1.043)	0.030	0.003
6	0.50	0.10	0.034	(1.039)	0.030	0.003
7	0.58	0.10	0.034	(1.035)	0.030	0.003
8	0.67	0.10	0.034	(1.031)	0.030	0.003
9	0.75	0.10	0.034	(1.027)	0.030	0.003
10	0.83	0.13	0.045	(1.023)	0.040	0.004
11	0.92	0.13	0.045	(1.019)	0.040	0.004
12	1.00	0.13	0.045	(1.015)	0.040	0.004
13	1.08	0.10	0.034	(1.011)	0.030	0.003
14	1.17	0.10	0.034	(1.007)	0.030	0.003
15	1.25	0.10	0.034	(1.003)	0.030	0.003
16	1.33	0.10	0.034	(0.999)	0.030	0.003
17	1.42	0.10	0.034	(0.995)	0.030	0.003
18	1.50	0.10	0.034	(0.991)	0.030	0.003
19	1.58	0.10	0.034	(0.987)	0.030	0.003
20	1.67	0.10	0.034	(0.983)	0.030	0.003
21	1.75	0.10	0.034	(0.979)	0.030	0.003
22	1.83	0.13	0.045	(0.975)	0.040	0.004
23	1.92	0.13	0.045	(0.971)	0.040	0.004
24	2.00	0.13	0.045	(0.967)	0.040	0.004
25	2.08	0.13	0.045	(0.963)	0.040	0.004
26	2.17	0.13	0.045	(0.959)	0.040	0.004
27	2.25	0.13	0.045	(0.955)	0.040	0.004
28	2.33	0.13	0.045	(0.951)	0.040	0.004
29	2.42	0.13	0.045	(0.947)	0.040	0.004
30	2.50	0.13	0.045	(0.944)	0.040	0.004
31	2.58	0.17	0.056	(0.940)	0.050	0.006
32	2.67	0.17	0.056	(0.936)	0.050	0.006
33	2.75	0.17	0.056	(0.932)	0.050	0.006
34	2.83	0.17	0.056	(0.928)	0.050	0.006
35	2.92	0.17	0.056	(0.924)	0.050	0.006
36	3.00	0.17	0.056	(0.921)	0.050	0.006
37	3.08	0.17	0.056	(0.917)	0.050	0.006
38	3.17	0.17	0.056	(0.913)	0.050	0.006
39	3.25	0.17	0.056	(0.909)	0.050	0.006
40	3.33	0.17	0.056	(0.905)	0.050	0.006

41	3.42	0.17	0.056	(0.902)	0.050	0.006
42	3.50	0.17	0.056	(0.898)	0.050	0.006
43	3.58	0.17	0.056	(0.894)	0.050	0.006
44	3.67	0.17	0.056	(0.890)	0.050	0.006
45	3.75	0.17	0.056	(0.887)	0.050	0.006
46	3.83	0.20	0.067	(0.883)	0.060	0.007
47	3.92	0.20	0.067	(0.879)	0.060	0.007
48	4.00	0.20	0.067	(0.875)	0.060	0.007
49	4.08	0.20	0.067	(0.872)	0.060	0.007
50	4.17	0.20	0.067	(0.868)	0.060	0.007
51	4.25	0.20	0.067	(0.864)	0.060	0.007
52	4.33	0.23	0.078	(0.861)	0.071	0.008
53	4.42	0.23	0.078	(0.857)	0.071	0.008
54	4.50	0.23	0.078	(0.853)	0.071	0.008
55	4.58	0.23	0.078	(0.850)	0.071	0.008
56	4.67	0.23	0.078	(0.846)	0.071	0.008
57	4.75	0.23	0.078	(0.842)	0.071	0.008
58	4.83	0.27	0.090	(0.839)	0.081	0.009
59	4.92	0.27	0.090	(0.835)	0.081	0.009
60	5.00	0.27	0.090	(0.831)	0.081	0.009
61	5.08	0.20	0.067	(0.828)	0.060	0.007
62	5.17	0.20	0.067	(0.824)	0.060	0.007
63	5.25	0.20	0.067	(0.821)	0.060	0.007
64	5.33	0.23	0.078	(0.817)	0.071	0.008
65	5.42	0.23	0.078	(0.813)	0.071	0.008
66	5.50	0.23	0.078	(0.810)	0.071	0.008
67	5.58	0.27	0.090	(0.806)	0.081	0.009
68	5.67	0.27	0.090	(0.803)	0.081	0.009
69	5.75	0.27	0.090	(0.799)	0.081	0.009
70	5.83	0.27	0.090	(0.796)	0.081	0.009
71	5.92	0.27	0.090	(0.792)	0.081	0.009
72	6.00	0.27	0.090	(0.789)	0.081	0.009
73	6.08	0.30	0.101	(0.785)	0.091	0.010
74	6.17	0.30	0.101	(0.782)	0.091	0.010
75	6.25	0.30	0.101	(0.778)	0.091	0.010
76	6.33	0.30	0.101	(0.775)	0.091	0.010
77	6.42	0.30	0.101	(0.771)	0.091	0.010
78	6.50	0.30	0.101	(0.768)	0.091	0.010
79	6.58	0.33	0.112	(0.764)	0.101	0.011
80	6.67	0.33	0.112	(0.761)	0.101	0.011
81	6.75	0.33	0.112	(0.757)	0.101	0.011
82	6.83	0.33	0.112	(0.754)	0.101	0.011
83	6.92	0.33	0.112	(0.751)	0.101	0.011
84	7.00	0.33	0.112	(0.747)	0.101	0.011
85	7.08	0.33	0.112	(0.744)	0.101	0.011
86	7.17	0.33	0.112	(0.740)	0.101	0.011
87	7.25	0.33	0.112	(0.737)	0.101	0.011
88	7.33	0.37	0.123	(0.734)	0.111	0.012
89	7.42	0.37	0.123	(0.730)	0.111	0.012
90	7.50	0.37	0.123	(0.727)	0.111	0.012

91	7.58	0.40	0.134	(0.724)	0.121	0.013
92	7.67	0.40	0.134	(0.720)	0.121	0.013
93	7.75	0.40	0.134	(0.717)	0.121	0.013
94	7.83	0.43	0.146	(0.714)	0.131	0.015
95	7.92	0.43	0.146	(0.710)	0.131	0.015
96	8.00	0.43	0.146	(0.707)	0.131	0.015
97	8.08	0.50	0.168	(0.704)	0.151	0.017
98	8.17	0.50	0.168	(0.701)	0.151	0.017
99	8.25	0.50	0.168	(0.697)	0.151	0.017
100	8.33	0.50	0.168	(0.694)	0.151	0.017
101	8.42	0.50	0.168	(0.691)	0.151	0.017
102	8.50	0.50	0.168	(0.688)	0.151	0.017
103	8.58	0.53	0.179	(0.684)	0.161	0.018
104	8.67	0.53	0.179	(0.681)	0.161	0.018
105	8.75	0.53	0.179	(0.678)	0.161	0.018
106	8.83	0.57	0.190	(0.675)	0.171	0.019
107	8.92	0.57	0.190	(0.671)	0.171	0.019
108	9.00	0.57	0.190	(0.668)	0.171	0.019
109	9.08	0.63	0.213	(0.665)	0.191	0.021
110	9.17	0.63	0.213	(0.662)	0.191	0.021
111	9.25	0.63	0.213	(0.659)	0.191	0.021
112	9.33	0.67	0.224	(0.656)	0.202	0.022
113	9.42	0.67	0.224	(0.653)	0.202	0.022
114	9.50	0.67	0.224	(0.649)	0.202	0.022
115	9.58	0.70	0.235	(0.646)	0.212	0.024
116	9.67	0.70	0.235	(0.643)	0.212	0.024
117	9.75	0.70	0.235	(0.640)	0.212	0.024
118	9.83	0.73	0.246	(0.637)	0.222	0.025
119	9.92	0.73	0.246	(0.634)	0.222	0.025
120	10.00	0.73	0.246	(0.631)	0.222	0.025
121	10.08	0.50	0.168	(0.628)	0.151	0.017
122	10.17	0.50	0.168	(0.625)	0.151	0.017
123	10.25	0.50	0.168	(0.622)	0.151	0.017
124	10.33	0.50	0.168	(0.619)	0.151	0.017
125	10.42	0.50	0.168	(0.616)	0.151	0.017
126	10.50	0.50	0.168	(0.613)	0.151	0.017
127	10.58	0.67	0.224	(0.610)	0.202	0.022
128	10.67	0.67	0.224	(0.607)	0.202	0.022
129	10.75	0.67	0.224	(0.604)	0.202	0.022
130	10.83	0.67	0.224	(0.601)	0.202	0.022
131	10.92	0.67	0.224	(0.598)	0.202	0.022
132	11.00	0.67	0.224	(0.595)	0.202	0.022
133	11.08	0.63	0.213	(0.592)	0.191	0.021
134	11.17	0.63	0.213	(0.589)	0.191	0.021
135	11.25	0.63	0.213	(0.586)	0.191	0.021
136	11.33	0.63	0.213	(0.583)	0.191	0.021
137	11.42	0.63	0.213	(0.580)	0.191	0.021
138	11.50	0.63	0.213	(0.578)	0.191	0.021
139	11.58	0.57	0.190	(0.575)	0.171	0.019
140	11.67	0.57	0.190	(0.572)	0.171	0.019

141	11.75	0.57	0.190	(0.569)	0.171	0.019
142	11.83	0.60	0.202	(0.566)	0.181	0.020
143	11.92	0.60	0.202	(0.563)	0.181	0.020
144	12.00	0.60	0.202	(0.561)	0.181	0.020
145	12.08	0.83	0.280	(0.558)	0.252	0.028
146	12.17	0.83	0.280	(0.555)	0.252	0.028
147	12.25	0.83	0.280	(0.552)	0.252	0.028
148	12.33	0.87	0.291	(0.549)	0.262	0.029
149	12.42	0.87	0.291	(0.547)	0.262	0.029
150	12.50	0.87	0.291	(0.544)	0.262	0.029
151	12.58	0.93	0.314	(0.541)	0.282	0.031
152	12.67	0.93	0.314	(0.538)	0.282	0.031
153	12.75	0.93	0.314	(0.536)	0.282	0.031
154	12.83	0.97	0.325	(0.533)	0.292	0.032
155	12.92	0.97	0.325	(0.530)	0.292	0.032
156	13.00	0.97	0.325	(0.528)	0.292	0.032
157	13.08	1.13	0.381	(0.525)	0.343	0.038
158	13.17	1.13	0.381	(0.522)	0.343	0.038
159	13.25	1.13	0.381	(0.520)	0.343	0.038
160	13.33	1.13	0.381	(0.517)	0.343	0.038
161	13.42	1.13	0.381	(0.514)	0.343	0.038
162	13.50	1.13	0.381	(0.512)	0.343	0.038
163	13.58	0.77	0.258	(0.509)	0.232	0.026
164	13.67	0.77	0.258	(0.507)	0.232	0.026
165	13.75	0.77	0.258	(0.504)	0.232	0.026
166	13.83	0.77	0.258	(0.501)	0.232	0.026
167	13.92	0.77	0.258	(0.499)	0.232	0.026
168	14.00	0.77	0.258	(0.496)	0.232	0.026
169	14.08	0.90	0.302	(0.494)	0.272	0.030
170	14.17	0.90	0.302	(0.491)	0.272	0.030
171	14.25	0.90	0.302	(0.489)	0.272	0.030
172	14.33	0.87	0.291	(0.486)	0.262	0.029
173	14.42	0.87	0.291	(0.484)	0.262	0.029
174	14.50	0.87	0.291	(0.481)	0.262	0.029
175	14.58	0.87	0.291	(0.479)	0.262	0.029
176	14.67	0.87	0.291	(0.476)	0.262	0.029
177	14.75	0.87	0.291	(0.474)	0.262	0.029
178	14.83	0.83	0.280	(0.471)	0.252	0.028
179	14.92	0.83	0.280	(0.469)	0.252	0.028
180	15.00	0.83	0.280	(0.467)	0.252	0.028
181	15.08	0.80	0.269	(0.464)	0.242	0.027
182	15.17	0.80	0.269	(0.462)	0.242	0.027
183	15.25	0.80	0.269	(0.460)	0.242	0.027
184	15.33	0.77	0.258	(0.457)	0.232	0.026
185	15.42	0.77	0.258	(0.455)	0.232	0.026
186	15.50	0.77	0.258	(0.452)	0.232	0.026
187	15.58	0.63	0.213	(0.450)	0.191	0.021
188	15.67	0.63	0.213	(0.448)	0.191	0.021
189	15.75	0.63	0.213	(0.446)	0.191	0.021
190	15.83	0.63	0.213	(0.443)	0.191	0.021

191	15.92	0.63	0.213	(0.441)	0.191	0.021
192	16.00	0.63	0.213	(0.439)	0.191	0.021
193	16.08	0.13	0.045	(0.437)	0.040	0.004
194	16.17	0.13	0.045	(0.434)	0.040	0.004
195	16.25	0.13	0.045	(0.432)	0.040	0.004
196	16.33	0.13	0.045	(0.430)	0.040	0.004
197	16.42	0.13	0.045	(0.428)	0.040	0.004
198	16.50	0.13	0.045	(0.425)	0.040	0.004
199	16.58	0.10	0.034	(0.423)	0.030	0.003
200	16.67	0.10	0.034	(0.421)	0.030	0.003
201	16.75	0.10	0.034	(0.419)	0.030	0.003
202	16.83	0.10	0.034	(0.417)	0.030	0.003
203	16.92	0.10	0.034	(0.415)	0.030	0.003
204	17.00	0.10	0.034	(0.413)	0.030	0.003
205	17.08	0.17	0.056	(0.411)	0.050	0.006
206	17.17	0.17	0.056	(0.409)	0.050	0.006
207	17.25	0.17	0.056	(0.407)	0.050	0.006
208	17.33	0.17	0.056	(0.404)	0.050	0.006
209	17.42	0.17	0.056	(0.402)	0.050	0.006
210	17.50	0.17	0.056	(0.400)	0.050	0.006
211	17.58	0.17	0.056	(0.398)	0.050	0.006
212	17.67	0.17	0.056	(0.396)	0.050	0.006
213	17.75	0.17	0.056	(0.394)	0.050	0.006
214	17.83	0.13	0.045	(0.392)	0.040	0.004
215	17.92	0.13	0.045	(0.391)	0.040	0.004
216	18.00	0.13	0.045	(0.389)	0.040	0.004
217	18.08	0.13	0.045	(0.387)	0.040	0.004
218	18.17	0.13	0.045	(0.385)	0.040	0.004
219	18.25	0.13	0.045	(0.383)	0.040	0.004
220	18.33	0.13	0.045	(0.381)	0.040	0.004
221	18.42	0.13	0.045	(0.379)	0.040	0.004
222	18.50	0.13	0.045	(0.377)	0.040	0.004
223	18.58	0.10	0.034	(0.376)	0.030	0.003
224	18.67	0.10	0.034	(0.374)	0.030	0.003
225	18.75	0.10	0.034	(0.372)	0.030	0.003
226	18.83	0.07	0.022	(0.370)	0.020	0.002
227	18.92	0.07	0.022	(0.368)	0.020	0.002
228	19.00	0.07	0.022	(0.367)	0.020	0.002
229	19.08	0.10	0.034	(0.365)	0.030	0.003
230	19.17	0.10	0.034	(0.363)	0.030	0.003
231	19.25	0.10	0.034	(0.361)	0.030	0.003
232	19.33	0.13	0.045	(0.360)	0.040	0.004
233	19.42	0.13	0.045	(0.358)	0.040	0.004
234	19.50	0.13	0.045	(0.356)	0.040	0.004
235	19.58	0.10	0.034	(0.355)	0.030	0.003
236	19.67	0.10	0.034	(0.353)	0.030	0.003
237	19.75	0.10	0.034	(0.352)	0.030	0.003
238	19.83	0.07	0.022	(0.350)	0.020	0.002
239	19.92	0.07	0.022	(0.348)	0.020	0.002
240	20.00	0.07	0.022	(0.347)	0.020	0.002

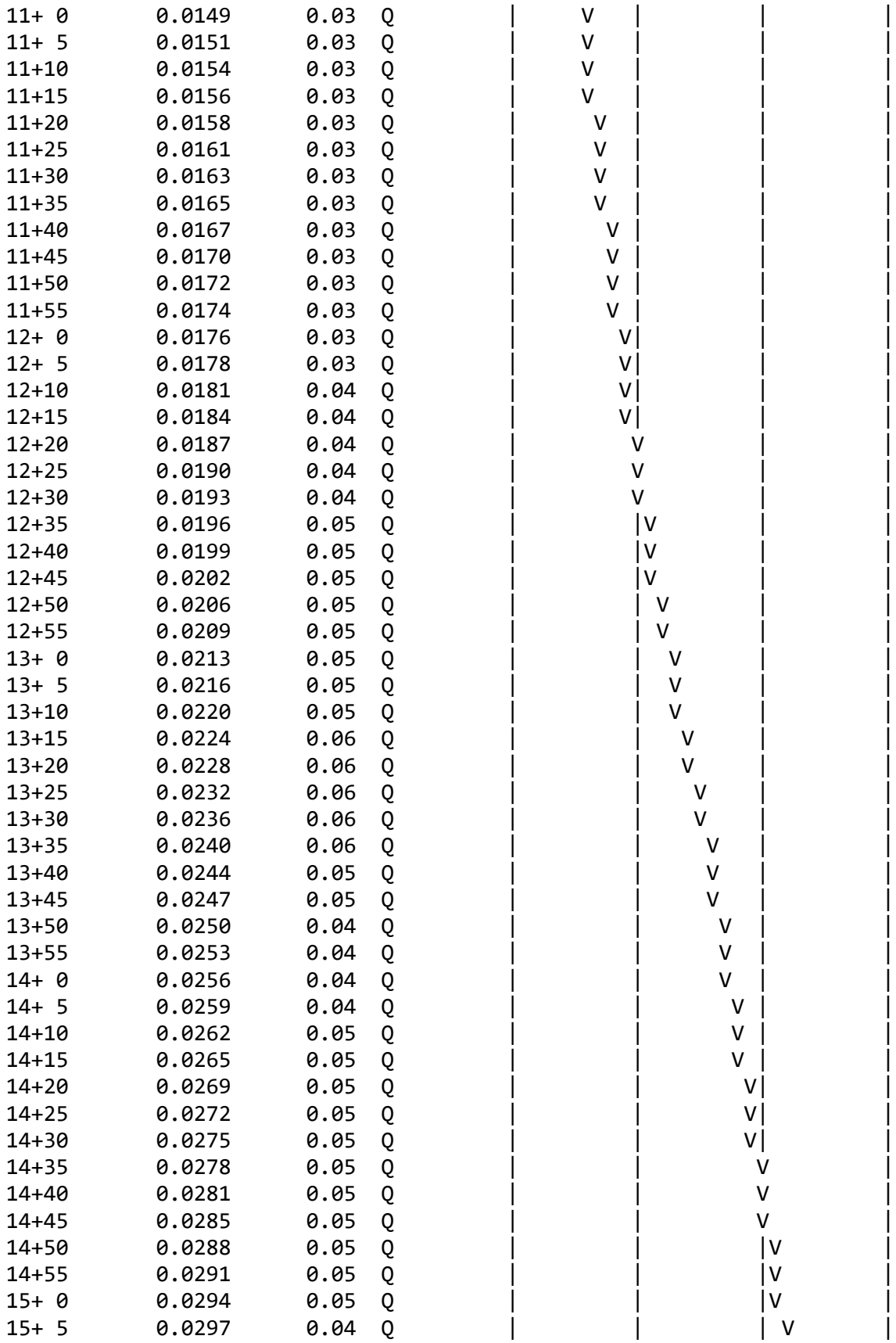
241	20.08	0.10	0.034	(0.345)	0.030	0.003
242	20.17	0.10	0.034	(0.344)	0.030	0.003
243	20.25	0.10	0.034	(0.342)	0.030	0.003
244	20.33	0.10	0.034	(0.341)	0.030	0.003
245	20.42	0.10	0.034	(0.339)	0.030	0.003
246	20.50	0.10	0.034	(0.338)	0.030	0.003
247	20.58	0.10	0.034	(0.337)	0.030	0.003
248	20.67	0.10	0.034	(0.335)	0.030	0.003
249	20.75	0.10	0.034	(0.334)	0.030	0.003
250	20.83	0.07	0.022	(0.332)	0.020	0.002
251	20.92	0.07	0.022	(0.331)	0.020	0.002
252	21.00	0.07	0.022	(0.330)	0.020	0.002
253	21.08	0.10	0.034	(0.328)	0.030	0.003
254	21.17	0.10	0.034	(0.327)	0.030	0.003
255	21.25	0.10	0.034	(0.326)	0.030	0.003
256	21.33	0.07	0.022	(0.325)	0.020	0.002
257	21.42	0.07	0.022	(0.323)	0.020	0.002
258	21.50	0.07	0.022	(0.322)	0.020	0.002
259	21.58	0.10	0.034	(0.321)	0.030	0.003
260	21.67	0.10	0.034	(0.320)	0.030	0.003
261	21.75	0.10	0.034	(0.319)	0.030	0.003
262	21.83	0.07	0.022	(0.318)	0.020	0.002
263	21.92	0.07	0.022	(0.317)	0.020	0.002
264	22.00	0.07	0.022	(0.315)	0.020	0.002
265	22.08	0.10	0.034	(0.314)	0.030	0.003
266	22.17	0.10	0.034	(0.313)	0.030	0.003
267	22.25	0.10	0.034	(0.312)	0.030	0.003
268	22.33	0.07	0.022	(0.311)	0.020	0.002
269	22.42	0.07	0.022	(0.310)	0.020	0.002
270	22.50	0.07	0.022	(0.310)	0.020	0.002
271	22.58	0.07	0.022	(0.309)	0.020	0.002
272	22.67	0.07	0.022	(0.308)	0.020	0.002
273	22.75	0.07	0.022	(0.307)	0.020	0.002
274	22.83	0.07	0.022	(0.306)	0.020	0.002
275	22.92	0.07	0.022	(0.305)	0.020	0.002
276	23.00	0.07	0.022	(0.305)	0.020	0.002
277	23.08	0.07	0.022	(0.304)	0.020	0.002
278	23.17	0.07	0.022	(0.303)	0.020	0.002
279	23.25	0.07	0.022	(0.303)	0.020	0.002
280	23.33	0.07	0.022	(0.302)	0.020	0.002
281	23.42	0.07	0.022	(0.301)	0.020	0.002
282	23.50	0.07	0.022	(0.301)	0.020	0.002
283	23.58	0.07	0.022	(0.300)	0.020	0.002
284	23.67	0.07	0.022	(0.300)	0.020	0.002
285	23.75	0.07	0.022	(0.300)	0.020	0.002
286	23.83	0.07	0.022	(0.299)	0.020	0.002
287	23.92	0.07	0.022	(0.299)	0.020	0.002
288	24.00	0.07	0.022	(0.299)	0.020	0.002
		(Loss Rate Not Used)				
	Sum =	100.0			Sum =	3.4

```
      Flood volume = Effective rainfall      0.28(In)
       times area       1.6(Ac.)/[(In)/(Ft.)] =       0.0(Ac.Ft)
      Total soil loss =      2.52(In)
      Total soil loss =     0.332(Ac.Ft)
      Total rainfall =      2.80(In)
      Flood volume =        1605.6 Cubic Feet
      Total soil loss =       14450.7 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.060(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0000      0.00  Q         |         |         |         |
  0+10       0.0000      0.00  Q         |         |         |         |
  0+15       0.0000      0.00  Q         |         |         |         |
  0+20       0.0000      0.00  Q         |         |         |         |
  0+25       0.0001      0.00  Q         |         |         |         |
  0+30       0.0001      0.00  Q         |         |         |         |
  0+35       0.0001      0.00  Q         |         |         |         |
  0+40       0.0002      0.00  Q         |         |         |         |
  0+45       0.0002      0.01  Q         |         |         |         |
  0+50       0.0002      0.01  Q         |         |         |         |
  0+55       0.0003      0.01  Q         |         |         |         |
  1+ 0       0.0003      0.01  Q         |         |         |         |
  1+ 5       0.0004      0.01  Q         |         |         |         |
  1+10       0.0004      0.01  Q         |         |         |         |
  1+15       0.0005      0.01  Q         |         |         |         |
  1+20       0.0005      0.01  Q         |         |         |         |
  1+25       0.0005      0.01  Q         |         |         |         |
  1+30       0.0006      0.01  Q         |         |         |         |
  1+35       0.0006      0.01  Q         |         |         |         |
  1+40       0.0006      0.01  Q         |         |         |         |
  1+45       0.0007      0.01  Q         |         |         |         |
  1+50       0.0007      0.01  Q         |         |         |         |
  1+55       0.0008      0.01  Q         |         |         |         |
  2+ 0       0.0008      0.01  Q         |         |         |         |
  2+ 5       0.0009      0.01  Q         |         |         |         |
  2+10       0.0009      0.01  Q         |         |         |         |
  2+15       0.0009      0.01  QV        |         |         |         |
  2+20       0.0010      0.01  QV        |         |         |         |
  2+25       0.0010      0.01  QV        |         |         |         |
  2+30       0.0011      0.01  QV        |         |         |         |
  2+35       0.0011      0.01  QV        |         |         |         |
```

```
2+40       0.0012      0.01  QV        |          |          |          |
2+45       0.0013      0.01  QV        |          |          |          |
2+50       0.0013      0.01  QV        |          |          |          |
2+55       0.0014      0.01  QV        |          |          |          |
3+ 0       0.0014      0.01  QV        |          |          |          |
3+ 5       0.0015      0.01  QV        |          |          |          |
3+10       0.0016      0.01  QV        |          |          |          |
3+15       0.0016      0.01  QV        |          |          |          |
3+20       0.0017      0.01  QV        |          |          |          |
3+25       0.0017      0.01  QV        |          |          |          |
3+30       0.0018      0.01  QV        |          |          |          |
3+35       0.0019      0.01  Q V       |          |          |          |
3+40       0.0019      0.01  Q V       |          |          |          |
3+45       0.0020      0.01  Q V       |          |          |          |
3+50       0.0020      0.01  Q V       |          |          |          |
3+55       0.0021      0.01  Q V       |          |          |          |
4+ 0       0.0022      0.01  Q V       |          |          |          |
4+ 5       0.0023      0.01  Q V       |          |          |          |
4+10       0.0023      0.01  Q V       |          |          |          |
4+15       0.0024      0.01  Q V       |          |          |          |
4+20       0.0025      0.01  Q V       |          |          |          |
4+25       0.0025      0.01  Q V       |          |          |          |
4+30       0.0026      0.01  Q V       |          |          |          |
4+35       0.0027      0.01  Q V       |          |          |          |
4+40       0.0028      0.01  Q  V      |          |          |          |
4+45       0.0029      0.01  Q  V      |          |          |          |
4+50       0.0030      0.01  Q  V      |          |          |          |
4+55       0.0031      0.01  Q  V      |          |          |          |
5+ 0       0.0032      0.01  Q  V      |          |          |          |
5+ 5       0.0032      0.01  Q  V      |          |          |          |
5+10       0.0033      0.01  Q  V      |          |          |          |
5+15       0.0034      0.01  Q  V      |          |          |          |
5+20       0.0035      0.01  Q  V      |          |          |          |
5+25       0.0036      0.01  Q  V      |          |          |          |
5+30       0.0037      0.01  Q  V      |          |          |          |
5+35       0.0037      0.01  Q   V     |          |          |          |
5+40       0.0038      0.01  Q   V     |          |          |          |
5+45       0.0039      0.01  Q   V     |          |          |          |
5+50       0.0040      0.01  Q   V     |          |          |          |
5+55       0.0041      0.01  Q   V     |          |          |          |
6+ 0       0.0042      0.01  Q   V     |          |          |          |
6+ 5       0.0043      0.01  Q   V     |          |          |          |
6+10       0.0044      0.01  Q   V     |          |          |          |
6+15       0.0045      0.02  Q   V     |          |          |          |
6+20       0.0046      0.02  Q    V    |          |          |          |
6+25       0.0047      0.02  Q    V    |          |          |          |
6+30       0.0048      0.02  Q    V    |          |          |          |
6+35       0.0050      0.02  Q    V    |          |          |          |
6+40       0.0051      0.02  Q    V    |          |          |          |
6+45       0.0052      0.02  Q    V    |          |          |          |
```

```
 6+50       0.0053      0.02  Q    V    |          |          |          |
 6+55       0.0054      0.02  Q    V    |          |          |          |
 7+ 0       0.0056      0.02  Q     V   |          |          |          |
 7+ 5       0.0057      0.02  Q     V   |          |          |          |
 7+10       0.0058      0.02  Q     V   |          |          |          |
 7+15       0.0059      0.02  Q     V   |          |          |          |
 7+20       0.0060      0.02  Q     V   |          |          |          |
 7+25       0.0062      0.02  Q     V   |          |          |          |
 7+30       0.0063      0.02  Q     V   |          |          |          |
 7+35       0.0064      0.02  Q     V   |          |          |          |
 7+40       0.0066      0.02  Q      V  |          |          |          |
 7+45       0.0067      0.02  Q      V  |          |          |          |
 7+50       0.0069      0.02  Q      V  |          |          |          |
 7+55       0.0070      0.02  Q      V  |          |          |          |
 8+ 0       0.0072      0.02  Q      V  |          |          |          |
 8+ 5       0.0073      0.02  Q      V  |          |          |          |
 8+10       0.0075      0.02  Q       V |          |          |          |
 8+15       0.0077      0.03  Q       V |          |          |          |
 8+20       0.0078      0.03  Q       V |          |          |          |
 8+25       0.0080      0.03  Q       V |          |          |          |
 8+30       0.0082      0.03  Q       V |          |          |          |
 8+35       0.0084      0.03  Q        V|          |          |          |
 8+40       0.0086      0.03  Q        V|          |          |          |
 8+45       0.0088      0.03  Q        V|          |          |          |
 8+50       0.0090      0.03  Q        V|          |          |          |
 8+55       0.0092      0.03  Q        V|          |          |          |
 9+ 0       0.0094      0.03  Q         V          |          |          |
 9+ 5       0.0096      0.03  Q         V          |          |          |
 9+10       0.0098      0.03  Q         V          |          |          |
 9+15       0.0100      0.03  Q         V          |          |          |
 9+20       0.0102      0.03  Q         |V         |          |          |
 9+25       0.0105      0.03  Q         |V         |          |          |
 9+30       0.0107      0.03  Q         |V         |          |          |
 9+35       0.0110      0.04  Q         |V         |          |          |
 9+40       0.0112      0.04  Q         | V        |          |          |
 9+45       0.0115      0.04  Q         | V        |          |          |
 9+50       0.0117      0.04  Q         | V        |          |          |
 9+55       0.0120      0.04  Q         | V        |          |          |
10+ 0       0.0122      0.04  Q         |  V       |          |          |
10+ 5       0.0125      0.04  Q         |  V       |          |          |
10+10       0.0127      0.03  Q         |  V       |          |          |
10+15       0.0129      0.03  Q         |   V      |          |          |
10+20       0.0131      0.03  Q         |   V      |          |          |
10+25       0.0133      0.03  Q         |   V      |          |          |
10+30       0.0135      0.03  Q         |   V      |          |          |
10+35       0.0137      0.03  Q         |   V      |          |          |
10+40       0.0139      0.03  Q         |    V     |          |          |
10+45       0.0142      0.03  Q         |    V     |          |          |
10+50       0.0144      0.03  Q         |    V     |          |          |
10+55       0.0146      0.03  Q         |    V     |          |          |
```



```
15+10       0.0300      0.04  Q        |          |          | V        |
15+15       0.0303      0.04  Q        |          |          | V        |
15+20       0.0306      0.04  Q        |          |          |  V       |
15+25       0.0309      0.04  Q        |          |          |  V       |
15+30       0.0312      0.04  Q        |          |          |  V       |
15+35       0.0315      0.04  Q        |          |          |   V      |
15+40       0.0317      0.04  Q        |          |          |   V      |
15+45       0.0320      0.04  Q        |          |          |   V      |
15+50       0.0322      0.04  Q        |          |          |   V      |
15+55       0.0325      0.04  Q        |          |          |    V     |
16+ 0       0.0327      0.03  Q        |          |          |    V     |
16+ 5       0.0329      0.03  Q        |          |          |    V     |
16+10       0.0331      0.02  Q        |          |          |    V     |
16+15       0.0332      0.02  Q        |          |          |     V    |
16+20       0.0333      0.01  Q        |          |          |     V    |
16+25       0.0334      0.01  Q        |          |          |     V    |
16+30       0.0334      0.01  Q        |          |          |     V    |
16+35       0.0335      0.01  Q        |          |          |     V    |
16+40       0.0336      0.01  Q        |          |          |     V    |
16+45       0.0336      0.01  Q        |          |          |     V    |
16+50       0.0337      0.01  Q        |          |          |     V    |
16+55       0.0337      0.01  Q        |          |          |     V    |
17+ 0       0.0337      0.01  Q        |          |          |     V    |
17+ 5       0.0338      0.01  Q        |          |          |     V    |
17+10       0.0338      0.01  Q        |          |          |     V    |
17+15       0.0339      0.01  Q        |          |          |     V    |
17+20       0.0339      0.01  Q        |          |          |     V    |
17+25       0.0340      0.01  Q        |          |          |     V    |
17+30       0.0341      0.01  Q        |          |          |     V    |
17+35       0.0341      0.01  Q        |          |          |      V   |
17+40       0.0342      0.01  Q        |          |          |      V   |
17+45       0.0342      0.01  Q        |          |          |      V   |
17+50       0.0343      0.01  Q        |          |          |      V   |
17+55       0.0344      0.01  Q        |          |          |      V   |
18+ 0       0.0344      0.01  Q        |          |          |      V   |
18+ 5       0.0345      0.01  Q        |          |          |      V   |
18+10       0.0345      0.01  Q        |          |          |      V   |
18+15       0.0346      0.01  Q        |          |          |      V   |
18+20       0.0346      0.01  Q        |          |          |      V   |
18+25       0.0347      0.01  Q        |          |          |      V   |
18+30       0.0347      0.01  Q        |          |          |      V   |
18+35       0.0348      0.01  Q        |          |          |      V   |
18+40       0.0348      0.01  Q        |          |          |      V   |
18+45       0.0348      0.01  Q        |          |          |      V   |
18+50       0.0349      0.01  Q        |          |          |      V   |
18+55       0.0349      0.00  Q        |          |          |      V   |
19+ 0       0.0349      0.00  Q        |          |          |      V   |
19+ 5       0.0350      0.00  Q        |          |          |      V   |
19+10       0.0350      0.00  Q        |          |          |      V   |
19+15       0.0350      0.01  Q        |          |          |       V  |
```

```
19+20       0.0351      0.01  Q         |         |         |        V |
19+25       0.0351      0.01  Q         |         |         |        V |
19+30       0.0352      0.01  Q         |         |         |        V |
19+35       0.0352      0.01  Q         |         |         |        V |
19+40       0.0352      0.01  Q         |         |         |        V |
19+45       0.0353      0.01  Q         |         |         |        V |
19+50       0.0353      0.01  Q         |         |         |        V |
19+55       0.0354      0.00  Q         |         |         |        V |
20+ 0       0.0354      0.00  Q         |         |         |        V |
20+ 5       0.0354      0.00  Q         |         |         |        V |
20+10       0.0354      0.00  Q         |         |         |        V |
20+15       0.0355      0.01  Q         |         |         |        V |
20+20       0.0355      0.01  Q         |         |         |        V |
20+25       0.0356      0.01  Q         |         |         |        V |
20+30       0.0356      0.01  Q         |         |         |        V |
20+35       0.0356      0.01  Q         |         |         |        V |
20+40       0.0357      0.01  Q         |         |         |        V |
20+45       0.0357      0.01  Q         |         |         |        V |
20+50       0.0357      0.01  Q         |         |         |        V |
20+55       0.0358      0.00  Q         |         |         |        V |
21+ 0       0.0358      0.00  Q         |         |         |        V |
21+ 5       0.0358      0.00  Q         |         |         |        V |
21+10       0.0359      0.00  Q         |         |         |        V |
21+15       0.0359      0.00  Q         |         |         |        V |
21+20       0.0359      0.00  Q         |         |         |        V |
21+25       0.0360      0.00  Q         |         |         |         V|
21+30       0.0360      0.00  Q         |         |         |         V|
21+35       0.0360      0.00  Q         |         |         |         V|
21+40       0.0360      0.00  Q         |         |         |         V|
21+45       0.0361      0.00  Q         |         |         |         V|
21+50       0.0361      0.00  Q         |         |         |         V|
21+55       0.0361      0.00  Q         |         |         |         V|
22+ 0       0.0362      0.00  Q         |         |         |         V|
22+ 5       0.0362      0.00  Q         |         |         |         V|
22+10       0.0362      0.00  Q         |         |         |         V|
22+15       0.0363      0.00  Q         |         |         |         V|
22+20       0.0363      0.00  Q         |         |         |         V|
22+25       0.0363      0.00  Q         |         |         |         V|
22+30       0.0363      0.00  Q         |         |         |         V|
22+35       0.0364      0.00  Q         |         |         |         V|
22+40       0.0364      0.00  Q         |         |         |         V|
22+45       0.0364      0.00  Q         |         |         |         V|
22+50       0.0365      0.00  Q         |         |         |         V|
22+55       0.0365      0.00  Q         |         |         |         V|
23+ 0       0.0365      0.00  Q         |         |         |         V|
23+ 5       0.0365      0.00  Q         |         |         |         V|
23+10       0.0366      0.00  Q         |         |         |         V|
23+15       0.0366      0.00  Q         |         |         |         V|
23+20       0.0366      0.00  Q         |         |         |         V|
23+25       0.0366      0.00  Q         |         |         |         V|
```

```
   23+30       0.0367      0.00  Q          |          |          |         V|
   23+35       0.0367      0.00  Q          |          |          |         V|
   23+40       0.0367      0.00  Q          |          |          |         V|
   23+45       0.0367      0.00  Q          |          |          |         V|
   23+50       0.0367      0.00  Q          |          |          |         V|
   23+55       0.0368      0.00  Q          |          |          |         V|
   24+ 0       0.0368      0.00  Q          |          |          |         V|
   24+ 5       0.0368      0.00  Q          |          |          |         V|
   24+10       0.0368      0.00  Q          |          |          |         V|
   24+15       0.0368      0.00  Q          |          |          |         V|
   24+20       0.0368      0.00  Q          |          |          |         V|
   24+25       0.0369      0.00  Q          |          |          |         V|
   24+30       0.0369      0.00  Q          |          |          |         V|
   24+35       0.0369      0.00  Q          |          |          |         V|
   24+40       0.0369      0.00  Q          |          |          |         V|
   24+45       0.0369      0.00  Q          |          |          |         V|
   24+50       0.0369      0.00  Q          |          |          |         V|
   24+55       0.0369      0.00  Q          |          |          |         V|
   25+ 0       0.0369      0.00  Q          |          |          |         V|
   25+ 5       0.0369      0.00  Q          |          |          |          V
-------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/06/22 File: Iris110.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
10 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.49	0.78

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            1.35                    2.13

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    0.493(In)
Area Averaged 100-Year Rainfall =    1.350(In)

Point rain (area averaged) =    0.846(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    0.846(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           67.00          0.000
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
67.0  67.0      0.394     0.000        0.394       1.000      0.394
                                                 Sum (F) =   0.394
Area averaged mean soil loss (F) (In/Hr) =  0.394
Minimum soil loss rate ((In/Hr)) =  0.197
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5000
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------
    1   0.083         59.952          8.204              0.131
    2   0.167        119.904         33.934              0.540
    3   0.250        179.856         26.599              0.424
    4   0.333        239.808         10.311              0.164
    5   0.417        299.760          6.100              0.097
    6   0.500        359.712          4.123              0.066
    7   0.583        419.664          2.936              0.047
    8   0.667        479.616          2.066              0.033
    9   0.750        539.568          1.709              0.027
   10   0.833        599.520          1.265              0.020
   11   0.917        659.472          0.962              0.015
```

12	1.000	719.424	0.685	0.011
13	1.083	779.376	0.600	0.010
14	1.167	839.329	0.506	0.008
			Sum = 100.000 Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.20	0.426	(0.394)	0.384	0.043
2	0.17	4.30	0.436	(0.394)	0.393	0.044
3	0.25	5.00	0.507	0.394	(0.457)	0.113
4	0.33	5.00	0.507	0.394	(0.457)	0.113
5	0.42	5.80	0.589	0.394	(0.530)	0.194
6	0.50	6.50	0.660	0.394	(0.594)	0.265
7	0.58	7.40	0.751	0.394	(0.676)	0.356
8	0.67	8.60	0.873	0.394	(0.785)	0.478
9	0.75	12.30	1.248	0.394	(1.123)	0.854
10	0.83	29.10	2.953	0.394	(2.657)	2.558
11	0.92	6.80	0.690	0.394	(0.621)	0.296
12	1.00	5.00	0.507	0.394	(0.457)	0.113
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.4

Flood volume = Effective rainfall 0.45(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.1(Ac.Ft)
Total soil loss = 0.39(In)
Total soil loss = 0.052(Ac.Ft)
Total rainfall = 0.85(In)
Flood volume = 2593.6 Cubic Feet
Total soil loss = 2256.0 Cubic Feet

Peak flow rate of this hydrograph = 1.931(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.01 Q	|	|	|	|	
0+10	0.0002	0.03 Q	|	|	|	|	
0+15	0.0006	0.06 Q	|	|	|	|	
0+20	0.0013	0.10 Q	|	|	|	|	
0+25	0.0023	0.15 QV	|	|	|	|	

```
    0+30       0.0038      0.21  Q V       |          |          |          |
    0+35       0.0059      0.31  |Q V      |          |          |          |
    0+40       0.0088      0.42  |Q   V    |          |          |          |
    0+45       0.0129      0.60  | Q     V |          |          |          |
    0+50       0.0206      1.11  |   Q     |  V       |          |          |
    0+55       0.0339      1.93  |      Q  |          | V        |          |
    1+ 0       0.0441      1.49  |    Q    |          |        V |          |
    1+ 5       0.0494      0.76  |  Q      |          |          |  V       |
    1+10       0.0525      0.45  |Q        |          |          |    V     |
    1+15       0.0545      0.29  |Q        |          |          |     V    |
    1+20       0.0559      0.21  Q         |          |          |      V   |
    1+25       0.0569      0.15  Q         |          |          |       V  |
    1+30       0.0577      0.12  Q         |          |          |       V  |
    1+35       0.0583      0.09  Q         |          |          |        V |
    1+40       0.0588      0.06  Q         |          |          |        V |
    1+45       0.0591      0.05  Q         |          |          |        V |
    1+50       0.0593      0.04  Q         |          |          |        V |
    1+55       0.0595      0.02  Q         |          |          |        V |
    2+ 0       0.0595      0.00  Q         |          |          |        V |
    2+ 5       0.0595      0.00  Q         |          |          |        V |
---------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/06/22 File: Iris310.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
10 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.87	1.37

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.10	3.32

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.869(In)
Area Averaged 100-Year Rainfall = 2.100(In)

Point rain (area averaged) = 1.375(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.375(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.580	67.00	0.000

Total Area Entered = 1.58(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
67.0	67.0	0.394	0.000	0.394	1.000	0.394
					Sum (F) =	0.394

Area averaged mean soil loss (F) (In/Hr) = 0.394
Minimum soil loss rate ((In/Hr)) = 0.197
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	59.952	8.204	0.131
2	0.167	119.904	33.934	0.540
3	0.250	179.856	26.599	0.424
4	0.333	239.808	10.311	0.164
5	0.417	299.760	6.100	0.097
6	0.500	359.712	4.123	0.066
7	0.583	419.664	2.936	0.047
8	0.667	479.616	2.066	0.033
9	0.750	539.568	1.709	0.027
10	0.833	599.520	1.265	0.020
11	0.917	659.472	0.962	0.015
12	1.000	719.424	0.685	0.011
13	1.083	779.376	0.600	0.010

14	1.167	839.329	0.506		0.008
			Sum = 100.000	Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.215	(0.394)	0.193	0.021
2	0.17	1.30	0.215	(0.394)	0.193	0.021
3	0.25	1.10	0.182	(0.394)	0.163	0.018
4	0.33	1.50	0.248	(0.394)	0.223	0.025
5	0.42	1.50	0.248	(0.394)	0.223	0.025
6	0.50	1.80	0.297	(0.394)	0.267	0.030
7	0.58	1.50	0.248	(0.394)	0.223	0.025
8	0.67	1.80	0.297	(0.394)	0.267	0.030
9	0.75	1.80	0.297	(0.394)	0.267	0.030
10	0.83	1.50	0.248	(0.394)	0.223	0.025
11	0.92	1.60	0.264	(0.394)	0.238	0.026
12	1.00	1.80	0.297	(0.394)	0.267	0.030
13	1.08	2.20	0.363	(0.394)	0.327	0.036
14	1.17	2.20	0.363	(0.394)	0.327	0.036
15	1.25	2.20	0.363	(0.394)	0.327	0.036
16	1.33	2.00	0.330	(0.394)	0.297	0.033
17	1.42	2.60	0.429	(0.394)	0.386	0.043
18	1.50	2.70	0.446	0.394	(0.401)	0.051
19	1.58	2.40	0.396	(0.394)	0.357	0.040
20	1.67	2.70	0.446	0.394	(0.401)	0.051
21	1.75	3.30	0.545	0.394	(0.490)	0.150
22	1.83	3.10	0.512	0.394	(0.460)	0.117
23	1.92	2.90	0.479	0.394	(0.431)	0.084
24	2.00	3.00	0.495	0.394	(0.446)	0.101
25	2.08	3.10	0.512	0.394	(0.460)	0.117
26	2.17	4.20	0.693	0.394	(0.624)	0.299
27	2.25	5.00	0.825	0.394	(0.743)	0.431
28	2.33	3.50	0.578	0.394	(0.520)	0.183
29	2.42	6.80	1.122	0.394	(1.010)	0.728
30	2.50	7.30	1.205	0.394	(1.084)	0.810
31	2.58	8.20	1.353	0.394	(1.218)	0.959
32	2.67	5.90	0.974	0.394	(0.876)	0.579
33	2.75	2.00	0.330	(0.394)	0.297	0.033
34	2.83	1.80	0.297	(0.394)	0.267	0.030
35	2.92	1.80	0.297	(0.394)	0.267	0.030
36	3.00	0.60	0.099	(0.394)	0.089	0.010
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.3

Flood volume = Effective rainfall 0.44(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.1(Ac.Ft)

```
      Total soil loss =      0.93(In)
      Total soil loss =     0.123(Ac.Ft)
      Total rainfall =      1.38(In)
      Flood volume =        2530.4 Cubic Feet
      Total soil loss =        5358.3 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      1.130(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          3 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0000      0.00  Q         |         |         |         |
  0+10       0.0001      0.01  Q         |         |         |         |
  0+15       0.0003      0.02  Q         |         |         |         |
  0+20       0.0005      0.03  Q         |         |         |         |
  0+25       0.0007      0.03  Q         |         |         |         |
  0+30       0.0009      0.03  Q         |         |         |         |
  0+35       0.0012      0.04  Q         |         |         |         |
  0+40       0.0014      0.04  Q         |         |         |         |
  0+45       0.0017      0.04  QV        |         |         |         |
  0+50       0.0020      0.04  QV        |         |         |         |
  0+55       0.0023      0.04  QV        |         |         |         |
  1+ 0       0.0026      0.04  QV        |         |         |         |
  1+ 5       0.0029      0.04  QV        |         |         |         |
  1+10       0.0032      0.05  Q V       |         |         |         |
  1+15       0.0036      0.05  Q V       |         |         |         |
  1+20       0.0040      0.05  Q V       |         |         |         |
  1+25       0.0044      0.05  Q  V      |         |         |         |
  1+30       0.0048      0.06  Q  V      |         |         |         |
  1+35       0.0052      0.07  Q  V      |         |         |         |
  1+40       0.0057      0.07  Q  V      |         |         |         |
  1+45       0.0063      0.08  Q   V     |         |         |         |
  1+50       0.0072      0.14  Q   V     |         |         |         |
  1+55       0.0083      0.16  Q    V    |         |         |         |
  2+ 0       0.0094      0.15  Q     V   |         |         |         |
  2+ 5       0.0104      0.15  Q      V  |         |         |         |
  2+10       0.0117      0.19  Q       V |         |         |         |
  2+15       0.0138      0.31  |Q       V|         |         |         |
  2+20       0.0168      0.43  |Q        |V        |         |         |
  2+25       0.0200      0.46  |Q        |  V      |         |         |
  2+30       0.0248      0.70  | Q       |      V  |         |         |
  2+35       0.0316      0.98  |  Q      |         |V        |         |
  2+40       0.0393      1.13  |   Q     |         |      V  |         |
  2+45       0.0461      0.98  |  Q      |         |         |V        |
```

```
    2+50       0.0501      0.59  | Q       |         |         |   V     |
    2+55       0.0525      0.34  |Q        |         |         |     V   |
    3+ 0       0.0541      0.24  Q         |         |         |      V  |
    3+ 5       0.0553      0.17  Q         |         |         |       V |
    3+10       0.0561      0.12  Q         |         |         |       V |
    3+15       0.0567      0.09  Q         |         |         |        V|
    3+20       0.0572      0.07  Q         |         |         |        V|
    3+25       0.0575      0.05  Q         |         |         |        V|
    3+30       0.0578      0.04  Q         |         |         |        V|
    3+35       0.0579      0.02  Q         |         |         |        V|
    3+40       0.0580      0.01  Q         |         |         |        V|
    3+45       0.0581      0.01  Q         |         |         |        V|
    3+50       0.0581      0.00  Q         |         |         |        V|
    3+55       0.0581      0.00  Q         |         |         |        V|
    4+ 0       0.0581      0.00  Q         |         |         |        V|
    4+ 5       0.0581      0.00  Q         |         |         |         V
---------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/06/22 File: Iris610.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
10 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	1.22	1.93

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            2.87                   4.53

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    1.220(In)
Area Averaged 100-Year Rainfall =    2.870(In)

Point rain (area averaged) =    1.899(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    1.899(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           67.00          0.000
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
67.0  67.0      0.394     0.000        0.394       1.000      0.394
                                                 Sum (F) =   0.394
Area averaged mean soil loss (F) (In/Hr) =  0.394
Minimum soil loss rate ((In/Hr)) =  0.197
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         59.952          8.204              0.131
    2   0.167        119.904         33.934              0.540
    3   0.250        179.856         26.599              0.424
    4   0.333        239.808         10.311              0.164
    5   0.417        299.760          6.100              0.097
    6   0.500        359.712          4.123              0.066
    7   0.583        419.664          2.936              0.047
    8   0.667        479.616          2.066              0.033
    9   0.750        539.568          1.709              0.027
   10   0.833        599.520          1.265              0.020
   11   0.917        659.472          0.962              0.015
   12   1.000        719.424          0.685              0.011
   13   1.083        779.376          0.600              0.010
```

	14	1.167	839.329	0.506		0.008
				Sum = 100.000	Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.114	(0.394)	0.103	0.011
2	0.17	0.60	0.137	(0.394)	0.123	0.014
3	0.25	0.60	0.137	(0.394)	0.123	0.014
4	0.33	0.60	0.137	(0.394)	0.123	0.014
5	0.42	0.60	0.137	(0.394)	0.123	0.014
6	0.50	0.70	0.160	(0.394)	0.144	0.016
7	0.58	0.70	0.160	(0.394)	0.144	0.016
8	0.67	0.70	0.160	(0.394)	0.144	0.016
9	0.75	0.70	0.160	(0.394)	0.144	0.016
10	0.83	0.70	0.160	(0.394)	0.144	0.016
11	0.92	0.70	0.160	(0.394)	0.144	0.016
12	1.00	0.80	0.182	(0.394)	0.164	0.018
13	1.08	0.80	0.182	(0.394)	0.164	0.018
14	1.17	0.80	0.182	(0.394)	0.164	0.018
15	1.25	0.80	0.182	(0.394)	0.164	0.018
16	1.33	0.80	0.182	(0.394)	0.164	0.018
17	1.42	0.80	0.182	(0.394)	0.164	0.018
18	1.50	0.80	0.182	(0.394)	0.164	0.018
19	1.58	0.80	0.182	(0.394)	0.164	0.018
20	1.67	0.80	0.182	(0.394)	0.164	0.018
21	1.75	0.80	0.182	(0.394)	0.164	0.018
22	1.83	0.80	0.182	(0.394)	0.164	0.018
23	1.92	0.80	0.182	(0.394)	0.164	0.018
24	2.00	0.90	0.205	(0.394)	0.185	0.021
25	2.08	0.80	0.182	(0.394)	0.164	0.018
26	2.17	0.90	0.205	(0.394)	0.185	0.021
27	2.25	0.90	0.205	(0.394)	0.185	0.021
28	2.33	0.90	0.205	(0.394)	0.185	0.021
29	2.42	0.90	0.205	(0.394)	0.185	0.021
30	2.50	0.90	0.205	(0.394)	0.185	0.021
31	2.58	0.90	0.205	(0.394)	0.185	0.021
32	2.67	0.90	0.205	(0.394)	0.185	0.021
33	2.75	1.00	0.228	(0.394)	0.205	0.023
34	2.83	1.00	0.228	(0.394)	0.205	0.023
35	2.92	1.00	0.228	(0.394)	0.205	0.023
36	3.00	1.00	0.228	(0.394)	0.205	0.023
37	3.08	1.00	0.228	(0.394)	0.205	0.023
38	3.17	1.10	0.251	(0.394)	0.226	0.025
39	3.25	1.10	0.251	(0.394)	0.226	0.025
40	3.33	1.10	0.251	(0.394)	0.226	0.025

41	3.42	1.20	0.273	(	0.394)	0.246	0.027
42	3.50	1.30	0.296	(	0.394)	0.267	0.030
43	3.58	1.40	0.319	(	0.394)	0.287	0.032
44	3.67	1.40	0.319	(	0.394)	0.287	0.032
45	3.75	1.50	0.342	(	0.394)	0.308	0.034
46	3.83	1.50	0.342	(	0.394)	0.308	0.034
47	3.92	1.60	0.365	(	0.394)	0.328	0.036
48	4.00	1.60	0.365	(	0.394)	0.328	0.036
49	4.08	1.70	0.387	(	0.394)	0.349	0.039
50	4.17	1.80	0.410	(	0.394)	0.369	0.041
51	4.25	1.90	0.433	(	0.394)	0.390	0.043
52	4.33	2.00	0.456		0.394	(0.410)	0.061
53	4.42	2.10	0.479		0.394	(0.431)	0.084
54	4.50	2.10	0.479		0.394	(0.431)	0.084
55	4.58	2.20	0.501		0.394	(0.451)	0.107
56	4.67	2.30	0.524		0.394	(0.472)	0.130
57	4.75	2.40	0.547		0.394	(0.492)	0.152
58	4.83	2.40	0.547		0.394	(0.492)	0.152
59	4.92	2.50	0.570		0.394	(0.513)	0.175
60	5.00	2.60	0.592		0.394	(0.533)	0.198
61	5.08	3.10	0.706		0.394	(0.636)	0.312
62	5.17	3.60	0.820		0.394	(0.738)	0.426
63	5.25	3.90	0.889		0.394	(0.800)	0.494
64	5.33	4.20	0.957		0.394	(0.861)	0.563
65	5.42	4.70	1.071		0.394	(0.964)	0.677
66	5.50	5.60	1.276		0.394	(1.148)	0.882
67	5.58	1.90	0.433	(	0.394)	0.390	0.043
68	5.67	0.90	0.205	(	0.394)	0.185	0.021
69	5.75	0.60	0.137	(	0.394)	0.123	0.014
70	5.83	0.50	0.114	(	0.394)	0.103	0.011
71	5.92	0.30	0.068	(	0.394)	0.062	0.007
72	6.00	0.20	0.046	(	0.394)	0.041	0.005

(Loss Rate Not Used)

Sum = 100.0 Sum = 5.7

Flood volume = Effective rainfall 0.48(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.1(Ac.Ft)
Total soil loss = 1.42(In)
Total soil loss = 0.187(Ac.Ft)
Total rainfall = 1.90(In)
Flood volume = 2740.7 Cubic Feet
Total soil loss = 8149.7 Cubic Feet

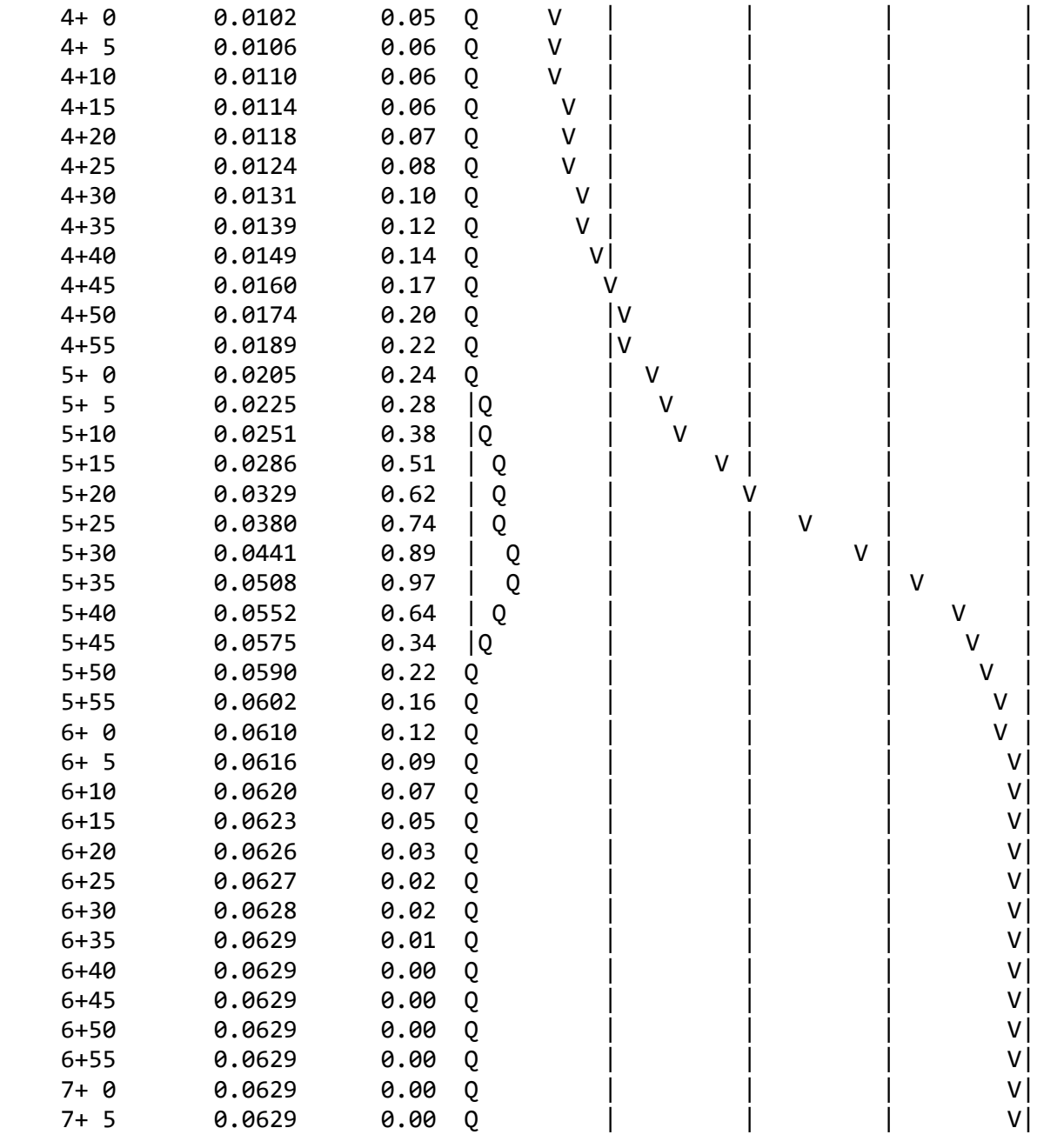
Peak flow rate of this hydrograph = 0.972(CFS)

++

6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.00	Q				
0+10	0.0001	0.01	Q				
0+15	0.0002	0.01	Q				
0+20	0.0003	0.02	Q				
0+25	0.0004	0.02	Q				
0+30	0.0005	0.02	Q				
0+35	0.0007	0.02	Q				
0+40	0.0008	0.02	Q				
0+45	0.0010	0.02	Q				
0+50	0.0012	0.02	Q				
0+55	0.0013	0.02	Q				
1+ 0	0.0015	0.03	Q				
1+ 5	0.0017	0.03	QV				
1+10	0.0019	0.03	QV				
1+15	0.0021	0.03	QV				
1+20	0.0023	0.03	QV				
1+25	0.0025	0.03	QV				
1+30	0.0027	0.03	QV				
1+35	0.0029	0.03	QV				
1+40	0.0031	0.03	QV				
1+45	0.0033	0.03	Q V				
1+50	0.0035	0.03	Q V				
1+55	0.0037	0.03	Q V				
2+ 0	0.0039	0.03	Q V				
2+ 5	0.0041	0.03	Q V				
2+10	0.0043	0.03	Q V				
2+15	0.0045	0.03	Q V				
2+20	0.0047	0.03	Q V				
2+25	0.0049	0.03	Q V				
2+30	0.0052	0.03	Q V				
2+35	0.0054	0.03	Q V				
2+40	0.0056	0.03	Q V				
2+45	0.0058	0.03	Q V				
2+50	0.0061	0.03	Q V				
2+55	0.0063	0.04	Q V				
3+ 0	0.0066	0.04	Q V				
3+ 5	0.0068	0.04	Q V				
3+10	0.0071	0.04	Q V				
3+15	0.0073	0.04	Q V				
3+20	0.0076	0.04	Q V				
3+25	0.0079	0.04	Q V				
3+30	0.0081	0.04	Q V				
3+35	0.0084	0.04	Q V				
3+40	0.0088	0.05	Q V				
3+45	0.0091	0.05	Q V				
3+50	0.0094	0.05	Q V				
3+55	0.0098	0.05	Q V				


4+ 0 0.0102 0.05
4+ 5 0.0106 0.06
4+10 0.0110 0.06
4+15 0.0114 0.06
4+20 0.0118 0.07
4+25 0.0124 0.08
4+30 0.0131 0.10
4+35 0.0139 0.12
4+40 0.0149 0.14
4+45 0.0160 0.17
4+50 0.0174 0.20
4+55 0.0189 0.22
5+ 0 0.0205 0.24
5+ 5 0.0225 0.28
5+10 0.0251 0.38
5+15 0.0286 0.51
5+20 0.0329 0.62
5+25 0.0380 0.74
5+30 0.0441 0.89
5+35 0.0508 0.97
5+40 0.0552 0.64
5+45 0.0575 0.34
5+50 0.0590 0.22
5+55 0.0602 0.16
6+ 0 0.0610 0.12
6+ 5 0.0616 0.09
6+10 0.0620 0.07
6+15 0.0623 0.05
6+20 0.0626 0.03
6+25 0.0627 0.02
6+30 0.0628 0.02
6+35 0.0629 0.01
6+40 0.0629 0.00
6+45 0.0629 0.00
6+50 0.0629 0.00
6+55 0.0629 0.00
7+ 0 0.0629 0.00
7+ 5 0.0629 0.00

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/06/22 File: Iris2410.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
10 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.05	3.24

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            5.25                   8.29

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    2.050(In)
Area Averaged 100-Year Rainfall =    5.250(In)

Point rain (area averaged) =    3.367(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    3.366(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           67.00         0.000
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
67.0  67.0      0.394     0.000        0.394       1.000      0.394
                                                 Sum (F) =   0.394
Area averaged mean soil loss (F) (In/Hr) =  0.394
Minimum soil loss rate ((In/Hr)) =  0.197
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         59.952          8.204              0.131
    2   0.167        119.904         33.934              0.540
    3   0.250        179.856         26.599              0.424
    4   0.333        239.808         10.311              0.164
    5   0.417        299.760          6.100              0.097
    6   0.500        359.712          4.123              0.066
    7   0.583        419.664          2.936              0.047
    8   0.667        479.616          2.066              0.033
    9   0.750        539.568          1.709              0.027
   10   0.833        599.520          1.265              0.020
   11   0.917        659.472          0.962              0.015
   12   1.000        719.424          0.685              0.011
   13   1.083        779.376          0.600              0.010
```

	14	1.167	839.329	0.506		0.008
				Sum = 100.000	Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.027	(0.699)	0.024	0.003
2	0.17	0.07	0.027	(0.696)	0.024	0.003
3	0.25	0.07	0.027	(0.694)	0.024	0.003
4	0.33	0.10	0.040	(0.691)	0.036	0.004
5	0.42	0.10	0.040	(0.688)	0.036	0.004
6	0.50	0.10	0.040	(0.686)	0.036	0.004
7	0.58	0.10	0.040	(0.683)	0.036	0.004
8	0.67	0.10	0.040	(0.680)	0.036	0.004
9	0.75	0.10	0.040	(0.678)	0.036	0.004
10	0.83	0.13	0.054	(0.675)	0.048	0.005
11	0.92	0.13	0.054	(0.672)	0.048	0.005
12	1.00	0.13	0.054	(0.670)	0.048	0.005
13	1.08	0.10	0.040	(0.667)	0.036	0.004
14	1.17	0.10	0.040	(0.664)	0.036	0.004
15	1.25	0.10	0.040	(0.662)	0.036	0.004
16	1.33	0.10	0.040	(0.659)	0.036	0.004
17	1.42	0.10	0.040	(0.657)	0.036	0.004
18	1.50	0.10	0.040	(0.654)	0.036	0.004
19	1.58	0.10	0.040	(0.651)	0.036	0.004
20	1.67	0.10	0.040	(0.649)	0.036	0.004
21	1.75	0.10	0.040	(0.646)	0.036	0.004
22	1.83	0.13	0.054	(0.643)	0.048	0.005
23	1.92	0.13	0.054	(0.641)	0.048	0.005
24	2.00	0.13	0.054	(0.638)	0.048	0.005
25	2.08	0.13	0.054	(0.636)	0.048	0.005
26	2.17	0.13	0.054	(0.633)	0.048	0.005
27	2.25	0.13	0.054	(0.631)	0.048	0.005
28	2.33	0.13	0.054	(0.628)	0.048	0.005
29	2.42	0.13	0.054	(0.625)	0.048	0.005
30	2.50	0.13	0.054	(0.623)	0.048	0.005
31	2.58	0.17	0.067	(0.620)	0.061	0.007
32	2.67	0.17	0.067	(0.618)	0.061	0.007
33	2.75	0.17	0.067	(0.615)	0.061	0.007
34	2.83	0.17	0.067	(0.613)	0.061	0.007
35	2.92	0.17	0.067	(0.610)	0.061	0.007
36	3.00	0.17	0.067	(0.608)	0.061	0.007
37	3.08	0.17	0.067	(0.605)	0.061	0.007
38	3.17	0.17	0.067	(0.603)	0.061	0.007
39	3.25	0.17	0.067	(0.600)	0.061	0.007
40	3.33	0.17	0.067	(0.598)	0.061	0.007

41	3.42	0.17	0.067	(0.595)	0.061	0.007
42	3.50	0.17	0.067	(0.593)	0.061	0.007
43	3.58	0.17	0.067	(0.590)	0.061	0.007
44	3.67	0.17	0.067	(0.588)	0.061	0.007
45	3.75	0.17	0.067	(0.585)	0.061	0.007
46	3.83	0.20	0.081	(0.583)	0.073	0.008
47	3.92	0.20	0.081	(0.580)	0.073	0.008
48	4.00	0.20	0.081	(0.578)	0.073	0.008
49	4.08	0.20	0.081	(0.575)	0.073	0.008
50	4.17	0.20	0.081	(0.573)	0.073	0.008
51	4.25	0.20	0.081	(0.571)	0.073	0.008
52	4.33	0.23	0.094	(0.568)	0.085	0.009
53	4.42	0.23	0.094	(0.566)	0.085	0.009
54	4.50	0.23	0.094	(0.563)	0.085	0.009
55	4.58	0.23	0.094	(0.561)	0.085	0.009
56	4.67	0.23	0.094	(0.558)	0.085	0.009
57	4.75	0.23	0.094	(0.556)	0.085	0.009
58	4.83	0.27	0.108	(0.554)	0.097	0.011
59	4.92	0.27	0.108	(0.551)	0.097	0.011
60	5.00	0.27	0.108	(0.549)	0.097	0.011
61	5.08	0.20	0.081	(0.546)	0.073	0.008
62	5.17	0.20	0.081	(0.544)	0.073	0.008
63	5.25	0.20	0.081	(0.542)	0.073	0.008
64	5.33	0.23	0.094	(0.539)	0.085	0.009
65	5.42	0.23	0.094	(0.537)	0.085	0.009
66	5.50	0.23	0.094	(0.535)	0.085	0.009
67	5.58	0.27	0.108	(0.532)	0.097	0.011
68	5.67	0.27	0.108	(0.530)	0.097	0.011
69	5.75	0.27	0.108	(0.528)	0.097	0.011
70	5.83	0.27	0.108	(0.525)	0.097	0.011
71	5.92	0.27	0.108	(0.523)	0.097	0.011
72	6.00	0.27	0.108	(0.521)	0.097	0.011
73	6.08	0.30	0.121	(0.518)	0.109	0.012
74	6.17	0.30	0.121	(0.516)	0.109	0.012
75	6.25	0.30	0.121	(0.514)	0.109	0.012
76	6.33	0.30	0.121	(0.511)	0.109	0.012
77	6.42	0.30	0.121	(0.509)	0.109	0.012
78	6.50	0.30	0.121	(0.507)	0.109	0.012
79	6.58	0.33	0.135	(0.505)	0.121	0.013
80	6.67	0.33	0.135	(0.502)	0.121	0.013
81	6.75	0.33	0.135	(0.500)	0.121	0.013
82	6.83	0.33	0.135	(0.498)	0.121	0.013
83	6.92	0.33	0.135	(0.495)	0.121	0.013
84	7.00	0.33	0.135	(0.493)	0.121	0.013
85	7.08	0.33	0.135	(0.491)	0.121	0.013
86	7.17	0.33	0.135	(0.489)	0.121	0.013
87	7.25	0.33	0.135	(0.487)	0.121	0.013
88	7.33	0.37	0.148	(0.484)	0.133	0.015
89	7.42	0.37	0.148	(0.482)	0.133	0.015
90	7.50	0.37	0.148	(0.480)	0.133	0.015

91	7.58	0.40	0.162	(0.478)	0.145	0.016
92	7.67	0.40	0.162	(0.475)	0.145	0.016
93	7.75	0.40	0.162	(0.473)	0.145	0.016
94	7.83	0.43	0.175	(0.471)	0.158	0.018
95	7.92	0.43	0.175	(0.469)	0.158	0.018
96	8.00	0.43	0.175	(0.467)	0.158	0.018
97	8.08	0.50	0.202	(0.465)	0.182	0.020
98	8.17	0.50	0.202	(0.462)	0.182	0.020
99	8.25	0.50	0.202	(0.460)	0.182	0.020
100	8.33	0.50	0.202	(0.458)	0.182	0.020
101	8.42	0.50	0.202	(0.456)	0.182	0.020
102	8.50	0.50	0.202	(0.454)	0.182	0.020
103	8.58	0.53	0.215	(0.452)	0.194	0.022
104	8.67	0.53	0.215	(0.450)	0.194	0.022
105	8.75	0.53	0.215	(0.447)	0.194	0.022
106	8.83	0.57	0.229	(0.445)	0.206	0.023
107	8.92	0.57	0.229	(0.443)	0.206	0.023
108	9.00	0.57	0.229	(0.441)	0.206	0.023
109	9.08	0.63	0.256	(0.439)	0.230	0.026
110	9.17	0.63	0.256	(0.437)	0.230	0.026
111	9.25	0.63	0.256	(0.435)	0.230	0.026
112	9.33	0.67	0.269	(0.433)	0.242	0.027
113	9.42	0.67	0.269	(0.431)	0.242	0.027
114	9.50	0.67	0.269	(0.429)	0.242	0.027
115	9.58	0.70	0.283	(0.427)	0.255	0.028
116	9.67	0.70	0.283	(0.425)	0.255	0.028
117	9.75	0.70	0.283	(0.423)	0.255	0.028
118	9.83	0.73	0.296	(0.421)	0.267	0.030
119	9.92	0.73	0.296	(0.419)	0.267	0.030
120	10.00	0.73	0.296	(0.416)	0.267	0.030
121	10.08	0.50	0.202	(0.414)	0.182	0.020
122	10.17	0.50	0.202	(0.412)	0.182	0.020
123	10.25	0.50	0.202	(0.410)	0.182	0.020
124	10.33	0.50	0.202	(0.408)	0.182	0.020
125	10.42	0.50	0.202	(0.406)	0.182	0.020
126	10.50	0.50	0.202	(0.405)	0.182	0.020
127	10.58	0.67	0.269	(0.403)	0.242	0.027
128	10.67	0.67	0.269	(0.401)	0.242	0.027
129	10.75	0.67	0.269	(0.399)	0.242	0.027
130	10.83	0.67	0.269	(0.397)	0.242	0.027
131	10.92	0.67	0.269	(0.395)	0.242	0.027
132	11.00	0.67	0.269	(0.393)	0.242	0.027
133	11.08	0.63	0.256	(0.391)	0.230	0.026
134	11.17	0.63	0.256	(0.389)	0.230	0.026
135	11.25	0.63	0.256	(0.387)	0.230	0.026
136	11.33	0.63	0.256	(0.385)	0.230	0.026
137	11.42	0.63	0.256	(0.383)	0.230	0.026
138	11.50	0.63	0.256	(0.381)	0.230	0.026
139	11.58	0.57	0.229	(0.379)	0.206	0.023
140	11.67	0.57	0.229	(0.377)	0.206	0.023

141	11.75	0.57	0.229	(0.376)	0.206	0.023
142	11.83	0.60	0.242	(0.374)	0.218	0.024
143	11.92	0.60	0.242	(0.372)	0.218	0.024
144	12.00	0.60	0.242	(0.370)	0.218	0.024
145	12.08	0.83	0.337	(0.368)	0.303	0.034
146	12.17	0.83	0.337	(0.366)	0.303	0.034
147	12.25	0.83	0.337	(0.364)	0.303	0.034
148	12.33	0.87	0.350	(0.363)	0.315	0.035
149	12.42	0.87	0.350	(0.361)	0.315	0.035
150	12.50	0.87	0.350	(0.359)	0.315	0.035
151	12.58	0.93	0.377	(0.357)	0.339	0.038
152	12.67	0.93	0.377	(0.355)	0.339	0.038
153	12.75	0.93	0.377	(0.354)	0.339	0.038
154	12.83	0.97	0.391	(0.352)	0.351	0.039
155	12.92	0.97	0.391	0.350	(0.351)	0.040
156	13.00	0.97	0.391	0.348	(0.351)	0.042
157	13.08	1.13	0.458	0.347	(0.412)	0.111
158	13.17	1.13	0.458	0.345	(0.412)	0.113
159	13.25	1.13	0.458	0.343	(0.412)	0.115
160	13.33	1.13	0.458	0.341	(0.412)	0.117
161	13.42	1.13	0.458	0.340	(0.412)	0.118
162	13.50	1.13	0.458	0.338	(0.412)	0.120
163	13.58	0.77	0.310	(0.336)	0.279	0.031
164	13.67	0.77	0.310	(0.334)	0.279	0.031
165	13.75	0.77	0.310	(0.333)	0.279	0.031
166	13.83	0.77	0.310	(0.331)	0.279	0.031
167	13.92	0.77	0.310	(0.329)	0.279	0.031
168	14.00	0.77	0.310	(0.328)	0.279	0.031
169	14.08	0.90	0.364	0.326	(0.327)	0.038
170	14.17	0.90	0.364	0.324	(0.327)	0.039
171	14.25	0.90	0.364	0.323	(0.327)	0.041
172	14.33	0.87	0.350	(0.321)	0.315	0.035
173	14.42	0.87	0.350	(0.319)	0.315	0.035
174	14.50	0.87	0.350	(0.318)	0.315	0.035
175	14.58	0.87	0.350	(0.316)	0.315	0.035
176	14.67	0.87	0.350	0.314	(0.315)	0.036
177	14.75	0.87	0.350	0.313	(0.315)	0.037
178	14.83	0.83	0.337	(0.311)	0.303	0.034
179	14.92	0.83	0.337	(0.310)	0.303	0.034
180	15.00	0.83	0.337	(0.308)	0.303	0.034
181	15.08	0.80	0.323	(0.306)	0.291	0.032
182	15.17	0.80	0.323	(0.305)	0.291	0.032
183	15.25	0.80	0.323	(0.303)	0.291	0.032
184	15.33	0.77	0.310	(0.302)	0.279	0.031
185	15.42	0.77	0.310	(0.300)	0.279	0.031
186	15.50	0.77	0.310	(0.299)	0.279	0.031
187	15.58	0.63	0.256	(0.297)	0.230	0.026
188	15.67	0.63	0.256	(0.296)	0.230	0.026
189	15.75	0.63	0.256	(0.294)	0.230	0.026
190	15.83	0.63	0.256	(0.293)	0.230	0.026

191	15.92	0.63	0.256	(0.291)	0.230	0.026
192	16.00	0.63	0.256	(0.290)	0.230	0.026
193	16.08	0.13	0.054	(0.288)	0.048	0.005
194	16.17	0.13	0.054	(0.287)	0.048	0.005
195	16.25	0.13	0.054	(0.285)	0.048	0.005
196	16.33	0.13	0.054	(0.284)	0.048	0.005
197	16.42	0.13	0.054	(0.282)	0.048	0.005
198	16.50	0.13	0.054	(0.281)	0.048	0.005
199	16.58	0.10	0.040	(0.279)	0.036	0.004
200	16.67	0.10	0.040	(0.278)	0.036	0.004
201	16.75	0.10	0.040	(0.277)	0.036	0.004
202	16.83	0.10	0.040	(0.275)	0.036	0.004
203	16.92	0.10	0.040	(0.274)	0.036	0.004
204	17.00	0.10	0.040	(0.272)	0.036	0.004
205	17.08	0.17	0.067	(0.271)	0.061	0.007
206	17.17	0.17	0.067	(0.270)	0.061	0.007
207	17.25	0.17	0.067	(0.268)	0.061	0.007
208	17.33	0.17	0.067	(0.267)	0.061	0.007
209	17.42	0.17	0.067	(0.266)	0.061	0.007
210	17.50	0.17	0.067	(0.264)	0.061	0.007
211	17.58	0.17	0.067	(0.263)	0.061	0.007
212	17.67	0.17	0.067	(0.262)	0.061	0.007
213	17.75	0.17	0.067	(0.260)	0.061	0.007
214	17.83	0.13	0.054	(0.259)	0.048	0.005
215	17.92	0.13	0.054	(0.258)	0.048	0.005
216	18.00	0.13	0.054	(0.257)	0.048	0.005
217	18.08	0.13	0.054	(0.255)	0.048	0.005
218	18.17	0.13	0.054	(0.254)	0.048	0.005
219	18.25	0.13	0.054	(0.253)	0.048	0.005
220	18.33	0.13	0.054	(0.252)	0.048	0.005
221	18.42	0.13	0.054	(0.250)	0.048	0.005
222	18.50	0.13	0.054	(0.249)	0.048	0.005
223	18.58	0.10	0.040	(0.248)	0.036	0.004
224	18.67	0.10	0.040	(0.247)	0.036	0.004
225	18.75	0.10	0.040	(0.246)	0.036	0.004
226	18.83	0.07	0.027	(0.244)	0.024	0.003
227	18.92	0.07	0.027	(0.243)	0.024	0.003
228	19.00	0.07	0.027	(0.242)	0.024	0.003
229	19.08	0.10	0.040	(0.241)	0.036	0.004
230	19.17	0.10	0.040	(0.240)	0.036	0.004
231	19.25	0.10	0.040	(0.239)	0.036	0.004
232	19.33	0.13	0.054	(0.238)	0.048	0.005
233	19.42	0.13	0.054	(0.236)	0.048	0.005
234	19.50	0.13	0.054	(0.235)	0.048	0.005
235	19.58	0.10	0.040	(0.234)	0.036	0.004
236	19.67	0.10	0.040	(0.233)	0.036	0.004
237	19.75	0.10	0.040	(0.232)	0.036	0.004
238	19.83	0.07	0.027	(0.231)	0.024	0.003
239	19.92	0.07	0.027	(0.230)	0.024	0.003
240	20.00	0.07	0.027	(0.229)	0.024	0.003

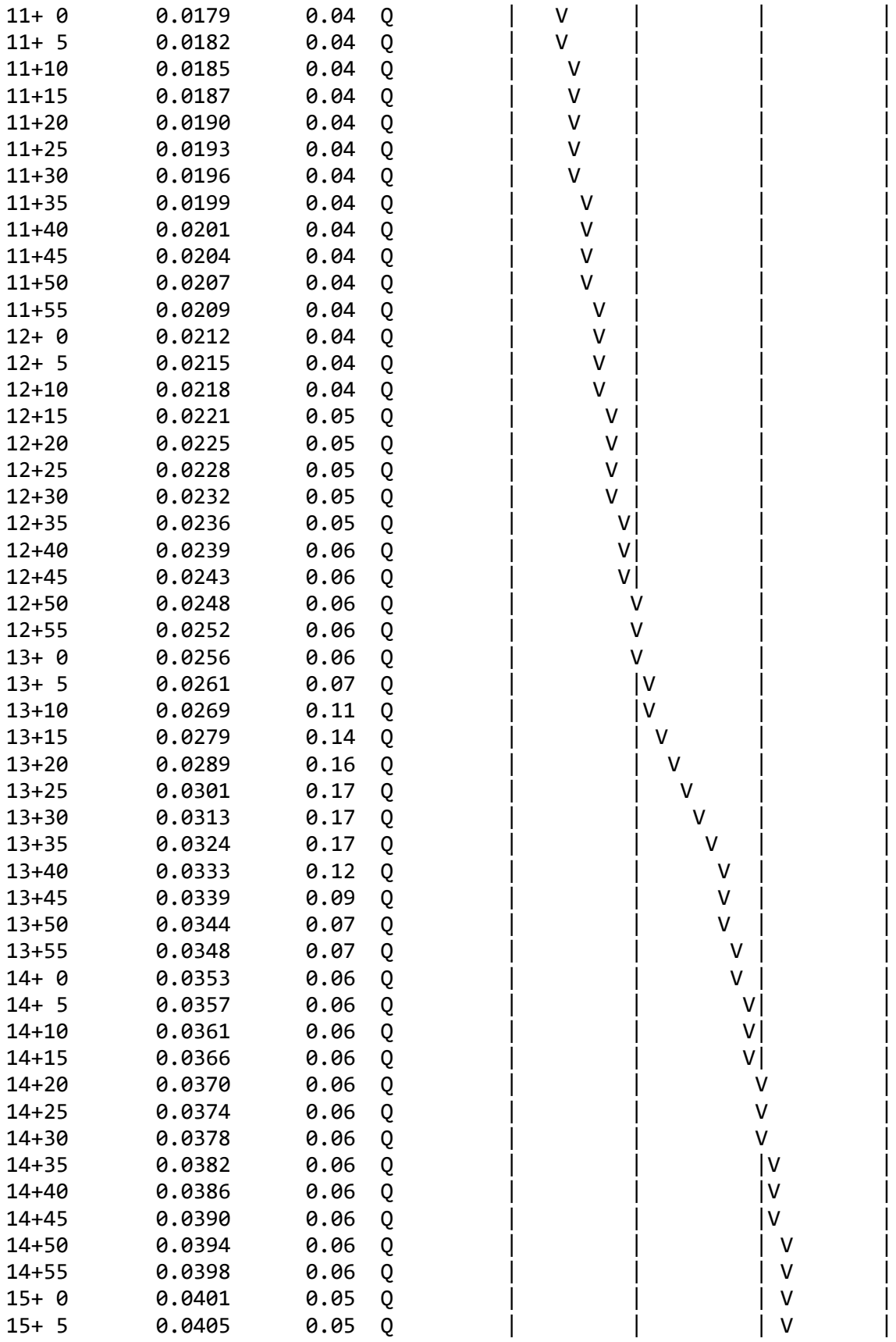
241	20.08	0.10	0.040	(0.228)	0.036	0.004
242	20.17	0.10	0.040	(0.227)	0.036	0.004
243	20.25	0.10	0.040	(0.226)	0.036	0.004
244	20.33	0.10	0.040	(0.225)	0.036	0.004
245	20.42	0.10	0.040	(0.224)	0.036	0.004
246	20.50	0.10	0.040	(0.223)	0.036	0.004
247	20.58	0.10	0.040	(0.222)	0.036	0.004
248	20.67	0.10	0.040	(0.221)	0.036	0.004
249	20.75	0.10	0.040	(0.220)	0.036	0.004
250	20.83	0.07	0.027	(0.219)	0.024	0.003
251	20.92	0.07	0.027	(0.219)	0.024	0.003
252	21.00	0.07	0.027	(0.218)	0.024	0.003
253	21.08	0.10	0.040	(0.217)	0.036	0.004
254	21.17	0.10	0.040	(0.216)	0.036	0.004
255	21.25	0.10	0.040	(0.215)	0.036	0.004
256	21.33	0.07	0.027	(0.214)	0.024	0.003
257	21.42	0.07	0.027	(0.213)	0.024	0.003
258	21.50	0.07	0.027	(0.213)	0.024	0.003
259	21.58	0.10	0.040	(0.212)	0.036	0.004
260	21.67	0.10	0.040	(0.211)	0.036	0.004
261	21.75	0.10	0.040	(0.210)	0.036	0.004
262	21.83	0.07	0.027	(0.210)	0.024	0.003
263	21.92	0.07	0.027	(0.209)	0.024	0.003
264	22.00	0.07	0.027	(0.208)	0.024	0.003
265	22.08	0.10	0.040	(0.208)	0.036	0.004
266	22.17	0.10	0.040	(0.207)	0.036	0.004
267	22.25	0.10	0.040	(0.206)	0.036	0.004
268	22.33	0.07	0.027	(0.206)	0.024	0.003
269	22.42	0.07	0.027	(0.205)	0.024	0.003
270	22.50	0.07	0.027	(0.204)	0.024	0.003
271	22.58	0.07	0.027	(0.204)	0.024	0.003
272	22.67	0.07	0.027	(0.203)	0.024	0.003
273	22.75	0.07	0.027	(0.203)	0.024	0.003
274	22.83	0.07	0.027	(0.202)	0.024	0.003
275	22.92	0.07	0.027	(0.202)	0.024	0.003
276	23.00	0.07	0.027	(0.201)	0.024	0.003
277	23.08	0.07	0.027	(0.201)	0.024	0.003
278	23.17	0.07	0.027	(0.200)	0.024	0.003
279	23.25	0.07	0.027	(0.200)	0.024	0.003
280	23.33	0.07	0.027	(0.199)	0.024	0.003
281	23.42	0.07	0.027	(0.199)	0.024	0.003
282	23.50	0.07	0.027	(0.199)	0.024	0.003
283	23.58	0.07	0.027	(0.198)	0.024	0.003
284	23.67	0.07	0.027	(0.198)	0.024	0.003
285	23.75	0.07	0.027	(0.198)	0.024	0.003
286	23.83	0.07	0.027	(0.198)	0.024	0.003
287	23.92	0.07	0.027	(0.197)	0.024	0.003
288	24.00	0.07	0.027	(0.197)	0.024	0.003
		(Loss Rate Not Used)				
	Sum =	100.0			Sum =	4.5

```
      Flood volume = Effective rainfall      0.37(In)
       times area       1.6(Ac.)/[(In)/(Ft.)] =       0.0(Ac.Ft)
      Total soil loss =      2.99(In)
      Total soil loss =     0.394(Ac.Ft)
      Total rainfall =      3.37(In)
      Flood volume =        2139.1 Cubic Feet
      Total soil loss =       17169.1 Cubic Feet
      ----------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.173(CFS)
      ----------------------------------------------------------------------
      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ----------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ----------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
----------------------------------------------------------------------------
  0+ 5       0.0000      0.00  Q         |         |         |         |
  0+10       0.0000      0.00  Q         |         |         |         |
  0+15       0.0000      0.00  Q         |         |         |         |
  0+20       0.0001      0.00  Q         |         |         |         |
  0+25       0.0001      0.00  Q         |         |         |         |
  0+30       0.0001      0.01  Q         |         |         |         |
  0+35       0.0002      0.01  Q         |         |         |         |
  0+40       0.0002      0.01  Q         |         |         |         |
  0+45       0.0002      0.01  Q         |         |         |         |
  0+50       0.0003      0.01  Q         |         |         |         |
  0+55       0.0003      0.01  Q         |         |         |         |
  1+ 0       0.0004      0.01  Q         |         |         |         |
  1+ 5       0.0004      0.01  Q         |         |         |         |
  1+10       0.0005      0.01  Q         |         |         |         |
  1+15       0.0005      0.01  Q         |         |         |         |
  1+20       0.0006      0.01  Q         |         |         |         |
  1+25       0.0006      0.01  Q         |         |         |         |
  1+30       0.0007      0.01  Q         |         |         |         |
  1+35       0.0007      0.01  Q         |         |         |         |
  1+40       0.0008      0.01  Q         |         |         |         |
  1+45       0.0008      0.01  Q         |         |         |         |
  1+50       0.0009      0.01  Q         |         |         |         |
  1+55       0.0009      0.01  Q         |         |         |         |
  2+ 0       0.0010      0.01  Q         |         |         |         |
  2+ 5       0.0010      0.01  Q         |         |         |         |
  2+10       0.0011      0.01  Q         |         |         |         |
  2+15       0.0011      0.01  Q         |         |         |         |
  2+20       0.0012      0.01  Q         |         |         |         |
  2+25       0.0013      0.01  QV        |         |         |         |
  2+30       0.0013      0.01  QV        |         |         |         |
  2+35       0.0014      0.01  QV        |         |         |         |
```

2+40	0.0014	0.01	QV	|	|	|	|
2+45	0.0015	0.01	QV	|	|	|	|
2+50	0.0016	0.01	QV	|	|	|	|
2+55	0.0017	0.01	QV	|	|	|	|
3+ 0	0.0017	0.01	QV	|	|	|	|
3+ 5	0.0018	0.01	QV	|	|	|	|
3+10	0.0019	0.01	QV	|	|	|	|
3+15	0.0019	0.01	QV	|	|	|	|
3+20	0.0020	0.01	QV	|	|	|	|
3+25	0.0021	0.01	QV	|	|	|	|
3+30	0.0022	0.01	QV	|	|	|	|
3+35	0.0022	0.01	QV	|	|	|	|
3+40	0.0023	0.01	QV	|	|	|	|
3+45	0.0024	0.01	QV	|	|	|	|
3+50	0.0025	0.01	Q V	|	|	|	|
3+55	0.0025	0.01	Q V	|	|	|	|
4+ 0	0.0026	0.01	Q V	|	|	|	|
4+ 5	0.0027	0.01	Q V	|	|	|	|
4+10	0.0028	0.01	Q V	|	|	|	|
4+15	0.0029	0.01	Q V	|	|	|	|
4+20	0.0030	0.01	Q V	|	|	|	|
4+25	0.0031	0.01	Q V	|	|	|	|
4+30	0.0032	0.01	Q V	|	|	|	|
4+35	0.0033	0.01	Q V	|	|	|	|
4+40	0.0034	0.01	Q V	|	|	|	|
4+45	0.0035	0.01	Q V	|	|	|	|
4+50	0.0036	0.02	Q V	|	|	|	|
4+55	0.0037	0.02	Q V	|	|	|	|
5+ 0	0.0038	0.02	Q V	|	|	|	|
5+ 5	0.0039	0.02	Q V	|	|	|	|
5+10	0.0040	0.01	Q V	|	|	|	|
5+15	0.0041	0.01	Q V	|	|	|	|
5+20	0.0042	0.01	Q V	|	|	|	|
5+25	0.0043	0.01	Q V	|	|	|	|
5+30	0.0044	0.01	Q V	|	|	|	|
5+35	0.0045	0.02	Q V	|	|	|	|
5+40	0.0046	0.02	Q V	|	|	|	|
5+45	0.0047	0.02	Q V	|	|	|	|
5+50	0.0048	0.02	Q V	|	|	|	|
5+55	0.0050	0.02	Q V	|	|	|	|
6+ 0	0.0051	0.02	Q V	|	|	|	|
6+ 5	0.0052	0.02	Q V	|	|	|	|
6+10	0.0053	0.02	Q V	|	|	|	|
6+15	0.0054	0.02	Q V	|	|	|	|
6+20	0.0056	0.02	Q V	|	|	|	|
6+25	0.0057	0.02	Q V	|	|	|	|
6+30	0.0058	0.02	Q V	|	|	|	|
6+35	0.0060	0.02	Q V	|	|	|	|
6+40	0.0061	0.02	Q V	|	|	|	|
6+45	0.0062	0.02	Q V	|	|	|	|

```
 6+50       0.0064      0.02  Q    V    |          |          |          |
 6+55       0.0065      0.02  Q    V    |          |          |          |
 7+ 0       0.0067      0.02  Q    V    |          |          |          |
 7+ 5       0.0068      0.02  Q    V    |          |          |          |
 7+10       0.0070      0.02  Q    V    |          |          |          |
 7+15       0.0071      0.02  Q    V    |          |          |          |
 7+20       0.0073      0.02  Q    V    |          |          |          |
 7+25       0.0074      0.02  Q     V   |          |          |          |
 7+30       0.0076      0.02  Q     V   |          |          |          |
 7+35       0.0077      0.02  Q     V   |          |          |          |
 7+40       0.0079      0.02  Q     V   |          |          |          |
 7+45       0.0081      0.02  Q     V   |          |          |          |
 7+50       0.0083      0.03  Q     V   |          |          |          |
 7+55       0.0084      0.03  Q     V   |          |          |          |
 8+ 0       0.0086      0.03  Q      V  |          |          |          |
 8+ 5       0.0088      0.03  Q      V  |          |          |          |
 8+10       0.0090      0.03  Q      V  |          |          |          |
 8+15       0.0092      0.03  Q      V  |          |          |          |
 8+20       0.0094      0.03  Q      V  |          |          |          |
 8+25       0.0097      0.03  Q      V  |          |          |          |
 8+30       0.0099      0.03  Q       V |          |          |          |
 8+35       0.0101      0.03  Q       V |          |          |          |
 8+40       0.0103      0.03  Q       V |          |          |          |
 8+45       0.0105      0.03  Q       V |          |          |          |
 8+50       0.0108      0.03  Q       V |          |          |          |
 8+55       0.0110      0.03  Q       V |          |          |          |
 9+ 0       0.0113      0.04  Q        V|          |          |          |
 9+ 5       0.0115      0.04  Q        V|          |          |          |
 9+10       0.0118      0.04  Q        V|          |          |          |
 9+15       0.0120      0.04  Q        V|          |          |          |
 9+20       0.0123      0.04  Q         V          |          |          |
 9+25       0.0126      0.04  Q         V          |          |          |
 9+30       0.0129      0.04  Q         V          |          |          |
 9+35       0.0132      0.04  Q         V          |          |          |
 9+40       0.0135      0.04  Q         V          |          |          |
 9+45       0.0138      0.04  Q         |V         |          |          |
 9+50       0.0141      0.04  Q         |V         |          |          |
 9+55       0.0144      0.05  Q         |V         |          |          |
10+ 0       0.0147      0.05  Q         |V         |          |          |
10+ 5       0.0150      0.05  Q         | V        |          |          |
10+10       0.0153      0.04  Q         | V        |          |          |
10+15       0.0156      0.04  Q         | V        |          |          |
10+20       0.0158      0.04  Q         | V        |          |          |
10+25       0.0160      0.03  Q         |  V       |          |          |
10+30       0.0163      0.03  Q         |  V       |          |          |
10+35       0.0165      0.03  Q         |  V       |          |          |
10+40       0.0168      0.04  Q         |  V       |          |          |
10+45       0.0170      0.04  Q         |  V       |          |          |
10+50       0.0173      0.04  Q         |   V      |          |          |
10+55       0.0176      0.04  Q         |   V      |          |          |
```



15+10	0.0409	0.05	Q	|	|	| V	|
15+15	0.0412	0.05	Q	|	|	| V	|
15+20	0.0416	0.05	Q	|	|	| V	|
15+25	0.0420	0.05	Q	|	|	| V	|
15+30	0.0423	0.05	Q	|	|	| V	|
15+35	0.0426	0.05	Q	|	|	| V	|
15+40	0.0430	0.05	Q	|	|	| V	|
15+45	0.0433	0.04	Q	|	|	| V	|
15+50	0.0436	0.04	Q	|	|	| V	|
15+55	0.0438	0.04	Q	|	|	| V	|
16+ 0	0.0441	0.04	Q	|	|	| V	|
16+ 5	0.0444	0.04	Q	|	|	| V	|
16+10	0.0446	0.03	Q	|	|	| V	|
16+15	0.0447	0.02	Q	|	|	| V	|
16+20	0.0448	0.02	Q	|	|	| V	|
16+25	0.0449	0.01	Q	|	|	| V	|
16+30	0.0450	0.01	Q	|	|	| V	|
16+35	0.0451	0.01	Q	|	|	| V	|
16+40	0.0451	0.01	Q	|	|	| V	|
16+45	0.0452	0.01	Q	|	|	| V	|
16+50	0.0453	0.01	Q	|	|	| V	|
16+55	0.0453	0.01	Q	|	|	| V	|
17+ 0	0.0454	0.01	Q	|	|	| V	|
17+ 5	0.0454	0.01	Q	|	|	| V	|
17+10	0.0455	0.01	Q	|	|	| V	|
17+15	0.0455	0.01	Q	|	|	| V	|
17+20	0.0456	0.01	Q	|	|	| V	|
17+25	0.0457	0.01	Q	|	|	| V	|
17+30	0.0457	0.01	Q	|	|	| V	|
17+35	0.0458	0.01	Q	|	|	| V	|
17+40	0.0459	0.01	Q	|	|	| V	|
17+45	0.0460	0.01	Q	|	|	| V	|
17+50	0.0460	0.01	Q	|	|	| V	|
17+55	0.0461	0.01	Q	|	|	| V	|
18+ 0	0.0462	0.01	Q	|	|	| V	|
18+ 5	0.0462	0.01	Q	|	|	| V	|
18+10	0.0463	0.01	Q	|	|	| V	|
18+15	0.0463	0.01	Q	|	|	| V	|
18+20	0.0464	0.01	Q	|	|	| V	|
18+25	0.0465	0.01	Q	|	|	| V	|
18+30	0.0465	0.01	Q	|	|	| V	|
18+35	0.0466	0.01	Q	|	|	| V	|
18+40	0.0466	0.01	Q	|	|	| V	|
18+45	0.0467	0.01	Q	|	|	| V	|
18+50	0.0467	0.01	Q	|	|	| V	|
18+55	0.0468	0.01	Q	|	|	| V	|
19+ 0	0.0468	0.01	Q	|	|	| V	|
19+ 5	0.0468	0.01	Q	|	|	| V	|
19+10	0.0469	0.01	Q	|	|	| V	|
19+15	0.0469	0.01	Q	|	|	| V	|

19+20	0.0470	0.01	Q	|	|	|	V |
19+25	0.0470	0.01	Q	|	|	|	V |
19+30	0.0471	0.01	Q	|	|	|	V |
19+35	0.0471	0.01	Q	|	|	|	V |
19+40	0.0472	0.01	Q	|	|	|	V |
19+45	0.0472	0.01	Q	|	|	|	V |
19+50	0.0473	0.01	Q	|	|	|	V |
19+55	0.0473	0.01	Q	|	|	|	V |
20+ 0	0.0473	0.01	Q	|	|	|	V |
20+ 5	0.0474	0.01	Q	|	|	|	V |
20+10	0.0474	0.01	Q	|	|	|	V |
20+15	0.0475	0.01	Q	|	|	|	V |
20+20	0.0475	0.01	Q	|	|	|	V |
20+25	0.0475	0.01	Q	|	|	|	V |
20+30	0.0476	0.01	Q	|	|	|	V |
20+35	0.0476	0.01	Q	|	|	|	V |
20+40	0.0477	0.01	Q	|	|	|	V |
20+45	0.0477	0.01	Q	|	|	|	V |
20+50	0.0478	0.01	Q	|	|	|	V |
20+55	0.0478	0.01	Q	|	|	|	V |
21+ 0	0.0478	0.00	Q	|	|	|	V |
21+ 5	0.0479	0.00	Q	|	|	|	V |
21+10	0.0479	0.01	Q	|	|	|	V|
21+15	0.0479	0.01	Q	|	|	|	V|
21+20	0.0480	0.01	Q	|	|	|	V|
21+25	0.0480	0.01	Q	|	|	|	V|
21+30	0.0481	0.00	Q	|	|	|	V|
21+35	0.0481	0.00	Q	|	|	|	V|
21+40	0.0481	0.01	Q	|	|	|	V|
21+45	0.0482	0.01	Q	|	|	|	V|
21+50	0.0482	0.01	Q	|	|	|	V|
21+55	0.0482	0.01	Q	|	|	|	V|
22+ 0	0.0483	0.00	Q	|	|	|	V|
22+ 5	0.0483	0.00	Q	|	|	|	V|
22+10	0.0483	0.01	Q	|	|	|	V|
22+15	0.0484	0.01	Q	|	|	|	V|
22+20	0.0484	0.01	Q	|	|	|	V|
22+25	0.0485	0.01	Q	|	|	|	V|
22+30	0.0485	0.00	Q	|	|	|	V|
22+35	0.0485	0.00	Q	|	|	|	V|
22+40	0.0486	0.00	Q	|	|	|	V|
22+45	0.0486	0.00	Q	|	|	|	V|
22+50	0.0486	0.00	Q	|	|	|	V|
22+55	0.0486	0.00	Q	|	|	|	V|
23+ 0	0.0487	0.00	Q	|	|	|	V|
23+ 5	0.0487	0.00	Q	|	|	|	V|
23+10	0.0487	0.00	Q	|	|	|	V|
23+15	0.0488	0.00	Q	|	|	|	V|
23+20	0.0488	0.00	Q	|	|	|	V|
23+25	0.0488	0.00	Q	|	|	|	V|

```
   23+30       0.0489      0.00  Q          |          |          |         V|
   23+35       0.0489      0.00  Q          |          |          |         V|
   23+40       0.0489      0.00  Q          |          |          |         V|
   23+45       0.0489      0.00  Q          |          |          |         V|
   23+50       0.0490      0.00  Q          |          |          |         V|
   23+55       0.0490      0.00  Q          |          |          |         V|
   24+ 0       0.0490      0.00  Q          |          |          |         V|
   24+ 5       0.0491      0.00  Q          |          |          |         V|
   24+10       0.0491      0.00  Q          |          |          |         V|
   24+15       0.0491      0.00  Q          |          |          |         V|
   24+20       0.0491      0.00  Q          |          |          |         V|
   24+25       0.0491      0.00  Q          |          |          |         V|
   24+30       0.0491      0.00  Q          |          |          |         V|
   24+35       0.0491      0.00  Q          |          |          |         V|
   24+40       0.0491      0.00  Q          |          |          |         V|
   24+45       0.0491      0.00  Q          |          |          |         V|
   24+50       0.0491      0.00  Q          |          |          |         V|
   24+55       0.0491      0.00  Q          |          |          |         V|
   25+ 0       0.0491      0.00  Q          |          |          |         V|
   25+ 5       0.0491      0.00  Q          |          |          |          V
---------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/06/22 File: Iris1100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
100 YR

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.49	0.78

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	1.35	2.13

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.493(In)
Area Averaged 100-Year Rainfall = 1.350(In)

Point rain (area averaged) = 1.350(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.350(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.580	67.00	0.000

Total Area Entered = 1.58(Ac.)

RI AMC2	RI AMC-3	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
67.0	83.2	0.208	0.000	0.208	1.000	0.208
					Sum (F) =	0.208

Area averaged mean soil loss (F) (In/Hr) = 0.208
Minimum soil loss rate ((In/Hr)) = 0.104
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

Slope of intensity-duration curve for a 1 hour storm =0.5000

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	59.952	8.204	0.131
2	0.167	119.904	33.934	0.540
3	0.250	179.856	26.599	0.424
4	0.333	239.808	10.311	0.164
5	0.417	299.760	6.100	0.097
6	0.500	359.712	4.123	0.066
7	0.583	419.664	2.936	0.047
8	0.667	479.616	2.066	0.033
9	0.750	539.568	1.709	0.027
10	0.833	599.520	1.265	0.020
11	0.917	659.472	0.962	0.015

12	1.000	719.424	0.685	0.011
13	1.083	779.376	0.600	0.010
14	1.167	839.329	0.506	0.008
		Sum = 100.000	Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.20	0.680	0.208	(0.612)	0.473
2	0.17	4.30	0.697	0.208	(0.627)	0.489
3	0.25	5.00	0.810	0.208	(0.729)	0.602
4	0.33	5.00	0.810	0.208	(0.729)	0.602
5	0.42	5.80	0.940	0.208	(0.846)	0.732
6	0.50	6.50	1.053	0.208	(0.948)	0.845
7	0.58	7.40	1.199	0.208	(1.079)	0.991
8	0.67	8.60	1.393	0.208	(1.254)	1.186
9	0.75	12.30	1.993	0.208	(1.793)	1.785
10	0.83	29.10	4.714	0.208	(4.243)	4.507
11	0.92	6.80	1.102	0.208	(0.991)	0.894
12	1.00	5.00	0.810	0.208	(0.729)	0.602
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	13.7

Flood volume = Effective rainfall 1.14(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 0.21(In)
Total soil loss = 0.027(Ac.Ft)
Total rainfall = 1.35(In)
Flood volume = 6552.5 Cubic Feet
Total soil loss = 1190.2 Cubic Feet

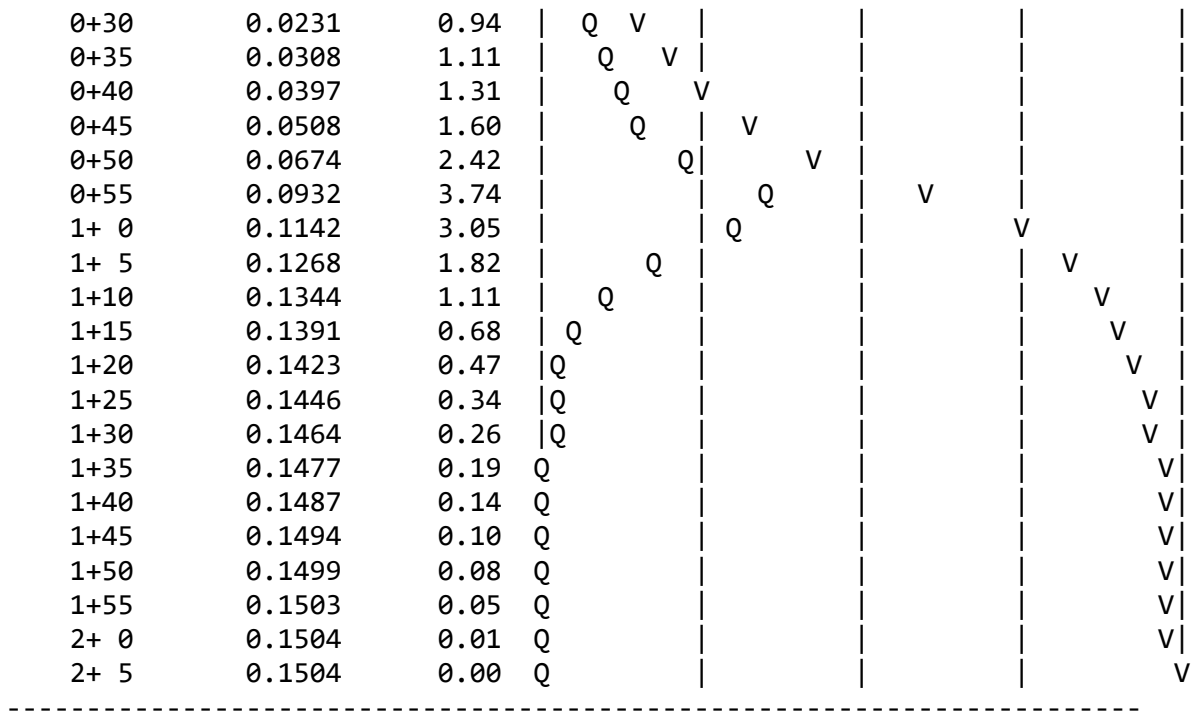
Peak flow rate of this hydrograph = 3.744(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0004	0.06	Q	|	|	|	|
0+10	0.0026	0.32	VQ	|	|	|	|
0+15	0.0064	0.54	|VQ	|	|	|	|
0+20	0.0111	0.69	| Q	|	|	|	|
0+25	0.0166	0.80	| QV	|	|	|	|


0+30 0.0231 0.94
0+35 0.0308 1.11
0+40 0.0397 1.31
0+45 0.0508 1.60
0+50 0.0674 2.42
0+55 0.0932 3.74
1+ 0 0.1142 3.05
1+ 5 0.1268 1.82
1+10 0.1344 1.11
1+15 0.1391 0.68
1+20 0.1423 0.47
1+25 0.1446 0.34
1+30 0.1464 0.26
1+35 0.1477 0.19
1+40 0.1487 0.14
1+45 0.1494 0.10
1+50 0.1499 0.08
1+55 0.1503 0.05
2+ 0 0.1504 0.01
2+ 5 0.1504 0.00

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/06/22 File: Iris3100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
100 YR

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.87	1.37

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            2.10                   3.32

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    0.869(In)
Area Averaged 100-Year Rainfall =    2.100(In)

Point rain (area averaged) =    2.100(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    2.100(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           67.00         0.000
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-3     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
67.0  83.2      0.208     0.000        0.208       1.000      0.208
                                                 Sum (F) =   0.208
Area averaged mean soil loss (F) (In/Hr) =  0.208
Minimum soil loss rate ((In/Hr)) =  0.104
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
------------------------------------------------------------------------
    1   0.083         59.952          8.204             0.131
    2   0.167        119.904         33.934             0.540
    3   0.250        179.856         26.599             0.424
    4   0.333        239.808         10.311             0.164
    5   0.417        299.760          6.100             0.097
    6   0.500        359.712          4.123             0.066
    7   0.583        419.664          2.936             0.047
    8   0.667        479.616          2.066             0.033
    9   0.750        539.568          1.709             0.027
   10   0.833        599.520          1.265             0.020
   11   0.917        659.472          0.962             0.015
   12   1.000        719.424          0.685             0.011
   13   1.083        779.376          0.600             0.010
```

14	1.167	839.329	0.506		0.008
			Sum = 100.000	Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max		Low	Effective (In/Hr)
1	0.08	1.30	0.328	0.208	(	0.295)	0.120
2	0.17	1.30	0.328	0.208	(	0.295)	0.120
3	0.25	1.10	0.277	0.208	(	0.249)	0.070
4	0.33	1.50	0.378	0.208	(	0.340)	0.170
5	0.42	1.50	0.378	0.208	(	0.340)	0.170
6	0.50	1.80	0.454	0.208	(	0.408)	0.246
7	0.58	1.50	0.378	0.208	(	0.340)	0.170
8	0.67	1.80	0.454	0.208	(	0.408)	0.246
9	0.75	1.80	0.454	0.208	(	0.408)	0.246
10	0.83	1.50	0.378	0.208	(	0.340)	0.170
11	0.92	1.60	0.403	0.208	(	0.363)	0.196
12	1.00	1.80	0.454	0.208	(	0.408)	0.246
13	1.08	2.20	0.554	0.208	(	0.499)	0.347
14	1.17	2.20	0.554	0.208	(	0.499)	0.347
15	1.25	2.20	0.554	0.208	(	0.499)	0.347
16	1.33	2.00	0.504	0.208	(	0.454)	0.296
17	1.42	2.60	0.655	0.208	(	0.590)	0.448
18	1.50	2.70	0.680	0.208	(	0.612)	0.473
19	1.58	2.40	0.605	0.208	(	0.544)	0.397
20	1.67	2.70	0.680	0.208	(	0.612)	0.473
21	1.75	3.30	0.832	0.208	(	0.748)	0.624
22	1.83	3.10	0.781	0.208	(	0.703)	0.574
23	1.92	2.90	0.731	0.208	(	0.658)	0.523
24	2.00	3.00	0.756	0.208	(	0.680)	0.548
25	2.08	3.10	0.781	0.208	(	0.703)	0.574
26	2.17	4.20	1.058	0.208	(	0.953)	0.851
27	2.25	5.00	1.260	0.208	(	1.134)	1.052
28	2.33	3.50	0.882	0.208	(	0.794)	0.674
29	2.42	6.80	1.714	0.208	(	1.542)	1.506
30	2.50	7.30	1.840	0.208	(	1.656)	1.632
31	2.58	8.20	2.066	0.208	(	1.860)	1.859
32	2.67	5.90	1.487	0.208	(	1.338)	1.279
33	2.75	2.00	0.504	0.208	(	0.454)	0.296
34	2.83	1.80	0.454	0.208	(	0.408)	0.246
35	2.92	1.80	0.454	0.208	(	0.408)	0.246
36	3.00	0.60	0.151	(0.208)		0.136	0.015
		(Loss Rate Not Used)					
Sum =		100.0				Sum =	17.8

Flood volume = Effective rainfall 1.48(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)

```
      Total soil loss =      0.62(In)
      Total soil loss =     0.081(Ac.Ft)
      Total rainfall =      2.10(In)
      Flood volume =        8507.8 Cubic Feet
      Total soil loss =        3536.5 Cubic Feet
      ---------------------------------------------------------------
       Peak flow rate of this hydrograph =      2.353(CFS)
      ---------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          3 - H O U R    S T O R M
                     R u n o f f     H y d r o g r a p h
      ---------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0001      0.02  Q         |         |         |         |
  0+10       0.0007      0.08  Q         |         |         |         |
  0+15       0.0015      0.12  Q         |         |         |         |
  0+20       0.0024      0.13  Q         |         |         |         |
  0+25       0.0036      0.18  Q         |         |         |         |
  0+30       0.0052      0.23  QV        |         |         |         |
  0+35       0.0071      0.28  |Q        |         |         |         |
  0+40       0.0091      0.29  |Q        |         |         |         |
  0+45       0.0113      0.32  |QV       |         |         |         |
  0+50       0.0136      0.34  |QV       |         |         |         |
  0+55       0.0158      0.31  |Q V      |         |         |         |
  1+ 0       0.0179      0.31  |Q V      |         |         |         |
  1+ 5       0.0204      0.36  |Q  V     |         |         |         |
  1+10       0.0234      0.43  |Q  V     |         |         |         |
  1+15       0.0267      0.49  |Q   V    |         |         |         |
  1+20       0.0302      0.50  | Q   V   |         |         |         |
  1+25       0.0336      0.51  | Q   V   |         |         |         |
  1+30       0.0376      0.58  | Q    V  |         |         |         |
  1+35       0.0421      0.65  | Q     V |         |         |         |
  1+40       0.0466      0.65  | Q      V|         |         |         |
  1+45       0.0514      0.70  | Q       V         |         |         |
  1+50       0.0569      0.80  |  Q      |V        |         |         |
  1+55       0.0628      0.85  |  Q      | V       |         |         |
  2+ 0       0.0685      0.84  |  Q      |   V     |         |         |
  2+ 5       0.0743      0.85  |  Q      |    V    |         |         |
  2+10       0.0806      0.91  |  Q      |     V   |         |         |
  2+15       0.0882      1.10  |   Q     |       V |         |         |
  2+20       0.0970      1.29  |    Q    |        V|         |         |
  2+25       0.1062      1.33  |    Q    |         |V        |         |
  2+30       0.1179      1.70  |     Q   |         |   V     |         |
  2+35       0.1325      2.13  |       Q |         |      V  |         |
  2+40       0.1487      2.35  |        Q|         |         V         |
  2+45       0.1632      2.10  |       Q |         |         |  V      |
```

```
    2+50       0.1730      1.42  |    Q    |         |         |    V    |
    2+55       0.1796      0.95  |  Q      |         |         |     V   |
    3+ 0       0.1846      0.73  | Q       |         |         |      V  |
    3+ 5       0.1880      0.50  |Q        |         |         |       V |
    3+10       0.1902      0.32  |Q        |         |         |       V |
    3+15       0.1918      0.23  Q         |         |         |        V|
    3+20       0.1929      0.17  Q         |         |         |        V|
    3+25       0.1938      0.12  Q         |         |         |        V|
    3+30       0.1944      0.09  Q         |         |         |        V|
    3+35       0.1948      0.06  Q         |         |         |        V|
    3+40       0.1951      0.04  Q         |         |         |        V|
    3+45       0.1952      0.02  Q         |         |         |        V|
    3+50       0.1953      0.01  Q         |         |         |        V|
    3+55       0.1953      0.00  Q         |         |         |        V|
    4+ 0       0.1953      0.00  Q         |         |         |        V|
    4+ 5       0.1953      0.00  Q         |         |         |         V
---------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/06/22 File: Iris6100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
100 YR

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	1.22	1.93

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.87	4.53

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.220(In)
Area Averaged 100-Year Rainfall = 2.870(In)

Point rain (area averaged) = 2.870(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 2.870(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.580	67.00	0.000

Total Area Entered = 1.58(Ac.)

RI AMC2	RI AMC-3	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
67.0	83.2	0.208	0.000	0.208	1.000	0.208
					Sum (F) =	0.208

Area averaged mean soil loss (F) (In/Hr) = 0.208
Minimum soil loss rate ((In/Hr)) = 0.104
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	59.952	8.204	0.131
2	0.167	119.904	33.934	0.540
3	0.250	179.856	26.599	0.424
4	0.333	239.808	10.311	0.164
5	0.417	299.760	6.100	0.097
6	0.500	359.712	4.123	0.066
7	0.583	419.664	2.936	0.047
8	0.667	479.616	2.066	0.033
9	0.750	539.568	1.709	0.027
10	0.833	599.520	1.265	0.020
11	0.917	659.472	0.962	0.015
12	1.000	719.424	0.685	0.011
13	1.083	779.376	0.600	0.010

14	1.167	839.329	0.506			0.008
			Sum = 100.000		Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.172	(0.208)	0.155	0.017
2	0.17	0.60	0.207	(0.208)	0.186	0.021
3	0.25	0.60	0.207	(0.208)	0.186	0.021
4	0.33	0.60	0.207	(0.208)	0.186	0.021
5	0.42	0.60	0.207	(0.208)	0.186	0.021
6	0.50	0.70	0.241	0.208	(0.217)	0.034
7	0.58	0.70	0.241	0.208	(0.217)	0.034
8	0.67	0.70	0.241	0.208	(0.217)	0.034
9	0.75	0.70	0.241	0.208	(0.217)	0.034
10	0.83	0.70	0.241	0.208	(0.217)	0.034
11	0.92	0.70	0.241	0.208	(0.217)	0.034
12	1.00	0.80	0.276	0.208	(0.248)	0.068
13	1.08	0.80	0.276	0.208	(0.248)	0.068
14	1.17	0.80	0.276	0.208	(0.248)	0.068
15	1.25	0.80	0.276	0.208	(0.248)	0.068
16	1.33	0.80	0.276	0.208	(0.248)	0.068
17	1.42	0.80	0.276	0.208	(0.248)	0.068
18	1.50	0.80	0.276	0.208	(0.248)	0.068
19	1.58	0.80	0.276	0.208	(0.248)	0.068
20	1.67	0.80	0.276	0.208	(0.248)	0.068
21	1.75	0.80	0.276	0.208	(0.248)	0.068
22	1.83	0.80	0.276	0.208	(0.248)	0.068
23	1.92	0.80	0.276	0.208	(0.248)	0.068
24	2.00	0.90	0.310	0.208	(0.279)	0.102
25	2.08	0.80	0.276	0.208	(0.248)	0.068
26	2.17	0.90	0.310	0.208	(0.279)	0.102
27	2.25	0.90	0.310	0.208	(0.279)	0.102
28	2.33	0.90	0.310	0.208	(0.279)	0.102
29	2.42	0.90	0.310	0.208	(0.279)	0.102
30	2.50	0.90	0.310	0.208	(0.279)	0.102
31	2.58	0.90	0.310	0.208	(0.279)	0.102
32	2.67	0.90	0.310	0.208	(0.279)	0.102
33	2.75	1.00	0.344	0.208	(0.310)	0.137
34	2.83	1.00	0.344	0.208	(0.310)	0.137
35	2.92	1.00	0.344	0.208	(0.310)	0.137
36	3.00	1.00	0.344	0.208	(0.310)	0.137
37	3.08	1.00	0.344	0.208	(0.310)	0.137
38	3.17	1.10	0.379	0.208	(0.341)	0.171
39	3.25	1.10	0.379	0.208	(0.341)	0.171
40	3.33	1.10	0.379	0.208	(0.341)	0.171

41	3.42	1.20	0.413	0.208	(0.372)	0.206	
42	3.50	1.30	0.448	0.208	(0.403)	0.240	
43	3.58	1.40	0.482	0.208	(0.434)	0.275	
44	3.67	1.40	0.482	0.208	(0.434)	0.275	
45	3.75	1.50	0.517	0.208	(0.465)	0.309	
46	3.83	1.50	0.517	0.208	(0.465)	0.309	
47	3.92	1.60	0.551	0.208	(0.496)	0.344	
48	4.00	1.60	0.551	0.208	(0.496)	0.344	
49	4.08	1.70	0.585	0.208	(0.527)	0.378	
50	4.17	1.80	0.620	0.208	(0.558)	0.412	
51	4.25	1.90	0.654	0.208	(0.589)	0.447	
52	4.33	2.00	0.689	0.208	(0.620)	0.481	
53	4.42	2.10	0.723	0.208	(0.651)	0.516	
54	4.50	2.10	0.723	0.208	(0.651)	0.516	
55	4.58	2.20	0.758	0.208	(0.682)	0.550	
56	4.67	2.30	0.792	0.208	(0.713)	0.585	
57	4.75	2.40	0.827	0.208	(0.744)	0.619	
58	4.83	2.40	0.827	0.208	(0.744)	0.619	
59	4.92	2.50	0.861	0.208	(0.775)	0.653	
60	5.00	2.60	0.895	0.208	(0.806)	0.688	
61	5.08	3.10	1.068	0.208	(0.961)	0.860	
62	5.17	3.60	1.240	0.208	(1.116)	1.032	
63	5.25	3.90	1.343	0.208	(1.209)	1.136	
64	5.33	4.20	1.446	0.208	(1.302)	1.239	
65	5.42	4.70	1.619	0.208	(1.457)	1.411	
66	5.50	5.60	1.929	0.208	(1.736)	1.721	
67	5.58	1.90	0.654	0.208	(0.589)	0.447	
68	5.67	0.90	0.310	0.208	(0.279)	0.102	
69	5.75	0.60	0.207	(0.208)	0.186	0.021	
70	5.83	0.50	0.172	(0.208)	0.155	0.017	
71	5.92	0.30	0.103	(0.208)	0.093	0.010	
72	6.00	0.20	0.069	(0.208)	0.062	0.007	

(Loss Rate Not Used)

Sum = 100.0 Sum = 20.0

Flood volume = Effective rainfall 1.66(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 1.21(In)
Total soil loss = 0.159(Ac.Ft)
Total rainfall = 2.87(In)
Flood volume = 9545.3 Cubic Feet
Total soil loss = 6915.3 Cubic Feet

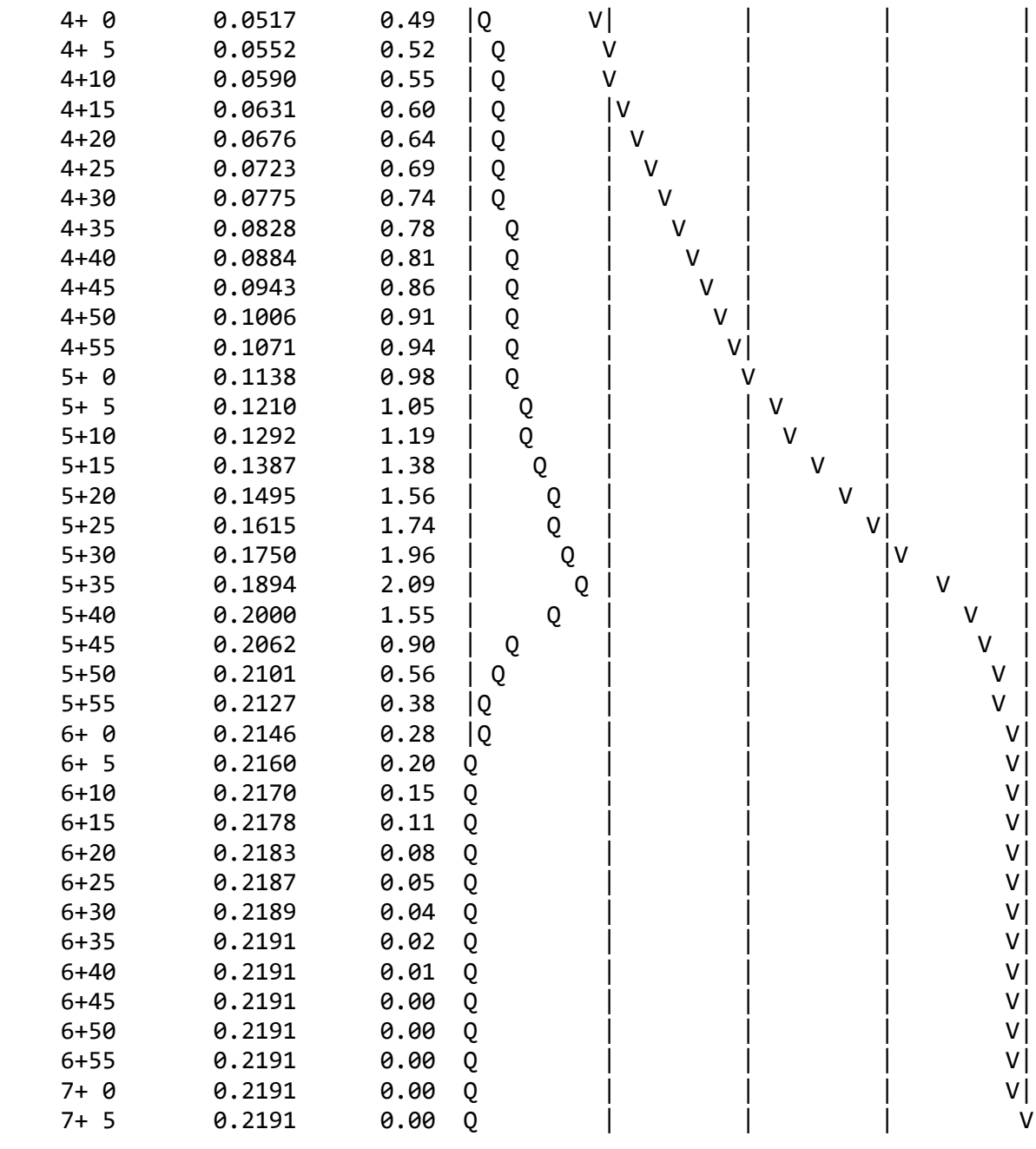
Peak flow rate of this hydrograph = 2.087(CFS)

++

6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.00	Q				
0+10	0.0001	0.01	Q				
0+15	0.0002	0.02	Q				
0+20	0.0004	0.03	Q				
0+25	0.0006	0.03	Q				
0+30	0.0008	0.03	Q				
0+35	0.0011	0.04	Q				
0+40	0.0014	0.05	Q				
0+45	0.0017	0.05	Q				
0+50	0.0021	0.05	Q				
0+55	0.0024	0.05	Q				
1+ 0	0.0028	0.06	Q				
1+ 5	0.0033	0.08	Q				
1+10	0.0039	0.09	Q				
1+15	0.0046	0.10	Q				
1+20	0.0053	0.10	Q				
1+25	0.0060	0.10	QV				
1+30	0.0067	0.10	QV				
1+35	0.0074	0.11	QV				
1+40	0.0082	0.11	QV				
1+45	0.0089	0.11	QV				
1+50	0.0096	0.11	QV				
1+55	0.0104	0.11	QV				
2+ 0	0.0112	0.11	Q V				
2+ 5	0.0120	0.13	Q V				
2+10	0.0129	0.13	Q V				
2+15	0.0139	0.14	Q V				
2+20	0.0149	0.15	Q V				
2+25	0.0159	0.15	Q V				
2+30	0.0170	0.16	Q V				
2+35	0.0181	0.16	Q V				
2+40	0.0192	0.16	Q V				
2+45	0.0204	0.17	Q V				
2+50	0.0216	0.18	Q V				
2+55	0.0230	0.20	Q V				
3+ 0	0.0244	0.21	Q V				
3+ 5	0.0259	0.21	Q V				
3+10	0.0274	0.22	Q V				
3+15	0.0290	0.24	Q V				
3+20	0.0307	0.25	|Q V				
3+25	0.0325	0.26	|Q V				
3+30	0.0345	0.29	|Q V				
3+35	0.0368	0.33	|Q V				
3+40	0.0394	0.37	|Q V				
3+45	0.0422	0.40	|Q V				
3+50	0.0451	0.43	|Q V				
3+55	0.0483	0.46	|Q V				


4+ 0 0.0517 0.49
4+ 5 0.0552 0.52
4+10 0.0590 0.55
4+15 0.0631 0.60
4+20 0.0676 0.64
4+25 0.0723 0.69
4+30 0.0775 0.74
4+35 0.0828 0.78
4+40 0.0884 0.81
4+45 0.0943 0.86
4+50 0.1006 0.91
4+55 0.1071 0.94
5+ 0 0.1138 0.98
5+ 5 0.1210 1.05
5+10 0.1292 1.19
5+15 0.1387 1.38
5+20 0.1495 1.56
5+25 0.1615 1.74
5+30 0.1750 1.96
5+35 0.1894 2.09
5+40 0.2000 1.55
5+45 0.2062 0.90
5+50 0.2101 0.56
5+55 0.2127 0.38
6+ 0 0.2146 0.28
6+ 5 0.2160 0.20
6+10 0.2170 0.15
6+15 0.2178 0.11
6+20 0.2183 0.08
6+25 0.2187 0.05
6+30 0.2189 0.04
6+35 0.2191 0.02
6+40 0.2191 0.01
6+45 0.2191 0.00
6+50 0.2191 0.00
6+55 0.2191 0.00
7+ 0 0.2191 0.00
7+ 5 0.2191 0.00

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/06/22 File: Iris24100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Pre Development
100 YR

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.139 Hr.
Lag time = 8.34 Min.
25% of lag time = 2.09 Min.
40% of lag time = 3.34 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.05	3.24

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	5.25	8.29

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 2.050(In)
Area Averaged 100-Year Rainfall = 5.250(In)

Point rain (area averaged) = 5.250(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 5.250(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.580	67.00	0.000

Total Area Entered = 1.58(Ac.)

RI AMC2	RI AMC-3	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
67.0	83.2	0.208	0.000	0.208	1.000	0.208
					Sum (F) =	0.208

Area averaged mean soil loss (F) (In/Hr) = 0.208
Minimum soil loss rate ((In/Hr)) = 0.104
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	59.952	8.204	0.131
2	0.167	119.904	33.934	0.540
3	0.250	179.856	26.599	0.424
4	0.333	239.808	10.311	0.164
5	0.417	299.760	6.100	0.097
6	0.500	359.712	4.123	0.066
7	0.583	419.664	2.936	0.047
8	0.667	479.616	2.066	0.033
9	0.750	539.568	1.709	0.027
10	0.833	599.520	1.265	0.020
11	0.917	659.472	0.962	0.015
12	1.000	719.424	0.685	0.011
13	1.083	779.376	0.600	0.010

14	1.167	839.329	0.506			0.008
			Sum = 100.000		Sum=	1.592

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.042	(0.368)	0.038	0.004
2	0.17	0.07	0.042	(0.366)	0.038	0.004
3	0.25	0.07	0.042	(0.365)	0.038	0.004
4	0.33	0.10	0.063	(0.364)	0.057	0.006
5	0.42	0.10	0.063	(0.362)	0.057	0.006
6	0.50	0.10	0.063	(0.361)	0.057	0.006
7	0.58	0.10	0.063	(0.359)	0.057	0.006
8	0.67	0.10	0.063	(0.358)	0.057	0.006
9	0.75	0.10	0.063	(0.357)	0.057	0.006
10	0.83	0.13	0.084	(0.355)	0.076	0.008
11	0.92	0.13	0.084	(0.354)	0.076	0.008
12	1.00	0.13	0.084	(0.352)	0.076	0.008
13	1.08	0.10	0.063	(0.351)	0.057	0.006
14	1.17	0.10	0.063	(0.350)	0.057	0.006
15	1.25	0.10	0.063	(0.348)	0.057	0.006
16	1.33	0.10	0.063	(0.347)	0.057	0.006
17	1.42	0.10	0.063	(0.345)	0.057	0.006
18	1.50	0.10	0.063	(0.344)	0.057	0.006
19	1.58	0.10	0.063	(0.343)	0.057	0.006
20	1.67	0.10	0.063	(0.341)	0.057	0.006
21	1.75	0.10	0.063	(0.340)	0.057	0.006
22	1.83	0.13	0.084	(0.339)	0.076	0.008
23	1.92	0.13	0.084	(0.337)	0.076	0.008
24	2.00	0.13	0.084	(0.336)	0.076	0.008
25	2.08	0.13	0.084	(0.334)	0.076	0.008
26	2.17	0.13	0.084	(0.333)	0.076	0.008
27	2.25	0.13	0.084	(0.332)	0.076	0.008
28	2.33	0.13	0.084	(0.330)	0.076	0.008
29	2.42	0.13	0.084	(0.329)	0.076	0.008
30	2.50	0.13	0.084	(0.328)	0.076	0.008
31	2.58	0.17	0.105	(0.326)	0.094	0.010
32	2.67	0.17	0.105	(0.325)	0.094	0.010
33	2.75	0.17	0.105	(0.324)	0.094	0.010
34	2.83	0.17	0.105	(0.322)	0.094	0.010
35	2.92	0.17	0.105	(0.321)	0.094	0.010
36	3.00	0.17	0.105	(0.320)	0.094	0.010
37	3.08	0.17	0.105	(0.318)	0.094	0.010
38	3.17	0.17	0.105	(0.317)	0.094	0.010
39	3.25	0.17	0.105	(0.316)	0.094	0.010
40	3.33	0.17	0.105	(0.314)	0.094	0.010

41	3.42	0.17	0.105	(0.313)	0.094	0.010
42	3.50	0.17	0.105	(0.312)	0.094	0.010
43	3.58	0.17	0.105	(0.311)	0.094	0.010
44	3.67	0.17	0.105	(0.309)	0.094	0.010
45	3.75	0.17	0.105	(0.308)	0.094	0.010
46	3.83	0.20	0.126	(0.307)	0.113	0.013
47	3.92	0.20	0.126	(0.305)	0.113	0.013
48	4.00	0.20	0.126	(0.304)	0.113	0.013
49	4.08	0.20	0.126	(0.303)	0.113	0.013
50	4.17	0.20	0.126	(0.301)	0.113	0.013
51	4.25	0.20	0.126	(0.300)	0.113	0.013
52	4.33	0.23	0.147	(0.299)	0.132	0.015
53	4.42	0.23	0.147	(0.298)	0.132	0.015
54	4.50	0.23	0.147	(0.296)	0.132	0.015
55	4.58	0.23	0.147	(0.295)	0.132	0.015
56	4.67	0.23	0.147	(0.294)	0.132	0.015
57	4.75	0.23	0.147	(0.293)	0.132	0.015
58	4.83	0.27	0.168	(0.291)	0.151	0.017
59	4.92	0.27	0.168	(0.290)	0.151	0.017
60	5.00	0.27	0.168	(0.289)	0.151	0.017
61	5.08	0.20	0.126	(0.288)	0.113	0.013
62	5.17	0.20	0.126	(0.286)	0.113	0.013
63	5.25	0.20	0.126	(0.285)	0.113	0.013
64	5.33	0.23	0.147	(0.284)	0.132	0.015
65	5.42	0.23	0.147	(0.283)	0.132	0.015
66	5.50	0.23	0.147	(0.281)	0.132	0.015
67	5.58	0.27	0.168	(0.280)	0.151	0.017
68	5.67	0.27	0.168	(0.279)	0.151	0.017
69	5.75	0.27	0.168	(0.278)	0.151	0.017
70	5.83	0.27	0.168	(0.276)	0.151	0.017
71	5.92	0.27	0.168	(0.275)	0.151	0.017
72	6.00	0.27	0.168	(0.274)	0.151	0.017
73	6.08	0.30	0.189	(0.273)	0.170	0.019
74	6.17	0.30	0.189	(0.271)	0.170	0.019
75	6.25	0.30	0.189	(0.270)	0.170	0.019
76	6.33	0.30	0.189	(0.269)	0.170	0.019
77	6.42	0.30	0.189	(0.268)	0.170	0.019
78	6.50	0.30	0.189	(0.267)	0.170	0.019
79	6.58	0.33	0.210	(0.265)	0.189	0.021
80	6.67	0.33	0.210	(0.264)	0.189	0.021
81	6.75	0.33	0.210	(0.263)	0.189	0.021
82	6.83	0.33	0.210	(0.262)	0.189	0.021
83	6.92	0.33	0.210	(0.261)	0.189	0.021
84	7.00	0.33	0.210	(0.260)	0.189	0.021
85	7.08	0.33	0.210	(0.258)	0.189	0.021
86	7.17	0.33	0.210	(0.257)	0.189	0.021
87	7.25	0.33	0.210	(0.256)	0.189	0.021
88	7.33	0.37	0.231	(0.255)	0.208	0.023
89	7.42	0.37	0.231	(0.254)	0.208	0.023
90	7.50	0.37	0.231	(0.253)	0.208	0.023

91	7.58	0.40	0.252	(0.251)	0.227	0.025
92	7.67	0.40	0.252	(0.250)	0.227	0.025
93	7.75	0.40	0.252	(0.249)	0.227	0.025
94	7.83	0.43	0.273	(0.248)	0.246	0.027
95	7.92	0.43	0.273	(0.247)	0.246	0.027
96	8.00	0.43	0.273	0.246	(0.246)	0.027
97	8.08	0.50	0.315	0.244	(0.283)	0.071
98	8.17	0.50	0.315	0.243	(0.283)	0.072
99	8.25	0.50	0.315	0.242	(0.283)	0.073
100	8.33	0.50	0.315	0.241	(0.283)	0.074
101	8.42	0.50	0.315	0.240	(0.283)	0.075
102	8.50	0.50	0.315	0.239	(0.283)	0.076
103	8.58	0.53	0.336	0.238	(0.302)	0.098
104	8.67	0.53	0.336	0.237	(0.302)	0.099
105	8.75	0.53	0.336	0.235	(0.302)	0.101
106	8.83	0.57	0.357	0.234	(0.321)	0.123
107	8.92	0.57	0.357	0.233	(0.321)	0.124
108	9.00	0.57	0.357	0.232	(0.321)	0.125
109	9.08	0.63	0.399	0.231	(0.359)	0.168
110	9.17	0.63	0.399	0.230	(0.359)	0.169
111	9.25	0.63	0.399	0.229	(0.359)	0.170
112	9.33	0.67	0.420	0.228	(0.378)	0.192
113	9.42	0.67	0.420	0.227	(0.378)	0.193
114	9.50	0.67	0.420	0.226	(0.378)	0.194
115	9.58	0.70	0.441	0.224	(0.397)	0.217
116	9.67	0.70	0.441	0.223	(0.397)	0.218
117	9.75	0.70	0.441	0.222	(0.397)	0.219
118	9.83	0.73	0.462	0.221	(0.416)	0.241
119	9.92	0.73	0.462	0.220	(0.416)	0.242
120	10.00	0.73	0.462	0.219	(0.416)	0.243
121	10.08	0.50	0.315	0.218	(0.283)	0.097
122	10.17	0.50	0.315	0.217	(0.283)	0.098
123	10.25	0.50	0.315	0.216	(0.283)	0.099
124	10.33	0.50	0.315	0.215	(0.283)	0.100
125	10.42	0.50	0.315	0.214	(0.283)	0.101
126	10.50	0.50	0.315	0.213	(0.283)	0.102
127	10.58	0.67	0.420	0.212	(0.378)	0.208
128	10.67	0.67	0.420	0.211	(0.378)	0.209
129	10.75	0.67	0.420	0.210	(0.378)	0.210
130	10.83	0.67	0.420	0.209	(0.378)	0.211
131	10.92	0.67	0.420	0.208	(0.378)	0.212
132	11.00	0.67	0.420	0.207	(0.378)	0.213
133	11.08	0.63	0.399	0.206	(0.359)	0.193
134	11.17	0.63	0.399	0.205	(0.359)	0.194
135	11.25	0.63	0.399	0.204	(0.359)	0.195
136	11.33	0.63	0.399	0.203	(0.359)	0.196
137	11.42	0.63	0.399	0.202	(0.359)	0.197
138	11.50	0.63	0.399	0.201	(0.359)	0.198
139	11.58	0.57	0.357	0.200	(0.321)	0.157
140	11.67	0.57	0.357	0.199	(0.321)	0.158

141	11.75	0.57	0.357	0.198	(	0.321)	0.159
142	11.83	0.60	0.378	0.197	(	0.340)	0.181
143	11.92	0.60	0.378	0.196	(	0.340)	0.182
144	12.00	0.60	0.378	0.195	(	0.340)	0.183
145	12.08	0.83	0.525	0.194	(	0.472)	0.331
146	12.17	0.83	0.525	0.193	(	0.472)	0.332
147	12.25	0.83	0.525	0.192	(	0.472)	0.333
148	12.33	0.87	0.546	0.191	(	0.491)	0.355
149	12.42	0.87	0.546	0.190	(	0.491)	0.356
150	12.50	0.87	0.546	0.189	(	0.491)	0.357
151	12.58	0.93	0.588	0.188	(	0.529)	0.400
152	12.67	0.93	0.588	0.187	(	0.529)	0.401
153	12.75	0.93	0.588	0.186	(	0.529)	0.402
154	12.83	0.97	0.609	0.185	(	0.548)	0.424
155	12.92	0.97	0.609	0.184	(	0.548)	0.425
156	13.00	0.97	0.609	0.183	(	0.548)	0.426
157	13.08	1.13	0.714	0.182	(	0.643)	0.532
158	13.17	1.13	0.714	0.181	(	0.643)	0.533
159	13.25	1.13	0.714	0.180	(	0.643)	0.534
160	13.33	1.13	0.714	0.180	(	0.643)	0.534
161	13.42	1.13	0.714	0.179	(	0.643)	0.535
162	13.50	1.13	0.714	0.178	(	0.643)	0.536
163	13.58	0.77	0.483	0.177	(	0.435)	0.306
164	13.67	0.77	0.483	0.176	(	0.435)	0.307
165	13.75	0.77	0.483	0.175	(	0.435)	0.308
166	13.83	0.77	0.483	0.174	(	0.435)	0.309
167	13.92	0.77	0.483	0.173	(	0.435)	0.310
168	14.00	0.77	0.483	0.172	(	0.435)	0.311
169	14.08	0.90	0.567	0.171	(	0.510)	0.396
170	14.17	0.90	0.567	0.171	(	0.510)	0.396
171	14.25	0.90	0.567	0.170	(	0.510)	0.397
172	14.33	0.87	0.546	0.169	(	0.491)	0.377
173	14.42	0.87	0.546	0.168	(	0.491)	0.378
174	14.50	0.87	0.546	0.167	(	0.491)	0.379
175	14.58	0.87	0.546	0.166	(	0.491)	0.380
176	14.67	0.87	0.546	0.165	(	0.491)	0.381
177	14.75	0.87	0.546	0.165	(	0.491)	0.381
178	14.83	0.83	0.525	0.164	(	0.472)	0.361
179	14.92	0.83	0.525	0.163	(	0.472)	0.362
180	15.00	0.83	0.525	0.162	(	0.472)	0.363
181	15.08	0.80	0.504	0.161	(	0.454)	0.343
182	15.17	0.80	0.504	0.160	(	0.454)	0.344
183	15.25	0.80	0.504	0.160	(	0.454)	0.344
184	15.33	0.77	0.483	0.159	(	0.435)	0.324
185	15.42	0.77	0.483	0.158	(	0.435)	0.325
186	15.50	0.77	0.483	0.157	(	0.435)	0.326
187	15.58	0.63	0.399	0.156	(	0.359)	0.243
188	15.67	0.63	0.399	0.156	(	0.359)	0.243
189	15.75	0.63	0.399	0.155	(	0.359)	0.244
190	15.83	0.63	0.399	0.154	(	0.359)	0.245

191	15.92	0.63	0.399		0.153	(	0.359)		0.246
192	16.00	0.63	0.399		0.152	(	0.359)		0.247
193	16.08	0.13	0.084	(	0.152)		0.076		0.008
194	16.17	0.13	0.084	(	0.151)		0.076		0.008
195	16.25	0.13	0.084	(	0.150)		0.076		0.008
196	16.33	0.13	0.084	(	0.149)		0.076		0.008
197	16.42	0.13	0.084	(	0.149)		0.076		0.008
198	16.50	0.13	0.084	(	0.148)		0.076		0.008
199	16.58	0.10	0.063	(	0.147)		0.057		0.006
200	16.67	0.10	0.063	(	0.146)		0.057		0.006
201	16.75	0.10	0.063	(	0.146)		0.057		0.006
202	16.83	0.10	0.063	(	0.145)		0.057		0.006
203	16.92	0.10	0.063	(	0.144)		0.057		0.006
204	17.00	0.10	0.063	(	0.143)		0.057		0.006
205	17.08	0.17	0.105	(	0.143)		0.094		0.010
206	17.17	0.17	0.105	(	0.142)		0.094		0.010
207	17.25	0.17	0.105	(	0.141)		0.094		0.010
208	17.33	0.17	0.105	(	0.140)		0.094		0.010
209	17.42	0.17	0.105	(	0.140)		0.094		0.010
210	17.50	0.17	0.105	(	0.139)		0.094		0.010
211	17.58	0.17	0.105	(	0.138)		0.094		0.010
212	17.67	0.17	0.105	(	0.138)		0.094		0.010
213	17.75	0.17	0.105	(	0.137)		0.094		0.010
214	17.83	0.13	0.084	(	0.136)		0.076		0.008
215	17.92	0.13	0.084	(	0.136)		0.076		0.008
216	18.00	0.13	0.084	(	0.135)		0.076		0.008
217	18.08	0.13	0.084	(	0.134)		0.076		0.008
218	18.17	0.13	0.084	(	0.134)		0.076		0.008
219	18.25	0.13	0.084	(	0.133)		0.076		0.008
220	18.33	0.13	0.084	(	0.132)		0.076		0.008
221	18.42	0.13	0.084	(	0.132)		0.076		0.008
222	18.50	0.13	0.084	(	0.131)		0.076		0.008
223	18.58	0.10	0.063	(	0.130)		0.057		0.006
224	18.67	0.10	0.063	(	0.130)		0.057		0.006
225	18.75	0.10	0.063	(	0.129)		0.057		0.006
226	18.83	0.07	0.042	(	0.129)		0.038		0.004
227	18.92	0.07	0.042	(	0.128)		0.038		0.004
228	19.00	0.07	0.042	(	0.127)		0.038		0.004
229	19.08	0.10	0.063	(	0.127)		0.057		0.006
230	19.17	0.10	0.063	(	0.126)		0.057		0.006
231	19.25	0.10	0.063	(	0.126)		0.057		0.006
232	19.33	0.13	0.084	(	0.125)		0.076		0.008
233	19.42	0.13	0.084	(	0.124)		0.076		0.008
234	19.50	0.13	0.084	(	0.124)		0.076		0.008
235	19.58	0.10	0.063	(	0.123)		0.057		0.006
236	19.67	0.10	0.063	(	0.123)		0.057		0.006
237	19.75	0.10	0.063	(	0.122)		0.057		0.006
238	19.83	0.07	0.042	(	0.122)		0.038		0.004
239	19.92	0.07	0.042	(	0.121)		0.038		0.004
240	20.00	0.07	0.042	(	0.121)		0.038		0.004

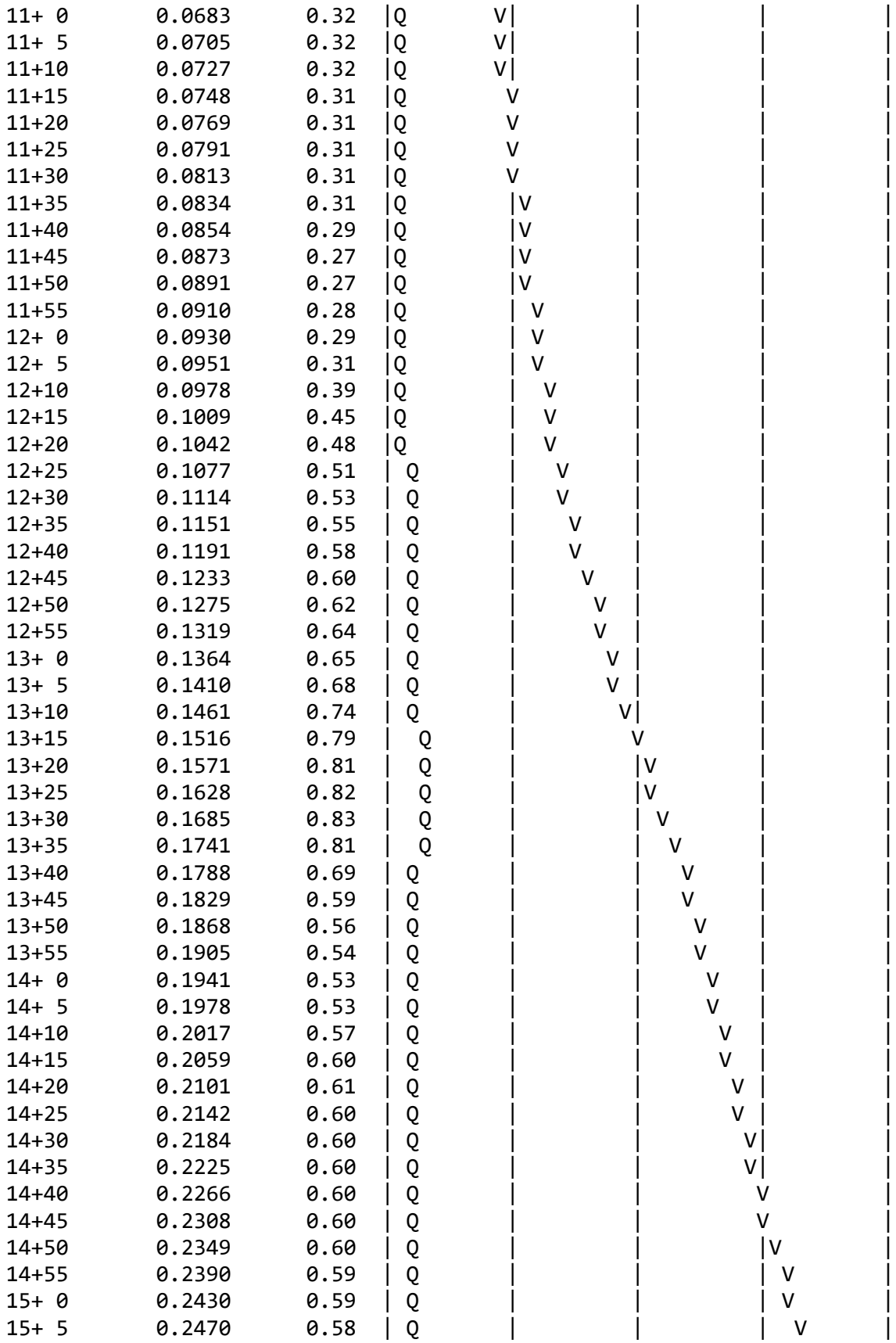
241	20.08	0.10	0.063	(0.120)	0.057	0.006
242	20.17	0.10	0.063	(0.119)	0.057	0.006
243	20.25	0.10	0.063	(0.119)	0.057	0.006
244	20.33	0.10	0.063	(0.118)	0.057	0.006
245	20.42	0.10	0.063	(0.118)	0.057	0.006
246	20.50	0.10	0.063	(0.117)	0.057	0.006
247	20.58	0.10	0.063	(0.117)	0.057	0.006
248	20.67	0.10	0.063	(0.116)	0.057	0.006
249	20.75	0.10	0.063	(0.116)	0.057	0.006
250	20.83	0.07	0.042	(0.115)	0.038	0.004
251	20.92	0.07	0.042	(0.115)	0.038	0.004
252	21.00	0.07	0.042	(0.115)	0.038	0.004
253	21.08	0.10	0.063	(0.114)	0.057	0.006
254	21.17	0.10	0.063	(0.114)	0.057	0.006
255	21.25	0.10	0.063	(0.113)	0.057	0.006
256	21.33	0.07	0.042	(0.113)	0.038	0.004
257	21.42	0.07	0.042	(0.112)	0.038	0.004
258	21.50	0.07	0.042	(0.112)	0.038	0.004
259	21.58	0.10	0.063	(0.112)	0.057	0.006
260	21.67	0.10	0.063	(0.111)	0.057	0.006
261	21.75	0.10	0.063	(0.111)	0.057	0.006
262	21.83	0.07	0.042	(0.110)	0.038	0.004
263	21.92	0.07	0.042	(0.110)	0.038	0.004
264	22.00	0.07	0.042	(0.110)	0.038	0.004
265	22.08	0.10	0.063	(0.109)	0.057	0.006
266	22.17	0.10	0.063	(0.109)	0.057	0.006
267	22.25	0.10	0.063	(0.109)	0.057	0.006
268	22.33	0.07	0.042	(0.108)	0.038	0.004
269	22.42	0.07	0.042	(0.108)	0.038	0.004
270	22.50	0.07	0.042	(0.108)	0.038	0.004
271	22.58	0.07	0.042	(0.107)	0.038	0.004
272	22.67	0.07	0.042	(0.107)	0.038	0.004
273	22.75	0.07	0.042	(0.107)	0.038	0.004
274	22.83	0.07	0.042	(0.106)	0.038	0.004
275	22.92	0.07	0.042	(0.106)	0.038	0.004
276	23.00	0.07	0.042	(0.106)	0.038	0.004
277	23.08	0.07	0.042	(0.106)	0.038	0.004
278	23.17	0.07	0.042	(0.105)	0.038	0.004
279	23.25	0.07	0.042	(0.105)	0.038	0.004
280	23.33	0.07	0.042	(0.105)	0.038	0.004
281	23.42	0.07	0.042	(0.105)	0.038	0.004
282	23.50	0.07	0.042	(0.105)	0.038	0.004
283	23.58	0.07	0.042	(0.104)	0.038	0.004
284	23.67	0.07	0.042	(0.104)	0.038	0.004
285	23.75	0.07	0.042	(0.104)	0.038	0.004
286	23.83	0.07	0.042	(0.104)	0.038	0.004
287	23.92	0.07	0.042	(0.104)	0.038	0.004
288	24.00	0.07	0.042	(0.104)	0.038	0.004
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	27.2

```
      Flood volume = Effective rainfall      2.26(In)
       times area       1.6(Ac.)/[(In)/(Ft.)] =       0.3(Ac.Ft)
      Total soil loss =      2.99(In)
      Total soil loss =     0.393(Ac.Ft)
      Total rainfall =      5.25(In)
      Flood volume =       12977.5 Cubic Feet
      Total soil loss =       17133.3 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.831(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                           24 - H O U R    S T O R M
                      R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0000      0.00  Q         |         |         |         |
  0+10       0.0000      0.00  Q         |         |         |         |
  0+15       0.0001      0.00  Q         |         |         |         |
  0+20       0.0001      0.01  Q         |         |         |         |
  0+25       0.0001      0.01  Q         |         |         |         |
  0+30       0.0002      0.01  Q         |         |         |         |
  0+35       0.0003      0.01  Q         |         |         |         |
  0+40       0.0003      0.01  Q         |         |         |         |
  0+45       0.0004      0.01  Q         |         |         |         |
  0+50       0.0005      0.01  Q         |         |         |         |
  0+55       0.0005      0.01  Q         |         |         |         |
  1+ 0       0.0006      0.01  Q         |         |         |         |
  1+ 5       0.0007      0.01  Q         |         |         |         |
  1+10       0.0008      0.01  Q         |         |         |         |
  1+15       0.0009      0.01  Q         |         |         |         |
  1+20       0.0009      0.01  Q         |         |         |         |
  1+25       0.0010      0.01  Q         |         |         |         |
  1+30       0.0011      0.01  Q         |         |         |         |
  1+35       0.0011      0.01  Q         |         |         |         |
  1+40       0.0012      0.01  Q         |         |         |         |
  1+45       0.0013      0.01  Q         |         |         |         |
  1+50       0.0013      0.01  Q         |         |         |         |
  1+55       0.0014      0.01  Q         |         |         |         |
  2+ 0       0.0015      0.01  Q         |         |         |         |
  2+ 5       0.0016      0.01  Q         |         |         |         |
  2+10       0.0017      0.01  Q         |         |         |         |
  2+15       0.0018      0.01  Q         |         |         |         |
  2+20       0.0019      0.01  Q         |         |         |         |
  2+25       0.0020      0.01  Q         |         |         |         |
  2+30       0.0021      0.01  Q         |         |         |         |
  2+35       0.0021      0.01  Q         |         |         |         |
```

2+40	0.0022	0.01	Q				
2+45	0.0024	0.02	Q				
2+50	0.0025	0.02	Q				
2+55	0.0026	0.02	Q				
3+ 0	0.0027	0.02	Q				
3+ 5	0.0028	0.02	Q				
3+10	0.0029	0.02	Q				
3+15	0.0030	0.02	Q				
3+20	0.0031	0.02	Q				
3+25	0.0033	0.02	Q				
3+30	0.0034	0.02	Q				
3+35	0.0035	0.02	Q				
3+40	0.0036	0.02	Q				
3+45	0.0037	0.02	Q				
3+50	0.0038	0.02	Q				
3+55	0.0040	0.02	Q				
4+ 0	0.0041	0.02	Q				
4+ 5	0.0042	0.02	Q				
4+10	0.0044	0.02	Q				
4+15	0.0045	0.02	Q				
4+20	0.0046	0.02	Q				
4+25	0.0048	0.02	Q				
4+30	0.0049	0.02	Q				
4+35	0.0051	0.02	Q				
4+40	0.0052	0.02	Q				
4+45	0.0054	0.02	Q				
4+50	0.0056	0.02	Q				
4+55	0.0057	0.02	Q				
5+ 0	0.0059	0.03	Q				
5+ 5	0.0061	0.03	Q				
5+10	0.0063	0.02	Q				
5+15	0.0064	0.02	Q				
5+20	0.0065	0.02	Q				
5+25	0.0067	0.02	Q				
5+30	0.0069	0.02	Q				
5+35	0.0070	0.02	Q				
5+40	0.0072	0.02	Q				
5+45	0.0074	0.03	Q				
5+50	0.0075	0.03	QV				
5+55	0.0077	0.03	QV				
6+ 0	0.0079	0.03	QV				
6+ 5	0.0081	0.03	QV				
6+10	0.0083	0.03	QV				
6+15	0.0085	0.03	QV				
6+20	0.0087	0.03	QV				
6+25	0.0089	0.03	QV				
6+30	0.0091	0.03	QV				
6+35	0.0093	0.03	QV				
6+40	0.0095	0.03	QV				
6+45	0.0097	0.03	QV				

6+50	0.0100	0.03	QV	|	|	|	|
6+55	0.0102	0.03	QV	|	|	|	|
7+ 0	0.0104	0.03	QV	|	|	|	|
7+ 5	0.0106	0.03	QV	|	|	|	|
7+10	0.0109	0.03	QV	|	|	|	|
7+15	0.0111	0.03	QV	|	|	|	|
7+20	0.0113	0.03	QV	|	|	|	|
7+25	0.0116	0.03	QV	|	|	|	|
7+30	0.0118	0.04	QV	|	|	|	|
7+35	0.0121	0.04	QV	|	|	|	|
7+40	0.0123	0.04	QV	|	|	|	|
7+45	0.0126	0.04	QV	|	|	|	|
7+50	0.0129	0.04	QV	|	|	|	|
7+55	0.0132	0.04	QV	|	|	|	|
8+ 0	0.0134	0.04	QV	|	|	|	|
8+ 5	0.0138	0.05	QV	|	|	|	|
8+10	0.0143	0.07	QV	|	|	|	|
8+15	0.0149	0.09	Q V	|	|	|	|
8+20	0.0156	0.10	Q V	|	|	|	|
8+25	0.0163	0.11	Q V	|	|	|	|
8+30	0.0171	0.11	Q V	|	|	|	|
8+35	0.0179	0.12	Q V	|	|	|	|
8+40	0.0188	0.13	Q V	|	|	|	|
8+45	0.0198	0.14	Q V	|	|	|	|
8+50	0.0208	0.15	Q V	|	|	|	|
8+55	0.0219	0.17	Q V	|	|	|	|
9+ 0	0.0232	0.18	Q V	|	|	|	|
9+ 5	0.0245	0.19	Q V	|	|	|	|
9+10	0.0260	0.22	Q V	|	|	|	|
9+15	0.0277	0.24	Q V	|	|	|	|
9+20	0.0294	0.25	|Q V	|	|	|	|
9+25	0.0313	0.27	|Q V	|	|	|	|
9+30	0.0333	0.29	|Q V	|	|	|	|
9+35	0.0353	0.30	|Q V	|	|	|	|
9+40	0.0375	0.31	|Q V	|	|	|	|
9+45	0.0397	0.33	|Q V	|	|	|	|
9+50	0.0420	0.34	|Q V	|	|	|	|
9+55	0.0445	0.35	|Q V	|	|	|	|
10+ 0	0.0470	0.37	|Q V	|	|	|	|
10+ 5	0.0494	0.35	|Q V	|	|	|	|
10+10	0.0514	0.28	|Q V	|	|	|	|
10+15	0.0529	0.22	Q V	|	|	|	|
10+20	0.0543	0.20	Q V	|	|	|	|
10+25	0.0556	0.19	Q V	|	|	|	|
10+30	0.0568	0.18	Q V	|	|	|	|
10+35	0.0581	0.19	Q V	|	|	|	|
10+40	0.0598	0.25	Q V	|	|	|	|
10+45	0.0618	0.29	|Q V	|	|	|	|
10+50	0.0639	0.30	|Q V	|	|	|	|
10+55	0.0661	0.31	|Q V	|	|	|	|


11+ 0 0.0683 0.32 |Q V| | | |
11+ 5 0.0705 0.32 |Q V| | | |
11+10 0.0727 0.32 |Q V| | | |
11+15 0.0748 0.31 |Q V | | | |
11+20 0.0769 0.31 |Q V | | | |
11+25 0.0791 0.31 |Q V | | | |
11+30 0.0813 0.31 |Q V | | | |
11+35 0.0834 0.31 |Q |V | | | |
11+40 0.0854 0.29 |Q |V | | | |
11+45 0.0873 0.27 |Q |V | | | |
11+50 0.0891 0.27 |Q |V | | | |
11+55 0.0910 0.28 |Q | V | | | |
12+ 0 0.0930 0.29 |Q | V | | | |
12+ 5 0.0951 0.31 |Q | V | | | |
12+10 0.0978 0.39 |Q | V | | | |
12+15 0.1009 0.45 |Q | V | | | |
12+20 0.1042 0.48 |Q | V | | | |
12+25 0.1077 0.51 | Q | V | | | |
12+30 0.1114 0.53 | Q | V | | | |
12+35 0.1151 0.55 | Q | V | | | |
12+40 0.1191 0.58 | Q | V | | | |
12+45 0.1233 0.60 | Q | V | | | |
12+50 0.1275 0.62 | Q | V | | | |
12+55 0.1319 0.64 | Q | V | | | |
13+ 0 0.1364 0.65 | Q | V | | | |
13+ 5 0.1410 0.68 | Q | V | | | |
13+10 0.1461 0.74 | Q | V| | | |
13+15 0.1516 0.79 | Q | V | | |
13+20 0.1571 0.81 | Q | |V | | |
13+25 0.1628 0.82 | Q | |V | | |
13+30 0.1685 0.83 | Q | | V | | |
13+35 0.1741 0.81 | Q | | V | | |
13+40 0.1788 0.69 | Q | | V | | |
13+45 0.1829 0.59 | Q | | V | | |
13+50 0.1868 0.56 | Q | | V | | |
13+55 0.1905 0.54 | Q | | V | | |
14+ 0 0.1941 0.53 | Q | | V | | |
14+ 5 0.1978 0.53 | Q | | V | | |
14+10 0.2017 0.57 | Q | | V | | |
14+15 0.2059 0.60 | Q | | V | | |
14+20 0.2101 0.61 | Q | | V | | |
14+25 0.2142 0.60 | Q | | V | | |
14+30 0.2184 0.60 | Q | | V| | |
14+35 0.2225 0.60 | Q | | V| | |
14+40 0.2266 0.60 | Q | | V | |
14+45 0.2308 0.60 | Q | | V | |
14+50 0.2349 0.60 | Q | | |V | |
14+55 0.2390 0.59 | Q | | | V | |
15+ 0 0.2430 0.59 | Q | | | V | |
15+ 5 0.2470 0.58 | Q | | | V | |

```
15+10       0.2510      0.57  | Q       |         |         |  V      |
15+15       0.2548      0.56  | Q       |         |         |   V     |
15+20       0.2586      0.55  | Q       |         |         |   V     |
15+25       0.2624      0.54  | Q       |         |         |    V    |
15+30       0.2660      0.53  | Q       |         |         |    V    |
15+35       0.2696      0.52  | Q       |         |         |     V   |
15+40       0.2728      0.47  |Q        |         |         |     V   |
15+45       0.2758      0.43  |Q        |         |         |      V  |
15+50       0.2787      0.42  |Q        |         |         |      V  |
15+55       0.2815      0.41  |Q        |         |         |      V  |
16+ 0       0.2843      0.41  |Q        |         |         |       V |
16+ 5       0.2869      0.37  |Q        |         |         |       V |
16+10       0.2885      0.24  Q         |         |         |       V |
16+15       0.2895      0.14  Q         |         |         |       V |
16+20       0.2901      0.10  Q         |         |         |       V |
16+25       0.2906      0.07  Q         |         |         |        V|
16+30       0.2910      0.06  Q         |         |         |        V|
16+35       0.2913      0.04  Q         |         |         |        V|
16+40       0.2915      0.03  Q         |         |         |        V|
16+45       0.2917      0.03  Q         |         |         |        V|
16+50       0.2918      0.02  Q         |         |         |        V|
16+55       0.2920      0.02  Q         |         |         |        V|
17+ 0       0.2921      0.01  Q         |         |         |        V|
17+ 5       0.2921      0.01  Q         |         |         |        V|
17+10       0.2922      0.01  Q         |         |         |        V|
17+15       0.2923      0.01  Q         |         |         |        V|
17+20       0.2924      0.02  Q         |         |         |        V|
17+25       0.2926      0.02  Q         |         |         |        V|
17+30       0.2927      0.02  Q         |         |         |        V|
17+35       0.2928      0.02  Q         |         |         |        V|
17+40       0.2929      0.02  Q         |         |         |        V|
17+45       0.2930      0.02  Q         |         |         |        V|
17+50       0.2931      0.02  Q         |         |         |        V|
17+55       0.2932      0.02  Q         |         |         |        V|
18+ 0       0.2933      0.01  Q         |         |         |        V|
18+ 5       0.2934      0.01  Q         |         |         |        V|
18+10       0.2935      0.01  Q         |         |         |        V|
18+15       0.2936      0.01  Q         |         |         |        V|
18+20       0.2937      0.01  Q         |         |         |        V|
18+25       0.2938      0.01  Q         |         |         |        V|
18+30       0.2939      0.01  Q         |         |         |        V|
18+35       0.2940      0.01  Q         |         |         |        V|
18+40       0.2941      0.01  Q         |         |         |        V|
18+45       0.2941      0.01  Q         |         |         |        V|
18+50       0.2942      0.01  Q         |         |         |        V|
18+55       0.2943      0.01  Q         |         |         |        V|
19+ 0       0.2943      0.01  Q         |         |         |        V|
19+ 5       0.2944      0.01  Q         |         |         |        V|
19+10       0.2944      0.01  Q         |         |         |        V|
19+15       0.2945      0.01  Q         |         |         |        V|
```

19+20	0.2946	0.01	Q	|	|	|	V|
19+25	0.2947	0.01	Q	|	|	|	V|
19+30	0.2947	0.01	Q	|	|	|	V|
19+35	0.2948	0.01	Q	|	|	|	V|
19+40	0.2949	0.01	Q	|	|	|	V|
19+45	0.2950	0.01	Q	|	|	|	V|
19+50	0.2950	0.01	Q	|	|	|	V|
19+55	0.2951	0.01	Q	|	|	|	V|
20+ 0	0.2952	0.01	Q	|	|	|	V|
20+ 5	0.2952	0.01	Q	|	|	|	V|
20+10	0.2953	0.01	Q	|	|	|	V|
20+15	0.2953	0.01	Q	|	|	|	V|
20+20	0.2954	0.01	Q	|	|	|	V|
20+25	0.2955	0.01	Q	|	|	|	V|
20+30	0.2955	0.01	Q	|	|	|	V|
20+35	0.2956	0.01	Q	|	|	|	V|
20+40	0.2957	0.01	Q	|	|	|	V|
20+45	0.2957	0.01	Q	|	|	|	V|
20+50	0.2958	0.01	Q	|	|	|	V|
20+55	0.2959	0.01	Q	|	|	|	V|
21+ 0	0.2959	0.01	Q	|	|	|	V|
21+ 5	0.2960	0.01	Q	|	|	|	V|
21+10	0.2960	0.01	Q	|	|	|	V|
21+15	0.2961	0.01	Q	|	|	|	V|
21+20	0.2962	0.01	Q	|	|	|	V|
21+25	0.2962	0.01	Q	|	|	|	V|
21+30	0.2963	0.01	Q	|	|	|	V|
21+35	0.2963	0.01	Q	|	|	|	V|
21+40	0.2964	0.01	Q	|	|	|	V|
21+45	0.2964	0.01	Q	|	|	|	V|
21+50	0.2965	0.01	Q	|	|	|	V|
21+55	0.2966	0.01	Q	|	|	|	V|
22+ 0	0.2966	0.01	Q	|	|	|	V|
22+ 5	0.2967	0.01	Q	|	|	|	V|
22+10	0.2967	0.01	Q	|	|	|	V|
22+15	0.2968	0.01	Q	|	|	|	V|
22+20	0.2969	0.01	Q	|	|	|	V|
22+25	0.2969	0.01	Q	|	|	|	V|
22+30	0.2970	0.01	Q	|	|	|	V|
22+35	0.2970	0.01	Q	|	|	|	V|
22+40	0.2971	0.01	Q	|	|	|	V|
22+45	0.2971	0.01	Q	|	|	|	V|
22+50	0.2972	0.01	Q	|	|	|	V|
22+55	0.2972	0.01	Q	|	|	|	V|
23+ 0	0.2973	0.01	Q	|	|	|	V|
23+ 5	0.2973	0.01	Q	|	|	|	V|
23+10	0.2973	0.01	Q	|	|	|	V|
23+15	0.2974	0.01	Q	|	|	|	V|
23+20	0.2974	0.01	Q	|	|	|	V|
23+25	0.2975	0.01	Q	|	|	|	V|

23+30	0.2975	0.01	Q	|	|	|	V|
23+35	0.2976	0.01	Q	|	|	|	V|
23+40	0.2976	0.01	Q	|	|	|	V|
23+45	0.2977	0.01	Q	|	|	|	V|
23+50	0.2977	0.01	Q	|	|	|	V|
23+55	0.2978	0.01	Q	|	|	|	V|
24+ 0	0.2978	0.01	Q	|	|	|	V|
24+ 5	0.2978	0.01	Q	|	|	|	V|
24+10	0.2979	0.00	Q	|	|	|	V|
24+15	0.2979	0.00	Q	|	|	|	V|
24+20	0.2979	0.00	Q	|	|	|	V|
24+25	0.2979	0.00	Q	|	|	|	V|
24+30	0.2979	0.00	Q	|	|	|	V|
24+35	0.2979	0.00	Q	|	|	|	V|
24+40	0.2979	0.00	Q	|	|	|	V|
24+45	0.2979	0.00	Q	|	|	|	V|
24+50	0.2979	0.00	Q	|	|	|	V|
24+55	0.2979	0.00	Q	|	|	|	V|
25+ 0	0.2979	0.00	Q	|	|	|	V|
25+ 5	0.2979	0.00	Q	|	|	|	V|

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris12.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
2 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.49	0.78

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            1.35                  2.13

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    0.493(In)
Area Averaged 100-Year Rainfall =    1.350(In)

Point rain (area averaged) =    0.493(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    0.493(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  16.2      0.870     0.900        0.165       1.000      0.165
                                                 Sum (F) =   0.165
Area averaged mean soil loss (F) (In/Hr) =  0.165
Minimum soil loss rate ((In/Hr)) =  0.083
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5000
------------------------------------------------------------------------

                U n i t  H y d r o g r a p h
                        VALLEY S-Curve
------------------------------------------------------------------------
                Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                              Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.20	0.248	(0.165)	0.045	0.204
2	0.17	4.30	0.254	(0.165)	0.046	0.209
3	0.25	5.00	0.296	(0.165)	0.053	0.243
4	0.33	5.00	0.296	(0.165)	0.053	0.243
5	0.42	5.80	0.343	(0.165)	0.062	0.281
6	0.50	6.50	0.385	(0.165)	0.069	0.315
7	0.58	7.40	0.438	(0.165)	0.079	0.359
8	0.67	8.60	0.509	(0.165)	0.092	0.417
9	0.75	12.30	0.728	(0.165)	0.131	0.597
10	0.83	29.10	1.722	0.165	(0.310)	1.556
11	0.92	6.80	0.402	(0.165)	0.072	0.330
12	1.00	5.00	0.296	(0.165)	0.053	0.243
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.0

Flood volume = Effective rainfall 0.42(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.1(Ac.Ft)
Total soil loss = 0.08(In)
Total soil loss = 0.010(Ac.Ft)
Total rainfall = 0.49(In)
Flood volume = 2387.6 Cubic Feet
Total soil loss = 439.9 Cubic Feet

Peak flow rate of this hydrograph = 1.540(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0004	0.06	Q				
0+10	0.0019	0.22	QV				
0+15	0.0038	0.28	QV				
0+20	0.0061	0.33	Q V				
0+25	0.0086	0.37	Q V				
0+30	0.0115	0.42	Q V				
0+35	0.0148	0.48	Q V				
0+40	0.0185	0.54	Q V				
0+45	0.0231	0.66	Q V				
0+50	0.0307	1.10	Q V				

```
    0+55       0.0413      1.54  |     Q   |         |         V         |
    1+ 0       0.0472      0.85  |  Q      |         |         |   V     |
    1+ 5       0.0508      0.53  | Q       |         |         |      V  |
    1+10       0.0525      0.25  |Q        |         |         |       V |
    1+15       0.0535      0.14  Q         |         |         |        V|
    1+20       0.0541      0.09  Q         |         |         |        V|
    1+25       0.0545      0.05  Q         |         |         |        V|
    1+30       0.0547      0.03  Q         |         |         |        V|
    1+35       0.0548      0.01  Q         |         |         |        V|
    1+40       0.0548      0.00  Q         |         |         |         V
---------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris32.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
2 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.87	1.37

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            2.10                  3.32

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    0.869(In)
Area Averaged 100-Year Rainfall =    2.100(In)

Point rain (area averaged) =    0.869(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    0.869(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  16.2      0.870     0.900        0.165       1.000      0.165
                                                 Sum (F) =   0.165
Area averaged mean soil loss (F) (In/Hr) =  0.165
Minimum soil loss rate ((In/Hr)) =  0.083
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                               Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.136	(0.165)	0.024	0.111
2	0.17	1.30	0.136	(0.165)	0.024	0.111
3	0.25	1.10	0.115	(0.165)	0.021	0.094
4	0.33	1.50	0.156	(0.165)	0.028	0.128
5	0.42	1.50	0.156	(0.165)	0.028	0.128
6	0.50	1.80	0.188	(0.165)	0.034	0.154
7	0.58	1.50	0.156	(0.165)	0.028	0.128
8	0.67	1.80	0.188	(0.165)	0.034	0.154
9	0.75	1.80	0.188	(0.165)	0.034	0.154
10	0.83	1.50	0.156	(0.165)	0.028	0.128
11	0.92	1.60	0.167	(0.165)	0.030	0.137
12	1.00	1.80	0.188	(0.165)	0.034	0.154
13	1.08	2.20	0.229	(0.165)	0.041	0.188
14	1.17	2.20	0.229	(0.165)	0.041	0.188
15	1.25	2.20	0.229	(0.165)	0.041	0.188
16	1.33	2.00	0.209	(0.165)	0.038	0.171
17	1.42	2.60	0.271	(0.165)	0.049	0.222
18	1.50	2.70	0.282	(0.165)	0.051	0.231
19	1.58	2.40	0.250	(0.165)	0.045	0.205
20	1.67	2.70	0.282	(0.165)	0.051	0.231
21	1.75	3.30	0.344	(0.165)	0.062	0.282
22	1.83	3.10	0.323	(0.165)	0.058	0.265
23	1.92	2.90	0.302	(0.165)	0.054	0.248
24	2.00	3.00	0.313	(0.165)	0.056	0.257
25	2.08	3.10	0.323	(0.165)	0.058	0.265
26	2.17	4.20	0.438	(0.165)	0.079	0.359
27	2.25	5.00	0.521	(0.165)	0.094	0.428
28	2.33	3.50	0.365	(0.165)	0.066	0.299
29	2.42	6.80	0.709	(0.165)	0.128	0.581
30	2.50	7.30	0.761	(0.165)	0.137	0.624
31	2.58	8.20	0.855	(0.165)	0.154	0.701
32	2.67	5.90	0.615	(0.165)	0.111	0.505
33	2.75	2.00	0.209	(0.165)	0.038	0.171
34	2.83	1.80	0.188	(0.165)	0.034	0.154
35	2.92	1.80	0.188	(0.165)	0.034	0.154
36	3.00	0.60	0.063	(0.165)	0.011	0.051
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	8.6

Flood volume = Effective rainfall 0.71(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.1(Ac.Ft)
Total soil loss = 0.16(In)
Total soil loss = 0.021(Ac.Ft)
Total rainfall = 0.87(In)
Flood volume = 4086.9 Cubic Feet
Total soil loss = 897.1 Cubic Feet

```
      ------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.966(CFS)
      ------------------------------------------------------------------
      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                         3 - H O U R    S T O R M
                    R u n o f f     H y d r o g r a p h
      ------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-----------------------------------------------------------------------
  0+ 5       0.0002      0.03  Q         |         |         |         |
  0+10       0.0010      0.12  Q         |         |         |         |
  0+15       0.0020      0.14  Q         |         |         |         |
  0+20       0.0030      0.15  QV        |         |         |         |
  0+25       0.0043      0.18  QV        |         |         |         |
  0+30       0.0056      0.20  Q V       |         |         |         |
  0+35       0.0071      0.22  Q  V      |         |         |         |
  0+40       0.0086      0.21  Q  V
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris62.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
2 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	1.22	1.93

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            2.87                   4.53

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    1.220(In)
Area Averaged 100-Year Rainfall =    2.870(In)

Point rain (area averaged) =    1.220(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    1.220(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  16.2      0.870     0.900        0.165       1.000      0.165
                                                 Sum (F) =   0.165
Area averaged mean soil loss (F) (In/Hr) =  0.165
Minimum soil loss rate ((In/Hr)) =  0.083
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                               Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

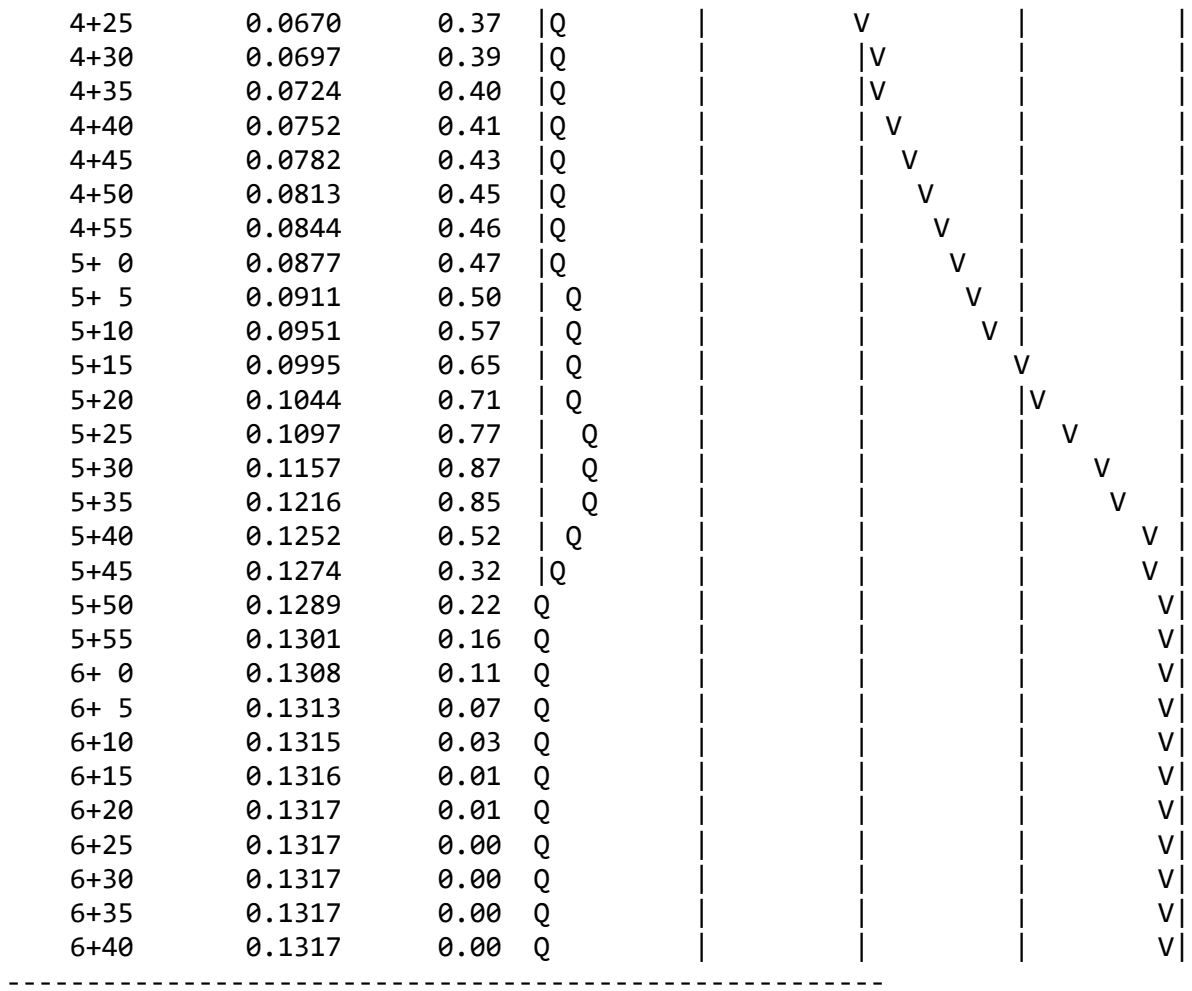
The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.073	(0.165)	0.013	0.060
2	0.17	0.60	0.088	(0.165)	0.016	0.072
3	0.25	0.60	0.088	(0.165)	0.016	0.072
4	0.33	0.60	0.088	(0.165)	0.016	0.072
5	0.42	0.60	0.088	(0.165)	0.016	0.072
6	0.50	0.70	0.102	(0.165)	0.018	0.084
7	0.58	0.70	0.102	(0.165)	0.018	0.084
8	0.67	0.70	0.102	(0.165)	0.018	0.084
9	0.75	0.70	0.102	(0.165)	0.018	0.084
10	0.83	0.70	0.102	(0.165)	0.018	0.084
11	0.92	0.70	0.102	(0.165)	0.018	0.084
12	1.00	0.80	0.117	(0.165)	0.021	0.096
13	1.08	0.80	0.117	(0.165)	0.021	0.096
14	1.17	0.80	0.117	(0.165)	0.021	0.096
15	1.25	0.80	0.117	(0.165)	0.021	0.096
16	1.33	0.80	0.117	(0.165)	0.021	0.096
17	1.42	0.80	0.117	(0.165)	0.021	0.096
18	1.50	0.80	0.117	(0.165)	0.021	0.096
19	1.58	0.80	0.117	(0.165)	0.021	0.096
20	1.67	0.80	0.117	(0.165)	0.021	0.096
21	1.75	0.80	0.117	(0.165)	0.021	0.096
22	1.83	0.80	0.117	(0.165)	0.021	0.096
23	1.92	0.80	0.117	(0.165)	0.021	0.096
24	2.00	0.90	0.132	(0.165)	0.024	0.108
25	2.08	0.80	0.117	(0.165)	0.021	0.096
26	2.17	0.90	0.132	(0.165)	0.024	0.108
27	2.25	0.90	0.132	(0.165)	0.024	0.108
28	2.33	0.90	0.132	(0.165)	0.024	0.108
29	2.42	0.90	0.132	(0.165)	0.024	0.108
30	2.50	0.90	0.132	(0.165)	0.024	0.108
31	2.58	0.90	0.132	(0.165)	0.024	0.108
32	2.67	0.90	0.132	(0.165)	0.024	0.108
33	2.75	1.00	0.146	(0.165)	0.026	0.120
34	2.83	1.00	0.146	(0.165)	0.026	0.120
35	2.92	1.00	0.146	(0.165)	0.026	0.120
36	3.00	1.00	0.146	(0.165)	0.026	0.120
37	3.08	1.00	0.146	(0.165)	0.026	0.120
38	3.17	1.10	0.161	(0.165)	0.029	0.132
39	3.25	1.10	0.161	(0.165)	0.029	0.132
40	3.33	1.10	0.161	(0.165)	0.029	0.132
41	3.42	1.20	0.176	(0.165)	0.032	0.144
42	3.50	1.30	0.190	(0.165)	0.034	0.156
43	3.58	1.40	0.205	(0.165)	0.037	0.168
44	3.67	1.40	0.205	(0.165)	0.037	0.168
45	3.75	1.50	0.220	(0.165)	0.040	0.180

```
46   3.83     1.50      0.220       (  0.165)       0.040        0.180
47   3.92     1.60      0.234       (  0.165)       0.042        0.192
48   4.00     1.60      0.234       (  0.165)       0.042        0.192
49   4.08     1.70      0.249       (  0.165)       0.045        0.204
50   4.17     1.80      0.264       (  0.165)       0.047        0.216
51   4.25     1.90      0.278       (  0.165)       0.050        0.228
52   4.33     2.00      0.293       (  0.165)       0.053        0.240
53   4.42     2.10      0.307       (  0.165)       0.055        0.252
54   4.50     2.10      0.307       (  0.165)       0.055        0.252
55   4.58     2.20      0.322       (  0.165)       0.058        0.264
56   4.67     2.30      0.337       (  0.165)       0.061        0.276
57   4.75     2.40      0.351       (  0.165)       0.063        0.288
58   4.83     2.40      0.351       (  0.165)       0.063        0.288
59   4.92     2.50      0.366       (  0.165)       0.066        0.300
60   5.00     2.60      0.381       (  0.165)       0.069        0.312
61   5.08     3.10      0.454       (  0.165)       0.082        0.372
62   5.17     3.60      0.527       (  0.165)       0.095        0.432
63   5.25     3.90      0.571       (  0.165)       0.103        0.468
64   5.33     4.20      0.615       (  0.165)       0.111        0.504
65   5.42     4.70      0.688       (  0.165)       0.124        0.564
66   5.50     5.60      0.820       (  0.165)       0.148        0.672
67   5.58     1.90      0.278       (  0.165)       0.050        0.228
68   5.67     0.90      0.132       (  0.165)       0.024        0.108
69   5.75     0.60      0.088       (  0.165)       0.016        0.072
70   5.83     0.50      0.073       (  0.165)       0.013        0.060
71   5.92     0.30      0.044       (  0.165)       0.008        0.036
72   6.00     0.20      0.029       (  0.165)       0.005        0.024
               (Loss Rate Not Used)
   Sum =     100.0                                    Sum =    12.0
      Flood volume = Effective rainfall      1.00(In)
       times area       1.6(Ac.)/[(In)/(Ft.)] =       0.1(Ac.Ft)
      Total soil loss =      0.22(In)
      Total soil loss =     0.029(Ac.Ft)
      Total rainfall =      1.22(In)
      Flood volume =        5737.7 Cubic Feet
      Total soil loss =        1259.5 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.871(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0001      0.02  Q         |         |         |         |
  0+10       0.0006      0.07  Q         |         |         |         |
```

```
0+15       0.0012      0.09  Q         |         |         |         |
0+20       0.0019      0.10  Q         |         |         |         |
0+25       0.0026      0.11  Q         |         |         |         |
0+30       0.0034      0.11  QV        |         |         |         |
0+35       0.0043      0.12  QV        |         |         |         |
0+40       0.0052      0.13  QV        |         |         |         |
0+45       0.0061      0.13  QV        |         |         |         |
0+50       0.0070      0.13  Q V       |         |         |         |
0+55       0.0079      0.13  Q V       |         |         |         |
1+ 0       0.0089      0.14  Q V       |         |         |         |
1+ 5       0.0099      0.15  Q V       |         |         |         |
1+10       0.0109      0.15  Q  V      |         |         |         |
1+15       0.0119      0.15  Q  V      |         |         |         |
1+20       0.0130      0.15  Q  V      |         |         |         |
1+25       0.0140      0.15  Q   V     |         |         |         |
1+30       0.0151      0.15  Q   V     |         |         |         |
1+35       0.0161      0.15  Q   V     |         |         |         |
1+40       0.0172      0.15  Q    V    |         |         |         |
1+45       0.0182      0.15  Q    V    |         |         |         |
1+50       0.0193      0.15  Q    V    |         |         |         |
1+55       0.0203      0.15  Q     V   |         |         |         |
2+ 0       0.0214      0.16  Q     V   |         |         |         |
2+ 5       0.0225      0.16  Q     V   |         |         |         |
2+10       0.0236      0.16  Q      V  |         |         |         |
2+15       0.0248      0.17  Q      V  |         |         |         |
2+20       0.0260      0.17  Q      V  |         |         |         |
2+25       0.0271      0.17  Q       V |         |         |         |
2+30       0.0283      0.17  Q       V |         |         |         |
2+35       0.0295      0.17  Q       V |         |         |         |
2+40       0.0307      0.17  Q        V|         |         |         |
2+45       0.0319      0.18  Q        V|         |         |         |
2+50       0.0332      0.18  Q         V         |         |         |
2+55       0.0344      0.19  Q         V         |         |         |
3+ 0       0.0358      0.19  Q         V         |         |         |
3+ 5       0.0371      0.19  Q         |V        |         |         |
3+10       0.0384      0.19  Q         |V        |         |         |
3+15       0.0398      0.20  Q         | V       |         |         |
3+20       0.0412      0.21  Q         | V       |         |         |
3+25       0.0427      0.21  Q         | V       |         |         |
3+30       0.0442      0.23  Q         |  V      |         |         |
3+35       0.0459      0.24  Q         |  V      |         |         |
3+40       0.0477      0.26  |Q        |   V     |         |         |
3+45       0.0495      0.26  |Q        |    V    |         |         |
3+50       0.0514      0.28  |Q        |    V    |         |         |
3+55       0.0533      0.28  |Q        |     V   |         |         |
4+ 0       0.0554      0.30  |Q        |     V   |         |         |
4+ 5       0.0575      0.30  |Q        |      V  |         |         |
4+10       0.0597      0.32  |Q        |       V |         |         |
4+15       0.0620      0.34  |Q        |       V |         |         |
4+20       0.0644      0.35  |Q        |        V|         |         |
```


4+25 0.0670 0.37
4+30 0.0697 0.39
4+35 0.0724 0.40
4+40 0.0752 0.41
4+45 0.0782 0.43
4+50 0.0813 0.45
4+55 0.0844 0.46
5+ 0 0.0877 0.47
5+ 5 0.0911 0.50
5+10 0.0951 0.57
5+15 0.0995 0.65
5+20 0.1044 0.71
5+25 0.1097 0.77
5+30 0.1157 0.87
5+35 0.1216 0.85
5+40 0.1252 0.52
5+45 0.1274 0.32
5+50 0.1289 0.22
5+55 0.1301 0.16
6+ 0 0.1308 0.11
6+ 5 0.1313 0.07
6+10 0.1315 0.03
6+15 0.1316 0.01
6+20 0.1317 0.01
6+25 0.1317 0.00
6+30 0.1317 0.00
6+35 0.1317 0.00
6+40 0.1317 0.00

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris242.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
2 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.05	3.24

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            5.25                   8.29

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    2.050(In)
Area Averaged 100-Year Rainfall =    5.250(In)

Point rain (area averaged) =    2.050(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    2.050(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  16.2      0.870     0.900        0.165       1.000      0.165
                                                 Sum (F) =   0.165
Area averaged mean soil loss (F) (In/Hr) =  0.165
Minimum soil loss rate ((In/Hr)) =  0.083
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                               Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.016	(0.293)	0.003	0.013
2	0.17	0.07	0.016	(0.292)	0.003	0.013
3	0.25	0.07	0.016	(0.291)	0.003	0.013
4	0.33	0.10	0.025	(0.290)	0.004	0.020
5	0.42	0.10	0.025	(0.289)	0.004	0.020
6	0.50	0.10	0.025	(0.288)	0.004	0.020
7	0.58	0.10	0.025	(0.286)	0.004	0.020
8	0.67	0.10	0.025	(0.285)	0.004	0.020
9	0.75	0.10	0.025	(0.284)	0.004	0.020
10	0.83	0.13	0.033	(0.283)	0.006	0.027
11	0.92	0.13	0.033	(0.282)	0.006	0.027
12	1.00	0.13	0.033	(0.281)	0.006	0.027
13	1.08	0.10	0.025	(0.280)	0.004	0.020
14	1.17	0.10	0.025	(0.279)	0.004	0.020
15	1.25	0.10	0.025	(0.277)	0.004	0.020
16	1.33	0.10	0.025	(0.276)	0.004	0.020
17	1.42	0.10	0.025	(0.275)	0.004	0.020
18	1.50	0.10	0.025	(0.274)	0.004	0.020
19	1.58	0.10	0.025	(0.273)	0.004	0.020
20	1.67	0.10	0.025	(0.272)	0.004	0.020
21	1.75	0.10	0.025	(0.271)	0.004	0.020
22	1.83	0.13	0.033	(0.270)	0.006	0.027
23	1.92	0.13	0.033	(0.269)	0.006	0.027
24	2.00	0.13	0.033	(0.268)	0.006	0.027
25	2.08	0.13	0.033	(0.267)	0.006	0.027
26	2.17	0.13	0.033	(0.265)	0.006	0.027
27	2.25	0.13	0.033	(0.264)	0.006	0.027
28	2.33	0.13	0.033	(0.263)	0.006	0.027
29	2.42	0.13	0.033	(0.262)	0.006	0.027
30	2.50	0.13	0.033	(0.261)	0.006	0.027
31	2.58	0.17	0.041	(0.260)	0.007	0.034
32	2.67	0.17	0.041	(0.259)	0.007	0.034
33	2.75	0.17	0.041	(0.258)	0.007	0.034
34	2.83	0.17	0.041	(0.257)	0.007	0.034
35	2.92	0.17	0.041	(0.256)	0.007	0.034
36	3.00	0.17	0.041	(0.255)	0.007	0.034
37	3.08	0.17	0.041	(0.254)	0.007	0.034
38	3.17	0.17	0.041	(0.253)	0.007	0.034
39	3.25	0.17	0.041	(0.252)	0.007	0.034
40	3.33	0.17	0.041	(0.251)	0.007	0.034
41	3.42	0.17	0.041	(0.250)	0.007	0.034
42	3.50	0.17	0.041	(0.249)	0.007	0.034
43	3.58	0.17	0.041	(0.247)	0.007	0.034
44	3.67	0.17	0.041	(0.246)	0.007	0.034
45	3.75	0.17	0.041	(0.245)	0.007	0.034

46	3.83	0.20	0.049	(0.244)	0.009	0.040
47	3.92	0.20	0.049	(0.243)	0.009	0.040
48	4.00	0.20	0.049	(0.242)	0.009	0.040
49	4.08	0.20	0.049	(0.241)	0.009	0.040
50	4.17	0.20	0.049	(0.240)	0.009	0.040
51	4.25	0.20	0.049	(0.239)	0.009	0.040
52	4.33	0.23	0.057	(0.238)	0.010	0.047
53	4.42	0.23	0.057	(0.237)	0.010	0.047
54	4.50	0.23	0.057	(0.236)	0.010	0.047
55	4.58	0.23	0.057	(0.235)	0.010	0.047
56	4.67	0.23	0.057	(0.234)	0.010	0.047
57	4.75	0.23	0.057	(0.233)	0.010	0.047
58	4.83	0.27	0.066	(0.232)	0.012	0.054
59	4.92	0.27	0.066	(0.231)	0.012	0.054
60	5.00	0.27	0.066	(0.230)	0.012	0.054
61	5.08	0.20	0.049	(0.229)	0.009	0.040
62	5.17	0.20	0.049	(0.228)	0.009	0.040
63	5.25	0.20	0.049	(0.227)	0.009	0.040
64	5.33	0.23	0.057	(0.226)	0.010	0.047
65	5.42	0.23	0.057	(0.225)	0.010	0.047
66	5.50	0.23	0.057	(0.224)	0.010	0.047
67	5.58	0.27	0.066	(0.223)	0.012	0.054
68	5.67	0.27	0.066	(0.222)	0.012	0.054
69	5.75	0.27	0.066	(0.221)	0.012	0.054
70	5.83	0.27	0.066	(0.220)	0.012	0.054
71	5.92	0.27	0.066	(0.219)	0.012	0.054
72	6.00	0.27	0.066	(0.218)	0.012	0.054
73	6.08	0.30	0.074	(0.217)	0.013	0.061
74	6.17	0.30	0.074	(0.216)	0.013	0.061
75	6.25	0.30	0.074	(0.215)	0.013	0.061
76	6.33	0.30	0.074	(0.214)	0.013	0.061
77	6.42	0.30	0.074	(0.213)	0.013	0.061
78	6.50	0.30	0.074	(0.213)	0.013	0.061
79	6.58	0.33	0.082	(0.212)	0.015	0.067
80	6.67	0.33	0.082	(0.211)	0.015	0.067
81	6.75	0.33	0.082	(0.210)	0.015	0.067
82	6.83	0.33	0.082	(0.209)	0.015	0.067
83	6.92	0.33	0.082	(0.208)	0.015	0.067
84	7.00	0.33	0.082	(0.207)	0.015	0.067
85	7.08	0.33	0.082	(0.206)	0.015	0.067
86	7.17	0.33	0.082	(0.205)	0.015	0.067
87	7.25	0.33	0.082	(0.204)	0.015	0.067
88	7.33	0.37	0.090	(0.203)	0.016	0.074
89	7.42	0.37	0.090	(0.202)	0.016	0.074
90	7.50	0.37	0.090	(0.201)	0.016	0.074
91	7.58	0.40	0.098	(0.200)	0.018	0.081
92	7.67	0.40	0.098	(0.199)	0.018	0.081
93	7.75	0.40	0.098	(0.198)	0.018	0.081
94	7.83	0.43	0.107	(0.198)	0.019	0.087
95	7.92	0.43	0.107	(0.197)	0.019	0.087

96	8.00	0.43	0.107	(0.196)	0.019	0.087
97	8.08	0.50	0.123	(0.195)	0.022	0.101
98	8.17	0.50	0.123	(0.194)	0.022	0.101
99	8.25	0.50	0.123	(0.193)	0.022	0.101
100	8.33	0.50	0.123	(0.192)	0.022	0.101
101	8.42	0.50	0.123	(0.191)	0.022	0.101
102	8.50	0.50	0.123	(0.190)	0.022	0.101
103	8.58	0.53	0.131	(0.189)	0.024	0.108
104	8.67	0.53	0.131	(0.189)	0.024	0.108
105	8.75	0.53	0.131	(0.188)	0.024	0.108
106	8.83	0.57	0.139	(0.187)	0.025	0.114
107	8.92	0.57	0.139	(0.186)	0.025	0.114
108	9.00	0.57	0.139	(0.185)	0.025	0.114
109	9.08	0.63	0.156	(0.184)	0.028	0.128
110	9.17	0.63	0.156	(0.183)	0.028	0.128
111	9.25	0.63	0.156	(0.182)	0.028	0.128
112	9.33	0.67	0.164	(0.181)	0.030	0.134
113	9.42	0.67	0.164	(0.181)	0.030	0.134
114	9.50	0.67	0.164	(0.180)	0.030	0.134
115	9.58	0.70	0.172	(0.179)	0.031	0.141
116	9.67	0.70	0.172	(0.178)	0.031	0.141
117	9.75	0.70	0.172	(0.177)	0.031	0.141
118	9.83	0.73	0.180	(0.176)	0.032	0.148
119	9.92	0.73	0.180	(0.175)	0.032	0.148
120	10.00	0.73	0.180	(0.175)	0.032	0.148
121	10.08	0.50	0.123	(0.174)	0.022	0.101
122	10.17	0.50	0.123	(0.173)	0.022	0.101
123	10.25	0.50	0.123	(0.172)	0.022	0.101
124	10.33	0.50	0.123	(0.171)	0.022	0.101
125	10.42	0.50	0.123	(0.170)	0.022	0.101
126	10.50	0.50	0.123	(0.170)	0.022	0.101
127	10.58	0.67	0.164	(0.169)	0.030	0.134
128	10.67	0.67	0.164	(0.168)	0.030	0.134
129	10.75	0.67	0.164	(0.167)	0.030	0.134
130	10.83	0.67	0.164	(0.166)	0.030	0.134
131	10.92	0.67	0.164	(0.166)	0.030	0.134
132	11.00	0.67	0.164	(0.165)	0.030	0.134
133	11.08	0.63	0.156	(0.164)	0.028	0.128
134	11.17	0.63	0.156	(0.163)	0.028	0.128
135	11.25	0.63	0.156	(0.162)	0.028	0.128
136	11.33	0.63	0.156	(0.161)	0.028	0.128
137	11.42	0.63	0.156	(0.161)	0.028	0.128
138	11.50	0.63	0.156	(0.160)	0.028	0.128
139	11.58	0.57	0.139	(0.159)	0.025	0.114
140	11.67	0.57	0.139	(0.158)	0.025	0.114
141	11.75	0.57	0.139	(0.157)	0.025	0.114
142	11.83	0.60	0.148	(0.157)	0.027	0.121
143	11.92	0.60	0.148	(0.156)	0.027	0.121
144	12.00	0.60	0.148	(0.155)	0.027	0.121
145	12.08	0.83	0.205	(0.154)	0.037	0.168

146	12.17	0.83	0.205	(0.154)	0.037	0.168
147	12.25	0.83	0.205	(0.153)	0.037	0.168
148	12.33	0.87	0.213	(0.152)	0.038	0.175
149	12.42	0.87	0.213	(0.151)	0.038	0.175
150	12.50	0.87	0.213	(0.151)	0.038	0.175
151	12.58	0.93	0.230	(0.150)	0.041	0.188
152	12.67	0.93	0.230	(0.149)	0.041	0.188
153	12.75	0.93	0.230	(0.148)	0.041	0.188
154	12.83	0.97	0.238	(0.148)	0.043	0.195
155	12.92	0.97	0.238	(0.147)	0.043	0.195
156	13.00	0.97	0.238	(0.146)	0.043	0.195
157	13.08	1.13	0.279	(0.145)	0.050	0.229
158	13.17	1.13	0.279	(0.145)	0.050	0.229
159	13.25	1.13	0.279	(0.144)	0.050	0.229
160	13.33	1.13	0.279	(0.143)	0.050	0.229
161	13.42	1.13	0.279	(0.142)	0.050	0.229
162	13.50	1.13	0.279	(0.142)	0.050	0.229
163	13.58	0.77	0.189	(0.141)	0.034	0.155
164	13.67	0.77	0.189	(0.140)	0.034	0.155
165	13.75	0.77	0.189	(0.139)	0.034	0.155
166	13.83	0.77	0.189	(0.139)	0.034	0.155
167	13.92	0.77	0.189	(0.138)	0.034	0.155
168	14.00	0.77	0.189	(0.137)	0.034	0.155
169	14.08	0.90	0.221	(0.137)	0.040	0.182
170	14.17	0.90	0.221	(0.136)	0.040	0.182
171	14.25	0.90	0.221	(0.135)	0.040	0.182
172	14.33	0.87	0.213	(0.135)	0.038	0.175
173	14.42	0.87	0.213	(0.134)	0.038	0.175
174	14.50	0.87	0.213	(0.133)	0.038	0.175
175	14.58	0.87	0.213	(0.133)	0.038	0.175
176	14.67	0.87	0.213	(0.132)	0.038	0.175
177	14.75	0.87	0.213	(0.131)	0.038	0.175
178	14.83	0.83	0.205	(0.130)	0.037	0.168
179	14.92	0.83	0.205	(0.130)	0.037	0.168
180	15.00	0.83	0.205	(0.129)	0.037	0.168
181	15.08	0.80	0.197	(0.129)	0.035	0.161
182	15.17	0.80	0.197	(0.128)	0.035	0.161
183	15.25	0.80	0.197	(0.127)	0.035	0.161
184	15.33	0.77	0.189	(0.127)	0.034	0.155
185	15.42	0.77	0.189	(0.126)	0.034	0.155
186	15.50	0.77	0.189	(0.125)	0.034	0.155
187	15.58	0.63	0.156	(0.125)	0.028	0.128
188	15.67	0.63	0.156	(0.124)	0.028	0.128
189	15.75	0.63	0.156	(0.123)	0.028	0.128
190	15.83	0.63	0.156	(0.123)	0.028	0.128
191	15.92	0.63	0.156	(0.122)	0.028	0.128
192	16.00	0.63	0.156	(0.121)	0.028	0.128
193	16.08	0.13	0.033	(0.121)	0.006	0.027
194	16.17	0.13	0.033	(0.120)	0.006	0.027
195	16.25	0.13	0.033	(0.120)	0.006	0.027

196	16.33	0.13	0.033	(0.119)	0.006	0.027
197	16.42	0.13	0.033	(0.118)	0.006	0.027
198	16.50	0.13	0.033	(0.118)	0.006	0.027
199	16.58	0.10	0.025	(0.117)	0.004	0.020
200	16.67	0.10	0.025	(0.117)	0.004	0.020
201	16.75	0.10	0.025	(0.116)	0.004	0.020
202	16.83	0.10	0.025	(0.115)	0.004	0.020
203	16.92	0.10	0.025	(0.115)	0.004	0.020
204	17.00	0.10	0.025	(0.114)	0.004	0.020
205	17.08	0.17	0.041	(0.114)	0.007	0.034
206	17.17	0.17	0.041	(0.113)	0.007	0.034
207	17.25	0.17	0.041	(0.113)	0.007	0.034
208	17.33	0.17	0.041	(0.112)	0.007	0.034
209	17.42	0.17	0.041	(0.111)	0.007	0.034
210	17.50	0.17	0.041	(0.111)	0.007	0.034
211	17.58	0.17	0.041	(0.110)	0.007	0.034
212	17.67	0.17	0.041	(0.110)	0.007	0.034
213	17.75	0.17	0.041	(0.109)	0.007	0.034
214	17.83	0.13	0.033	(0.109)	0.006	0.027
215	17.92	0.13	0.033	(0.108)	0.006	0.027
216	18.00	0.13	0.033	(0.108)	0.006	0.027
217	18.08	0.13	0.033	(0.107)	0.006	0.027
218	18.17	0.13	0.033	(0.107)	0.006	0.027
219	18.25	0.13	0.033	(0.106)	0.006	0.027
220	18.33	0.13	0.033	(0.105)	0.006	0.027
221	18.42	0.13	0.033	(0.105)	0.006	0.027
222	18.50	0.13	0.033	(0.104)	0.006	0.027
223	18.58	0.10	0.025	(0.104)	0.004	0.020
224	18.67	0.10	0.025	(0.103)	0.004	0.020
225	18.75	0.10	0.025	(0.103)	0.004	0.020
226	18.83	0.07	0.016	(0.102)	0.003	0.013
227	18.92	0.07	0.016	(0.102)	0.003	0.013
228	19.00	0.07	0.016	(0.101)	0.003	0.013
229	19.08	0.10	0.025	(0.101)	0.004	0.020
230	19.17	0.10	0.025	(0.101)	0.004	0.020
231	19.25	0.10	0.025	(0.100)	0.004	0.020
232	19.33	0.13	0.033	(0.100)	0.006	0.027
233	19.42	0.13	0.033	(0.099)	0.006	0.027
234	19.50	0.13	0.033	(0.099)	0.006	0.027
235	19.58	0.10	0.025	(0.098)	0.004	0.020
236	19.67	0.10	0.025	(0.098)	0.004	0.020
237	19.75	0.10	0.025	(0.097)	0.004	0.020
238	19.83	0.07	0.016	(0.097)	0.003	0.013
239	19.92	0.07	0.016	(0.096)	0.003	0.013
240	20.00	0.07	0.016	(0.096)	0.003	0.013
241	20.08	0.10	0.025	(0.096)	0.004	0.020
242	20.17	0.10	0.025	(0.095)	0.004	0.020
243	20.25	0.10	0.025	(0.095)	0.004	0.020
244	20.33	0.10	0.025	(0.094)	0.004	0.020
245	20.42	0.10	0.025	(0.094)	0.004	0.020

246	20.50	0.10	0.025	(0.094)	0.004	0.020
247	20.58	0.10	0.025	(0.093)	0.004	0.020
248	20.67	0.10	0.025	(0.093)	0.004	0.020
249	20.75	0.10	0.025	(0.092)	0.004	0.020
250	20.83	0.07	0.016	(0.092)	0.003	0.013
251	20.92	0.07	0.016	(0.092)	0.003	0.013
252	21.00	0.07	0.016	(0.091)	0.003	0.013
253	21.08	0.10	0.025	(0.091)	0.004	0.020
254	21.17	0.10	0.025	(0.091)	0.004	0.020
255	21.25	0.10	0.025	(0.090)	0.004	0.020
256	21.33	0.07	0.016	(0.090)	0.003	0.013
257	21.42	0.07	0.016	(0.090)	0.003	0.013
258	21.50	0.07	0.016	(0.089)	0.003	0.013
259	21.58	0.10	0.025	(0.089)	0.004	0.020
260	21.67	0.10	0.025	(0.089)	0.004	0.020
261	21.75	0.10	0.025	(0.088)	0.004	0.020
262	21.83	0.07	0.016	(0.088)	0.003	0.013
263	21.92	0.07	0.016	(0.088)	0.003	0.013
264	22.00	0.07	0.016	(0.087)	0.003	0.013
265	22.08	0.10	0.025	(0.087)	0.004	0.020
266	22.17	0.10	0.025	(0.087)	0.004	0.020
267	22.25	0.10	0.025	(0.086)	0.004	0.020
268	22.33	0.07	0.016	(0.086)	0.003	0.013
269	22.42	0.07	0.016	(0.086)	0.003	0.013
270	22.50	0.07	0.016	(0.086)	0.003	0.013
271	22.58	0.07	0.016	(0.085)	0.003	0.013
272	22.67	0.07	0.016	(0.085)	0.003	0.013
273	22.75	0.07	0.016	(0.085)	0.003	0.013
274	22.83	0.07	0.016	(0.085)	0.003	0.013
275	22.92	0.07	0.016	(0.085)	0.003	0.013
276	23.00	0.07	0.016	(0.084)	0.003	0.013
277	23.08	0.07	0.016	(0.084)	0.003	0.013
278	23.17	0.07	0.016	(0.084)	0.003	0.013
279	23.25	0.07	0.016	(0.084)	0.003	0.013
280	23.33	0.07	0.016	(0.084)	0.003	0.013
281	23.42	0.07	0.016	(0.083)	0.003	0.013
282	23.50	0.07	0.016	(0.083)	0.003	0.013
283	23.58	0.07	0.016	(0.083)	0.003	0.013
284	23.67	0.07	0.016	(0.083)	0.003	0.013
285	23.75	0.07	0.016	(0.083)	0.003	0.013
286	23.83	0.07	0.016	(0.083)	0.003	0.013
287	23.92	0.07	0.016	(0.083)	0.003	0.013
288	24.00	0.07	0.016	(0.083)	0.003	0.013

(Loss Rate Not Used)

Sum = 100.0 Sum = 20.2

Flood volume = Effective rainfall 1.68(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 0.37(In)
Total soil loss = 0.049(Ac.Ft)
Total rainfall = 2.05(In)

Flood volume = 9641.2 Cubic Feet
Total soil loss = 2116.4 Cubic Feet

Peak flow rate of this hydrograph = 0.362(CFS)

++

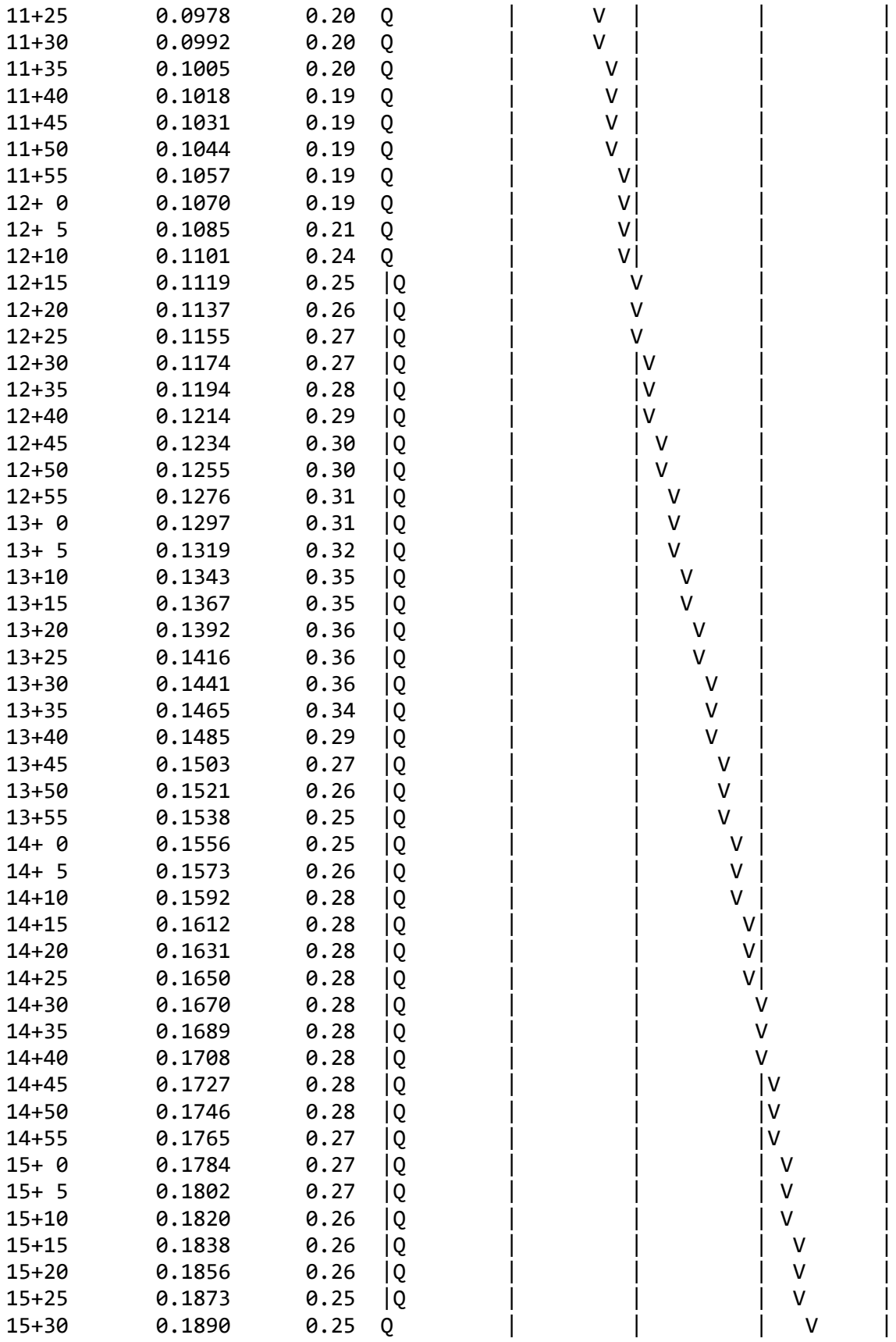
24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.00	Q				
0+10	0.0001	0.01	Q				
0+15	0.0002	0.02	Q				
0+20	0.0004	0.02	Q				
0+25	0.0006	0.03	Q				
0+30	0.0008	0.03	Q				
0+35	0.0010	0.03	Q				
0+40	0.0012	0.03	Q				
0+45	0.0014	0.03	Q				
0+50	0.0017	0.03	Q				
0+55	0.0019	0.04	Q				
1+ 0	0.0022	0.04	Q				
1+ 5	0.0025	0.04	Q				
1+10	0.0027	0.04	Q				
1+15	0.0030	0.03	Q				
1+20	0.0032	0.03	Q				
1+25	0.0034	0.03	Q				
1+30	0.0036	0.03	Q				
1+35	0.0039	0.03	Q				
1+40	0.0041	0.03	Q				
1+45	0.0043	0.03	Q				
1+50	0.0045	0.03	Q				
1+55	0.0048	0.04	Q				
2+ 0	0.0051	0.04	Q				
2+ 5	0.0054	0.04	Q				
2+10	0.0057	0.04	QV				
2+15	0.0060	0.04	QV				
2+20	0.0063	0.04	QV				
2+25	0.0065	0.04	QV				
2+30	0.0068	0.04	QV				
2+35	0.0071	0.04	QV				
2+40	0.0075	0.05	QV				
2+45	0.0078	0.05	QV				
2+50	0.0082	0.05	QV				
2+55	0.0086	0.05	QV				
3+ 0	0.0089	0.05	QV				

3+ 5	0.0093	0.05	QV	|	|	|	|
3+10	0.0097	0.05	QV	|	|	|	|
3+15	0.0100	0.05	QV	|	|	|	|
3+20	0.0104	0.05	QV	|	|	|	|
3+25	0.0108	0.05	QV	|	|	|	|
3+30	0.0112	0.05	Q V	|	|	|	|
3+35	0.0115	0.05	Q V	|	|	|	|
3+40	0.0119	0.05	Q V	|	|	|	|
3+45	0.0123	0.05	Q V	|	|	|	|
3+50	0.0126	0.06	Q V	|	|	|	|
3+55	0.0131	0.06	Q V	|	|	|	|
4+ 0	0.0135	0.06	Q V	|	|	|	|
4+ 5	0.0139	0.06	Q V	|	|	|	|
4+10	0.0144	0.06	Q V	|	|	|	|
4+15	0.0148	0.06	Q V	|	|	|	|
4+20	0.0153	0.07	Q V	|	|	|	|
4+25	0.0157	0.07	Q V	|	|	|	|
4+30	0.0162	0.07	Q V	|	|	|	|
4+35	0.0168	0.07	Q V	|	|	|	|
4+40	0.0173	0.07	Q V	|	|	|	|
4+45	0.0178	0.07	Q V	|	|	|	|
4+50	0.0183	0.08	Q V	|	|	|	|
4+55	0.0189	0.08	Q V	|	|	|	|
5+ 0	0.0195	0.08	Q V	|	|	|	|
5+ 5	0.0200	0.08	Q V	|	|	|	|
5+10	0.0205	0.07	Q V	|	|	|	|
5+15	0.0210	0.07	Q V	|	|	|	|
5+20	0.0214	0.07	Q V	|	|	|	|
5+25	0.0219	0.07	Q V	|	|	|	|
5+30	0.0224	0.07	Q V	|	|	|	|
5+35	0.0230	0.08	Q V	|	|	|	|
5+40	0.0235	0.08	Q V	|	|	|	|
5+45	0.0241	0.08	Q V	|	|	|	|
5+50	0.0247	0.08	Q V	|	|	|	|
5+55	0.0253	0.08	Q V	|	|	|	|
6+ 0	0.0259	0.09	Q V	|	|	|	|
6+ 5	0.0265	0.09	Q V	|	|	|	|
6+10	0.0271	0.09	Q V	|	|	|	|
6+15	0.0277	0.09	Q V	|	|	|	|
6+20	0.0284	0.10	Q V	|	|	|	|
6+25	0.0291	0.10	Q V	|	|	|	|
6+30	0.0297	0.10	Q V	|	|	|	|
6+35	0.0304	0.10	Q V	|	|	|	|
6+40	0.0311	0.10	Q V	|	|	|	|
6+45	0.0318	0.11	Q V	|	|	|	|
6+50	0.0326	0.11	Q V	|	|	|	|
6+55	0.0333	0.11	Q V	|	|	|	|
7+ 0	0.0340	0.11	Q V	|	|	|	|
7+ 5	0.0348	0.11	Q V	|	|	|	|
7+10	0.0355	0.11	Q V	|	|	|	|

7+15	0.0362	0.11	Q	V	|	|	|	|
7+20	0.0370	0.11	Q	V	|	|	|	|
7+25	0.0378	0.11	Q	V	|	|	|	|
7+30	0.0386	0.12	Q	V	|	|	|	|
7+35	0.0394	0.12	Q	V	|	|	|	|
7+40	0.0403	0.12	Q	V	|	|	|	|
7+45	0.0411	0.13	Q	V	|	|	|	|
7+50	0.0420	0.13	Q	V	|	|	|	|
7+55	0.0429	0.13	Q	V	|	|	|	|
8+ 0	0.0439	0.14	Q	V	|	|	|	|
8+ 5	0.0449	0.14	Q	V	|	|	|	|
8+10	0.0459	0.15	Q	V	|	|	|	|
8+15	0.0470	0.16	Q	V	|	|	|	|
8+20	0.0481	0.16	Q	V	|	|	|	|
8+25	0.0492	0.16	Q	V	|	|	|	|
8+30	0.0503	0.16	Q	V	|	|	|	|
8+35	0.0514	0.16	Q	V	|	|	|	|
8+40	0.0526	0.17	Q	V	|	|	|	|
8+45	0.0537	0.17	Q	V	|	|	|	|
8+50	0.0549	0.17	Q	V	|	|	|	|
8+55	0.0561	0.18	Q	V	|	|	|	|
9+ 0	0.0574	0.18	Q	V	|	|	|	|
9+ 5	0.0586	0.18	Q	V	|	|	|	|
9+10	0.0600	0.20	Q	V	|	|	|	|
9+15	0.0614	0.20	Q	V	|	|	|	|
9+20	0.0628	0.20	Q	V	|	|	|	|
9+25	0.0642	0.21	Q	V	|	|	|	|
9+30	0.0657	0.21	Q	V	|	|	|	|
9+35	0.0671	0.21	Q	V	|	|	|	|
9+40	0.0687	0.22	Q	V	|	|	|	|
9+45	0.0702	0.22	Q	V	|	|	|	|
9+50	0.0717	0.23	Q	V	|	|	|	|
9+55	0.0733	0.23	Q	V	|	|	|	|
10+ 0	0.0749	0.23	Q	V	|	|	|	|
10+ 5	0.0765	0.22	Q	V	|	|	|	|
10+10	0.0777	0.19	Q	V	|	|	|	|
10+15	0.0789	0.17	Q	V	|	|	|	|
10+20	0.0801	0.17	Q	V	|	|	|	|
10+25	0.0812	0.17	Q	V	|	|	|	|
10+30	0.0824	0.16	Q	V	|	|	|	|
10+35	0.0835	0.17	Q	V	|	|	|	|
10+40	0.0849	0.20	Q	V	|	|	|	|
10+45	0.0863	0.20	Q	V	|	|	|	|
10+50	0.0877	0.21	Q	V	|	|	|	|
10+55	0.0892	0.21	Q	V	|	|	|	|
11+ 0	0.0907	0.21	Q	V	|	|	|	|
11+ 5	0.0921	0.21	Q	V	|	|	|	|
11+10	0.0935	0.21	Q	V	|	|	|	|
11+15	0.0949	0.21	Q	V	|	|	|	|
11+20	0.0964	0.20	Q	V	|	|	|	|



15+35	0.1906	0.24	Q	|	|	|	V |
15+40	0.1922	0.22	Q	|	|	|	V |
15+45	0.1936	0.21	Q	|	|	|	V |
15+50	0.1950	0.21	Q	|	|	|	V |
15+55	0.1965	0.21	Q	|	|	|	V |
16+ 0	0.1979	0.21	Q	|	|	|	V |
16+ 5	0.1991	0.18	Q	|	|	|	V |
16+10	0.1998	0.10	Q	|	|	|	V |
16+15	0.2002	0.07	Q	|	|	|	V |
16+20	0.2007	0.06	Q	|	|	|	V |
16+25	0.2010	0.05	Q	|	|	|	V |
16+30	0.2014	0.05	Q	|	|	|	V |
16+35	0.2017	0.04	Q	|	|	|	V |
16+40	0.2019	0.04	Q	|	|	|	V |
16+45	0.2022	0.03	Q	|	|	|	V |
16+50	0.2024	0.03	Q	|	|	|	V |
16+55	0.2026	0.03	Q	|	|	|	V |
17+ 0	0.2028	0.03	Q	|	|	|	V |
17+ 5	0.2031	0.04	Q	|	|	|	V |
17+10	0.2034	0.05	Q	|	|	|	V |
17+15	0.2037	0.05	Q	|	|	|	V |
17+20	0.2041	0.05	Q	|	|	|	V |
17+25	0.2045	0.05	Q	|	|	|	V |
17+30	0.2048	0.05	Q	|	|	|	V |
17+35	0.2052	0.05	Q	|	|	|	V |
17+40	0.2056	0.05	Q	|	|	|	V |
17+45	0.2059	0.05	Q	|	|	|	V |
17+50	0.2063	0.05	Q	|	|	|	V |
17+55	0.2066	0.05	Q	|	|	|	V |
18+ 0	0.2069	0.04	Q	|	|	|	V |
18+ 5	0.2072	0.04	Q	|	|	|	V |
18+10	0.2075	0.04	Q	|	|	|	V |
18+15	0.2078	0.04	Q	|	|	|	V |
18+20	0.2081	0.04	Q	|	|	|	V |
18+25	0.2084	0.04	Q	|	|	|	V |
18+30	0.2087	0.04	Q	|	|	|	V |
18+35	0.2090	0.04	Q	|	|	|	V |
18+40	0.2092	0.04	Q	|	|	|	V |
18+45	0.2095	0.03	Q	|	|	|	V |
18+50	0.2097	0.03	Q	|	|	|	V |
18+55	0.2099	0.03	Q	|	|	|	V |
19+ 0	0.2100	0.02	Q	|	|	|	V |
19+ 5	0.2102	0.02	Q	|	|	|	V |
19+10	0.2104	0.03	Q	|	|	|	V |
19+15	0.2106	0.03	Q	|	|	|	V |
19+20	0.2108	0.03	Q	|	|	|	V |
19+25	0.2111	0.04	Q	|	|	|	V |
19+30	0.2114	0.04	Q	|	|	|	V |
19+35	0.2116	0.04	Q	|	|	|	V |
19+40	0.2119	0.04	Q	|	|	|	V |

```
19+45       0.2121      0.03  Q         |          |          |        V |
19+50       0.2123      0.03  Q         |          |          |        V |
19+55       0.2125      0.03  Q         |          |          |        V |
20+ 0       0.2127      0.02  Q         |          |          |        V |
20+ 5       0.2128      0.02  Q         |          |          |        V |
20+10       0.2130      0.03  Q         |          |          |        V |
20+15       0.2133      0.03  Q         |          |          |        V |
20+20       0.2135      0.03  Q         |          |          |        V |
20+25       0.2137      0.03  Q         |          |          |        V |
20+30       0.2139      0.03  Q         |          |          |        V |
20+35       0.2141      0.03  Q         |          |          |        V |
20+40       0.2143      0.03  Q         |          |          |        V |
20+45       0.2146      0.03  Q         |          |          |        V |
20+50       0.2148      0.03  Q         |          |          |        V |
20+55       0.2149      0.03  Q         |          |          |        V |
21+ 0       0.2151      0.02  Q         |          |          |        V |
21+ 5       0.2153      0.02  Q         |          |          |        V |
21+10       0.2155      0.03  Q         |          |          |        V |
21+15       0.2157      0.03  Q         |          |          |        V |
21+20       0.2159      0.03  Q         |          |          |         V|
21+25       0.2161      0.02  Q         |          |          |         V|
21+30       0.2162      0.02  Q         |          |          |         V|
21+35       0.2164      0.02  Q         |          |          |         V|
21+40       0.2166      0.03  Q         |          |          |         V|
21+45       0.2168      0.03  Q         |          |          |         V|
21+50       0.2170      0.03  Q         |          |          |         V|
21+55       0.2172      0.02  Q         |          |          |         V|
22+ 0       0.2173      0.02  Q         |          |          |         V|
22+ 5       0.2175      0.02  Q         |          |          |         V|
22+10       0.2177      0.03  Q         |          |          |         V|
22+15       0.2179      0.03  Q         |          |          |         V|
22+20       0.2181      0.03  Q         |          |          |         V|
22+25       0.2183      0.02  Q         |          |          |         V|
22+30       0.2184      0.02  Q         |          |          |         V|
22+35       0.2186      0.02  Q         |          |          |         V|
22+40       0.2187      0.02  Q         |          |          |         V|
22+45       0.2189      0.02  Q         |          |          |         V|
22+50       0.2190      0.02  Q         |          |          |         V|
22+55       0.2192      0.02  Q         |          |          |         V|
23+ 0       0.2193      0.02  Q         |          |          |         V|
23+ 5       0.2195      0.02  Q         |          |          |         V|
23+10       0.2196      0.02  Q         |          |          |         V|
23+15       0.2198      0.02  Q         |          |          |         V|
23+20       0.2199      0.02  Q         |          |          |         V|
23+25       0.2201      0.02  Q         |          |          |         V|
23+30       0.2202      0.02  Q         |          |          |         V|
23+35       0.2204      0.02  Q         |          |          |         V|
23+40       0.2205      0.02  Q         |          |          |         V|
23+45       0.2207      0.02  Q         |          |          |         V|
23+50       0.2208      0.02  Q         |          |          |         V|
```

```
   23+55       0.2210      0.02  Q         |          |          |         V|
   24+ 0       0.2211      0.02  Q         |          |          |         V|
   24+ 5       0.2212      0.02  Q         |          |          |         V|
   24+10       0.2213      0.01  Q         |          |          |         V|
   24+15       0.2213      0.00  Q         |          |          |         V|
   24+20       0.2213      0.00  Q         |          |          |         V|
   24+25       0.2213      0.00  Q         |          |          |         V|
   24+30       0.2213      0.00  Q         |          |          |         V|
   24+35       0.2213      0.00  Q         |          |          |         V|
   24+40       0.2213      0.00  Q         |          |          |          V
-------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris15.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
5 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.49	0.78

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            1.35                  2.13

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.493(In)
Area Averaged 100-Year Rainfall =    1.350(In)

Point rain (area averaged) =    0.694(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    0.694(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  16.2      0.870     0.900        0.165       1.000      0.165
                                                 Sum (F) =   0.165
Area averaged mean soil loss (F) (In/Hr) =  0.165
Minimum soil loss rate ((In/Hr)) =  0.083
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5000
------------------------------------------------------------------------

                U n i t  H y d r o g r a p h
                        VALLEY S-Curve
-------------------------------------------------------------------
                Unit Hydrograph Data
-------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
-------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                              Sum = 100.000   Sum=       1.592
-------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.20	0.350	(0.165)	0.063	0.287
2	0.17	4.30	0.358	(0.165)	0.064	0.294
3	0.25	5.00	0.416	(0.165)	0.075	0.341
4	0.33	5.00	0.416	(0.165)	0.075	0.341
5	0.42	5.80	0.483	(0.165)	0.087	0.396
6	0.50	6.50	0.541	(0.165)	0.097	0.444
7	0.58	7.40	0.616	(0.165)	0.111	0.505
8	0.67	8.60	0.716	(0.165)	0.129	0.587
9	0.75	12.30	1.024	0.165	(0.184)	0.859
10	0.83	29.10	2.422	0.165	(0.436)	2.257
11	0.92	6.80	0.566	(0.165)	0.102	0.464
12	1.00	5.00	0.416	(0.165)	0.075	0.341
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	7.1

Flood volume = Effective rainfall 0.59(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.1(Ac.Ft)
Total soil loss = 0.10(In)
Total soil loss = 0.013(Ac.Ft)
Total rainfall = 0.69(In)
Flood volume = 3401.0 Cubic Feet
Total soil loss = 577.8 Cubic Feet

Peak flow rate of this hydrograph = 2.224(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0006	0.08	Q				
0+10	0.0027	0.30	Q				
0+15	0.0054	0.40	QV				
0+20	0.0086	0.47	Q V				
0+25	0.0122	0.52	Q V				
0+30	0.0162	0.59	Q V				
0+35	0.0208	0.67	Q V				
0+40	0.0261	0.77	Q V				
0+45	0.0325	0.94	Q V				
0+50	0.0434	1.58	Q		V		

```
    0+55       0.0587      2.22  |       Q |         |         V         |
    1+ 0       0.0672      1.22  |   Q     |         |         |   V     |
    1+ 5       0.0723      0.75  |  Q      |         |         |      V  |
    1+10       0.0748      0.36  |Q        |         |         |       V |
    1+15       0.0762      0.21  Q         |         |         |        V|
    1+20       0.0771      0.13  Q         |         |         |        V|
    1+25       0.0776      0.08  Q         |         |         |        V|
    1+30       0.0780      0.05  Q         |         |         |        V|
    1+35       0.0780      0.01  Q         |         |         |        V|
    1+40       0.0781      0.00  Q         |         |         |         V
-------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris35.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
5 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.87	1.37

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            2.10                  3.32

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.869(In)
Area Averaged 100-Year Rainfall =    2.100(In)

Point rain (area averaged) =    1.157(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    1.157(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  16.2      0.870     0.900        0.165       1.000      0.165
                                                 Sum (F) =   0.165
Area averaged mean soil loss (F) (In/Hr) =  0.165
Minimum soil loss rate ((In/Hr)) =  0.083
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                               Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.181	(0.165)	0.032	0.148
2	0.17	1.30	0.181	(0.165)	0.032	0.148
3	0.25	1.10	0.153	(0.165)	0.027	0.125
4	0.33	1.50	0.208	(0.165)	0.037	0.171
5	0.42	1.50	0.208	(0.165)	0.037	0.171
6	0.50	1.80	0.250	(0.165)	0.045	0.205
7	0.58	1.50	0.208	(0.165)	0.037	0.171
8	0.67	1.80	0.250	(0.165)	0.045	0.205
9	0.75	1.80	0.250	(0.165)	0.045	0.205
10	0.83	1.50	0.208	(0.165)	0.037	0.171
11	0.92	1.60	0.222	(0.165)	0.040	0.182
12	1.00	1.80	0.250	(0.165)	0.045	0.205
13	1.08	2.20	0.306	(0.165)	0.055	0.251
14	1.17	2.20	0.306	(0.165)	0.055	0.251
15	1.25	2.20	0.306	(0.165)	0.055	0.251
16	1.33	2.00	0.278	(0.165)	0.050	0.228
17	1.42	2.60	0.361	(0.165)	0.065	0.296
18	1.50	2.70	0.375	(0.165)	0.067	0.307
19	1.58	2.40	0.333	(0.165)	0.060	0.273
20	1.67	2.70	0.375	(0.165)	0.067	0.307
21	1.75	3.30	0.458	(0.165)	0.082	0.376
22	1.83	3.10	0.431	(0.165)	0.077	0.353
23	1.92	2.90	0.403	(0.165)	0.072	0.330
24	2.00	3.00	0.417	(0.165)	0.075	0.342
25	2.08	3.10	0.431	(0.165)	0.077	0.353
26	2.17	4.20	0.583	(0.165)	0.105	0.478
27	2.25	5.00	0.694	(0.165)	0.125	0.569
28	2.33	3.50	0.486	(0.165)	0.087	0.399
29	2.42	6.80	0.944	0.165	(0.170)	0.779
30	2.50	7.30	1.014	0.165	(0.182)	0.848
31	2.58	8.20	1.139	0.165	(0.205)	0.973
32	2.67	5.90	0.819	(0.165)	0.147	0.672
33	2.75	2.00	0.278	(0.165)	0.050	0.228
34	2.83	1.80	0.250	(0.165)	0.045	0.205
35	2.92	1.80	0.250	(0.165)	0.045	0.205
36	3.00	0.60	0.083	(0.165)	0.015	0.068
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	11.4

Flood volume = Effective rainfall 0.95(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.1(Ac.Ft)
Total soil loss = 0.20(In)
Total soil loss = 0.027(Ac.Ft)
Total rainfall = 1.16(In)
Flood volume = 5472.2 Cubic Feet
Total soil loss = 1165.5 Cubic Feet

Peak flow rate of this hydrograph = 1.322(CFS)

++

3 - H O U R S T O R M

R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0 2.5 5.0 7.5 10.0
0+ 5	0.0003	0.04	Q | | | |
0+10	0.0014	0.16	Q | | | |
0+15	0.0027	0.19	Q | | | |
0+20	0.0040	0.20	QV | | | |
0+25	0.0057	0.24	QV | | | |
0+30	0.0075	0.26	|QV | | | |
0+35	0.0095	0.29	|Q V | | | |
0+40	0.0115	0.29	|Q V | | | |
0+45	0.0136	0.31	|Q V | | | |
0+50	0.0157	0.31	|Q V | | | |
0+55	0.0177	0.29	|Q V | | | |
1+ 0	0.0198	0.30	|Q V | | | |
1+ 5	0.0220	0.33	|Q V | | | |
1+10	0.0246	0.37	|Q V | | | |
1+15	0.0272	0.38	|Q V | | | |
1+20	0.0298	0.38	|Q V| | | |
1+25	0.0325	0.39	|Q V | | |
1+30	0.0355	0.44	|Q |V | | |
1+35	0.0387	0.46	|Q | V | | |
1+40	0.0418	0.45	|Q | V | | |
1+45	0.0452	0.49	|Q | V | | |
1+50	0.0490	0.55	| Q | V | | |
1+55	0.0527	0.54	| Q | V | | |
2+ 0	0.0564	0.53	| Q | V | | |
2+ 5	0.0601	0.54	| Q | V| | |
2+10	0.0642	0.59	| Q | V | |
2+15	0.0691	0.72	| Q | | V | |
2+20	0.0744	0.77	| Q | | V | |
2+25	0.0799	0.79	| Q | | V | |
2+30	0.0873	1.07	| Q | | V |
2+35	0.0959	1.25	| Q | | V |
2+40	0.1050	1.32	| Q | | | V |
2+45	0.1121	1.03	| Q | | | V |
2+50	0.1165	0.64	| Q | | | V |
2+55	0.1198	0.49	|Q | | | V |
3+ 0	0.1225	0.38	|Q | | | V|
3+ 5	0.1240	0.22	Q | | | V|
3+10	0.1248	0.11	Q | | | V|

3+15	0.1252	0.06	Q	|	|	|	V|
3+20	0.1254	0.03	Q	|	|	|	V|
3+25	0.1255	0.02	Q	|	|	|	V|
3+30	0.1256	0.01	Q	|	|	|	V|
3+35	0.1256	0.00	Q	|	|	|	V|
3+40	0.1256	0.00	Q	|	|	|	V|

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris65.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
5 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	1.22	1.93

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            2.87                   4.53

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    1.220(In)
Area Averaged 100-Year Rainfall =    2.870(In)

Point rain (area averaged) =    1.606(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    1.606(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  16.2      0.870     0.900        0.165       1.000      0.165
                                                 Sum (F) =   0.165
Area averaged mean soil loss (F) (In/Hr) =  0.165
Minimum soil loss rate ((In/Hr)) =  0.083
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945             0.286
    2   0.167        191.791         48.003             0.764
    3   0.250        287.687         16.299             0.260
    4   0.333        383.583          7.288             0.116
    5   0.417        479.478          4.149             0.066
    6   0.500        575.374          2.689             0.043
    7   0.583        671.270          1.732             0.028
    8   0.667        767.165          1.088             0.017
    9   0.750        863.061          0.808             0.013
                              Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

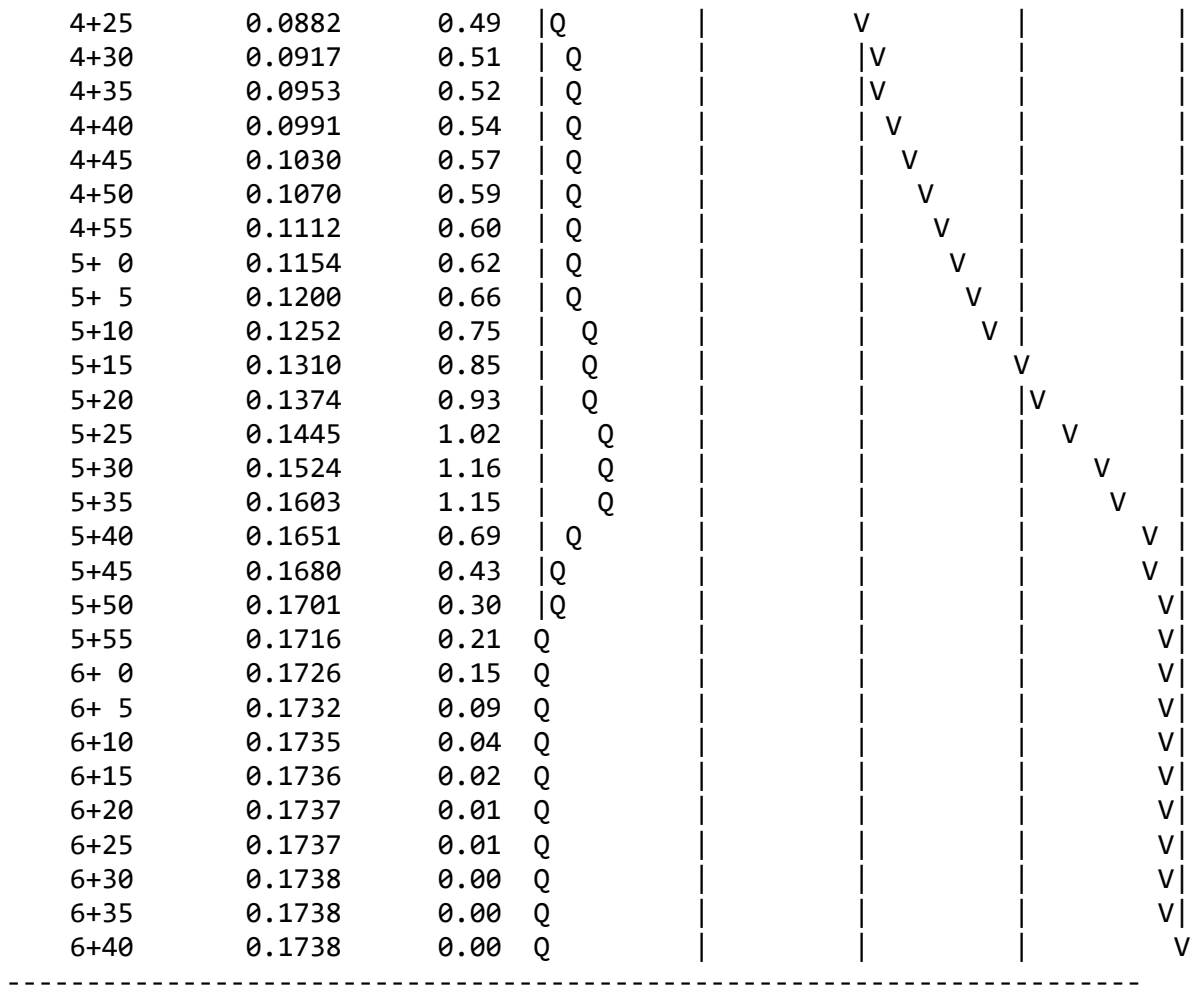
The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.096	(0.165)	0.017	0.079
2	0.17	0.60	0.116	(0.165)	0.021	0.095
3	0.25	0.60	0.116	(0.165)	0.021	0.095
4	0.33	0.60	0.116	(0.165)	0.021	0.095
5	0.42	0.60	0.116	(0.165)	0.021	0.095
6	0.50	0.70	0.135	(0.165)	0.024	0.111
7	0.58	0.70	0.135	(0.165)	0.024	0.111
8	0.67	0.70	0.135	(0.165)	0.024	0.111
9	0.75	0.70	0.135	(0.165)	0.024	0.111
10	0.83	0.70	0.135	(0.165)	0.024	0.111
11	0.92	0.70	0.135	(0.165)	0.024	0.111
12	1.00	0.80	0.154	(0.165)	0.028	0.126
13	1.08	0.80	0.154	(0.165)	0.028	0.126
14	1.17	0.80	0.154	(0.165)	0.028	0.126
15	1.25	0.80	0.154	(0.165)	0.028	0.126
16	1.33	0.80	0.154	(0.165)	0.028	0.126
17	1.42	0.80	0.154	(0.165)	0.028	0.126
18	1.50	0.80	0.154	(0.165)	0.028	0.126
19	1.58	0.80	0.154	(0.165)	0.028	0.126
20	1.67	0.80	0.154	(0.165)	0.028	0.126
21	1.75	0.80	0.154	(0.165)	0.028	0.126
22	1.83	0.80	0.154	(0.165)	0.028	0.126
23	1.92	0.80	0.154	(0.165)	0.028	0.126
24	2.00	0.90	0.173	(0.165)	0.031	0.142
25	2.08	0.80	0.154	(0.165)	0.028	0.126
26	2.17	0.90	0.173	(0.165)	0.031	0.142
27	2.25	0.90	0.173	(0.165)	0.031	0.142
28	2.33	0.90	0.173	(0.165)	0.031	0.142
29	2.42	0.90	0.173	(0.165)	0.031	0.142
30	2.50	0.90	0.173	(0.165)	0.031	0.142
31	2.58	0.90	0.173	(0.165)	0.031	0.142
32	2.67	0.90	0.173	(0.165)	0.031	0.142
33	2.75	1.00	0.193	(0.165)	0.035	0.158
34	2.83	1.00	0.193	(0.165)	0.035	0.158
35	2.92	1.00	0.193	(0.165)	0.035	0.158
36	3.00	1.00	0.193	(0.165)	0.035	0.158
37	3.08	1.00	0.193	(0.165)	0.035	0.158
38	3.17	1.10	0.212	(0.165)	0.038	0.174
39	3.25	1.10	0.212	(0.165)	0.038	0.174
40	3.33	1.10	0.212	(0.165)	0.038	0.174
41	3.42	1.20	0.231	(0.165)	0.042	0.190
42	3.50	1.30	0.251	(0.165)	0.045	0.205
43	3.58	1.40	0.270	(0.165)	0.049	0.221
44	3.67	1.40	0.270	(0.165)	0.049	0.221
45	3.75	1.50	0.289	(0.165)	0.052	0.237

```
46   3.83     1.50      0.289       (  0.165)       0.052        0.237
47   3.92     1.60      0.308       (  0.165)       0.056        0.253
48   4.00     1.60      0.308       (  0.165)       0.056        0.253
49   4.08     1.70      0.328       (  0.165)       0.059        0.269
50   4.17     1.80      0.347       (  0.165)       0.062        0.285
51   4.25     1.90      0.366       (  0.165)       0.066        0.300
52   4.33     2.00      0.386       (  0.165)       0.069        0.316
53   4.42     2.10      0.405       (  0.165)       0.073        0.332
54   4.50     2.10      0.405       (  0.165)       0.073        0.332
55   4.58     2.20      0.424       (  0.165)       0.076        0.348
56   4.67     2.30      0.443       (  0.165)       0.080        0.364
57   4.75     2.40      0.463       (  0.165)       0.083        0.379
58   4.83     2.40      0.463       (  0.165)       0.083        0.379
59   4.92     2.50      0.482       (  0.165)       0.087        0.395
60   5.00     2.60      0.501       (  0.165)       0.090        0.411
61   5.08     3.10      0.598       (  0.165)       0.108        0.490
62   5.17     3.60      0.694       (  0.165)       0.125        0.569
63   5.25     3.90      0.752       (  0.165)       0.135        0.616
64   5.33     4.20      0.810       (  0.165)       0.146        0.664
65   5.42     4.70      0.906       (  0.165)       0.163        0.743
66   5.50     5.60      1.080          0.165    (  0.194)       0.914
67   5.58     1.90      0.366       (  0.165)       0.066        0.300
68   5.67     0.90      0.173       (  0.165)       0.031        0.142
69   5.75     0.60      0.116       (  0.165)       0.021        0.095
70   5.83     0.50      0.096       (  0.165)       0.017        0.079
71   5.92     0.30      0.058       (  0.165)       0.010        0.047
72   6.00     0.20      0.039       (  0.165)       0.007        0.032
               (Loss Rate Not Used)
   Sum =     100.0                                    Sum =    15.8
      Flood volume = Effective rainfall      1.32(In)
       times area       1.6(Ac.)/[(In)/(Ft.)] =       0.2(Ac.Ft)
      Total soil loss =      0.29(In)
      Total soil loss =     0.038(Ac.Ft)
      Total rainfall =      1.61(In)
      Flood volume =        7569.1 Cubic Feet
      Total soil loss =        1644.6 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      1.155(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0002      0.02  Q         |         |         |         |
  0+10       0.0008      0.09  Q         |         |         |         |
```

```
0+15       0.0016      0.12  Q         |         |         |         |
0+20       0.0025      0.13  Q         |         |         |         |
0+25       0.0035      0.14  Q         |         |         |         |
0+30       0.0045      0.15  QV        |         |         |         |
0+35       0.0056      0.16  QV        |         |         |         |
0+40       0.0068      0.17  QV        |         |         |         |
0+45       0.0080      0.17  QV        |         |         |         |
0+50       0.0092      0.17  Q V       |         |         |         |
0+55       0.0104      0.18  Q V       |         |         |         |
1+ 0       0.0117      0.18  Q V       |         |         |         |
1+ 5       0.0130      0.19  Q V       |         |         |         |
1+10       0.0143      0.20  Q  V      |         |         |         |
1+15       0.0157      0.20  Q  V      |         |         |         |
1+20       0.0171      0.20  Q  V      |         |         |         |
1+25       0.0185      0.20  Q   V     |         |         |         |
1+30       0.0199      0.20  Q   V     |         |         |         |
1+35       0.0212      0.20  Q   V     |         |         |         |
1+40       0.0226      0.20  Q    V    |         |         |         |
1+45       0.0240      0.20  Q    V    |         |         |         |
1+50       0.0254      0.20  Q    V    |         |         |         |
1+55       0.0268      0.20  Q     V   |         |         |         |
2+ 0       0.0282      0.21  Q     V   |         |         |         |
2+ 5       0.0297      0.21  Q     V   |         |         |         |
2+10       0.0311      0.21  Q      V  |         |         |         |
2+15       0.0326      0.22  Q      V  |         |         |         |
2+20       0.0342      0.22  Q      V  |         |         |         |
2+25       0.0357      0.22  Q       V |         |         |         |
2+30       0.0373      0.23  Q       V |         |         |         |
2+35       0.0388      0.23  Q       V |         |         |         |
2+40       0.0404      0.23  Q        V|         |         |         |
2+45       0.0420      0.23  Q        V|         |         |         |
2+50       0.0437      0.24  Q         V         |         |         |
2+55       0.0454      0.25  Q         V         |         |         |
3+ 0       0.0471      0.25  Q         V         |         |         |
3+ 5       0.0488      0.25  |Q        |V         |         |         |
3+10       0.0506      0.26  |Q        |V         |         |         |
3+15       0.0524      0.27  |Q        | V        |         |         |
3+20       0.0543      0.27  |Q        | V        |         |         |
3+25       0.0562      0.28  |Q        | V        |         |         |
3+30       0.0582      0.30  |Q        |  V       |         |         |
3+35       0.0604      0.32  |Q        |  V       |         |         |
3+40       0.0628      0.34  |Q        |   V      |         |         |
3+45       0.0651      0.35  |Q        |   V      |         |         |
3+50       0.0677      0.36  |Q        |    V     |         |         |
3+55       0.0702      0.37  |Q        |     V    |         |         |
4+ 0       0.0729      0.39  |Q        |     V    |         |         |
4+ 5       0.0757      0.40  |Q        |      V   |         |         |
4+10       0.0786      0.42  |Q        |       V  |         |         |
4+15       0.0816      0.44  |Q        |       V  |         |         |
4+20       0.0848      0.47  |Q        |        V |         |         |
```


4+25 0.0882 0.49
4+30 0.0917 0.51
4+35 0.0953 0.52
4+40 0.0991 0.54
4+45 0.1030 0.57
4+50 0.1070 0.59
4+55 0.1112 0.60
5+ 0 0.1154 0.62
5+ 5 0.1200 0.66
5+10 0.1252 0.75
5+15 0.1310 0.85
5+20 0.1374 0.93
5+25 0.1445 1.02
5+30 0.1524 1.16
5+35 0.1603 1.15
5+40 0.1651 0.69
5+45 0.1680 0.43
5+50 0.1701 0.30
5+55 0.1716 0.21
6+ 0 0.1726 0.15
6+ 5 0.1732 0.09
6+10 0.1735 0.04
6+15 0.1736 0.02
6+20 0.1737 0.01
6+25 0.1737 0.01
6+30 0.1738 0.00
6+35 0.1738 0.00
6+40 0.1738 0.00

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris245.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
5 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.05	3.24

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            5.25                  8.29

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    2.050(In)
Area Averaged 100-Year Rainfall =    5.250(In)

Point rain (area averaged) =    2.800(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    2.800(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  16.2      0.870     0.900        0.165       1.000      0.165
                                                 Sum (F) =   0.165
Area averaged mean soil loss (F) (In/Hr) =  0.165
Minimum soil loss rate ((In/Hr)) =  0.083
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945             0.286
    2   0.167        191.791         48.003             0.764
    3   0.250        287.687         16.299             0.260
    4   0.333        383.583          7.288             0.116
    5   0.417        479.478          4.149             0.066
    6   0.500        575.374          2.689             0.043
    7   0.583        671.270          1.732             0.028
    8   0.667        767.165          1.088             0.017
    9   0.750        863.061          0.808             0.013
                              Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.022	(0.293)	0.004	0.018
2	0.17	0.07	0.022	(0.292)	0.004	0.018
3	0.25	0.07	0.022	(0.291)	0.004	0.018
4	0.33	0.10	0.034	(0.290)	0.006	0.028
5	0.42	0.10	0.034	(0.289)	0.006	0.028
6	0.50	0.10	0.034	(0.288)	0.006	0.028
7	0.58	0.10	0.034	(0.286)	0.006	0.028
8	0.67	0.10	0.034	(0.285)	0.006	0.028
9	0.75	0.10	0.034	(0.284)	0.006	0.028
10	0.83	0.13	0.045	(0.283)	0.008	0.037
11	0.92	0.13	0.045	(0.282)	0.008	0.037
12	1.00	0.13	0.045	(0.281)	0.008	0.037
13	1.08	0.10	0.034	(0.280)	0.006	0.028
14	1.17	0.10	0.034	(0.279)	0.006	0.028
15	1.25	0.10	0.034	(0.277)	0.006	0.028
16	1.33	0.10	0.034	(0.276)	0.006	0.028
17	1.42	0.10	0.034	(0.275)	0.006	0.028
18	1.50	0.10	0.034	(0.274)	0.006	0.028
19	1.58	0.10	0.034	(0.273)	0.006	0.028
20	1.67	0.10	0.034	(0.272)	0.006	0.028
21	1.75	0.10	0.034	(0.271)	0.006	0.028
22	1.83	0.13	0.045	(0.270)	0.008	0.037
23	1.92	0.13	0.045	(0.269)	0.008	0.037
24	2.00	0.13	0.045	(0.268)	0.008	0.037
25	2.08	0.13	0.045	(0.267)	0.008	0.037
26	2.17	0.13	0.045	(0.265)	0.008	0.037
27	2.25	0.13	0.045	(0.264)	0.008	0.037
28	2.33	0.13	0.045	(0.263)	0.008	0.037
29	2.42	0.13	0.045	(0.262)	0.008	0.037
30	2.50	0.13	0.045	(0.261)	0.008	0.037
31	2.58	0.17	0.056	(0.260)	0.010	0.046
32	2.67	0.17	0.056	(0.259)	0.010	0.046
33	2.75	0.17	0.056	(0.258)	0.010	0.046
34	2.83	0.17	0.056	(0.257)	0.010	0.046
35	2.92	0.17	0.056	(0.256)	0.010	0.046
36	3.00	0.17	0.056	(0.255)	0.010	0.046
37	3.08	0.17	0.056	(0.254)	0.010	0.046
38	3.17	0.17	0.056	(0.253)	0.010	0.046
39	3.25	0.17	0.056	(0.252)	0.010	0.046
40	3.33	0.17	0.056	(0.251)	0.010	0.046
41	3.42	0.17	0.056	(0.250)	0.010	0.046
42	3.50	0.17	0.056	(0.249)	0.010	0.046
43	3.58	0.17	0.056	(0.247)	0.010	0.046
44	3.67	0.17	0.056	(0.246)	0.010	0.046
45	3.75	0.17	0.056	(0.245)	0.010	0.046

46	3.83	0.20	0.067	(0.244)	0.012	0.055
47	3.92	0.20	0.067	(0.243)	0.012	0.055
48	4.00	0.20	0.067	(0.242)	0.012	0.055
49	4.08	0.20	0.067	(0.241)	0.012	0.055
50	4.17	0.20	0.067	(0.240)	0.012	0.055
51	4.25	0.20	0.067	(0.239)	0.012	0.055
52	4.33	0.23	0.078	(0.238)	0.014	0.064
53	4.42	0.23	0.078	(0.237)	0.014	0.064
54	4.50	0.23	0.078	(0.236)	0.014	0.064
55	4.58	0.23	0.078	(0.235)	0.014	0.064
56	4.67	0.23	0.078	(0.234)	0.014	0.064
57	4.75	0.23	0.078	(0.233)	0.014	0.064
58	4.83	0.27	0.090	(0.232)	0.016	0.073
59	4.92	0.27	0.090	(0.231)	0.016	0.073
60	5.00	0.27	0.090	(0.230)	0.016	0.073
61	5.08	0.20	0.067	(0.229)	0.012	0.055
62	5.17	0.20	0.067	(0.228)	0.012	0.055
63	5.25	0.20	0.067	(0.227)	0.012	0.055
64	5.33	0.23	0.078	(0.226)	0.014	0.064
65	5.42	0.23	0.078	(0.225)	0.014	0.064
66	5.50	0.23	0.078	(0.224)	0.014	0.064
67	5.58	0.27	0.090	(0.223)	0.016	0.073
68	5.67	0.27	0.090	(0.222)	0.016	0.073
69	5.75	0.27	0.090	(0.221)	0.016	0.073
70	5.83	0.27	0.090	(0.220)	0.016	0.073
71	5.92	0.27	0.090	(0.219)	0.016	0.073
72	6.00	0.27	0.090	(0.218)	0.016	0.073
73	6.08	0.30	0.101	(0.217)	0.018	0.083
74	6.17	0.30	0.101	(0.216)	0.018	0.083
75	6.25	0.30	0.101	(0.215)	0.018	0.083
76	6.33	0.30	0.101	(0.214)	0.018	0.083
77	6.42	0.30	0.101	(0.213)	0.018	0.083
78	6.50	0.30	0.101	(0.213)	0.018	0.083
79	6.58	0.33	0.112	(0.212)	0.020	0.092
80	6.67	0.33	0.112	(0.211)	0.020	0.092
81	6.75	0.33	0.112	(0.210)	0.020	0.092
82	6.83	0.33	0.112	(0.209)	0.020	0.092
83	6.92	0.33	0.112	(0.208)	0.020	0.092
84	7.00	0.33	0.112	(0.207)	0.020	0.092
85	7.08	0.33	0.112	(0.206)	0.020	0.092
86	7.17	0.33	0.112	(0.205)	0.020	0.092
87	7.25	0.33	0.112	(0.204)	0.020	0.092
88	7.33	0.37	0.123	(0.203)	0.022	0.101
89	7.42	0.37	0.123	(0.202)	0.022	0.101
90	7.50	0.37	0.123	(0.201)	0.022	0.101
91	7.58	0.40	0.134	(0.200)	0.024	0.110
92	7.67	0.40	0.134	(0.199)	0.024	0.110
93	7.75	0.40	0.134	(0.198)	0.024	0.110
94	7.83	0.43	0.146	(0.198)	0.026	0.119
95	7.92	0.43	0.146	(0.197)	0.026	0.119

96	8.00	0.43	0.146	(0.196)	0.026	0.119
97	8.08	0.50	0.168	(0.195)	0.030	0.138
98	8.17	0.50	0.168	(0.194)	0.030	0.138
99	8.25	0.50	0.168	(0.193)	0.030	0.138
100	8.33	0.50	0.168	(0.192)	0.030	0.138
101	8.42	0.50	0.168	(0.191)	0.030	0.138
102	8.50	0.50	0.168	(0.190)	0.030	0.138
103	8.58	0.53	0.179	(0.189)	0.032	0.147
104	8.67	0.53	0.179	(0.189)	0.032	0.147
105	8.75	0.53	0.179	(0.188)	0.032	0.147
106	8.83	0.57	0.190	(0.187)	0.034	0.156
107	8.92	0.57	0.190	(0.186)	0.034	0.156
108	9.00	0.57	0.190	(0.185)	0.034	0.156
109	9.08	0.63	0.213	(0.184)	0.038	0.174
110	9.17	0.63	0.213	(0.183)	0.038	0.174
111	9.25	0.63	0.213	(0.182)	0.038	0.174
112	9.33	0.67	0.224	(0.181)	0.040	0.184
113	9.42	0.67	0.224	(0.181)	0.040	0.184
114	9.50	0.67	0.224	(0.180)	0.040	0.184
115	9.58	0.70	0.235	(0.179)	0.042	0.193
116	9.67	0.70	0.235	(0.178)	0.042	0.193
117	9.75	0.70	0.235	(0.177)	0.042	0.193
118	9.83	0.73	0.246	(0.176)	0.044	0.202
119	9.92	0.73	0.246	(0.175)	0.044	0.202
120	10.00	0.73	0.246	(0.175)	0.044	0.202
121	10.08	0.50	0.168	(0.174)	0.030	0.138
122	10.17	0.50	0.168	(0.173)	0.030	0.138
123	10.25	0.50	0.168	(0.172)	0.030	0.138
124	10.33	0.50	0.168	(0.171)	0.030	0.138
125	10.42	0.50	0.168	(0.170)	0.030	0.138
126	10.50	0.50	0.168	(0.170)	0.030	0.138
127	10.58	0.67	0.224	(0.169)	0.040	0.184
128	10.67	0.67	0.224	(0.168)	0.040	0.184
129	10.75	0.67	0.224	(0.167)	0.040	0.184
130	10.83	0.67	0.224	(0.166)	0.040	0.184
131	10.92	0.67	0.224	(0.166)	0.040	0.184
132	11.00	0.67	0.224	(0.165)	0.040	0.184
133	11.08	0.63	0.213	(0.164)	0.038	0.174
134	11.17	0.63	0.213	(0.163)	0.038	0.174
135	11.25	0.63	0.213	(0.162)	0.038	0.174
136	11.33	0.63	0.213	(0.161)	0.038	0.174
137	11.42	0.63	0.213	(0.161)	0.038	0.174
138	11.50	0.63	0.213	(0.160)	0.038	0.174
139	11.58	0.57	0.190	(0.159)	0.034	0.156
140	11.67	0.57	0.190	(0.158)	0.034	0.156
141	11.75	0.57	0.190	(0.157)	0.034	0.156
142	11.83	0.60	0.202	(0.157)	0.036	0.165
143	11.92	0.60	0.202	(0.156)	0.036	0.165
144	12.00	0.60	0.202	(0.155)	0.036	0.165
145	12.08	0.83	0.280	(0.154)	0.050	0.230

146	12.17	0.83	0.280	(0.154)	0.050	0.230
147	12.25	0.83	0.280	(0.153)	0.050	0.230
148	12.33	0.87	0.291	(0.152)	0.052	0.239
149	12.42	0.87	0.291	(0.151)	0.052	0.239
150	12.50	0.87	0.291	(0.151)	0.052	0.239
151	12.58	0.93	0.314	(0.150)	0.056	0.257
152	12.67	0.93	0.314	(0.149)	0.056	0.257
153	12.75	0.93	0.314	(0.148)	0.056	0.257
154	12.83	0.97	0.325	(0.148)	0.058	0.266
155	12.92	0.97	0.325	(0.147)	0.058	0.266
156	13.00	0.97	0.325	(0.146)	0.058	0.266
157	13.08	1.13	0.381	(0.145)	0.069	0.312
158	13.17	1.13	0.381	(0.145)	0.069	0.312
159	13.25	1.13	0.381	(0.144)	0.069	0.312
160	13.33	1.13	0.381	(0.143)	0.069	0.312
161	13.42	1.13	0.381	(0.142)	0.069	0.312
162	13.50	1.13	0.381	(0.142)	0.069	0.312
163	13.58	0.77	0.258	(0.141)	0.046	0.211
164	13.67	0.77	0.258	(0.140)	0.046	0.211
165	13.75	0.77	0.258	(0.139)	0.046	0.211
166	13.83	0.77	0.258	(0.139)	0.046	0.211
167	13.92	0.77	0.258	(0.138)	0.046	0.211
168	14.00	0.77	0.258	(0.137)	0.046	0.211
169	14.08	0.90	0.302	(0.137)	0.054	0.248
170	14.17	0.90	0.302	(0.136)	0.054	0.248
171	14.25	0.90	0.302	(0.135)	0.054	0.248
172	14.33	0.87	0.291	(0.135)	0.052	0.239
173	14.42	0.87	0.291	(0.134)	0.052	0.239
174	14.50	0.87	0.291	(0.133)	0.052	0.239
175	14.58	0.87	0.291	(0.133)	0.052	0.239
176	14.67	0.87	0.291	(0.132)	0.052	0.239
177	14.75	0.87	0.291	(0.131)	0.052	0.239
178	14.83	0.83	0.280	(0.130)	0.050	0.230
179	14.92	0.83	0.280	(0.130)	0.050	0.230
180	15.00	0.83	0.280	(0.129)	0.050	0.230
181	15.08	0.80	0.269	(0.129)	0.048	0.220
182	15.17	0.80	0.269	(0.128)	0.048	0.220
183	15.25	0.80	0.269	(0.127)	0.048	0.220
184	15.33	0.77	0.258	(0.127)	0.046	0.211
185	15.42	0.77	0.258	(0.126)	0.046	0.211
186	15.50	0.77	0.258	(0.125)	0.046	0.211
187	15.58	0.63	0.213	(0.125)	0.038	0.174
188	15.67	0.63	0.213	(0.124)	0.038	0.174
189	15.75	0.63	0.213	(0.123)	0.038	0.174
190	15.83	0.63	0.213	(0.123)	0.038	0.174
191	15.92	0.63	0.213	(0.122)	0.038	0.174
192	16.00	0.63	0.213	(0.121)	0.038	0.174
193	16.08	0.13	0.045	(0.121)	0.008	0.037
194	16.17	0.13	0.045	(0.120)	0.008	0.037
195	16.25	0.13	0.045	(0.120)	0.008	0.037

196	16.33	0.13	0.045	(0.119)	0.008	0.037
197	16.42	0.13	0.045	(0.118)	0.008	0.037
198	16.50	0.13	0.045	(0.118)	0.008	0.037
199	16.58	0.10	0.034	(0.117)	0.006	0.028
200	16.67	0.10	0.034	(0.117)	0.006	0.028
201	16.75	0.10	0.034	(0.116)	0.006	0.028
202	16.83	0.10	0.034	(0.115)	0.006	0.028
203	16.92	0.10	0.034	(0.115)	0.006	0.028
204	17.00	0.10	0.034	(0.114)	0.006	0.028
205	17.08	0.17	0.056	(0.114)	0.010	0.046
206	17.17	0.17	0.056	(0.113)	0.010	0.046
207	17.25	0.17	0.056	(0.113)	0.010	0.046
208	17.33	0.17	0.056	(0.112)	0.010	0.046
209	17.42	0.17	0.056	(0.111)	0.010	0.046
210	17.50	0.17	0.056	(0.111)	0.010	0.046
211	17.58	0.17	0.056	(0.110)	0.010	0.046
212	17.67	0.17	0.056	(0.110)	0.010	0.046
213	17.75	0.17	0.056	(0.109)	0.010	0.046
214	17.83	0.13	0.045	(0.109)	0.008	0.037
215	17.92	0.13	0.045	(0.108)	0.008	0.037
216	18.00	0.13	0.045	(0.108)	0.008	0.037
217	18.08	0.13	0.045	(0.107)	0.008	0.037
218	18.17	0.13	0.045	(0.107)	0.008	0.037
219	18.25	0.13	0.045	(0.106)	0.008	0.037
220	18.33	0.13	0.045	(0.105)	0.008	0.037
221	18.42	0.13	0.045	(0.105)	0.008	0.037
222	18.50	0.13	0.045	(0.104)	0.008	0.037
223	18.58	0.10	0.034	(0.104)	0.006	0.028
224	18.67	0.10	0.034	(0.103)	0.006	0.028
225	18.75	0.10	0.034	(0.103)	0.006	0.028
226	18.83	0.07	0.022	(0.102)	0.004	0.018
227	18.92	0.07	0.022	(0.102)	0.004	0.018
228	19.00	0.07	0.022	(0.101)	0.004	0.018
229	19.08	0.10	0.034	(0.101)	0.006	0.028
230	19.17	0.10	0.034	(0.101)	0.006	0.028
231	19.25	0.10	0.034	(0.100)	0.006	0.028
232	19.33	0.13	0.045	(0.100)	0.008	0.037
233	19.42	0.13	0.045	(0.099)	0.008	0.037
234	19.50	0.13	0.045	(0.099)	0.008	0.037
235	19.58	0.10	0.034	(0.098)	0.006	0.028
236	19.67	0.10	0.034	(0.098)	0.006	0.028
237	19.75	0.10	0.034	(0.097)	0.006	0.028
238	19.83	0.07	0.022	(0.097)	0.004	0.018
239	19.92	0.07	0.022	(0.096)	0.004	0.018
240	20.00	0.07	0.022	(0.096)	0.004	0.018
241	20.08	0.10	0.034	(0.096)	0.006	0.028
242	20.17	0.10	0.034	(0.095)	0.006	0.028
243	20.25	0.10	0.034	(0.095)	0.006	0.028
244	20.33	0.10	0.034	(0.094)	0.006	0.028
245	20.42	0.10	0.034	(0.094)	0.006	0.028

246	20.50	0.10	0.034	(0.094)	0.006	0.028
247	20.58	0.10	0.034	(0.093)	0.006	0.028
248	20.67	0.10	0.034	(0.093)	0.006	0.028
249	20.75	0.10	0.034	(0.092)	0.006	0.028
250	20.83	0.07	0.022	(0.092)	0.004	0.018
251	20.92	0.07	0.022	(0.092)	0.004	0.018
252	21.00	0.07	0.022	(0.091)	0.004	0.018
253	21.08	0.10	0.034	(0.091)	0.006	0.028
254	21.17	0.10	0.034	(0.091)	0.006	0.028
255	21.25	0.10	0.034	(0.090)	0.006	0.028
256	21.33	0.07	0.022	(0.090)	0.004	0.018
257	21.42	0.07	0.022	(0.090)	0.004	0.018
258	21.50	0.07	0.022	(0.089)	0.004	0.018
259	21.58	0.10	0.034	(0.089)	0.006	0.028
260	21.67	0.10	0.034	(0.089)	0.006	0.028
261	21.75	0.10	0.034	(0.088)	0.006	0.028
262	21.83	0.07	0.022	(0.088)	0.004	0.018
263	21.92	0.07	0.022	(0.088)	0.004	0.018
264	22.00	0.07	0.022	(0.087)	0.004	0.018
265	22.08	0.10	0.034	(0.087)	0.006	0.028
266	22.17	0.10	0.034	(0.087)	0.006	0.028
267	22.25	0.10	0.034	(0.086)	0.006	0.028
268	22.33	0.07	0.022	(0.086)	0.004	0.018
269	22.42	0.07	0.022	(0.086)	0.004	0.018
270	22.50	0.07	0.022	(0.086)	0.004	0.018
271	22.58	0.07	0.022	(0.085)	0.004	0.018
272	22.67	0.07	0.022	(0.085)	0.004	0.018
273	22.75	0.07	0.022	(0.085)	0.004	0.018
274	22.83	0.07	0.022	(0.085)	0.004	0.018
275	22.92	0.07	0.022	(0.085)	0.004	0.018
276	23.00	0.07	0.022	(0.084)	0.004	0.018
277	23.08	0.07	0.022	(0.084)	0.004	0.018
278	23.17	0.07	0.022	(0.084)	0.004	0.018
279	23.25	0.07	0.022	(0.084)	0.004	0.018
280	23.33	0.07	0.022	(0.084)	0.004	0.018
281	23.42	0.07	0.022	(0.083)	0.004	0.018
282	23.50	0.07	0.022	(0.083)	0.004	0.018
283	23.58	0.07	0.022	(0.083)	0.004	0.018
284	23.67	0.07	0.022	(0.083)	0.004	0.018
285	23.75	0.07	0.022	(0.083)	0.004	0.018
286	23.83	0.07	0.022	(0.083)	0.004	0.018
287	23.92	0.07	0.022	(0.083)	0.004	0.018
288	24.00	0.07	0.022	(0.083)	0.004	0.018

(Loss Rate Not Used)

Sum = 100.0 Sum = 27.5

Flood volume = Effective rainfall 2.30(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft)
Total soil loss = 0.50(In)
Total soil loss = 0.066(Ac.Ft)
Total rainfall = 2.80(In)

Flood volume = 13166.2 Cubic Feet
Total soil loss = 2890.1 Cubic Feet

Peak flow rate of this hydrograph = 0.495(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.01	Q				
0+10	0.0002	0.02	Q				
0+15	0.0003	0.02	Q				
0+20	0.0005	0.03	Q				
0+25	0.0008	0.04	Q				
0+30	0.0011	0.04	Q				
0+35	0.0014	0.04	Q				
0+40	0.0016	0.04	Q				
0+45	0.0019	0.04	Q				
0+50	0.0023	0.05	Q				
0+55	0.0026	0.05	Q				
1+ 0	0.0030	0.06	Q				
1+ 5	0.0034	0.05	Q				
1+10	0.0037	0.05	Q				
1+15	0.0040	0.05	Q				
1+20	0.0043	0.05	Q				
1+25	0.0047	0.04	Q				
1+30	0.0050	0.04	Q				
1+35	0.0053	0.04	Q				
1+40	0.0056	0.04	Q				
1+45	0.0059	0.04	Q				
1+50	0.0062	0.05	Q				
1+55	0.0066	0.05	Q				
2+ 0	0.0069	0.06	Q				
2+ 5	0.0073	0.06	Q				
2+10	0.0077	0.06	QV				
2+15	0.0081	0.06	QV				
2+20	0.0085	0.06	QV				
2+25	0.0089	0.06	QV				
2+30	0.0093	0.06	QV				
2+35	0.0098	0.06	QV				
2+40	0.0102	0.07	QV				
2+45	0.0107	0.07	QV				
2+50	0.0112	0.07	QV				
2+55	0.0117	0.07	QV				
3+ 0	0.0122	0.07	QV				

3+ 5	0.0127	0.07	QV	|	|	|	|
3+10	0.0132	0.07	QV	|	|	|	|
3+15	0.0137	0.07	QV	|	|	|	|
3+20	0.0142	0.07	QV	|	|	|	|
3+25	0.0147	0.07	QV	|	|	|	|
3+30	0.0152	0.07	Q V	|	|	|	|
3+35	0.0157	0.07	Q V	|	|	|	|
3+40	0.0162	0.07	Q V	|	|	|	|
3+45	0.0167	0.07	Q V	|	|	|	|
3+50	0.0173	0.08	Q V	|	|	|	|
3+55	0.0178	0.08	Q V	|	|	|	|
4+ 0	0.0184	0.09	Q V	|	|	|	|
4+ 5	0.0190	0.09	Q V	|	|	|	|
4+10	0.0196	0.09	Q V	|	|	|	|
4+15	0.0202	0.09	Q V	|	|	|	|
4+20	0.0208	0.09	Q V	|	|	|	|
4+25	0.0215	0.10	Q V	|	|	|	|
4+30	0.0222	0.10	Q V	|	|	|	|
4+35	0.0229	0.10	Q V	|	|	|	|
4+40	0.0236	0.10	Q V	|	|	|	|
4+45	0.0243	0.10	Q V	|	|	|	|
4+50	0.0250	0.10	Q V	|	|	|	|
4+55	0.0258	0.11	Q V	|	|	|	|
5+ 0	0.0266	0.11	Q V	|	|	|	|
5+ 5	0.0273	0.11	Q V	|	|	|	|
5+10	0.0280	0.10	Q V	|	|	|	|
5+15	0.0286	0.09	Q V	|	|	|	|
5+20	0.0293	0.09	Q V	|	|	|	|
5+25	0.0300	0.10	Q V	|	|	|	|
5+30	0.0306	0.10	Q V	|	|	|	|
5+35	0.0314	0.10	Q V	|	|	|	|
5+40	0.0321	0.11	Q V	|	|	|	|
5+45	0.0329	0.11	Q V	|	|	|	|
5+50	0.0337	0.12	Q V	|	|	|	|
5+55	0.0345	0.12	Q V	|	|	|	|
6+ 0	0.0353	0.12	Q V	|	|	|	|
6+ 5	0.0361	0.12	Q V	|	|	|	|
6+10	0.0370	0.13	Q V	|	|	|	|
6+15	0.0379	0.13	Q V	|	|	|	|
6+20	0.0388	0.13	Q V	|	|	|	|
6+25	0.0397	0.13	Q V	|	|	|	|
6+30	0.0406	0.13	Q V	|	|	|	|
6+35	0.0415	0.13	Q V	|	|	|	|
6+40	0.0425	0.14	Q V	|	|	|	|
6+45	0.0435	0.14	Q V	|	|	|	|
6+50	0.0445	0.14	Q V	|	|	|	|
6+55	0.0455	0.15	Q V	|	|	|	|
7+ 0	0.0465	0.15	Q V	|	|	|	|
7+ 5	0.0475	0.15	Q V	|	|	|	|
7+10	0.0485	0.15	Q V	|	|	|	|

```
 7+15       0.0495      0.15  Q     V   |          |          |          |
 7+20       0.0505      0.15  Q     V   |          |          |          |
 7+25       0.0516      0.16  Q     V   |          |          |          |
 7+30       0.0527      0.16  Q     V   |          |          |          |
 7+35       0.0538      0.16  Q      V  |          |          |          |
 7+40       0.0550      0.17  Q      V  |          |          |          |
 7+45       0.0562      0.17  Q      V  |          |          |          |
 7+50       0.0574      0.18  Q      V  |          |          |          |
 7+55       0.0586      0.18  Q      V  |          |          |          |
 8+ 0       0.0599      0.19  Q      V  |          |          |          |
 8+ 5       0.0613      0.19  Q       V |          |          |          |
 8+10       0.0627      0.21  Q       V |          |          |          |
 8+15       0.0642      0.21  Q       V |          |          |          |
 8+20       0.0657      0.22  Q       V |          |          |          |
 8+25       0.0672      0.22  Q       V |          |          |          |
 8+30       0.0687      0.22  Q        V|          |          |          |
 8+35       0.0702      0.22  Q        V|          |          |          |
 8+40       0.0718      0.23  Q        V|          |          |          |
 8+45       0.0734      0.23  Q        V|          |          |          |
 8+50       0.0750      0.24  Q        V|          |          |          |
 8+55       0.0767      0.24  Q         V          |          |          |
 9+ 0       0.0783      0.25  Q         V          |          |          |
 9+ 5       0.0801      0.25  |Q        V          |          |          |
 9+10       0.0819      0.27  |Q        V          |          |          |
 9+15       0.0838      0.27  |Q         |V         |          |          |
 9+20       0.0857      0.28  |Q         |V         |          |          |
 9+25       0.0877      0.29  |Q         |V         |          |          |
 9+30       0.0897      0.29  |Q         |V         |          |          |
 9+35       0.0917      0.29  |Q         | V        |          |          |
 9+40       0.0937      0.30  |Q         | V        |          |          |
 9+45       0.0958      0.30  |Q         | V        |          |          |
 9+50       0.0980      0.31  |Q         | V        |          |          |
 9+55       0.1001      0.32  |Q         |  V       |          |          |
10+ 0       0.1023      0.32  |Q         |  V       |          |          |
10+ 5       0.1044      0.30  |Q         |  V       |          |          |
10+10       0.1062      0.25  |Q         |   V      |          |          |
10+15       0.1078      0.24  Q          |   V      |          |          |
10+20       0.1094      0.23  Q          |   V      |          |          |
10+25       0.1109      0.23  Q          |   V      |          |          |
10+30       0.1125      0.22  Q          |   V      |          |          |
10+35       0.1141      0.23  Q          |    V     |          |          |
10+40       0.1159      0.27  |Q         |    V     |          |          |
10+45       0.1179      0.28  |Q         |    V     |          |          |
10+50       0.1198      0.28  |Q         |    V     |          |          |
10+55       0.1218      0.29  |Q         |     V    |          |          |
11+ 0       0.1238      0.29  |Q         |     V    |          |          |
11+ 5       0.1258      0.29  |Q         |     V    |          |          |
11+10       0.1277      0.28  |Q         |     V    |          |          |
11+15       0.1297      0.28  |Q         |      V   |          |          |
11+20       0.1316      0.28  |Q         |      V   |          |          |
```

```
11+25       0.1335      0.28  |Q        |      V  |         |         |
11+30       0.1354      0.28  |Q        |      V  |         |         |
11+35       0.1373      0.27  |Q        |       V |         |         |
11+40       0.1391      0.26  |Q        |       V |         |         |
11+45       0.1408      0.25  |Q        |       V |         |         |
11+50       0.1426      0.25  |Q        |       V |         |         |
11+55       0.1444      0.26  |Q        |        V|         |         |
12+ 0       0.1462      0.26  |Q        |        V|         |         |
12+ 5       0.1481      0.28  |Q        |        V|         |         |
12+10       0.1504      0.33  |Q        |        V|         |         |
12+15       0.1528      0.35  |Q        |         V         |         |
12+20       0.1552      0.36  |Q        |         V         |         |
12+25       0.1578      0.37  |Q        |         V         |         |
12+30       0.1604      0.37  |Q        |         |V        |         |
12+35       0.1630      0.38  |Q        |         |V        |         |
12+40       0.1657      0.40  |Q        |         |V        |         |
12+45       0.1685      0.40  |Q        |         | V       |         |
12+50       0.1713      0.41  |Q        |         | V       |         |
12+55       0.1742      0.42  |Q        |         |  V      |         |
13+ 0       0.1771      0.42  |Q        |         |  V      |         |
13+ 5       0.1801      0.44  |Q        |         |  V      |         |
13+10       0.1833      0.47  |Q        |         |   V     |         |
13+15       0.1867      0.48  |Q        |         |   V     |         |
13+20       0.1900      0.49  |Q        |         |    V    |         |
13+25       0.1934      0.49  |Q        |         |    V    |         |
13+30       0.1968      0.49  |Q        |         |     V   |         |
13+35       0.2001      0.47  |Q        |         |     V   |         |
13+40       0.2028      0.39  |Q        |         |     V   |         |
13+45       0.2053      0.37  |Q        |         |      V  |         |
13+50       0.2077      0.35  |Q        |         |      V  |         |
13+55       0.2101      0.35  |Q        |         |      V  |         |
14+ 0       0.2124      0.34  |Q        |         |       V |         |
14+ 5       0.2149      0.35  |Q        |         |       V |         |
14+10       0.2174      0.38  |Q        |         |       V |         |
14+15       0.2201      0.38  |Q        |         |        V|         |
14+20       0.2228      0.39  |Q        |         |        V|         |
14+25       0.2254      0.38  |Q        |         |        V|         |
14+30       0.2280      0.38  |Q        |         |         V         |
14+35       0.2306      0.38  |Q        |         |         V         |
14+40       0.2333      0.38  |Q        |         |         V         |
14+45       0.2359      0.38  |Q        |         |         |V        |
14+50       0.2385      0.38  |Q        |         |         |V        |
14+55       0.2410      0.37  |Q        |         |         |V        |
15+ 0       0.2436      0.37  |Q        |         |         | V       |
15+ 5       0.2461      0.36  |Q        |         |         | V       |
15+10       0.2485      0.36  |Q        |         |         | V       |
15+15       0.2510      0.35  |Q        |         |         |  V      |
15+20       0.2534      0.35  |Q        |         |         |  V      |
15+25       0.2557      0.34  |Q        |         |         |  V      |
15+30       0.2581      0.34  |Q        |         |         |   V     |
```

```
15+35       0.2603      0.33  |Q        |          |          |   V      |
15+40       0.2624      0.30  |Q        |          |          |   V      |
15+45       0.2644      0.29  |Q        |          |          |   V      |
15+50       0.2664      0.28  |Q        |          |          |    V     |
15+55       0.2683      0.28  |Q        |          |          |    V     |
16+ 0       0.2702      0.28  |Q        |          |          |    V     |
16+ 5       0.2719      0.24  Q         |          |          |    V     |
16+10       0.2728      0.13  Q         |          |          |     V    |
16+15       0.2735      0.10  Q         |          |          |     V    |
16+20       0.2740      0.08  Q         |          |          |     V    |
16+25       0.2745      0.07  Q         |          |          |     V    |
16+30       0.2750      0.07  Q         |          |          |     V    |
16+35       0.2754      0.06  Q         |          |          |     V    |
16+40       0.2757      0.05  Q         |          |          |     V    |
16+45       0.2761      0.05  Q         |          |          |     V    |
16+50       0.2764      0.05  Q         |          |          |     V    |
16+55       0.2767      0.04  Q         |          |          |     V    |
17+ 0       0.2770      0.04  Q         |          |          |     V    |
17+ 5       0.2773      0.05  Q         |          |          |     V    |
17+10       0.2778      0.06  Q         |          |          |     V    |
17+15       0.2782      0.07  Q         |          |          |     V    |
17+20       0.2787      0.07  Q         |          |          |     V    |
17+25       0.2792      0.07  Q         |          |          |     V    |
17+30       0.2797      0.07  Q         |          |          |      V   |
17+35       0.2802      0.07  Q         |          |          |      V   |
17+40       0.2807      0.07  Q         |          |          |      V   |
17+45       0.2812      0.07  Q         |          |          |      V   |
17+50       0.2817      0.07  Q         |          |          |      V   |
17+55       0.2821      0.06  Q         |          |          |      V   |
18+ 0       0.2826      0.06  Q         |          |          |      V   |
18+ 5       0.2830      0.06  Q         |          |          |      V   |
18+10       0.2834      0.06  Q         |          |          |      V   |
18+15       0.2838      0.06  Q         |          |          |      V   |
18+20       0.2842      0.06  Q         |          |          |      V   |
18+25       0.2846      0.06  Q         |          |          |      V   |
18+30       0.2850      0.06  Q         |          |          |      V   |
18+35       0.2854      0.06  Q         |          |          |      V   |
18+40       0.2857      0.05  Q         |          |          |      V   |
18+45       0.2860      0.05  Q         |          |          |      V   |
18+50       0.2863      0.04  Q         |          |          |      V   |
18+55       0.2866      0.04  Q         |          |          |      V   |
19+ 0       0.2868      0.03  Q         |          |          |      V   |
19+ 5       0.2870      0.03  Q         |          |          |      V   |
19+10       0.2873      0.04  Q         |          |          |       V  |
19+15       0.2876      0.04  Q         |          |          |       V  |
19+20       0.2879      0.05  Q         |          |          |       V  |
19+25       0.2883      0.05  Q         |          |          |       V  |
19+30       0.2887      0.06  Q         |          |          |       V  |
19+35       0.2890      0.05  Q         |          |          |       V  |
19+40       0.2894      0.05  Q         |          |          |       V  |
```

19+45	0.2897	0.05	Q	|	|	|	V |
19+50	0.2900	0.04	Q	|	|	|	V |
19+55	0.2902	0.04	Q	|	|	|	V |
20+ 0	0.2904	0.03	Q	|	|	|	V |
20+ 5	0.2907	0.03	Q	|	|	|	V |
20+10	0.2909	0.04	Q	|	|	|	V |
20+15	0.2912	0.04	Q	|	|	|	V |
20+20	0.2915	0.04	Q	|	|	|	V |
20+25	0.2918	0.04	Q	|	|	|	V |
20+30	0.2921	0.04	Q	|	|	|	V |
20+35	0.2924	0.04	Q	|	|	|	V |
20+40	0.2927	0.04	Q	|	|	|	V |
20+45	0.2930	0.04	Q	|	|	|	V |
20+50	0.2933	0.04	Q	|	|	|	V |
20+55	0.2935	0.03	Q	|	|	|	V |
21+ 0	0.2938	0.03	Q	|	|	|	V |
21+ 5	0.2940	0.03	Q	|	|	|	V |
21+10	0.2943	0.04	Q	|	|	|	V |
21+15	0.2945	0.04	Q	|	|	|	V |
21+20	0.2948	0.04	Q	|	|	|	V|
21+25	0.2951	0.03	Q	|	|	|	V|
21+30	0.2953	0.03	Q	|	|	|	V|
21+35	0.2955	0.03	Q	|	|	|	V|
21+40	0.2958	0.04	Q	|	|	|	V|
21+45	0.2961	0.04	Q	|	|	|	V|
21+50	0.2963	0.04	Q	|	|	|	V|
21+55	0.2966	0.03	Q	|	|	|	V|
22+ 0	0.2968	0.03	Q	|	|	|	V|
22+ 5	0.2970	0.03	Q	|	|	|	V|
22+10	0.2973	0.04	Q	|	|	|	V|
22+15	0.2976	0.04	Q	|	|	|	V|
22+20	0.2978	0.04	Q	|	|	|	V|
22+25	0.2981	0.03	Q	|	|	|	V|
22+30	0.2983	0.03	Q	|	|	|	V|
22+35	0.2985	0.03	Q	|	|	|	V|
22+40	0.2987	0.03	Q	|	|	|	V|
22+45	0.2989	0.03	Q	|	|	|	V|
22+50	0.2991	0.03	Q	|	|	|	V|
22+55	0.2993	0.03	Q	|	|	|	V|
23+ 0	0.2995	0.03	Q	|	|	|	V|
23+ 5	0.2997	0.03	Q	|	|	|	V|
23+10	0.2999	0.03	Q	|	|	|	V|
23+15	0.3001	0.03	Q	|	|	|	V|
23+20	0.3003	0.03	Q	|	|	|	V|
23+25	0.3005	0.03	Q	|	|	|	V|
23+30	0.3007	0.03	Q	|	|	|	V|
23+35	0.3009	0.03	Q	|	|	|	V|
23+40	0.3011	0.03	Q	|	|	|	V|
23+45	0.3013	0.03	Q	|	|	|	V|
23+50	0.3015	0.03	Q	|	|	|	V|

```
   23+55       0.3017      0.03  Q         |          |          |         V|
   24+ 0       0.3019      0.03  Q         |          |          |         V|
   24+ 5       0.3021      0.02  Q         |          |          |         V|
   24+10       0.3022      0.01  Q         |          |          |         V|
   24+15       0.3022      0.01  Q         |          |          |         V|
   24+20       0.3022      0.00  Q         |          |          |         V|
   24+25       0.3022      0.00  Q         |          |          |         V|
   24+30       0.3022      0.00  Q         |          |          |         V|
   24+35       0.3023      0.00  Q         |          |          |         V|
   24+40       0.3023      0.00  Q         |          |          |         V|
-------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris110.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
10 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.49	0.78

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            1.35                  2.13

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    0.493(In)
Area Averaged 100-Year Rainfall =    1.350(In)

Point rain (area averaged) =    0.846(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    0.846(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  32.0      0.742     0.900        0.141       1.000      0.141
                                                 Sum (F) =   0.141
Area averaged mean soil loss (F) (In/Hr) =  0.141
Minimum soil loss rate ((In/Hr)) =  0.070
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5000
------------------------------------------------------------------------

                U n i t  H y d r o g r a p h
                        VALLEY S-Curve
------------------------------------------------------------------------
                Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                              Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.20	0.426	(0.141)	0.077	0.349
2	0.17	4.30	0.436	(0.141)	0.079	0.358
3	0.25	5.00	0.507	(0.141)	0.091	0.416
4	0.33	5.00	0.507	(0.141)	0.091	0.416
5	0.42	5.80	0.589	(0.141)	0.106	0.483
6	0.50	6.50	0.660	(0.141)	0.119	0.541
7	0.58	7.40	0.751	(0.141)	0.135	0.616
8	0.67	8.60	0.873	0.141	(0.157)	0.732
9	0.75	12.30	1.248	0.141	(0.225)	1.107
10	0.83	29.10	2.953	0.141	(0.531)	2.812
11	0.92	6.80	0.690	(0.141)	0.124	0.566
12	1.00	5.00	0.507	(0.141)	0.091	0.416
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	8.8

Flood volume = Effective rainfall 0.73(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.1(Ac.Ft)
Total soil loss = 0.11(In)
Total soil loss = 0.015(Ac.Ft)
Total rainfall = 0.85(In)
Flood volume = 4211.0 Cubic Feet
Total soil loss = 638.6 Cubic Feet

Peak flow rate of this hydrograph = 2.774(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0007	0.10	Q				
0+10	0.0032	0.37	Q				
0+15	0.0066	0.48	QV				
0+20	0.0105	0.57	Q V				
0+25	0.0148	0.63	Q V				
0+30	0.0198	0.72	Q V				
0+35	0.0254	0.82	Q V				
0+40	0.0318	0.94	Q V				
0+45	0.0399	1.17	Q V				
0+50	0.0536	1.99	Q V				

```
    0+55       0.0727      2.77  |          |Q         |          V          |
    1+ 0       0.0832      1.51  |      Q   |          |          |   V      |
    1+ 5       0.0896      0.93  |  Q       |          |          |      V   |
    1+10       0.0926      0.44  |Q         |          |          |       V  |
    1+15       0.0944      0.26  |Q         |          |          |        V |
    1+20       0.0955      0.16  Q          |          |          |        V |
    1+25       0.0961      0.10  Q          |          |          |        V |
    1+30       0.0965      0.06  Q          |          |          |        V |
    1+35       0.0966      0.01  Q          |          |          |        V |
    1+40       0.0967      0.01  Q          |          |          |        V |
-------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris310.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
10 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.87	1.37

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            2.10                  3.32

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    0.869(In)
Area Averaged 100-Year Rainfall =    2.100(In)

Point rain (area averaged) =    1.375(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    1.375(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  32.0      0.742     0.900        0.141       1.000      0.141
                                                 Sum (F) =   0.141
Area averaged mean soil loss (F) (In/Hr) =  0.141
Minimum soil loss rate ((In/Hr)) =  0.070
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                               Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.215	(0.141)	0.039	0.176
2	0.17	1.30	0.215	(0.141)	0.039	0.176
3	0.25	1.10	0.182	(0.141)	0.033	0.149
4	0.33	1.50	0.248	(0.141)	0.045	0.203
5	0.42	1.50	0.248	(0.141)	0.045	0.203
6	0.50	1.80	0.297	(0.141)	0.053	0.244
7	0.58	1.50	0.248	(0.141)	0.045	0.203
8	0.67	1.80	0.297	(0.141)	0.053	0.244
9	0.75	1.80	0.297	(0.141)	0.053	0.244
10	0.83	1.50	0.248	(0.141)	0.045	0.203
11	0.92	1.60	0.264	(0.141)	0.048	0.217
12	1.00	1.80	0.297	(0.141)	0.053	0.244
13	1.08	2.20	0.363	(0.141)	0.065	0.298
14	1.17	2.20	0.363	(0.141)	0.065	0.298
15	1.25	2.20	0.363	(0.141)	0.065	0.298
16	1.33	2.00	0.330	(0.141)	0.059	0.271
17	1.42	2.60	0.429	(0.141)	0.077	0.352
18	1.50	2.70	0.446	(0.141)	0.080	0.365
19	1.58	2.40	0.396	(0.141)	0.071	0.325
20	1.67	2.70	0.446	(0.141)	0.080	0.365
21	1.75	3.30	0.545	(0.141)	0.098	0.447
22	1.83	3.10	0.512	(0.141)	0.092	0.420
23	1.92	2.90	0.479	(0.141)	0.086	0.392
24	2.00	3.00	0.495	(0.141)	0.089	0.406
25	2.08	3.10	0.512	(0.141)	0.092	0.420
26	2.17	4.20	0.693	(0.141)	0.125	0.568
27	2.25	5.00	0.825	0.141	(0.149)	0.684
28	2.33	3.50	0.578	(0.141)	0.104	0.474
29	2.42	6.80	1.122	0.141	(0.202)	0.981
30	2.50	7.30	1.205	0.141	(0.217)	1.064
31	2.58	8.20	1.353	0.141	(0.244)	1.212
32	2.67	5.90	0.974	0.141	(0.175)	0.833
33	2.75	2.00	0.330	(0.141)	0.059	0.271
34	2.83	1.80	0.297	(0.141)	0.053	0.244
35	2.92	1.80	0.297	(0.141)	0.053	0.244
36	3.00	0.60	0.099	(0.141)	0.018	0.081
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	13.8

Flood volume = Effective rainfall 1.15(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 0.22(In)
Total soil loss = 0.030(Ac.Ft)
Total rainfall = 1.38(In)
Flood volume = 6603.2 Cubic Feet
Total soil loss = 1285.4 Cubic Feet

Peak flow rate of this hydrograph = 1.644(CFS)

++

3 - H O U R S T O R M

R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0003	0.05	Q				
0+10	0.0016	0.18	Q				
0+15	0.0032	0.22	Q				
0+20	0.0048	0.24	QV				
0+25	0.0067	0.28	|Q				
0+30	0.0089	0.31	|QV				
0+35	0.0113	0.34	|QV				
0+40	0.0136	0.34	|Q V				
0+45	0.0161	0.37	|Q V				
0+50	0.0187	0.37	|Q V				
0+55	0.0210	0.34	|Q V				
1+ 0	0.0235	0.35	|Q V				
1+ 5	0.0262	0.39	|Q V				
1+10	0.0292	0.44	|Q V				
1+15	0.0323	0.46	|Q V				
1+20	0.0355	0.46	|Q V				
1+25	0.0386	0.46	|Q V				
1+30	0.0422	0.52	| Q |V				
1+35	0.0460	0.54	| Q | V				
1+40	0.0497	0.54	| Q | V				
1+45	0.0537	0.59	| Q | V				
1+50	0.0582	0.65	| Q | V				
1+55	0.0626	0.65	| Q | V				
2+ 0	0.0670	0.63	| Q | V				
2+ 5	0.0715	0.65	| Q | V				
2+10	0.0763	0.70	| Q | V				
2+15	0.0822	0.85	| Q |V				
2+20	0.0885	0.92	| Q | V				
2+25	0.0951	0.96	| Q | V				
2+30	0.1043	1.34	| Q | V				
2+35	0.1151	1.56	| Q | V				
2+40	0.1264	1.64	| Q | V				
2+45	0.1352	1.27	| Q | V				
2+50	0.1405	0.78	| Q | V				
2+55	0.1446	0.59	| Q | V				
3+ 0	0.1478	0.46	|Q | V				
3+ 5	0.1497	0.27	|Q | V				
3+10	0.1506	0.13	Q | V				

```
    3+15       0.1511      0.07  Q         |         |         |        V|
    3+20       0.1514      0.04  Q         |         |         |        V|
    3+25       0.1515      0.02  Q         |         |         |        V|
    3+30       0.1516      0.01  Q         |         |         |        V|
    3+35       0.1516      0.00  Q         |         |         |        V|
    3+40       0.1516      0.00  Q         |         |         |         V
---------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris610.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
10 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	1.22	1.93

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            2.87                   4.53

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    1.220(In)
Area Averaged 100-Year Rainfall =    2.870(In)

Point rain (area averaged) =    1.899(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    1.899(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  32.0      0.742     0.900        0.141       1.000      0.141
                                                 Sum (F) =   0.141
Area averaged mean soil loss (F) (In/Hr) =  0.141
Minimum soil loss rate ((In/Hr)) =  0.070
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                               Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

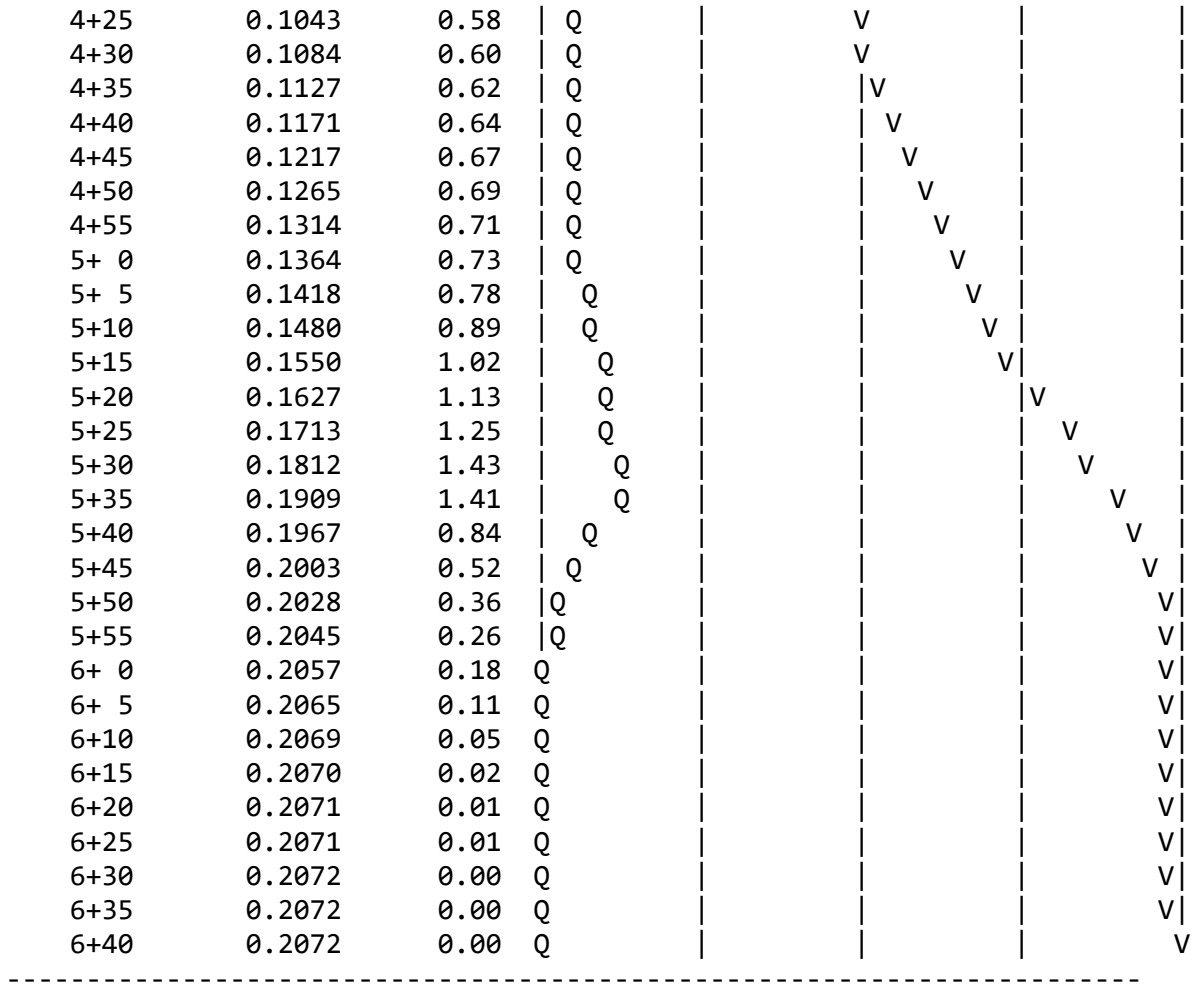
The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.114	(0.141)	0.021	0.093
2	0.17	0.60	0.137	(0.141)	0.025	0.112
3	0.25	0.60	0.137	(0.141)	0.025	0.112
4	0.33	0.60	0.137	(0.141)	0.025	0.112
5	0.42	0.60	0.137	(0.141)	0.025	0.112
6	0.50	0.70	0.160	(0.141)	0.029	0.131
7	0.58	0.70	0.160	(0.141)	0.029	0.131
8	0.67	0.70	0.160	(0.141)	0.029	0.131
9	0.75	0.70	0.160	(0.141)	0.029	0.131
10	0.83	0.70	0.160	(0.141)	0.029	0.131
11	0.92	0.70	0.160	(0.141)	0.029	0.131
12	1.00	0.80	0.182	(0.141)	0.033	0.149
13	1.08	0.80	0.182	(0.141)	0.033	0.149
14	1.17	0.80	0.182	(0.141)	0.033	0.149
15	1.25	0.80	0.182	(0.141)	0.033	0.149
16	1.33	0.80	0.182	(0.141)	0.033	0.149
17	1.42	0.80	0.182	(0.141)	0.033	0.149
18	1.50	0.80	0.182	(0.141)	0.033	0.149
19	1.58	0.80	0.182	(0.141)	0.033	0.149
20	1.67	0.80	0.182	(0.141)	0.033	0.149
21	1.75	0.80	0.182	(0.141)	0.033	0.149
22	1.83	0.80	0.182	(0.141)	0.033	0.149
23	1.92	0.80	0.182	(0.141)	0.033	0.149
24	2.00	0.90	0.205	(0.141)	0.037	0.168
25	2.08	0.80	0.182	(0.141)	0.033	0.149
26	2.17	0.90	0.205	(0.141)	0.037	0.168
27	2.25	0.90	0.205	(0.141)	0.037	0.168
28	2.33	0.90	0.205	(0.141)	0.037	0.168
29	2.42	0.90	0.205	(0.141)	0.037	0.168
30	2.50	0.90	0.205	(0.141)	0.037	0.168
31	2.58	0.90	0.205	(0.141)	0.037	0.168
32	2.67	0.90	0.205	(0.141)	0.037	0.168
33	2.75	1.00	0.228	(0.141)	0.041	0.187
34	2.83	1.00	0.228	(0.141)	0.041	0.187
35	2.92	1.00	0.228	(0.141)	0.041	0.187
36	3.00	1.00	0.228	(0.141)	0.041	0.187
37	3.08	1.00	0.228	(0.141)	0.041	0.187
38	3.17	1.10	0.251	(0.141)	0.045	0.206
39	3.25	1.10	0.251	(0.141)	0.045	0.206
40	3.33	1.10	0.251	(0.141)	0.045	0.206
41	3.42	1.20	0.273	(0.141)	0.049	0.224
42	3.50	1.30	0.296	(0.141)	0.053	0.243
43	3.58	1.40	0.319	(0.141)	0.057	0.262
44	3.67	1.40	0.319	(0.141)	0.057	0.262
45	3.75	1.50	0.342	(0.141)	0.062	0.280

```
46   3.83     1.50      0.342       (  0.141)       0.062        0.280
47   3.92     1.60      0.365       (  0.141)       0.066        0.299
48   4.00     1.60      0.365       (  0.141)       0.066        0.299
49   4.08     1.70      0.387       (  0.141)       0.070        0.318
50   4.17     1.80      0.410       (  0.141)       0.074        0.336
51   4.25     1.90      0.433       (  0.141)       0.078        0.355
52   4.33     2.00      0.456       (  0.141)       0.082        0.374
53   4.42     2.10      0.479       (  0.141)       0.086        0.392
54   4.50     2.10      0.479       (  0.141)       0.086        0.392
55   4.58     2.20      0.501       (  0.141)       0.090        0.411
56   4.67     2.30      0.524       (  0.141)       0.094        0.430
57   4.75     2.40      0.547       (  0.141)       0.098        0.448
58   4.83     2.40      0.547       (  0.141)       0.098        0.448
59   4.92     2.50      0.570       (  0.141)       0.103        0.467
60   5.00     2.60      0.592       (  0.141)       0.107        0.486
61   5.08     3.10      0.706       (  0.141)       0.127        0.579
62   5.17     3.60      0.820          0.141    (  0.148)        0.679
63   5.25     3.90      0.889          0.141    (  0.160)        0.748
64   5.33     4.20      0.957          0.141    (  0.172)        0.816
65   5.42     4.70      1.071          0.141    (  0.193)        0.930
66   5.50     5.60      1.276          0.141    (  0.230)        1.135
67   5.58     1.90      0.433       (  0.141)       0.078        0.355
68   5.67     0.90      0.205       (  0.141)       0.037        0.168
69   5.75     0.60      0.137       (  0.141)       0.025        0.112
70   5.83     0.50      0.114       (  0.141)       0.021        0.093
71   5.92     0.30      0.068       (  0.141)       0.012        0.056
72   6.00     0.20      0.046       (  0.141)       0.008        0.037
               (Loss Rate Not Used)
   Sum =     100.0                                    Sum =    18.9
      Flood volume = Effective rainfall      1.57(In)
       times area       1.6(Ac.)/[(In)/(Ft.)] =       0.2(Ac.Ft)
      Total soil loss =      0.33(In)
      Total soil loss =     0.043(Ac.Ft)
      Total rainfall =      1.90(In)
      Flood volume =        9024.5 Cubic Feet
      Total soil loss =        1865.9 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      1.431(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0002      0.03  Q         |         |         |         |
  0+10       0.0009      0.10  Q         |         |         |         |
```

```
0+15       0.0019      0.14  Q         |         |         |         |
0+20       0.0030      0.16  Q         |         |         |         |
0+25       0.0041      0.17  Q         |         |         |         |
0+30       0.0053      0.18  QV        |         |         |         |
0+35       0.0067      0.19  QV        |         |         |         |
0+40       0.0080      0.20  QV        |         |         |         |
0+45       0.0095      0.21  QV        |         |         |         |
0+50       0.0109      0.21  Q V       |         |         |         |
0+55       0.0123      0.21  Q V       |         |         |         |
1+ 0       0.0138      0.21  Q V       |         |         |         |
1+ 5       0.0153      0.23  Q V       |         |         |         |
1+10       0.0169      0.23  Q  V      |         |         |         |
1+15       0.0186      0.24  Q  V      |         |         |         |
1+20       0.0202      0.24  Q  V      |         |         |         |
1+25       0.0218      0.24  Q   V     |         |         |         |
1+30       0.0235      0.24  Q   V     |         |         |         |
1+35       0.0251      0.24  Q   V     |         |         |         |
1+40       0.0267      0.24  Q    V    |         |         |         |
1+45       0.0284      0.24  Q    V    |         |         |         |
1+50       0.0300      0.24  Q    V    |         |         |         |
1+55       0.0317      0.24  Q     V   |         |         |         |
2+ 0       0.0333      0.24  Q     V   |         |         |         |
2+ 5       0.0351      0.25  |Q    V   |         |         |         |
2+10       0.0368      0.25  Q      V  |         |         |         |
2+15       0.0386      0.26  |Q     V  |         |         |         |
2+20       0.0404      0.26  |Q     V  |         |         |         |
2+25       0.0422      0.27  |Q      V |         |         |         |
2+30       0.0441      0.27  |Q      V |         |         |         |
2+35       0.0459      0.27  |Q      V |         |         |         |
2+40       0.0477      0.27  |Q       V|         |         |         |
2+45       0.0496      0.27  |Q       V|         |         |         |
2+50       0.0516      0.29  |Q       V|         |         |         |
2+55       0.0536      0.29  |Q        V         |         |         |
3+ 0       0.0556      0.29  |Q        V         |         |         |
3+ 5       0.0577      0.30  |Q        |V        |         |         |
3+10       0.0598      0.30  |Q        |V        |         |         |
3+15       0.0619      0.32  |Q        |V        |         |         |
3+20       0.0642      0.32  |Q        | V       |         |         |
3+25       0.0664      0.33  |Q        | V       |         |         |
3+30       0.0688      0.35  |Q        |  V      |         |         |
3+35       0.0714      0.38  |Q        |  V      |         |         |
3+40       0.0742      0.40  |Q        |   V     |         |         |
3+45       0.0770      0.41  |Q        |   V     |         |         |
3+50       0.0800      0.43  |Q        |    V    |         |         |
3+55       0.0830      0.44  |Q        |     V   |         |         |
4+ 0       0.0862      0.46  |Q        |     V   |         |         |
4+ 5       0.0895      0.47  |Q        |      V  |         |         |
4+10       0.0929      0.50  |Q        |      V  |         |         |
4+15       0.0965      0.52  | Q       |       V |         |         |
4+20       0.1003      0.55  | Q       |        V|         |         |
```


4+25 0.1043 0.58
4+30 0.1084 0.60
4+35 0.1127 0.62
4+40 0.1171 0.64
4+45 0.1217 0.67
4+50 0.1265 0.69
4+55 0.1314 0.71
5+ 0 0.1364 0.73
5+ 5 0.1418 0.78
5+10 0.1480 0.89
5+15 0.1550 1.02
5+20 0.1627 1.13
5+25 0.1713 1.25
5+30 0.1812 1.43
5+35 0.1909 1.41
5+40 0.1967 0.84
5+45 0.2003 0.52
5+50 0.2028 0.36
5+55 0.2045 0.26
6+ 0 0.2057 0.18
6+ 5 0.2065 0.11
6+10 0.2069 0.05
6+15 0.2070 0.02
6+20 0.2071 0.01
6+25 0.2071 0.01
6+30 0.2072 0.00
6+35 0.2072 0.00
6+40 0.2072 0.00

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris2410.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
10 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.05	3.24

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            5.25                  8.29

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    2.050(In)
Area Averaged 100-Year Rainfall =    5.250(In)

Point rain (area averaged) =    3.367(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    3.366(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  32.0      0.742     0.900        0.141       1.000      0.141
                                                 Sum (F) =   0.141
Area averaged mean soil loss (F) (In/Hr) =  0.141
Minimum soil loss rate ((In/Hr)) =  0.070
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945             0.286
    2   0.167        191.791         48.003             0.764
    3   0.250        287.687         16.299             0.260
    4   0.333        383.583          7.288             0.116
    5   0.417        479.478          4.149             0.066
    6   0.500        575.374          2.689             0.043
    7   0.583        671.270          1.732             0.028
    8   0.667        767.165          1.088             0.017
    9   0.750        863.061          0.808             0.013
                               Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.027	(0.250)	0.005	0.022
2	0.17	0.07	0.027	(0.249)	0.005	0.022
3	0.25	0.07	0.027	(0.248)	0.005	0.022
4	0.33	0.10	0.040	(0.247)	0.007	0.033
5	0.42	0.10	0.040	(0.246)	0.007	0.033
6	0.50	0.10	0.040	(0.245)	0.007	0.033
7	0.58	0.10	0.040	(0.244)	0.007	0.033
8	0.67	0.10	0.040	(0.243)	0.007	0.033
9	0.75	0.10	0.040	(0.242)	0.007	0.033
10	0.83	0.13	0.054	(0.241)	0.010	0.044
11	0.92	0.13	0.054	(0.240)	0.010	0.044
12	1.00	0.13	0.054	(0.239)	0.010	0.044
13	1.08	0.10	0.040	(0.238)	0.007	0.033
14	1.17	0.10	0.040	(0.238)	0.007	0.033
15	1.25	0.10	0.040	(0.237)	0.007	0.033
16	1.33	0.10	0.040	(0.236)	0.007	0.033
17	1.42	0.10	0.040	(0.235)	0.007	0.033
18	1.50	0.10	0.040	(0.234)	0.007	0.033
19	1.58	0.10	0.040	(0.233)	0.007	0.033
20	1.67	0.10	0.040	(0.232)	0.007	0.033
21	1.75	0.10	0.040	(0.231)	0.007	0.033
22	1.83	0.13	0.054	(0.230)	0.010	0.044
23	1.92	0.13	0.054	(0.229)	0.010	0.044
24	2.00	0.13	0.054	(0.228)	0.010	0.044
25	2.08	0.13	0.054	(0.227)	0.010	0.044
26	2.17	0.13	0.054	(0.226)	0.010	0.044
27	2.25	0.13	0.054	(0.225)	0.010	0.044
28	2.33	0.13	0.054	(0.224)	0.010	0.044
29	2.42	0.13	0.054	(0.224)	0.010	0.044
30	2.50	0.13	0.054	(0.223)	0.010	0.044
31	2.58	0.17	0.067	(0.222)	0.012	0.055
32	2.67	0.17	0.067	(0.221)	0.012	0.055
33	2.75	0.17	0.067	(0.220)	0.012	0.055
34	2.83	0.17	0.067	(0.219)	0.012	0.055
35	2.92	0.17	0.067	(0.218)	0.012	0.055
36	3.00	0.17	0.067	(0.217)	0.012	0.055
37	3.08	0.17	0.067	(0.216)	0.012	0.055
38	3.17	0.17	0.067	(0.215)	0.012	0.055
39	3.25	0.17	0.067	(0.215)	0.012	0.055
40	3.33	0.17	0.067	(0.214)	0.012	0.055
41	3.42	0.17	0.067	(0.213)	0.012	0.055
42	3.50	0.17	0.067	(0.212)	0.012	0.055
43	3.58	0.17	0.067	(0.211)	0.012	0.055
44	3.67	0.17	0.067	(0.210)	0.012	0.055
45	3.75	0.17	0.067	(0.209)	0.012	0.055

46	3.83	0.20	0.081	(0.208)	0.015	0.066
47	3.92	0.20	0.081	(0.207)	0.015	0.066
48	4.00	0.20	0.081	(0.207)	0.015	0.066
49	4.08	0.20	0.081	(0.206)	0.015	0.066
50	4.17	0.20	0.081	(0.205)	0.015	0.066
51	4.25	0.20	0.081	(0.204)	0.015	0.066
52	4.33	0.23	0.094	(0.203)	0.017	0.077
53	4.42	0.23	0.094	(0.202)	0.017	0.077
54	4.50	0.23	0.094	(0.201)	0.017	0.077
55	4.58	0.23	0.094	(0.200)	0.017	0.077
56	4.67	0.23	0.094	(0.200)	0.017	0.077
57	4.75	0.23	0.094	(0.199)	0.017	0.077
58	4.83	0.27	0.108	(0.198)	0.019	0.088
59	4.92	0.27	0.108	(0.197)	0.019	0.088
60	5.00	0.27	0.108	(0.196)	0.019	0.088
61	5.08	0.20	0.081	(0.195)	0.015	0.066
62	5.17	0.20	0.081	(0.194)	0.015	0.066
63	5.25	0.20	0.081	(0.194)	0.015	0.066
64	5.33	0.23	0.094	(0.193)	0.017	0.077
65	5.42	0.23	0.094	(0.192)	0.017	0.077
66	5.50	0.23	0.094	(0.191)	0.017	0.077
67	5.58	0.27	0.108	(0.190)	0.019	0.088
68	5.67	0.27	0.108	(0.189)	0.019	0.088
69	5.75	0.27	0.108	(0.189)	0.019	0.088
70	5.83	0.27	0.108	(0.188)	0.019	0.088
71	5.92	0.27	0.108	(0.187)	0.019	0.088
72	6.00	0.27	0.108	(0.186)	0.019	0.088
73	6.08	0.30	0.121	(0.185)	0.022	0.099
74	6.17	0.30	0.121	(0.184)	0.022	0.099
75	6.25	0.30	0.121	(0.184)	0.022	0.099
76	6.33	0.30	0.121	(0.183)	0.022	0.099
77	6.42	0.30	0.121	(0.182)	0.022	0.099
78	6.50	0.30	0.121	(0.181)	0.022	0.099
79	6.58	0.33	0.135	(0.180)	0.024	0.110
80	6.67	0.33	0.135	(0.180)	0.024	0.110
81	6.75	0.33	0.135	(0.179)	0.024	0.110
82	6.83	0.33	0.135	(0.178)	0.024	0.110
83	6.92	0.33	0.135	(0.177)	0.024	0.110
84	7.00	0.33	0.135	(0.176)	0.024	0.110
85	7.08	0.33	0.135	(0.176)	0.024	0.110
86	7.17	0.33	0.135	(0.175)	0.024	0.110
87	7.25	0.33	0.135	(0.174)	0.024	0.110
88	7.33	0.37	0.148	(0.173)	0.027	0.121
89	7.42	0.37	0.148	(0.172)	0.027	0.121
90	7.50	0.37	0.148	(0.172)	0.027	0.121
91	7.58	0.40	0.162	(0.171)	0.029	0.133
92	7.67	0.40	0.162	(0.170)	0.029	0.133
93	7.75	0.40	0.162	(0.169)	0.029	0.133
94	7.83	0.43	0.175	(0.168)	0.032	0.144
95	7.92	0.43	0.175	(0.168)	0.032	0.144

96	8.00	0.43	0.175	(0.167)	0.032	0.144
97	8.08	0.50	0.202	(0.166)	0.036	0.166
98	8.17	0.50	0.202	(0.165)	0.036	0.166
99	8.25	0.50	0.202	(0.165)	0.036	0.166
100	8.33	0.50	0.202	(0.164)	0.036	0.166
101	8.42	0.50	0.202	(0.163)	0.036	0.166
102	8.50	0.50	0.202	(0.162)	0.036	0.166
103	8.58	0.53	0.215	(0.161)	0.039	0.177
104	8.67	0.53	0.215	(0.161)	0.039	0.177
105	8.75	0.53	0.215	(0.160)	0.039	0.177
106	8.83	0.57	0.229	(0.159)	0.041	0.188
107	8.92	0.57	0.229	(0.158)	0.041	0.188
108	9.00	0.57	0.229	(0.158)	0.041	0.188
109	9.08	0.63	0.256	(0.157)	0.046	0.210
110	9.17	0.63	0.256	(0.156)	0.046	0.210
111	9.25	0.63	0.256	(0.155)	0.046	0.210
112	9.33	0.67	0.269	(0.155)	0.048	0.221
113	9.42	0.67	0.269	(0.154)	0.048	0.221
114	9.50	0.67	0.269	(0.153)	0.048	0.221
115	9.58	0.70	0.283	(0.153)	0.051	0.232
116	9.67	0.70	0.283	(0.152)	0.051	0.232
117	9.75	0.70	0.283	(0.151)	0.051	0.232
118	9.83	0.73	0.296	(0.150)	0.053	0.243
119	9.92	0.73	0.296	(0.150)	0.053	0.243
120	10.00	0.73	0.296	(0.149)	0.053	0.243
121	10.08	0.50	0.202	(0.148)	0.036	0.166
122	10.17	0.50	0.202	(0.147)	0.036	0.166
123	10.25	0.50	0.202	(0.147)	0.036	0.166
124	10.33	0.50	0.202	(0.146)	0.036	0.166
125	10.42	0.50	0.202	(0.145)	0.036	0.166
126	10.50	0.50	0.202	(0.145)	0.036	0.166
127	10.58	0.67	0.269	(0.144)	0.048	0.221
128	10.67	0.67	0.269	(0.143)	0.048	0.221
129	10.75	0.67	0.269	(0.142)	0.048	0.221
130	10.83	0.67	0.269	(0.142)	0.048	0.221
131	10.92	0.67	0.269	(0.141)	0.048	0.221
132	11.00	0.67	0.269	(0.140)	0.048	0.221
133	11.08	0.63	0.256	(0.140)	0.046	0.210
134	11.17	0.63	0.256	(0.139)	0.046	0.210
135	11.25	0.63	0.256	(0.138)	0.046	0.210
136	11.33	0.63	0.256	(0.138)	0.046	0.210
137	11.42	0.63	0.256	(0.137)	0.046	0.210
138	11.50	0.63	0.256	(0.136)	0.046	0.210
139	11.58	0.57	0.229	(0.136)	0.041	0.188
140	11.67	0.57	0.229	(0.135)	0.041	0.188
141	11.75	0.57	0.229	(0.134)	0.041	0.188
142	11.83	0.60	0.242	(0.134)	0.044	0.199
143	11.92	0.60	0.242	(0.133)	0.044	0.199
144	12.00	0.60	0.242	(0.132)	0.044	0.199
145	12.08	0.83	0.337	(0.132)	0.061	0.276

146	12.17	0.83	0.337	(0.131)	0.061	0.276
147	12.25	0.83	0.337	(0.130)	0.061	0.276
148	12.33	0.87	0.350	(0.130)	0.063	0.287
149	12.42	0.87	0.350	(0.129)	0.063	0.287
150	12.50	0.87	0.350	(0.128)	0.063	0.287
151	12.58	0.93	0.377	(0.128)	0.068	0.309
152	12.67	0.93	0.377	(0.127)	0.068	0.309
153	12.75	0.93	0.377	(0.126)	0.068	0.309
154	12.83	0.97	0.391	(0.126)	0.070	0.320
155	12.92	0.97	0.391	(0.125)	0.070	0.320
156	13.00	0.97	0.391	(0.124)	0.070	0.320
157	13.08	1.13	0.458	(0.124)	0.082	0.375
158	13.17	1.13	0.458	(0.123)	0.082	0.375
159	13.25	1.13	0.458	(0.123)	0.082	0.375
160	13.33	1.13	0.458	(0.122)	0.082	0.375
161	13.42	1.13	0.458	(0.121)	0.082	0.375
162	13.50	1.13	0.458	(0.121)	0.082	0.375
163	13.58	0.77	0.310	(0.120)	0.056	0.254
164	13.67	0.77	0.310	(0.120)	0.056	0.254
165	13.75	0.77	0.310	(0.119)	0.056	0.254
166	13.83	0.77	0.310	(0.118)	0.056	0.254
167	13.92	0.77	0.310	(0.118)	0.056	0.254
168	14.00	0.77	0.310	(0.117)	0.056	0.254
169	14.08	0.90	0.364	(0.117)	0.065	0.298
170	14.17	0.90	0.364	(0.116)	0.065	0.298
171	14.25	0.90	0.364	(0.115)	0.065	0.298
172	14.33	0.87	0.350	(0.115)	0.063	0.287
173	14.42	0.87	0.350	(0.114)	0.063	0.287
174	14.50	0.87	0.350	(0.114)	0.063	0.287
175	14.58	0.87	0.350	(0.113)	0.063	0.287
176	14.67	0.87	0.350	(0.112)	0.063	0.287
177	14.75	0.87	0.350	(0.112)	0.063	0.287
178	14.83	0.83	0.337	(0.111)	0.061	0.276
179	14.92	0.83	0.337	(0.111)	0.061	0.276
180	15.00	0.83	0.337	(0.110)	0.061	0.276
181	15.08	0.80	0.323	(0.110)	0.058	0.265
182	15.17	0.80	0.323	(0.109)	0.058	0.265
183	15.25	0.80	0.323	(0.108)	0.058	0.265
184	15.33	0.77	0.310	(0.108)	0.056	0.254
185	15.42	0.77	0.310	(0.107)	0.056	0.254
186	15.50	0.77	0.310	(0.107)	0.056	0.254
187	15.58	0.63	0.256	(0.106)	0.046	0.210
188	15.67	0.63	0.256	(0.106)	0.046	0.210
189	15.75	0.63	0.256	(0.105)	0.046	0.210
190	15.83	0.63	0.256	(0.105)	0.046	0.210
191	15.92	0.63	0.256	(0.104)	0.046	0.210
192	16.00	0.63	0.256	(0.104)	0.046	0.210
193	16.08	0.13	0.054	(0.103)	0.010	0.044
194	16.17	0.13	0.054	(0.102)	0.010	0.044
195	16.25	0.13	0.054	(0.102)	0.010	0.044

196	16.33	0.13	0.054	(0.101)	0.010	0.044
197	16.42	0.13	0.054	(0.101)	0.010	0.044
198	16.50	0.13	0.054	(0.100)	0.010	0.044
199	16.58	0.10	0.040	(0.100)	0.007	0.033
200	16.67	0.10	0.040	(0.099)	0.007	0.033
201	16.75	0.10	0.040	(0.099)	0.007	0.033
202	16.83	0.10	0.040	(0.098)	0.007	0.033
203	16.92	0.10	0.040	(0.098)	0.007	0.033
204	17.00	0.10	0.040	(0.097)	0.007	0.033
205	17.08	0.17	0.067	(0.097)	0.012	0.055
206	17.17	0.17	0.067	(0.096)	0.012	0.055
207	17.25	0.17	0.067	(0.096)	0.012	0.055
208	17.33	0.17	0.067	(0.095)	0.012	0.055
209	17.42	0.17	0.067	(0.095)	0.012	0.055
210	17.50	0.17	0.067	(0.094)	0.012	0.055
211	17.58	0.17	0.067	(0.094)	0.012	0.055
212	17.67	0.17	0.067	(0.094)	0.012	0.055
213	17.75	0.17	0.067	(0.093)	0.012	0.055
214	17.83	0.13	0.054	(0.093)	0.010	0.044
215	17.92	0.13	0.054	(0.092)	0.010	0.044
216	18.00	0.13	0.054	(0.092)	0.010	0.044
217	18.08	0.13	0.054	(0.091)	0.010	0.044
218	18.17	0.13	0.054	(0.091)	0.010	0.044
219	18.25	0.13	0.054	(0.090)	0.010	0.044
220	18.33	0.13	0.054	(0.090)	0.010	0.044
221	18.42	0.13	0.054	(0.089)	0.010	0.044
222	18.50	0.13	0.054	(0.089)	0.010	0.044
223	18.58	0.10	0.040	(0.089)	0.007	0.033
224	18.67	0.10	0.040	(0.088)	0.007	0.033
225	18.75	0.10	0.040	(0.088)	0.007	0.033
226	18.83	0.07	0.027	(0.087)	0.005	0.022
227	18.92	0.07	0.027	(0.087)	0.005	0.022
228	19.00	0.07	0.027	(0.087)	0.005	0.022
229	19.08	0.10	0.040	(0.086)	0.007	0.033
230	19.17	0.10	0.040	(0.086)	0.007	0.033
231	19.25	0.10	0.040	(0.085)	0.007	0.033
232	19.33	0.13	0.054	(0.085)	0.010	0.044
233	19.42	0.13	0.054	(0.085)	0.010	0.044
234	19.50	0.13	0.054	(0.084)	0.010	0.044
235	19.58	0.10	0.040	(0.084)	0.007	0.033
236	19.67	0.10	0.040	(0.083)	0.007	0.033
237	19.75	0.10	0.040	(0.083)	0.007	0.033
238	19.83	0.07	0.027	(0.083)	0.005	0.022
239	19.92	0.07	0.027	(0.082)	0.005	0.022
240	20.00	0.07	0.027	(0.082)	0.005	0.022
241	20.08	0.10	0.040	(0.082)	0.007	0.033
242	20.17	0.10	0.040	(0.081)	0.007	0.033
243	20.25	0.10	0.040	(0.081)	0.007	0.033
244	20.33	0.10	0.040	(0.080)	0.007	0.033
245	20.42	0.10	0.040	(0.080)	0.007	0.033

246	20.50	0.10	0.040	(0.080)	0.007	0.033
247	20.58	0.10	0.040	(0.079)	0.007	0.033
248	20.67	0.10	0.040	(0.079)	0.007	0.033
249	20.75	0.10	0.040	(0.079)	0.007	0.033
250	20.83	0.07	0.027	(0.078)	0.005	0.022
251	20.92	0.07	0.027	(0.078)	0.005	0.022
252	21.00	0.07	0.027	(0.078)	0.005	0.022
253	21.08	0.10	0.040	(0.078)	0.007	0.033
254	21.17	0.10	0.040	(0.077)	0.007	0.033
255	21.25	0.10	0.040	(0.077)	0.007	0.033
256	21.33	0.07	0.027	(0.077)	0.005	0.022
257	21.42	0.07	0.027	(0.076)	0.005	0.022
258	21.50	0.07	0.027	(0.076)	0.005	0.022
259	21.58	0.10	0.040	(0.076)	0.007	0.033
260	21.67	0.10	0.040	(0.075)	0.007	0.033
261	21.75	0.10	0.040	(0.075)	0.007	0.033
262	21.83	0.07	0.027	(0.075)	0.005	0.022
263	21.92	0.07	0.027	(0.075)	0.005	0.022
264	22.00	0.07	0.027	(0.074)	0.005	0.022
265	22.08	0.10	0.040	(0.074)	0.007	0.033
266	22.17	0.10	0.040	(0.074)	0.007	0.033
267	22.25	0.10	0.040	(0.074)	0.007	0.033
268	22.33	0.07	0.027	(0.073)	0.005	0.022
269	22.42	0.07	0.027	(0.073)	0.005	0.022
270	22.50	0.07	0.027	(0.073)	0.005	0.022
271	22.58	0.07	0.027	(0.073)	0.005	0.022
272	22.67	0.07	0.027	(0.073)	0.005	0.022
273	22.75	0.07	0.027	(0.072)	0.005	0.022
274	22.83	0.07	0.027	(0.072)	0.005	0.022
275	22.92	0.07	0.027	(0.072)	0.005	0.022
276	23.00	0.07	0.027	(0.072)	0.005	0.022
277	23.08	0.07	0.027	(0.072)	0.005	0.022
278	23.17	0.07	0.027	(0.072)	0.005	0.022
279	23.25	0.07	0.027	(0.071)	0.005	0.022
280	23.33	0.07	0.027	(0.071)	0.005	0.022
281	23.42	0.07	0.027	(0.071)	0.005	0.022
282	23.50	0.07	0.027	(0.071)	0.005	0.022
283	23.58	0.07	0.027	(0.071)	0.005	0.022
284	23.67	0.07	0.027	(0.071)	0.005	0.022
285	23.75	0.07	0.027	(0.071)	0.005	0.022
286	23.83	0.07	0.027	(0.071)	0.005	0.022
287	23.92	0.07	0.027	(0.071)	0.005	0.022
288	24.00	0.07	0.027	(0.070)	0.005	0.022

(Loss Rate Not Used)

Sum = 100.0 Sum = 33.1

Flood volume = Effective rainfall 2.76(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.4(Ac.Ft)
Total soil loss = 0.61(In)
Total soil loss = 0.080(Ac.Ft)
Total rainfall = 3.37(In)

Flood volume = 15832.7 Cubic Feet
Total soil loss = 3475.5 Cubic Feet

Peak flow rate of this hydrograph = 0.595(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.01	Q				
0+10	0.0002	0.02	Q				
0+15	0.0004	0.03	Q				
0+20	0.0006	0.03	Q				
0+25	0.0009	0.04	Q				
0+30	0.0013	0.05	Q				
0+35	0.0016	0.05	Q				
0+40	0.0020	0.05	Q				
0+45	0.0023	0.05	Q				
0+50	0.0027	0.06	Q				
0+55	0.0032	0.06	Q				
1+ 0	0.0036	0.07	Q				
1+ 5	0.0041	0.07	Q				
1+10	0.0045	0.06	Q				
1+15	0.0049	0.06	Q				
1+20	0.0052	0.05	Q				
1+25	0.0056	0.05	Q				
1+30	0.0060	0.05	Q				
1+35	0.0063	0.05	Q				
1+40	0.0067	0.05	Q				
1+45	0.0071	0.05	Q				
1+50	0.0074	0.06	Q				
1+55	0.0079	0.06	Q				
2+ 0	0.0084	0.07	Q				
2+ 5	0.0088	0.07	Q				
2+10	0.0093	0.07	QV				
2+15	0.0098	0.07	QV				
2+20	0.0103	0.07	QV				
2+25	0.0107	0.07	QV				
2+30	0.0112	0.07	QV				
2+35	0.0117	0.07	QV				
2+40	0.0123	0.08	QV				
2+45	0.0129	0.08	QV				
2+50	0.0135	0.09	QV				
2+55	0.0141	0.09	QV				
3+ 0	0.0147	0.09	QV				

3+ 5	0.0153	0.09	QV	|	|	|	|
3+10	0.0159	0.09	QV	|	|	|	|
3+15	0.0165	0.09	QV	|	|	|	|
3+20	0.0171	0.09	QV	|	|	|	|
3+25	0.0177	0.09	QV	|	|	|	|
3+30	0.0183	0.09	Q V	|	|	|	|
3+35	0.0189	0.09	Q V	|	|	|	|
3+40	0.0195	0.09	Q V	|	|	|	|
3+45	0.0201	0.09	Q V	|	|	|	|
3+50	0.0208	0.09	Q V	|	|	|	|
3+55	0.0214	0.10	Q V	|	|	|	|
4+ 0	0.0221	0.10	Q V	|	|	|	|
4+ 5	0.0229	0.10	Q V	|	|	|	|
4+10	0.0236	0.10	Q V	|	|	|	|
4+15	0.0243	0.10	Q V	|	|	|	|
4+20	0.0251	0.11	Q V	|	|	|	|
4+25	0.0259	0.12	Q V	|	|	|	|
4+30	0.0267	0.12	Q V	|	|	|	|
4+35	0.0275	0.12	Q V	|	|	|	|
4+40	0.0284	0.12	Q V	|	|	|	|
4+45	0.0292	0.12	Q V	|	|	|	|
4+50	0.0301	0.13	Q V	|	|	|	|
4+55	0.0310	0.13	Q V	|	|	|	|
5+ 0	0.0319	0.14	Q V	|	|	|	|
5+ 5	0.0329	0.13	Q V	|	|	|	|
5+10	0.0337	0.12	Q V	|	|	|	|
5+15	0.0344	0.11	Q V	|	|	|	|
5+20	0.0352	0.11	Q V	|	|	|	|
5+25	0.0360	0.12	Q V	|	|	|	|
5+30	0.0369	0.12	Q V	|	|	|	|
5+35	0.0377	0.13	Q V	|	|	|	|
5+40	0.0386	0.13	Q V	|	|	|	|
5+45	0.0396	0.14	Q V	|	|	|	|
5+50	0.0405	0.14	Q V	|	|	|	|
5+55	0.0415	0.14	Q V	|	|	|	|
6+ 0	0.0425	0.14	Q V	|	|	|	|
6+ 5	0.0435	0.14	Q V	|	|	|	|
6+10	0.0445	0.15	Q V	|	|	|	|
6+15	0.0456	0.16	Q V	|	|	|	|
6+20	0.0466	0.16	Q V	|	|	|	|
6+25	0.0477	0.16	Q V	|	|	|	|
6+30	0.0488	0.16	Q V	|	|	|	|
6+35	0.0499	0.16	Q V	|	|	|	|
6+40	0.0511	0.17	Q V	|	|	|	|
6+45	0.0523	0.17	Q V	|	|	|	|
6+50	0.0535	0.17	Q V	|	|	|	|
6+55	0.0547	0.17	Q V	|	|	|	|
7+ 0	0.0559	0.18	Q V	|	|	|	|
7+ 5	0.0571	0.18	Q V	|	|	|	|
7+10	0.0583	0.18	Q V	|	|	|	|

```
 7+15       0.0595      0.18  Q     V   |           |           |           |
 7+20       0.0608      0.18  Q     V   |           |           |           |
 7+25       0.0620      0.19  Q     V   |           |           |           |
 7+30       0.0634      0.19  Q     V   |           |           |           |
 7+35       0.0647      0.19  Q      V  |           |           |           |
 7+40       0.0661      0.20  Q      V  |           |           |           |
 7+45       0.0675      0.21  Q      V  |           |           |           |
 7+50       0.0690      0.21  Q      V  |           |           |           |
 7+55       0.0705      0.22  Q      V  |           |           |           |
 8+ 0       0.0721      0.22  Q      V  |           |           |           |
 8+ 5       0.0737      0.23  Q       V |           |           |           |
 8+10       0.0754      0.25  |Q      V |           |           |           |
 8+15       0.0772      0.26  |Q      V |           |           |           |
 8+20       0.0790      0.26  |Q      V |           |           |           |
 8+25       0.0808      0.26  |Q      V |           |           |           |
 8+30       0.0826      0.26  |Q       V|           |           |           |
 8+35       0.0844      0.27  |Q       V|           |           |           |
 8+40       0.0863      0.28  |Q       V|           |           |           |
 8+45       0.0882      0.28  |Q       V|           |           |           |
 8+50       0.0902      0.28  |Q       V|           |           |           |
 8+55       0.0922      0.29  |Q        V           |           |           |
 9+ 0       0.0942      0.30  |Q        V           |           |           |
 9+ 5       0.0963      0.30  |Q        V           |           |           |
 9+10       0.0985      0.32  |Q        V           |           |           |
 9+15       0.1008      0.33  |Q         |V          |           |           |
 9+20       0.1031      0.33  |Q         |V          |           |           |
 9+25       0.1054      0.34  |Q         |V          |           |           |
 9+30       0.1078      0.35  |Q         |V          |           |           |
 9+35       0.1102      0.35  |Q         | V         |           |           |
 9+40       0.1127      0.36  |Q         | V         |           |           |
 9+45       0.1153      0.37  |Q         | V         |           |           |
 9+50       0.1178      0.37  |Q         | V         |           |           |
 9+55       0.1204      0.38  |Q         |  V        |           |           |
10+ 0       0.1231      0.38  |Q         |  V        |           |           |
10+ 5       0.1256      0.36  |Q         |  V        |           |           |
10+10       0.1277      0.30  |Q         |   V       |           |           |
10+15       0.1296      0.29  |Q         |   V       |           |           |
10+20       0.1315      0.28  |Q         |   V       |           |           |
10+25       0.1334      0.27  |Q         |   V       |           |           |
10+30       0.1352      0.27  |Q         |   V       |           |           |
10+35       0.1372      0.28  |Q         |    V      |           |           |
10+40       0.1394      0.32  |Q         |    V      |           |           |
10+45       0.1417      0.34  |Q         |    V      |           |           |
10+50       0.1441      0.34  |Q         |    V      |           |           |
10+55       0.1465      0.35  |Q         |     V     |           |           |
11+ 0       0.1489      0.35  |Q         |     V     |           |           |
11+ 5       0.1513      0.35  |Q         |     V     |           |           |
11+10       0.1536      0.34  |Q         |     V     |           |           |
11+15       0.1559      0.34  |Q         |      V    |           |           |
11+20       0.1582      0.34  |Q         |      V    |           |           |
```

```
11+25       0.1605      0.34  |Q        |      V  |         |         |
11+30       0.1629      0.33  |Q        |      V  |         |         |
11+35       0.1651      0.33  |Q        |       V |         |         |
11+40       0.1673      0.31  |Q        |       V |         |         |
11+45       0.1694      0.31  |Q        |       V |         |         |
11+50       0.1715      0.31  |Q        |       V |         |         |
11+55       0.1736      0.31  |Q        |        V|         |         |
12+ 0       0.1758      0.31  |Q        |        V|         |         |
12+ 5       0.1781      0.34  |Q        |        V|         |         |
12+10       0.1808      0.40  |Q        |        V|         |         |
12+15       0.1837      0.42  |Q        |         V         |         |
12+20       0.1867      0.43  |Q        |         V         |         |
12+25       0.1897      0.44  |Q        |         V         |         |
12+30       0.1928      0.45  |Q        |         |V        |         |
12+35       0.1960      0.46  |Q        |         |V        |         |
12+40       0.1993      0.48  |Q        |         |V        |         |
12+45       0.2026      0.49  |Q        |         | V       |         |
12+50       0.2060      0.49  |Q        |         | V       |         |
12+55       0.2095      0.50  | Q       |         |  V      |         |
13+ 0       0.2130      0.51  | Q       |         |  V      |         |
13+ 5       0.2166      0.52  | Q       |         |  V      |         |
13+10       0.2205      0.57  | Q       |         |   V     |         |
13+15       0.2245      0.58  | Q       |         |   V     |         |
13+20       0.2285      0.59  | Q       |         |    V    |         |
13+25       0.2326      0.59  | Q       |         |    V    |         |
13+30       0.2367      0.59  | Q       |         |     V   |         |
13+35       0.2406      0.56  | Q       |         |     V   |         |
13+40       0.2438      0.47  |Q        |         |     V   |         |
13+45       0.2468      0.44  |Q        |         |      V  |         |
13+50       0.2498      0.42  |Q        |         |      V  |         |
13+55       0.2526      0.42  |Q        |         |      V  |         |
14+ 0       0.2555      0.41  |Q        |         |       V |         |
14+ 5       0.2584      0.42  |Q        |         |       V |         |
14+10       0.2615      0.45  |Q        |         |       V |         |
14+15       0.2647      0.46  |Q        |         |        V|         |
14+20       0.2679      0.46  |Q        |         |        V|         |
14+25       0.2710      0.46  |Q        |         |        V|         |
14+30       0.2742      0.46  |Q        |         |         V         |
14+35       0.2773      0.46  |Q        |         |         V         |
14+40       0.2805      0.46  |Q        |         |         V         |
14+45       0.2836      0.46  |Q        |         |         |V        |
14+50       0.2868      0.45  |Q        |         |         |V        |
14+55       0.2898      0.45  |Q        |         |         |V        |
15+ 0       0.2929      0.44  |Q        |         |         | V       |
15+ 5       0.2959      0.44  |Q        |         |         | V       |
15+10       0.2989      0.43  |Q        |         |         | V       |
15+15       0.3018      0.43  |Q        |         |         |  V      |
15+20       0.3047      0.42  |Q        |         |         |  V      |
15+25       0.3075      0.41  |Q        |         |         |  V      |
15+30       0.3104      0.41  |Q        |         |         |   V     |
```

```
15+35       0.3131      0.39  |Q        |         |         |   V     |
15+40       0.3155      0.36  |Q        |         |         |   V     |
15+45       0.3179      0.35  |Q        |         |         |   V     |
15+50       0.3203      0.34  |Q        |         |         |    V    |
15+55       0.3226      0.34  |Q        |         |         |    V    |
16+ 0       0.3249      0.34  |Q        |         |         |    V    |
16+ 5       0.3269      0.29  |Q        |         |         |    V    |
16+10       0.3280      0.16  Q         |         |         |     V   |
16+15       0.3288      0.12  Q         |         |         |     V   |
16+20       0.3295      0.10  Q         |         |         |     V   |
16+25       0.3301      0.09  Q         |         |         |     V   |
16+30       0.3307      0.08  Q         |         |         |     V   |
16+35       0.3312      0.07  Q         |         |         |     V   |
16+40       0.3316      0.06  Q         |         |         |     V   |
16+45       0.3320      0.06  Q         |         |         |     V   |
16+50       0.3324      0.05  Q         |         |         |     V   |
16+55       0.3327      0.05  Q         |         |         |     V   |
17+ 0       0.3331      0.05  Q         |         |         |     V   |
17+ 5       0.3335      0.06  Q         |         |         |     V   |
17+10       0.3340      0.08  Q         |         |         |     V   |
17+15       0.3346      0.08  Q         |         |         |     V   |
17+20       0.3352      0.08  Q         |         |         |     V   |
17+25       0.3358      0.09  Q         |         |         |     V   |
17+30       0.3364      0.09  Q         |         |         |      V  |
17+35       0.3370      0.09  Q         |         |         |      V  |
17+40       0.3376      0.09  Q         |         |         |      V  |
17+45       0.3382      0.09  Q         |         |         |      V  |
17+50       0.3387      0.08  Q         |         |         |      V  |
17+55       0.3393      0.08  Q         |         |         |      V  |
18+ 0       0.3398      0.07  Q         |         |         |      V  |
18+ 5       0.3403      0.07  Q         |         |         |      V  |
18+10       0.3408      0.07  Q         |         |         |      V  |
18+15       0.3413      0.07  Q         |         |         |      V  |
18+20       0.3417      0.07  Q         |         |         |      V  |
18+25       0.3422      0.07  Q         |         |         |      V  |
18+30       0.3427      0.07  Q         |         |         |      V  |
18+35       0.3432      0.07  Q         |         |         |      V  |
18+40       0.3436      0.06  Q         |         |         |      V  |
18+45       0.3440      0.06  Q         |         |         |      V  |
18+50       0.3443      0.05  Q         |         |         |      V  |
18+55       0.3446      0.04  Q         |         |         |      V  |
19+ 0       0.3449      0.04  Q         |         |         |      V  |
19+ 5       0.3452      0.04  Q         |         |         |      V  |
19+10       0.3455      0.05  Q         |         |         |       V |
19+15       0.3458      0.05  Q         |         |         |       V |
19+20       0.3462      0.05  Q         |         |         |       V |
19+25       0.3467      0.06  Q         |         |         |       V |
19+30       0.3471      0.07  Q         |         |         |       V |
19+35       0.3476      0.07  Q         |         |         |       V |
19+40       0.3480      0.06  Q         |         |         |       V |
```

19+45	0.3483	0.06	Q	|	|	|	V |
19+50	0.3487	0.05	Q	|	|	|	V |
19+55	0.3490	0.04	Q	|	|	|	V |
20+ 0	0.3492	0.04	Q	|	|	|	V |
20+ 5	0.3495	0.04	Q	|	|	|	V |
20+10	0.3499	0.05	Q	|	|	|	V |
20+15	0.3502	0.05	Q	|	|	|	V |
20+20	0.3506	0.05	Q	|	|	|	V |
20+25	0.3509	0.05	Q	|	|	|	V |
20+30	0.3513	0.05	Q	|	|	|	V |
20+35	0.3516	0.05	Q	|	|	|	V |
20+40	0.3520	0.05	Q	|	|	|	V |
20+45	0.3524	0.05	Q	|	|	|	V |
20+50	0.3527	0.05	Q	|	|	|	V |
20+55	0.3530	0.04	Q	|	|	|	V |
21+ 0	0.3532	0.04	Q	|	|	|	V |
21+ 5	0.3535	0.04	Q	|	|	|	V |
21+10	0.3539	0.05	Q	|	|	|	V |
21+15	0.3542	0.05	Q	|	|	|	V |
21+20	0.3545	0.05	Q	|	|	|	V|
21+25	0.3548	0.04	Q	|	|	|	V|
21+30	0.3551	0.04	Q	|	|	|	V|
21+35	0.3553	0.04	Q	|	|	|	V|
21+40	0.3557	0.05	Q	|	|	|	V|
21+45	0.3560	0.05	Q	|	|	|	V|
21+50	0.3563	0.05	Q	|	|	|	V|
21+55	0.3566	0.04	Q	|	|	|	V|
22+ 0	0.3569	0.04	Q	|	|	|	V|
22+ 5	0.3572	0.04	Q	|	|	|	V|
22+10	0.3575	0.05	Q	|	|	|	V|
22+15	0.3578	0.05	Q	|	|	|	V|
22+20	0.3582	0.05	Q	|	|	|	V|
22+25	0.3584	0.04	Q	|	|	|	V|
22+30	0.3587	0.04	Q	|	|	|	V|
22+35	0.3590	0.04	Q	|	|	|	V|
22+40	0.3592	0.04	Q	|	|	|	V|
22+45	0.3595	0.04	Q	|	|	|	V|
22+50	0.3597	0.04	Q	|	|	|	V|
22+55	0.3599	0.04	Q	|	|	|	V|
23+ 0	0.3602	0.04	Q	|	|	|	V|
23+ 5	0.3604	0.04	Q	|	|	|	V|
23+10	0.3607	0.04	Q	|	|	|	V|
23+15	0.3609	0.04	Q	|	|	|	V|
23+20	0.3612	0.04	Q	|	|	|	V|
23+25	0.3614	0.04	Q	|	|	|	V|
23+30	0.3616	0.04	Q	|	|	|	V|
23+35	0.3619	0.04	Q	|	|	|	V|
23+40	0.3621	0.04	Q	|	|	|	V|
23+45	0.3624	0.04	Q	|	|	|	V|
23+50	0.3626	0.04	Q	|	|	|	V|

```
   23+55       0.3628      0.04  Q         |          |          |         V|
   24+ 0       0.3631      0.04  Q         |          |          |         V|
   24+ 5       0.3633      0.03  Q         |          |          |         V|
   24+10       0.3634      0.01  Q         |          |          |         V|
   24+15       0.3634      0.01  Q         |          |          |         V|
   24+20       0.3634      0.00  Q         |          |          |         V|
   24+25       0.3635      0.00  Q         |          |          |         V|
   24+30       0.3635      0.00  Q         |          |          |         V|
   24+35       0.3635      0.00  Q         |          |          |         V|
   24+40       0.3635      0.00  Q         |          |          |          V
-------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris1100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
100 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.49	0.78

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            1.35                  2.13

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    0.493(In)
Area Averaged 100-Year Rainfall =    1.350(In)

Point rain (area averaged) =    1.350(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    1.350(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-3     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  52.0      0.552     0.900        0.105       1.000      0.105
                                                 Sum (F) =   0.105
Area averaged mean soil loss (F) (In/Hr) =  0.105
Minimum soil loss rate ((In/Hr)) =  0.052
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5000
------------------------------------------------------------------------

                U n i t  H y d r o g r a p h
                        VALLEY S-Curve
------------------------------------------------------------------------
                Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                              Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.20	0.680	0.105	(0.122)	0.576
2	0.17	4.30	0.697	0.105	(0.125)	0.592
3	0.25	5.00	0.810	0.105	(0.146)	0.705
4	0.33	5.00	0.810	0.105	(0.146)	0.705
5	0.42	5.80	0.940	0.105	(0.169)	0.835
6	0.50	6.50	1.053	0.105	(0.190)	0.948
7	0.58	7.40	1.199	0.105	(0.216)	1.094
8	0.67	8.60	1.393	0.105	(0.251)	1.288
9	0.75	12.30	1.993	0.105	(0.359)	1.888
10	0.83	29.10	4.714	0.105	(0.849)	4.609
11	0.92	6.80	1.102	0.105	(0.198)	0.997
12	1.00	5.00	0.810	0.105	(0.146)	0.705
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	14.9

Flood volume = Effective rainfall 1.25(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 0.10(In)
Total soil loss = 0.014(Ac.Ft)
Total rainfall = 1.35(In)
Flood volume = 7141.6 Cubic Feet
Total soil loss = 601.1 Cubic Feet

Peak flow rate of this hydrograph = 4.607(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0 2.5 5.0 7.5 10.0
0+ 5	0.0011	0.16	Q | | | |
0+10	0.0053	0.61	VQ | | | |
0+15	0.0109	0.80	VQ | | | |
0+20	0.0175	0.96	QV | | | |
0+25	0.0248	1.07	Q V | | | |
0+30	0.0334	1.24	Q V | | | |
0+35	0.0432	1.42	Q V | | |
0+40	0.0546	1.65	Q | V | | |
0+45	0.0686	2.04	Q | V | |
0+50	0.0918	3.36	| Q | V | |

```
    0+55       0.1235      4.61  |          |       Q |          V          |
    1+ 0       0.1411      2.56  |          Q         |          |    V      |
    1+ 5       0.1519      1.57  |     Q    |         |          |       V   |
    1+10       0.1571      0.75  |  Q       |         |          |        V  |
    1+15       0.1601      0.43  |Q         |         |          |         V |
    1+20       0.1619      0.27  |Q         |         |          |         V |
    1+25       0.1631      0.16  Q          |         |          |         V |
    1+30       0.1637      0.10  Q          |         |          |         V |
    1+35       0.1639      0.03  Q          |         |          |         V |
    1+40       0.1639      0.01  Q          |         |          |          V
-------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris3100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
100 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	0.87	1.37

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            2.10                  3.32

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    0.869(In)
Area Averaged 100-Year Rainfall =    2.100(In)

Point rain (area averaged) =    2.100(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    2.100(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-3     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  52.0      0.552     0.900        0.105       1.000      0.105
                                                 Sum (F) =   0.105
Area averaged mean soil loss (F) (In/Hr) =  0.105
Minimum soil loss rate ((In/Hr)) =  0.052
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                               Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.328	(0.105)	0.059	0.269
2	0.17	1.30	0.328	(0.105)	0.059	0.269
3	0.25	1.10	0.277	(0.105)	0.050	0.227
4	0.33	1.50	0.378	(0.105)	0.068	0.310
5	0.42	1.50	0.378	(0.105)	0.068	0.310
6	0.50	1.80	0.454	(0.105)	0.082	0.372
7	0.58	1.50	0.378	(0.105)	0.068	0.310
8	0.67	1.80	0.454	(0.105)	0.082	0.372
9	0.75	1.80	0.454	(0.105)	0.082	0.372
10	0.83	1.50	0.378	(0.105)	0.068	0.310
11	0.92	1.60	0.403	(0.105)	0.073	0.331
12	1.00	1.80	0.454	(0.105)	0.082	0.372
13	1.08	2.20	0.554	(0.105)	0.100	0.455
14	1.17	2.20	0.554	(0.105)	0.100	0.455
15	1.25	2.20	0.554	(0.105)	0.100	0.455
16	1.33	2.00	0.504	(0.105)	0.091	0.413
17	1.42	2.60	0.655	0.105	(0.118)	0.550
18	1.50	2.70	0.680	0.105	(0.122)	0.576
19	1.58	2.40	0.605	0.105	(0.109)	0.500
20	1.67	2.70	0.680	0.105	(0.122)	0.576
21	1.75	3.30	0.832	0.105	(0.150)	0.727
22	1.83	3.10	0.781	0.105	(0.141)	0.676
23	1.92	2.90	0.731	0.105	(0.132)	0.626
24	2.00	3.00	0.756	0.105	(0.136)	0.651
25	2.08	3.10	0.781	0.105	(0.141)	0.676
26	2.17	4.20	1.058	0.105	(0.191)	0.954
27	2.25	5.00	1.260	0.105	(0.227)	1.155
28	2.33	3.50	0.882	0.105	(0.159)	0.777
29	2.42	6.80	1.714	0.105	(0.308)	1.609
30	2.50	7.30	1.840	0.105	(0.331)	1.735
31	2.58	8.20	2.066	0.105	(0.372)	1.962
32	2.67	5.90	1.487	0.105	(0.268)	1.382
33	2.75	2.00	0.504	(0.105)	0.091	0.413
34	2.83	1.80	0.454	(0.105)	0.082	0.372
35	2.92	1.80	0.454	(0.105)	0.082	0.372
36	3.00	0.60	0.151	(0.105)	0.027	0.124
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	22.0

Flood volume = Effective rainfall 1.83(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 0.27(In)
Total soil loss = 0.035(Ac.Ft)
Total rainfall = 2.10(In)
Flood volume = 10520.9 Cubic Feet
Total soil loss = 1523.4 Cubic Feet

Peak flow rate of this hydrograph = 2.680(CFS)

++

3 - H O U R S T O R M

R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0005	0.08	Q				
0+10	0.0025	0.28	VQ				
0+15	0.0048	0.34	VQ				
0+20	0.0073	0.36	|Q				
0+25	0.0103	0.43	|Q				
0+30	0.0136	0.48	|QV				
0+35	0.0172	0.52	| Q				
0+40	0.0208	0.52	| QV				
0+45	0.0247	0.56	| Q V				
0+50	0.0285	0.56	| Q V				
0+55	0.0321	0.52	| Q V				
1+ 0	0.0358	0.54	| Q V				
1+ 5	0.0399	0.60	| Q V				
1+10	0.0446	0.67	| Q V				
1+15	0.0493	0.69	| Q V				
1+20	0.0541	0.70	| Q V				
1+25	0.0590	0.71	| Q V				
1+30	0.0646	0.82	| Q V				
1+35	0.0705	0.85	| Q |V				
1+40	0.0762	0.83	| Q | V				
1+45	0.0826	0.92	| Q | V				
1+50	0.0898	1.04	| Q | V				
1+55	0.0969	1.04	| Q | V				
2+ 0	0.1039	1.02	| Q | V				
2+ 5	0.1110	1.04	| Q | V				
2+10	0.1189	1.14	| Q | V				
2+15	0.1286	1.42	| Q | V				
2+20	0.1392	1.54	| Q | V				
2+25	0.1501	1.58	| Q | V				
2+30	0.1652	2.19	| Q | V				
2+35	0.1828	2.55	| Q V				
2+40	0.2012	2.68	| Q V				
2+45	0.2156	2.08	| Q | V				
2+50	0.2241	1.25	| Q | V				
2+55	0.2306	0.94	| Q | V				
3+ 0	0.2356	0.73	| Q | V				
3+ 5	0.2385	0.43	|Q | V				
3+10	0.2400	0.21	Q | V				

3+15	0.2408	0.12	Q	|	|	|	V|
3+20	0.2412	0.06	Q	|	|	|	V|
3+25	0.2414	0.03	Q	|	|	|	V|
3+30	0.2415	0.01	Q	|	|	|	V|
3+35	0.2415	0.01	Q	|	|	|	V|
3+40	0.2415	0.00	Q	|	|	|	V|

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris6100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
100 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	1.22	1.93

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            2.87                   4.53

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    1.220(In)
Area Averaged 100-Year Rainfall =    2.870(In)

Point rain (area averaged) =    2.870(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    2.870(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-3     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  52.0      0.552     0.900        0.105       1.000      0.105
                                                 Sum (F) =   0.105
Area averaged mean soil loss (F) (In/Hr) =  0.105
Minimum soil loss rate ((In/Hr)) =  0.052
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                              Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

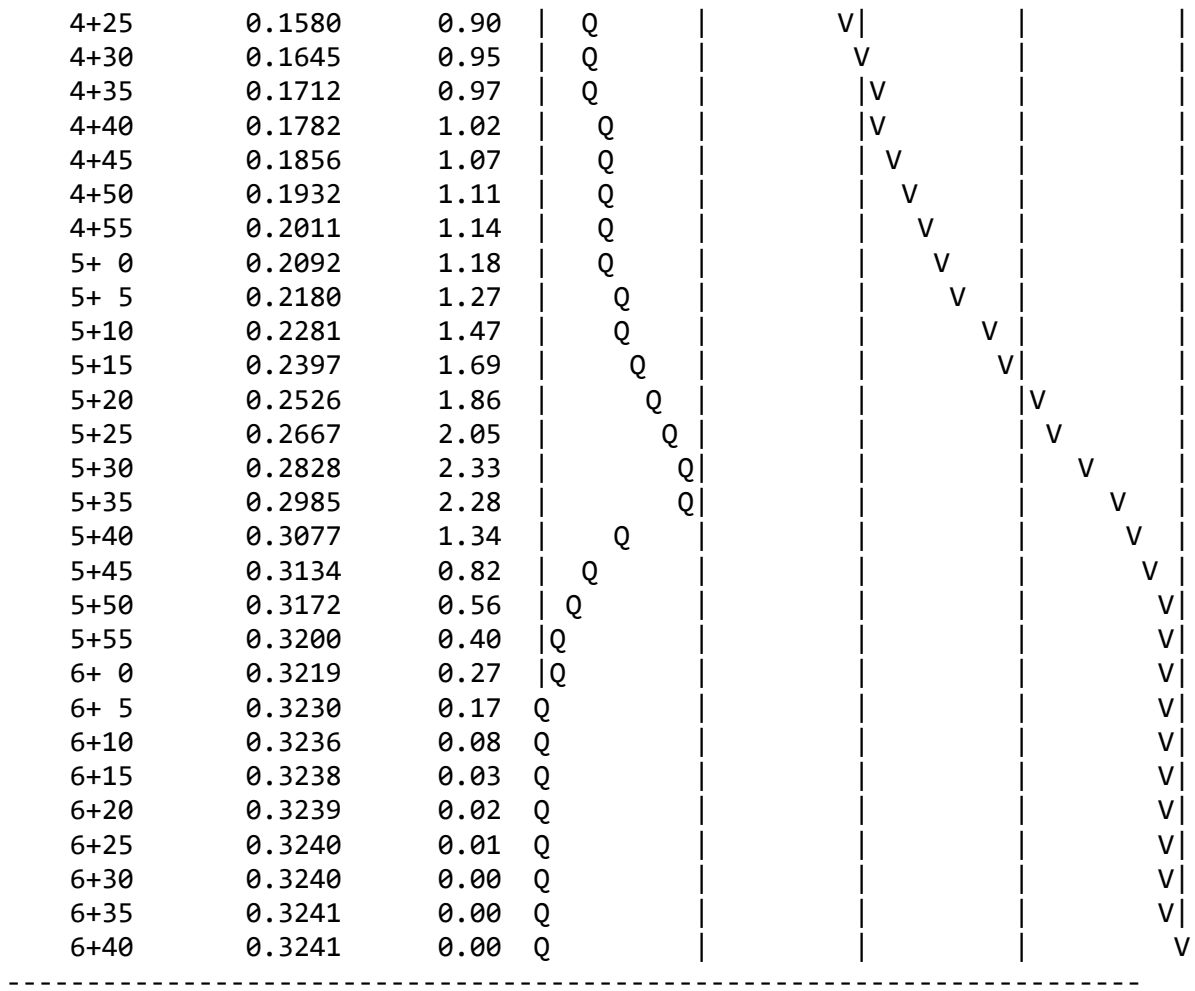
The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.172	(0.105)	0.031	0.141
2	0.17	0.60	0.207	(0.105)	0.037	0.169
3	0.25	0.60	0.207	(0.105)	0.037	0.169
4	0.33	0.60	0.207	(0.105)	0.037	0.169
5	0.42	0.60	0.207	(0.105)	0.037	0.169
6	0.50	0.70	0.241	(0.105)	0.043	0.198
7	0.58	0.70	0.241	(0.105)	0.043	0.198
8	0.67	0.70	0.241	(0.105)	0.043	0.198
9	0.75	0.70	0.241	(0.105)	0.043	0.198
10	0.83	0.70	0.241	(0.105)	0.043	0.198
11	0.92	0.70	0.241	(0.105)	0.043	0.198
12	1.00	0.80	0.276	(0.105)	0.050	0.226
13	1.08	0.80	0.276	(0.105)	0.050	0.226
14	1.17	0.80	0.276	(0.105)	0.050	0.226
15	1.25	0.80	0.276	(0.105)	0.050	0.226
16	1.33	0.80	0.276	(0.105)	0.050	0.226
17	1.42	0.80	0.276	(0.105)	0.050	0.226
18	1.50	0.80	0.276	(0.105)	0.050	0.226
19	1.58	0.80	0.276	(0.105)	0.050	0.226
20	1.67	0.80	0.276	(0.105)	0.050	0.226
21	1.75	0.80	0.276	(0.105)	0.050	0.226
22	1.83	0.80	0.276	(0.105)	0.050	0.226
23	1.92	0.80	0.276	(0.105)	0.050	0.226
24	2.00	0.90	0.310	(0.105)	0.056	0.254
25	2.08	0.80	0.276	(0.105)	0.050	0.226
26	2.17	0.90	0.310	(0.105)	0.056	0.254
27	2.25	0.90	0.310	(0.105)	0.056	0.254
28	2.33	0.90	0.310	(0.105)	0.056	0.254
29	2.42	0.90	0.310	(0.105)	0.056	0.254
30	2.50	0.90	0.310	(0.105)	0.056	0.254
31	2.58	0.90	0.310	(0.105)	0.056	0.254
32	2.67	0.90	0.310	(0.105)	0.056	0.254
33	2.75	1.00	0.344	(0.105)	0.062	0.282
34	2.83	1.00	0.344	(0.105)	0.062	0.282
35	2.92	1.00	0.344	(0.105)	0.062	0.282
36	3.00	1.00	0.344	(0.105)	0.062	0.282
37	3.08	1.00	0.344	(0.105)	0.062	0.282
38	3.17	1.10	0.379	(0.105)	0.068	0.311
39	3.25	1.10	0.379	(0.105)	0.068	0.311
40	3.33	1.10	0.379	(0.105)	0.068	0.311
41	3.42	1.20	0.413	(0.105)	0.074	0.339
42	3.50	1.30	0.448	(0.105)	0.081	0.367
43	3.58	1.40	0.482	(0.105)	0.087	0.395
44	3.67	1.40	0.482	(0.105)	0.087	0.395
45	3.75	1.50	0.517	(0.105)	0.093	0.424

```
46   3.83     1.50      0.517       (  0.105)       0.093        0.424
47   3.92     1.60      0.551       (  0.105)       0.099        0.452
48   4.00     1.60      0.551       (  0.105)       0.099        0.452
49   4.08     1.70      0.585          0.105    (  0.105)        0.481
50   4.17     1.80      0.620          0.105    (  0.112)        0.515
51   4.25     1.90      0.654          0.105    (  0.118)        0.550
52   4.33     2.00      0.689          0.105    (  0.124)        0.584
53   4.42     2.10      0.723          0.105    (  0.130)        0.618
54   4.50     2.10      0.723          0.105    (  0.130)        0.618
55   4.58     2.20      0.758          0.105    (  0.136)        0.653
56   4.67     2.30      0.792          0.105    (  0.143)        0.687
57   4.75     2.40      0.827          0.105    (  0.149)        0.722
58   4.83     2.40      0.827          0.105    (  0.149)        0.722
59   4.92     2.50      0.861          0.105    (  0.155)        0.756
60   5.00     2.60      0.895          0.105    (  0.161)        0.791
61   5.08     3.10      1.068          0.105    (  0.192)        0.963
62   5.17     3.60      1.240          0.105    (  0.223)        1.135
63   5.25     3.90      1.343          0.105    (  0.242)        1.238
64   5.33     4.20      1.446          0.105    (  0.260)        1.342
65   5.42     4.70      1.619          0.105    (  0.291)        1.514
66   5.50     5.60      1.929          0.105    (  0.347)        1.824
67   5.58     1.90      0.654          0.105    (  0.118)        0.550
68   5.67     0.90      0.310       (  0.105)       0.056        0.254
69   5.75     0.60      0.207       (  0.105)       0.037        0.169
70   5.83     0.50      0.172       (  0.105)       0.031        0.141
71   5.92     0.30      0.103       (  0.105)       0.019        0.085
72   6.00     0.20      0.069       (  0.105)       0.012        0.056
               (Loss Rate Not Used)
   Sum =     100.0                                    Sum =    29.5
      Flood volume = Effective rainfall      2.46(In)
       times area       1.6(Ac.)/[(In)/(Ft.)] =       0.3(Ac.Ft)
      Total soil loss =      0.41(In)
      Total soil loss =     0.054(Ac.Ft)
      Total rainfall =      2.87(In)
      Flood volume =       14116.2 Cubic Feet
      Total soil loss =        2344.3 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      2.332(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0003      0.04  Q         |         |         |         |
  0+10       0.0014      0.16  Q         |         |         |         |
```

```
0+15       0.0028      0.21  Q         |         |         |         |
0+20       0.0045      0.24  Q         |         |         |         |
0+25       0.0062      0.25  VQ        |         |         |         |
0+30       0.0080      0.27  VQ        |         |         |         |
0+35       0.0101      0.29  |Q        |         |         |         |
0+40       0.0122      0.30  |Q        |         |         |         |
0+45       0.0143      0.31  |Q        |         |         |         |
0+50       0.0164      0.31  |QV       |         |         |         |
0+55       0.0186      0.31  |QV       |         |         |         |
1+ 0       0.0208      0.32  |QV       |         |         |         |
1+ 5       0.0232      0.34  |QV       |         |         |         |
1+10       0.0256      0.35  |Q V      |         |         |         |
1+15       0.0281      0.36  |Q V      |         |         |         |
1+20       0.0305      0.36  |Q V      |         |         |         |
1+25       0.0330      0.36  |Q  V     |         |         |         |
1+30       0.0355      0.36  |Q  V     |         |         |         |
1+35       0.0379      0.36  |Q  V     |         |         |         |
1+40       0.0404      0.36  |Q  V     |         |         |         |
1+45       0.0429      0.36  |Q   V    |         |         |         |
1+50       0.0454      0.36  |Q   V    |         |         |         |
1+55       0.0479      0.36  |Q   V    |         |         |         |
2+ 0       0.0504      0.37  |Q    V   |         |         |         |
2+ 5       0.0530      0.38  |Q    V   |         |         |         |
2+10       0.0556      0.38  |Q    V   |         |         |         |
2+15       0.0583      0.39  |Q     V  |         |         |         |
2+20       0.0611      0.40  |Q     V  |         |         |         |
2+25       0.0638      0.40  |Q     V  |         |         |         |
2+30       0.0666      0.40  |Q      V |         |         |         |
2+35       0.0694      0.40  |Q      V |         |         |         |
2+40       0.0722      0.40  |Q      V |         |         |         |
2+45       0.0750      0.41  |Q       V|         |         |         |
2+50       0.0780      0.43  |Q       V|         |         |         |
2+55       0.0810      0.44  |Q        V         |         |         |
3+ 0       0.0841      0.45  |Q        V         |         |         |
3+ 5       0.0872      0.45  |Q        V         |         |         |
3+10       0.0903      0.46  |Q        |V        |         |         |
3+15       0.0936      0.48  |Q        |V        |         |         |
3+20       0.0970      0.49  |Q        |V        |         |         |
3+25       0.1004      0.50  |Q        | V       |         |         |
3+30       0.1041      0.53  | Q       | V       |         |         |
3+35       0.1080      0.57  | Q       |  V      |         |         |
3+40       0.1121      0.60  | Q       |  V      |         |         |
3+45       0.1164      0.62  | Q       |   V     |         |         |
3+50       0.1209      0.65  | Q       |   V     |         |         |
3+55       0.1255      0.67  | Q       |    V    |         |         |
4+ 0       0.1303      0.70  | Q       |     V   |         |         |
4+ 5       0.1352      0.72  | Q       |     V   |         |         |
4+10       0.1404      0.75  |  Q      |      V  |         |         |
4+15       0.1459      0.80  |  Q      |       V |         |         |
4+20       0.1518      0.85  |  Q      |       V |         |         |
```


4+25 0.1580 0.90
4+30 0.1645 0.95
4+35 0.1712 0.97
4+40 0.1782 1.02
4+45 0.1856 1.07
4+50 0.1932 1.11
4+55 0.2011 1.14
5+ 0 0.2092 1.18
5+ 5 0.2180 1.27
5+10 0.2281 1.47
5+15 0.2397 1.69
5+20 0.2526 1.86
5+25 0.2667 2.05
5+30 0.2828 2.33
5+35 0.2985 2.28
5+40 0.3077 1.34
5+45 0.3134 0.82
5+50 0.3172 0.56
5+55 0.3200 0.40
6+ 0 0.3219 0.27
6+ 5 0.3230 0.17
6+10 0.3236 0.08
6+15 0.3238 0.03
6+20 0.3239 0.02
6+25 0.3240 0.01
6+30 0.3240 0.00
6+35 0.3241 0.00
6+40 0.3241 0.00

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018, Version 9.0
Study date 08/07/22 File: Iris24100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6481

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Iris and Oliver
Post Development
100 yr

Drainage Area = 1.58(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.58(Ac.) = 0.002 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.087 Hr.
Lag time = 5.21 Min.
25% of lag time = 1.30 Min.
40% of lag time = 2.09 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.58	2.05	3.24

100 YEAR Area rainfall data:

```
Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        1.58            5.25                  8.29

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    2.050(In)
Area Averaged 100-Year Rainfall =    5.250(In)

Point rain (area averaged) =    5.250(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    5.250(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     1.580           32.00         0.900
 Total Area Entered =      1.58(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-3     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
32.0  52.0      0.552     0.900        0.105       1.000      0.105
                                                 Sum (F) =   0.105
Area averaged mean soil loss (F) (In/Hr) =  0.105
Minimum soil loss rate ((In/Hr)) =  0.052
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.180
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                       VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %            (CFS)
------------------------------------------------------------------------
    1   0.083         95.896         17.945              0.286
    2   0.167        191.791         48.003              0.764
    3   0.250        287.687         16.299              0.260
    4   0.333        383.583          7.288              0.116
    5   0.417        479.478          4.149              0.066
    6   0.500        575.374          2.689              0.043
    7   0.583        671.270          1.732              0.028
    8   0.667        767.165          1.088              0.017
    9   0.750        863.061          0.808              0.013
                               Sum = 100.000   Sum=       1.592
------------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.042	(0.186)	0.008	0.034
2	0.17	0.07	0.042	(0.185)	0.008	0.034
3	0.25	0.07	0.042	(0.184)	0.008	0.034
4	0.33	0.10	0.063	(0.184)	0.011	0.052
5	0.42	0.10	0.063	(0.183)	0.011	0.052
6	0.50	0.10	0.063	(0.182)	0.011	0.052
7	0.58	0.10	0.063	(0.181)	0.011	0.052
8	0.67	0.10	0.063	(0.181)	0.011	0.052
9	0.75	0.10	0.063	(0.180)	0.011	0.052
10	0.83	0.13	0.084	(0.179)	0.015	0.069
11	0.92	0.13	0.084	(0.179)	0.015	0.069
12	1.00	0.13	0.084	(0.178)	0.015	0.069
13	1.08	0.10	0.063	(0.177)	0.011	0.052
14	1.17	0.10	0.063	(0.177)	0.011	0.052
15	1.25	0.10	0.063	(0.176)	0.011	0.052
16	1.33	0.10	0.063	(0.175)	0.011	0.052
17	1.42	0.10	0.063	(0.174)	0.011	0.052
18	1.50	0.10	0.063	(0.174)	0.011	0.052
19	1.58	0.10	0.063	(0.173)	0.011	0.052
20	1.67	0.10	0.063	(0.172)	0.011	0.052
21	1.75	0.10	0.063	(0.172)	0.011	0.052
22	1.83	0.13	0.084	(0.171)	0.015	0.069
23	1.92	0.13	0.084	(0.170)	0.015	0.069
24	2.00	0.13	0.084	(0.170)	0.015	0.069
25	2.08	0.13	0.084	(0.169)	0.015	0.069
26	2.17	0.13	0.084	(0.168)	0.015	0.069
27	2.25	0.13	0.084	(0.168)	0.015	0.069
28	2.33	0.13	0.084	(0.167)	0.015	0.069
29	2.42	0.13	0.084	(0.166)	0.015	0.069
30	2.50	0.13	0.084	(0.166)	0.015	0.069
31	2.58	0.17	0.105	(0.165)	0.019	0.086
32	2.67	0.17	0.105	(0.164)	0.019	0.086
33	2.75	0.17	0.105	(0.163)	0.019	0.086
34	2.83	0.17	0.105	(0.163)	0.019	0.086
35	2.92	0.17	0.105	(0.162)	0.019	0.086
36	3.00	0.17	0.105	(0.161)	0.019	0.086
37	3.08	0.17	0.105	(0.161)	0.019	0.086
38	3.17	0.17	0.105	(0.160)	0.019	0.086
39	3.25	0.17	0.105	(0.159)	0.019	0.086
40	3.33	0.17	0.105	(0.159)	0.019	0.086
41	3.42	0.17	0.105	(0.158)	0.019	0.086
42	3.50	0.17	0.105	(0.157)	0.019	0.086
43	3.58	0.17	0.105	(0.157)	0.019	0.086
44	3.67	0.17	0.105	(0.156)	0.019	0.086
45	3.75	0.17	0.105	(0.156)	0.019	0.086

46	3.83	0.20	0.126	(0.155)	0.023	0.103
47	3.92	0.20	0.126	(0.154)	0.023	0.103
48	4.00	0.20	0.126	(0.154)	0.023	0.103
49	4.08	0.20	0.126	(0.153)	0.023	0.103
50	4.17	0.20	0.126	(0.152)	0.023	0.103
51	4.25	0.20	0.126	(0.152)	0.023	0.103
52	4.33	0.23	0.147	(0.151)	0.026	0.121
53	4.42	0.23	0.147	(0.150)	0.026	0.121
54	4.50	0.23	0.147	(0.150)	0.026	0.121
55	4.58	0.23	0.147	(0.149)	0.026	0.121
56	4.67	0.23	0.147	(0.148)	0.026	0.121
57	4.75	0.23	0.147	(0.148)	0.026	0.121
58	4.83	0.27	0.168	(0.147)	0.030	0.138
59	4.92	0.27	0.168	(0.146)	0.030	0.138
60	5.00	0.27	0.168	(0.146)	0.030	0.138
61	5.08	0.20	0.126	(0.145)	0.023	0.103
62	5.17	0.20	0.126	(0.145)	0.023	0.103
63	5.25	0.20	0.126	(0.144)	0.023	0.103
64	5.33	0.23	0.147	(0.143)	0.026	0.121
65	5.42	0.23	0.147	(0.143)	0.026	0.121
66	5.50	0.23	0.147	(0.142)	0.026	0.121
67	5.58	0.27	0.168	(0.141)	0.030	0.138
68	5.67	0.27	0.168	(0.141)	0.030	0.138
69	5.75	0.27	0.168	(0.140)	0.030	0.138
70	5.83	0.27	0.168	(0.140)	0.030	0.138
71	5.92	0.27	0.168	(0.139)	0.030	0.138
72	6.00	0.27	0.168	(0.138)	0.030	0.138
73	6.08	0.30	0.189	(0.138)	0.034	0.155
74	6.17	0.30	0.189	(0.137)	0.034	0.155
75	6.25	0.30	0.189	(0.137)	0.034	0.155
76	6.33	0.30	0.189	(0.136)	0.034	0.155
77	6.42	0.30	0.189	(0.135)	0.034	0.155
78	6.50	0.30	0.189	(0.135)	0.034	0.155
79	6.58	0.33	0.210	(0.134)	0.038	0.172
80	6.67	0.33	0.210	(0.133)	0.038	0.172
81	6.75	0.33	0.210	(0.133)	0.038	0.172
82	6.83	0.33	0.210	(0.132)	0.038	0.172
83	6.92	0.33	0.210	(0.132)	0.038	0.172
84	7.00	0.33	0.210	(0.131)	0.038	0.172
85	7.08	0.33	0.210	(0.130)	0.038	0.172
86	7.17	0.33	0.210	(0.130)	0.038	0.172
87	7.25	0.33	0.210	(0.129)	0.038	0.172
88	7.33	0.37	0.231	(0.129)	0.042	0.189
89	7.42	0.37	0.231	(0.128)	0.042	0.189
90	7.50	0.37	0.231	(0.128)	0.042	0.189
91	7.58	0.40	0.252	(0.127)	0.045	0.207
92	7.67	0.40	0.252	(0.126)	0.045	0.207
93	7.75	0.40	0.252	(0.126)	0.045	0.207
94	7.83	0.43	0.273	(0.125)	0.049	0.224
95	7.92	0.43	0.273	(0.125)	0.049	0.224

96	8.00	0.43	0.273	(0.124)	0.049	0.224
97	8.08	0.50	0.315	(0.123)	0.057	0.258
98	8.17	0.50	0.315	(0.123)	0.057	0.258
99	8.25	0.50	0.315	(0.122)	0.057	0.258
100	8.33	0.50	0.315	(0.122)	0.057	0.258
101	8.42	0.50	0.315	(0.121)	0.057	0.258
102	8.50	0.50	0.315	(0.121)	0.057	0.258
103	8.58	0.53	0.336	(0.120)	0.060	0.276
104	8.67	0.53	0.336	(0.119)	0.060	0.276
105	8.75	0.53	0.336	(0.119)	0.060	0.276
106	8.83	0.57	0.357	(0.118)	0.064	0.293
107	8.92	0.57	0.357	(0.118)	0.064	0.293
108	9.00	0.57	0.357	(0.117)	0.064	0.293
109	9.08	0.63	0.399	(0.117)	0.072	0.327
110	9.17	0.63	0.399	(0.116)	0.072	0.327
111	9.25	0.63	0.399	(0.116)	0.072	0.327
112	9.33	0.67	0.420	(0.115)	0.076	0.344
113	9.42	0.67	0.420	(0.114)	0.076	0.344
114	9.50	0.67	0.420	(0.114)	0.076	0.344
115	9.58	0.70	0.441	(0.113)	0.079	0.362
116	9.67	0.70	0.441	(0.113)	0.079	0.362
117	9.75	0.70	0.441	(0.112)	0.079	0.362
118	9.83	0.73	0.462	(0.112)	0.083	0.379
119	9.92	0.73	0.462	(0.111)	0.083	0.379
120	10.00	0.73	0.462	(0.111)	0.083	0.379
121	10.08	0.50	0.315	(0.110)	0.057	0.258
122	10.17	0.50	0.315	(0.110)	0.057	0.258
123	10.25	0.50	0.315	(0.109)	0.057	0.258
124	10.33	0.50	0.315	(0.109)	0.057	0.258
125	10.42	0.50	0.315	(0.108)	0.057	0.258
126	10.50	0.50	0.315	(0.107)	0.057	0.258
127	10.58	0.67	0.420	(0.107)	0.076	0.344
128	10.67	0.67	0.420	(0.106)	0.076	0.344
129	10.75	0.67	0.420	(0.106)	0.076	0.344
130	10.83	0.67	0.420	(0.105)	0.076	0.344
131	10.92	0.67	0.420	(0.105)	0.076	0.344
132	11.00	0.67	0.420	(0.104)	0.076	0.344
133	11.08	0.63	0.399	(0.104)	0.072	0.327
134	11.17	0.63	0.399	(0.103)	0.072	0.327
135	11.25	0.63	0.399	(0.103)	0.072	0.327
136	11.33	0.63	0.399	(0.102)	0.072	0.327
137	11.42	0.63	0.399	(0.102)	0.072	0.327
138	11.50	0.63	0.399	(0.101)	0.072	0.327
139	11.58	0.57	0.357	(0.101)	0.064	0.293
140	11.67	0.57	0.357	(0.100)	0.064	0.293
141	11.75	0.57	0.357	(0.100)	0.064	0.293
142	11.83	0.60	0.378	(0.099)	0.068	0.310
143	11.92	0.60	0.378	(0.099)	0.068	0.310
144	12.00	0.60	0.378	(0.098)	0.068	0.310
145	12.08	0.83	0.525	(0.098)	0.094	0.430

146	12.17	0.83	0.525	(0.097)	0.094	0.430
147	12.25	0.83	0.525	(0.097)	0.094	0.430
148	12.33	0.87	0.546	0.096	(0.098)	0.450
149	12.42	0.87	0.546	0.096	(0.098)	0.450
150	12.50	0.87	0.546	0.095	(0.098)	0.451
151	12.58	0.93	0.588	0.095	(0.106)	0.493
152	12.67	0.93	0.588	0.094	(0.106)	0.494
153	12.75	0.93	0.588	0.094	(0.106)	0.494
154	12.83	0.97	0.609	0.093	(0.110)	0.516
155	12.92	0.97	0.609	0.093	(0.110)	0.516
156	13.00	0.97	0.609	0.093	(0.110)	0.516
157	13.08	1.13	0.714	0.092	(0.129)	0.622
158	13.17	1.13	0.714	0.092	(0.129)	0.622
159	13.25	1.13	0.714	0.091	(0.129)	0.623
160	13.33	1.13	0.714	0.091	(0.129)	0.623
161	13.42	1.13	0.714	0.090	(0.129)	0.624
162	13.50	1.13	0.714	0.090	(0.129)	0.624
163	13.58	0.77	0.483	(0.089)	0.087	0.396
164	13.67	0.77	0.483	(0.089)	0.087	0.396
165	13.75	0.77	0.483	(0.088)	0.087	0.396
166	13.83	0.77	0.483	(0.088)	0.087	0.396
167	13.92	0.77	0.483	(0.088)	0.087	0.396
168	14.00	0.77	0.483	(0.087)	0.087	0.396
169	14.08	0.90	0.567	0.087	(0.102)	0.480
170	14.17	0.90	0.567	0.086	(0.102)	0.481
171	14.25	0.90	0.567	0.086	(0.102)	0.481
172	14.33	0.87	0.546	0.085	(0.098)	0.461
173	14.42	0.87	0.546	0.085	(0.098)	0.461
174	14.50	0.87	0.546	0.084	(0.098)	0.462
175	14.58	0.87	0.546	0.084	(0.098)	0.462
176	14.67	0.87	0.546	0.084	(0.098)	0.462
177	14.75	0.87	0.546	0.083	(0.098)	0.463
178	14.83	0.83	0.525	0.083	(0.094)	0.442
179	14.92	0.83	0.525	0.082	(0.094)	0.443
180	15.00	0.83	0.525	0.082	(0.094)	0.443
181	15.08	0.80	0.504	0.081	(0.091)	0.423
182	15.17	0.80	0.504	0.081	(0.091)	0.423
183	15.25	0.80	0.504	0.081	(0.091)	0.423
184	15.33	0.77	0.483	0.080	(0.087)	0.403
185	15.42	0.77	0.483	0.080	(0.087)	0.403
186	15.50	0.77	0.483	0.079	(0.087)	0.404
187	15.58	0.63	0.399	(0.079)	0.072	0.327
188	15.67	0.63	0.399	(0.079)	0.072	0.327
189	15.75	0.63	0.399	(0.078)	0.072	0.327
190	15.83	0.63	0.399	(0.078)	0.072	0.327
191	15.92	0.63	0.399	(0.077)	0.072	0.327
192	16.00	0.63	0.399	(0.077)	0.072	0.327
193	16.08	0.13	0.084	(0.077)	0.015	0.069
194	16.17	0.13	0.084	(0.076)	0.015	0.069
195	16.25	0.13	0.084	(0.076)	0.015	0.069

196	16.33	0.13	0.084	(0.075)	0.015	0.069
197	16.42	0.13	0.084	(0.075)	0.015	0.069
198	16.50	0.13	0.084	(0.075)	0.015	0.069
199	16.58	0.10	0.063	(0.074)	0.011	0.052
200	16.67	0.10	0.063	(0.074)	0.011	0.052
201	16.75	0.10	0.063	(0.074)	0.011	0.052
202	16.83	0.10	0.063	(0.073)	0.011	0.052
203	16.92	0.10	0.063	(0.073)	0.011	0.052
204	17.00	0.10	0.063	(0.072)	0.011	0.052
205	17.08	0.17	0.105	(0.072)	0.019	0.086
206	17.17	0.17	0.105	(0.072)	0.019	0.086
207	17.25	0.17	0.105	(0.071)	0.019	0.086
208	17.33	0.17	0.105	(0.071)	0.019	0.086
209	17.42	0.17	0.105	(0.071)	0.019	0.086
210	17.50	0.17	0.105	(0.070)	0.019	0.086
211	17.58	0.17	0.105	(0.070)	0.019	0.086
212	17.67	0.17	0.105	(0.070)	0.019	0.086
213	17.75	0.17	0.105	(0.069)	0.019	0.086
214	17.83	0.13	0.084	(0.069)	0.015	0.069
215	17.92	0.13	0.084	(0.069)	0.015	0.069
216	18.00	0.13	0.084	(0.068)	0.015	0.069
217	18.08	0.13	0.084	(0.068)	0.015	0.069
218	18.17	0.13	0.084	(0.067)	0.015	0.069
219	18.25	0.13	0.084	(0.067)	0.015	0.069
220	18.33	0.13	0.084	(0.067)	0.015	0.069
221	18.42	0.13	0.084	(0.067)	0.015	0.069
222	18.50	0.13	0.084	(0.066)	0.015	0.069
223	18.58	0.10	0.063	(0.066)	0.011	0.052
224	18.67	0.10	0.063	(0.066)	0.011	0.052
225	18.75	0.10	0.063	(0.065)	0.011	0.052
226	18.83	0.07	0.042	(0.065)	0.008	0.034
227	18.92	0.07	0.042	(0.065)	0.008	0.034
228	19.00	0.07	0.042	(0.064)	0.008	0.034
229	19.08	0.10	0.063	(0.064)	0.011	0.052
230	19.17	0.10	0.063	(0.064)	0.011	0.052
231	19.25	0.10	0.063	(0.063)	0.011	0.052
232	19.33	0.13	0.084	(0.063)	0.015	0.069
233	19.42	0.13	0.084	(0.063)	0.015	0.069
234	19.50	0.13	0.084	(0.063)	0.015	0.069
235	19.58	0.10	0.063	(0.062)	0.011	0.052
236	19.67	0.10	0.063	(0.062)	0.011	0.052
237	19.75	0.10	0.063	(0.062)	0.011	0.052
238	19.83	0.07	0.042	(0.061)	0.008	0.034
239	19.92	0.07	0.042	(0.061)	0.008	0.034
240	20.00	0.07	0.042	(0.061)	0.008	0.034
241	20.08	0.10	0.063	(0.061)	0.011	0.052
242	20.17	0.10	0.063	(0.060)	0.011	0.052
243	20.25	0.10	0.063	(0.060)	0.011	0.052
244	20.33	0.10	0.063	(0.060)	0.011	0.052
245	20.42	0.10	0.063	(0.060)	0.011	0.052

246	20.50	0.10	0.063	(0.059)	0.011	0.052
247	20.58	0.10	0.063	(0.059)	0.011	0.052
248	20.67	0.10	0.063	(0.059)	0.011	0.052
249	20.75	0.10	0.063	(0.059)	0.011	0.052
250	20.83	0.07	0.042	(0.058)	0.008	0.034
251	20.92	0.07	0.042	(0.058)	0.008	0.034
252	21.00	0.07	0.042	(0.058)	0.008	0.034
253	21.08	0.10	0.063	(0.058)	0.011	0.052
254	21.17	0.10	0.063	(0.057)	0.011	0.052
255	21.25	0.10	0.063	(0.057)	0.011	0.052
256	21.33	0.07	0.042	(0.057)	0.008	0.034
257	21.42	0.07	0.042	(0.057)	0.008	0.034
258	21.50	0.07	0.042	(0.057)	0.008	0.034
259	21.58	0.10	0.063	(0.056)	0.011	0.052
260	21.67	0.10	0.063	(0.056)	0.011	0.052
261	21.75	0.10	0.063	(0.056)	0.011	0.052
262	21.83	0.07	0.042	(0.056)	0.008	0.034
263	21.92	0.07	0.042	(0.056)	0.008	0.034
264	22.00	0.07	0.042	(0.055)	0.008	0.034
265	22.08	0.10	0.063	(0.055)	0.011	0.052
266	22.17	0.10	0.063	(0.055)	0.011	0.052
267	22.25	0.10	0.063	(0.055)	0.011	0.052
268	22.33	0.07	0.042	(0.055)	0.008	0.034
269	22.42	0.07	0.042	(0.054)	0.008	0.034
270	22.50	0.07	0.042	(0.054)	0.008	0.034
271	22.58	0.07	0.042	(0.054)	0.008	0.034
272	22.67	0.07	0.042	(0.054)	0.008	0.034
273	22.75	0.07	0.042	(0.054)	0.008	0.034
274	22.83	0.07	0.042	(0.054)	0.008	0.034
275	22.92	0.07	0.042	(0.054)	0.008	0.034
276	23.00	0.07	0.042	(0.053)	0.008	0.034
277	23.08	0.07	0.042	(0.053)	0.008	0.034
278	23.17	0.07	0.042	(0.053)	0.008	0.034
279	23.25	0.07	0.042	(0.053)	0.008	0.034
280	23.33	0.07	0.042	(0.053)	0.008	0.034
281	23.42	0.07	0.042	(0.053)	0.008	0.034
282	23.50	0.07	0.042	(0.053)	0.008	0.034
283	23.58	0.07	0.042	(0.053)	0.008	0.034
284	23.67	0.07	0.042	(0.053)	0.008	0.034
285	23.75	0.07	0.042	(0.053)	0.008	0.034
286	23.83	0.07	0.042	(0.052)	0.008	0.034
287	23.92	0.07	0.042	(0.052)	0.008	0.034
288	24.00	0.07	0.042	(0.052)	0.008	0.034

(Loss Rate Not Used)

Sum = 100.0 Sum = 52.2

Flood volume = Effective rainfall 4.35(In)
times area 1.6(Ac.)/[(In)/(Ft.)] = 0.6(Ac.Ft)
Total soil loss = 0.90(In)
Total soil loss = 0.119(Ac.Ft)
Total rainfall = 5.25(In)

Flood volume = 24947.1 Cubic Feet
Total soil loss = 5163.7 Cubic Feet

Peak flow rate of this hydrograph = 0.987(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.01	Q				
0+10	0.0003	0.04	Q				
0+15	0.0006	0.05	Q				
0+20	0.0010	0.05	Q				
0+25	0.0015	0.07	Q				
0+30	0.0020	0.08	Q				
0+35	0.0025	0.08	Q				
0+40	0.0031	0.08	Q				
0+45	0.0036	0.08	Q				
0+50	0.0042	0.09	Q				
0+55	0.0049	0.10	Q				
1+ 0	0.0057	0.10	Q				
1+ 5	0.0064	0.10	Q				
1+10	0.0070	0.09	Q				
1+15	0.0076	0.09	Q				
1+20	0.0082	0.08	Q				
1+25	0.0087	0.08	Q				
1+30	0.0093	0.08	Q				
1+35	0.0099	0.08	Q				
1+40	0.0104	0.08	Q				
1+45	0.0110	0.08	Q				
1+50	0.0116	0.09	Q				
1+55	0.0123	0.10	Q				
2+ 0	0.0130	0.10	Q				
2+ 5	0.0138	0.11	Q				
2+10	0.0145	0.11	QV				
2+15	0.0153	0.11	QV				
2+20	0.0160	0.11	QV				
2+25	0.0168	0.11	QV				
2+30	0.0175	0.11	QV				
2+35	0.0183	0.11	QV				
2+40	0.0192	0.13	QV				
2+45	0.0201	0.13	QV				
2+50	0.0210	0.13	QV				
2+55	0.0220	0.14	QV				
3+ 0	0.0229	0.14	QV				

```
3+ 5       0.0238      0.14  QV        |         |         |         |
3+10       0.0248      0.14  QV        |         |         |         |
3+15       0.0257      0.14  QV        |         |         |         |
3+20       0.0267      0.14  QV        |         |         |         |
3+25       0.0276      0.14  QV        |         |         |         |
3+30       0.0286      0.14  QV        |         |         |         |
3+35       0.0295      0.14  Q V       |         |         |         |
3+40       0.0304      0.14  Q V       |         |         |         |
3+45       0.0314      0.14  Q V       |         |         |         |
3+50       0.0324      0.14  Q V       |         |         |         |
3+55       0.0334      0.16  Q V       |         |         |         |
4+ 0       0.0345      0.16  Q V       |         |         |         |
4+ 5       0.0357      0.16  Q V       |         |         |         |
4+10       0.0368      0.16  Q V       |         |         |         |
4+15       0.0379      0.16  Q V       |         |         |         |
4+20       0.0391      0.17  Q V       |         |         |         |
4+25       0.0403      0.18  Q V       |         |         |         |
4+30       0.0416      0.19  Q V       |         |         |         |
4+35       0.0429      0.19  Q V       |         |         |         |
4+40       0.0442      0.19  Q  V      |         |         |         |
4+45       0.0455      0.19  Q  V      |         |         |         |
4+50       0.0469      0.20  Q  V      |         |         |         |
4+55       0.0483      0.21  Q  V      |         |         |         |
5+ 0       0.0498      0.21  Q  V      |         |         |         |
5+ 5       0.0512      0.21  Q  V      |         |         |         |
5+10       0.0525      0.18  Q  V      |         |         |         |
5+15       0.0537      0.17  Q  V      |         |         |         |
5+20       0.0549      0.17  Q  V      |         |         |         |
5+25       0.0562      0.19  Q  V      |         |         |         |
5+30       0.0575      0.19  Q   V     |         |         |         |
5+35       0.0588      0.20  Q   V     |         |         |         |
5+40       0.0603      0.21  Q   V     |         |         |         |
5+45       0.0617      0.21  Q   V     |         |         |         |
5+50       0.0632      0.22  Q   V     |         |         |         |
5+55       0.0647      0.22  Q   V     |         |         |         |
6+ 0       0.0662      0.22  Q   V     |         |         |         |
6+ 5       0.0678      0.22  Q   V     |         |         |         |
6+10       0.0694      0.24  Q   V     |         |         |         |
6+15       0.0711      0.24  Q   V     |         |         |         |
6+20       0.0727      0.24  Q    V    |         |         |         |
6+25       0.0744      0.25  Q    V    |         |         |         |
6+30       0.0761      0.25  Q    V    |         |         |         |
6+35       0.0779      0.25  |Q   V    |         |         |         |
6+40       0.0797      0.26  |Q   V    |         |         |         |
6+45       0.0815      0.27  |Q   V    |         |         |         |
6+50       0.0834      0.27  |Q   V    |         |         |         |
6+55       0.0853      0.27  |Q   V    |         |         |         |
7+ 0       0.0872      0.27  |Q    V   |         |         |         |
7+ 5       0.0890      0.27  |Q    V   |         |         |         |
7+10       0.0909      0.27  |Q    V   |         |         |         |
```

```
 7+15       0.0928      0.27  |Q    V   |          |          |          |
 7+20       0.0948      0.28  |Q    V   |          |          |          |
 7+25       0.0968      0.29  |Q    V   |          |          |          |
 7+30       0.0988      0.30  |Q    V   |          |          |          |
 7+35       0.1009      0.30  |Q     V  |          |          |          |
 7+40       0.1031      0.32  |Q     V  |          |          |          |
 7+45       0.1053      0.32  |Q     V  |          |          |          |
 7+50       0.1076      0.33  |Q     V  |          |          |          |
 7+55       0.1100      0.35  |Q     V  |          |          |          |
 8+ 0       0.1124      0.35  |Q     V  |          |          |          |
 8+ 5       0.1149      0.36  |Q      V |          |          |          |
 8+10       0.1176      0.39  |Q      V |          |          |          |
 8+15       0.1203      0.40  |Q      V |          |          |          |
 8+20       0.1231      0.41  |Q      V |          |          |          |
 8+25       0.1259      0.41  |Q      V |          |          |          |
 8+30       0.1288      0.41  |Q      V |          |          |          |
 8+35       0.1316      0.42  |Q       V|          |          |          |
 8+40       0.1346      0.43  |Q       V|          |          |          |
 8+45       0.1376      0.43  |Q       V|          |          |          |
 8+50       0.1406      0.44  |Q       V|          |          |          |
 8+55       0.1437      0.46  |Q        V          |          |          |
 9+ 0       0.1469      0.46  |Q        V          |          |          |
 9+ 5       0.1502      0.47  |Q        V          |          |          |
 9+10       0.1536      0.50  | Q       V          |          |          |
 9+15       0.1571      0.51  | Q       V          |          |          |
 9+20       0.1607      0.52  | Q       |V         |          |          |
 9+25       0.1644      0.54  | Q       |V         |          |          |
 9+30       0.1681      0.54  | Q       |V         |          |          |
 9+35       0.1719      0.55  | Q       | V        |          |          |
 9+40       0.1758      0.56  | Q       | V        |          |          |
 9+45       0.1797      0.57  | Q       | V        |          |          |
 9+50       0.1837      0.58  | Q       | V        |          |          |
 9+55       0.1878      0.59  | Q       |  V       |          |          |
10+ 0       0.1919      0.60  | Q       |  V       |          |          |
10+ 5       0.1958      0.57  | Q       |  V       |          |          |
10+10       0.1991      0.47  |Q        |  V       |          |          |
10+15       0.2021      0.44  |Q        |   V      |          |          |
10+20       0.2051      0.43  |Q        |   V      |          |          |
10+25       0.2080      0.42  |Q        |   V      |          |          |
10+30       0.2109      0.42  |Q        |   V      |          |          |
10+35       0.2139      0.44  |Q        |   V      |          |          |
10+40       0.2174      0.50  | Q       |    V     |          |          |
10+45       0.2210      0.52  | Q       |    V     |          |          |
10+50       0.2247      0.53  | Q       |    V     |          |          |
10+55       0.2284      0.54  | Q       |    V     |          |          |
11+ 0       0.2322      0.54  | Q       |     V    |          |          |
11+ 5       0.2359      0.54  | Q       |     V    |          |          |
11+10       0.2395      0.53  | Q       |     V    |          |          |
11+15       0.2432      0.53  | Q       |     V    |          |          |
11+20       0.2468      0.52  | Q       |      V   |          |          |
```

```
11+25       0.2504      0.52  | Q       |      V  |         |         |
11+30       0.2540      0.52  | Q       |      V  |         |         |
11+35       0.2575      0.51  | Q       |      V  |         |         |
11+40       0.2608      0.49  |Q        |       V |         |         |
11+45       0.2641      0.48  |Q        |       V |         |         |
11+50       0.2674      0.48  |Q        |       V |         |         |
11+55       0.2708      0.49  |Q        |       V |         |         |
12+ 0       0.2741      0.49  |Q        |        V|         |         |
12+ 5       0.2778      0.53  | Q       |        V|         |         |
12+10       0.2820      0.62  | Q       |        V|         |         |
12+15       0.2865      0.65  | Q       |         V         |         |
12+20       0.2911      0.67  | Q       |         V         |         |
12+25       0.2959      0.69  | Q       |         V         |         |
12+30       0.3008      0.70  | Q       |         |V        |         |
12+35       0.3057      0.72  | Q       |         |V        |         |
12+40       0.3110      0.76  |  Q      |         |V        |         |
12+45       0.3163      0.77  |  Q      |         | V       |         |
12+50       0.3217      0.79  |  Q      |         | V       |         |
12+55       0.3272      0.80  |  Q      |         | V       |         |
13+ 0       0.3328      0.81  |  Q      |         |  V      |         |
13+ 5       0.3387      0.85  |  Q      |         |  V      |         |
13+10       0.3451      0.93  |  Q      |         |   V     |         |
13+15       0.3517      0.96  |  Q      |         |   V     |         |
13+20       0.3584      0.97  |  Q      |         |    V    |         |
13+25       0.3652      0.98  |  Q      |         |    V    |         |
13+30       0.3720      0.99  |  Q      |         |    V    |         |
13+35       0.3783      0.93  |  Q      |         |     V   |         |
13+40       0.3835      0.75  |  Q      |         |     V   |         |
13+45       0.3883      0.70  | Q       |         |      V  |         |
13+50       0.3929      0.67  | Q       |         |      V  |         |
13+55       0.3974      0.65  | Q       |         |      V  |         |
14+ 0       0.4019      0.64  | Q       |         |       V |         |
14+ 5       0.4064      0.66  | Q       |         |       V |         |
14+10       0.4114      0.72  | Q       |         |       V |         |
14+15       0.4165      0.74  | Q       |         |        V|         |
14+20       0.4217      0.75  | Q       |         |        V|         |
14+25       0.4267      0.74  | Q       |         |        V|         |
14+30       0.4318      0.74  | Q       |         |         V         |
14+35       0.4369      0.74  | Q       |         |         V         |
14+40       0.4419      0.74  | Q       |         |         V         |
14+45       0.4470      0.74  | Q       |         |         |V        |
14+50       0.4521      0.73  | Q       |         |         |V        |
14+55       0.4570      0.72  | Q       |         |         |V        |
15+ 0       0.4619      0.71  | Q       |         |         | V       |
15+ 5       0.4667      0.70  | Q       |         |         | V       |
15+10       0.4714      0.69  | Q       |         |         | V       |
15+15       0.4761      0.68  | Q       |         |         |  V      |
15+20       0.4808      0.67  | Q       |         |         |  V      |
15+25       0.4853      0.66  | Q       |         |         |  V      |
15+30       0.4897      0.65  | Q       |         |         |   V     |
```

```
15+35       0.4941      0.62  | Q       |         |         |   V     |
15+40       0.4979      0.56  | Q       |         |         |   V     |
15+45       0.5017      0.54  | Q       |         |         |    V    |
15+50       0.5054      0.53  | Q       |         |         |    V    |
15+55       0.5090      0.53  | Q       |         |         |    V    |
16+ 0       0.5126      0.53  | Q       |         |         |    V    |
16+ 5       0.5157      0.45  |Q        |         |         |     V   |
16+10       0.5175      0.25  |Q        |         |         |     V   |
16+15       0.5187      0.18  Q         |         |         |     V   |
16+20       0.5198      0.15  Q         |         |         |     V   |
16+25       0.5207      0.14  Q         |         |         |     V   |
16+30       0.5216      0.12  Q         |         |         |     V   |
16+35       0.5223      0.11  Q         |         |         |     V   |
16+40       0.5230      0.09  Q         |         |         |     V   |
16+45       0.5236      0.09  Q         |         |         |     V   |
16+50       0.5242      0.09  Q         |         |         |     V   |
16+55       0.5248      0.08  Q         |         |         |     V   |
17+ 0       0.5253      0.08  Q         |         |         |     V   |
17+ 5       0.5260      0.09  Q         |         |         |     V   |
17+10       0.5268      0.12  Q         |         |         |     V   |
17+15       0.5277      0.13  Q         |         |         |     V   |
17+20       0.5286      0.13  Q         |         |         |     V   |
17+25       0.5295      0.13  Q         |         |         |     V   |
17+30       0.5304      0.14  Q         |         |         |      V  |
17+35       0.5314      0.14  Q         |         |         |      V  |
17+40       0.5323      0.14  Q         |         |         |      V  |
17+45       0.5332      0.14  Q         |         |         |      V  |
17+50       0.5342      0.13  Q         |         |         |      V  |
17+55       0.5350      0.12  Q         |         |         |      V  |
18+ 0       0.5358      0.11  Q         |         |         |      V  |
18+ 5       0.5365      0.11  Q         |         |         |      V  |
18+10       0.5373      0.11  Q         |         |         |      V  |
18+15       0.5381      0.11  Q         |         |         |      V  |
18+20       0.5388      0.11  Q         |         |         |      V  |
18+25       0.5396      0.11  Q         |         |         |      V  |
18+30       0.5403      0.11  Q         |         |         |      V  |
18+35       0.5411      0.10  Q         |         |         |      V  |
18+40       0.5417      0.09  Q         |         |         |      V  |
18+45       0.5423      0.09  Q         |         |         |      V  |
18+50       0.5429      0.08  Q         |         |         |      V  |
18+55       0.5433      0.07  Q         |         |         |      V  |
19+ 0       0.5437      0.06  Q         |         |         |      V  |
19+ 5       0.5442      0.06  Q         |         |         |       V |
19+10       0.5447      0.07  Q         |         |         |       V |
19+15       0.5452      0.08  Q         |         |         |       V |
19+20       0.5458      0.08  Q         |         |         |       V |
19+25       0.5465      0.10  Q         |         |         |       V |
19+30       0.5472      0.10  Q         |         |         |       V |
19+35       0.5479      0.10  Q         |         |         |       V |
19+40       0.5485      0.09  Q         |         |         |       V |
```

19+45	0.5491	0.09	Q	|	|	|	V |
19+50	0.5497	0.08	Q	|	|	|	V |
19+55	0.5501	0.07	Q	|	|	|	V |
20+ 0	0.5505	0.06	Q	|	|	|	V |
20+ 5	0.5510	0.06	Q	|	|	|	V |
20+10	0.5515	0.07	Q	|	|	|	V |
20+15	0.5520	0.08	Q	|	|	|	V |
20+20	0.5526	0.08	Q	|	|	|	V |
20+25	0.5531	0.08	Q	|	|	|	V |
20+30	0.5537	0.08	Q	|	|	|	V |
20+35	0.5542	0.08	Q	|	|	|	V |
20+40	0.5548	0.08	Q	|	|	|	V |
20+45	0.5554	0.08	Q	|	|	|	V |
20+50	0.5559	0.08	Q	|	|	|	V |
20+55	0.5564	0.06	Q	|	|	|	V |
21+ 0	0.5568	0.06	Q	|	|	|	V |
21+ 5	0.5572	0.06	Q	|	|	|	V |
21+10	0.5577	0.07	Q	|	|	|	V |
21+15	0.5583	0.08	Q	|	|	|	V |
21+20	0.5588	0.08	Q	|	|	|	V|
21+25	0.5592	0.06	Q	|	|	|	V|
21+30	0.5596	0.06	Q	|	|	|	V|
21+35	0.5600	0.06	Q	|	|	|	V|
21+40	0.5605	0.07	Q	|	|	|	V|
21+45	0.5611	0.08	Q	|	|	|	V|
21+50	0.5616	0.08	Q	|	|	|	V|
21+55	0.5620	0.06	Q	|	|	|	V|
22+ 0	0.5624	0.06	Q	|	|	|	V|
22+ 5	0.5629	0.06	Q	|	|	|	V|
22+10	0.5634	0.07	Q	|	|	|	V|
22+15	0.5639	0.08	Q	|	|	|	V|
22+20	0.5644	0.08	Q	|	|	|	V|
22+25	0.5649	0.06	Q	|	|	|	V|
22+30	0.5653	0.06	Q	|	|	|	V|
22+35	0.5657	0.06	Q	|	|	|	V|
22+40	0.5661	0.06	Q	|	|	|	V|
22+45	0.5664	0.06	Q	|	|	|	V|
22+50	0.5668	0.06	Q	|	|	|	V|
22+55	0.5672	0.06	Q	|	|	|	V|
23+ 0	0.5676	0.05	Q	|	|	|	V|
23+ 5	0.5680	0.05	Q	|	|	|	V|
23+10	0.5683	0.05	Q	|	|	|	V|
23+15	0.5687	0.05	Q	|	|	|	V|
23+20	0.5691	0.05	Q	|	|	|	V|
23+25	0.5695	0.05	Q	|	|	|	V|
23+30	0.5698	0.05	Q	|	|	|	V|
23+35	0.5702	0.05	Q	|	|	|	V|
23+40	0.5706	0.05	Q	|	|	|	V|
23+45	0.5710	0.05	Q	|	|	|	V|
23+50	0.5714	0.05	Q	|	|	|	V|

```
   23+55       0.5717      0.05  Q         |          |          |         V|
   24+ 0       0.5721      0.05  Q         |          |          |         V|
   24+ 5       0.5724      0.05  Q         |          |          |         V|
   24+10       0.5726      0.02  Q         |          |          |         V|
   24+15       0.5726      0.01  Q         |          |          |         V|
   24+20       0.5727      0.01  Q         |          |          |         V|
   24+25       0.5727      0.00  Q         |          |          |         V|
   24+30       0.5727      0.00  Q         |          |          |         V|
   24+35       0.5727      0.00  Q         |          |          |         V|
   24+40       0.5727      0.00  Q         |          |          |          V
-------------------------------------------------------------------------
```

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
2 yr
1 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris12.rte

**********HYDROGRAPH DATA**********

Number of intervals = 20
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.540 (CFS)
Total volume = 0.055 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++++++++++

Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 20
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.4 0.77 1.16 1.54	Depth (Ft.)
0.083	0.06	0.00	0.000	OI | | | |	0.01
0.167	0.22	0.00	0.001	O I | | | |	0.05
0.250	0.28	0.01	0.003	O I | | | |	0.12
0.333	0.33	0.01	0.005	O I | | | |	0.20
0.417	0.37	0.01	0.007	O I| | | |	0.30
0.500	0.42	0.02	0.010	O I | | |	0.41
0.583	0.48	0.02	0.013	O |I | | |	0.53
0.667	0.54	0.03	0.016	O | I | | |	0.67
0.750	0.66	0.04	0.020	O | I | | |	0.83
0.833	1.10	0.04	0.026	O | | I | |	1.04
0.917	1.54	0.04	0.035	O | | | I|	1.26
1.000	0.85	0.04	0.042	O | |I | |	1.46
1.083	0.53	0.04	0.047	O | I | | |	1.57
1.167	0.25	0.04	0.049	O I | | | |	1.63
1.250	0.14	0.04	0.050	O I | | | |	1.66
1.333	0.09	0.04	0.051	OI | | | |	1.67
1.417	0.05	0.04	0.051	OI | | | |	1.68
1.500	0.03	0.04	0.051	O | | | |	1.68
1.583	0.01	0.04	0.051	O | | | |	1.67
1.667	0.00	0.04	0.051	O | | | |	1.66
1.750	0.00	0.04	0.050	O | | | |	1.66
1.833	0.00	0.04	0.050	O | | | |	1.65
1.917	0.00	0.04	0.050	O | | | |	1.64
2.000	0.00	0.04	0.049	O | | | |	1.63
2.083	0.00	0.04	0.049	O | | | |	1.63
2.167	0.00	0.04	0.049	O | | | |	1.62
2.250	0.00	0.04	0.048	O | | | |	1.61
2.333	0.00	0.04	0.048	O | | | |	1.60

2.417	0.00	0.04	0.048	O				1.60
2.500	0.00	0.04	0.047	O				1.59
2.583	0.00	0.04	0.047	O				1.58
2.667	0.00	0.04	0.047	O				1.57
2.750	0.00	0.04	0.047	O				1.56
2.833	0.00	0.04	0.046	O				1.56
2.917	0.00	0.04	0.046	O				1.55
3.000	0.00	0.04	0.046	O				1.54
3.083	0.00	0.04	0.045	O				1.53
3.167	0.00	0.04	0.045	O				1.53
3.250	0.00	0.04	0.045	O				1.52
3.333	0.00	0.04	0.044	O				1.51
3.417	0.00	0.04	0.044	O				1.50
3.500	0.00	0.04	0.044	O				1.49
3.583	0.00	0.04	0.043	O				1.49
3.667	0.00	0.04	0.043	O				1.48
3.750	0.00	0.04	0.043	O				1.47
3.833	0.00	0.04	0.043	O				1.46
3.917	0.00	0.04	0.042	O				1.46
4.000	0.00	0.04	0.042	O				1.45
4.083	0.00	0.04	0.042	O				1.44
4.167	0.00	0.04	0.041	O				1.43
4.250	0.00	0.04	0.041	O				1.42
4.333	0.00	0.04	0.041	O				1.42
4.417	0.00	0.04	0.040	O				1.41
4.500	0.00	0.04	0.040	O				1.40
4.583	0.00	0.04	0.040	O				1.39
4.667	0.00	0.04	0.039	O				1.39
4.750	0.00	0.04	0.039	O				1.38
4.833	0.00	0.04	0.039	O				1.37
4.917	0.00	0.04	0.039	O				1.36
5.000	0.00	0.04	0.038	O				1.35
5.083	0.00	0.04	0.038	O				1.35
5.167	0.00	0.04	0.038	O				1.34
5.250	0.00	0.04	0.037	O				1.33
5.333	0.00	0.04	0.037	O				1.32
5.417	0.00	0.04	0.037	O				1.32
5.500	0.00	0.04	0.036	O				1.31
5.583	0.00	0.04	0.036	O				1.30
5.667	0.00	0.04	0.036	O				1.29
5.750	0.00	0.04	0.035	O				1.29
5.833	0.00	0.04	0.035	O				1.28
5.917	0.00	0.04	0.035	O				1.27
6.000	0.00	0.04	0.034	O				1.26
6.083	0.00	0.04	0.034	O				1.25
6.167	0.00	0.04	0.034	O				1.25
6.250	0.00	0.04	0.034	O				1.24
6.333	0.00	0.04	0.033	O				1.23
6.417	0.00	0.04	0.033	O				1.22
6.500	0.00	0.04	0.033	O				1.22

6.583	0.00	0.04	0.032	O				1.21
6.667	0.00	0.04	0.032	O				1.20
6.750	0.00	0.04	0.032	O				1.19
6.833	0.00	0.04	0.031	O				1.18
6.917	0.00	0.04	0.031	O				1.18
7.000	0.00	0.04	0.031	O				1.17
7.083	0.00	0.04	0.030	O				1.16
7.167	0.00	0.04	0.030	O				1.15
7.250	0.00	0.04	0.030	O				1.15
7.333	0.00	0.04	0.030	O				1.14
7.417	0.00	0.04	0.029	O				1.13
7.500	0.00	0.04	0.029	O				1.12
7.583	0.00	0.04	0.029	O				1.11
7.667	0.00	0.04	0.028	O				1.11
7.750	0.00	0.04	0.028	O				1.10
7.833	0.00	0.04	0.028	O				1.09
7.917	0.00	0.04	0.027	O				1.08
8.000	0.00	0.04	0.027	O				1.08
8.083	0.00	0.04	0.027	O				1.07
8.167	0.00	0.04	0.026	O				1.06
8.250	0.00	0.04	0.026	O				1.05
8.333	0.00	0.04	0.026	O				1.04
8.417	0.00	0.04	0.025	O				1.04
8.500	0.00	0.04	0.025	O				1.03
8.583	0.00	0.04	0.025	O				1.02
8.667	0.00	0.04	0.025	O				1.01
8.750	0.00	0.04	0.024	O				1.01
8.833	0.00	0.04	0.024	O				1.00
8.917	0.00	0.04	0.024	O				0.98
9.000	0.00	0.04	0.023	O				0.97
9.083	0.00	0.04	0.023	O				0.96
9.167	0.00	0.04	0.023	O				0.95
9.250	0.00	0.04	0.022	O				0.94
9.333	0.00	0.04	0.022	O				0.92
9.417	0.00	0.04	0.022	O				0.91
9.500	0.00	0.04	0.022	O				0.90
9.583	0.00	0.04	0.021	O				0.89
9.667	0.00	0.04	0.021	O				0.88
9.750	0.00	0.04	0.021	O				0.87
9.833	0.00	0.04	0.021	O				0.85
9.917	0.00	0.04	0.020	O				0.84
10.000	0.00	0.04	0.020	O				0.83
10.083	0.00	0.04	0.020	O				0.82
10.167	0.00	0.04	0.019	O				0.81
10.250	0.00	0.04	0.019	O				0.80
10.333	0.00	0.04	0.019	O				0.79
10.417	0.00	0.04	0.019	O				0.78
10.500	0.00	0.03	0.018	O				0.77
10.583	0.00	0.03	0.018	O				0.76
10.667	0.00	0.03	0.018	O				0.75

10.750	0.00	0.03	0.018	O	|	|	|	0.74
10.833	0.00	0.03	0.018	O	|	|	|	0.73
10.917	0.00	0.03	0.017	O	|	|	|	0.72
11.000	0.00	0.03	0.017	O	|	|	|	0.71
11.083	0.00	0.03	0.017	O	|	|	|	0.70
11.167	0.00	0.03	0.017	O	|	|	|	0.69
11.250	0.00	0.03	0.016	O	|	|	|	0.69
11.333	0.00	0.03	0.016	O	|	|	|	0.68
11.417	0.00	0.03	0.016	O	|	|	|	0.67
11.500	0.00	0.03	0.016	O	|	|	|	0.66
11.583	0.00	0.03	0.016	O	|	|	|	0.65
11.667	0.00	0.03	0.015	O	|	|	|	0.64
11.750	0.00	0.03	0.015	O	|	|	|	0.63
11.833	0.00	0.03	0.015	O	|	|	|	0.63
11.917	0.00	0.03	0.015	O	|	|	|	0.62
12.000	0.00	0.03	0.015	O	|	|	|	0.61
12.083	0.00	0.03	0.014	O	|	|	|	0.60
12.167	0.00	0.03	0.014	O	|	|	|	0.60
12.250	0.00	0.03	0.014	O	|	|	|	0.59
12.333	0.00	0.03	0.014	O	|	|	|	0.58
12.417	0.00	0.03	0.014	O	|	|	|	0.57
12.500	0.00	0.03	0.014	O	|	|	|	0.57
12.583	0.00	0.03	0.013	O	|	|	|	0.56
12.667	0.00	0.02	0.013	O	|	|	|	0.55
12.750	0.00	0.02	0.013	O	|	|	|	0.54
12.833	0.00	0.02	0.013	O	|	|	|	0.54
12.917	0.00	0.02	0.013	O	|	|	|	0.53
13.000	0.00	0.02	0.013	O	|	|	|	0.52
13.083	0.00	0.02	0.012	O	|	|	|	0.52
13.167	0.00	0.02	0.012	O	|	|	|	0.51
13.250	0.00	0.02	0.012	O	|	|	|	0.50
13.333	0.00	0.02	0.012	O	|	|	|	0.50
13.417	0.00	0.02	0.012	O	|	|	|	0.49
13.500	0.00	0.02	0.012	O	|	|	|	0.48
13.583	0.00	0.02	0.011	O	|	|	|	0.48
13.667	0.00	0.02	0.011	O	|	|	|	0.47
13.750	0.00	0.02	0.011	O	|	|	|	0.47
13.833	0.00	0.02	0.011	O	|	|	|	0.46
13.917	0.00	0.02	0.011	O	|	|	|	0.45
14.000	0.00	0.02	0.011	O	|	|	|	0.45
14.083	0.00	0.02	0.011	O	|	|	|	0.44
14.167	0.00	0.02	0.010	O	|	|	|	0.44
14.250	0.00	0.02	0.010	O	|	|	|	0.43
14.333	0.00	0.02	0.010	O	|	|	|	0.43
14.417	0.00	0.02	0.010	O	|	|	|	0.42
14.500	0.00	0.02	0.010	O	|	|	|	0.41
14.583	0.00	0.02	0.010	O	|	|	|	0.41
14.667	0.00	0.02	0.010	O	|	|	|	0.40
14.750	0.00	0.02	0.010	O	|	|	|	0.40
14.833	0.00	0.02	0.009	O	|	|	|	0.39

14.917	0.00	0.02	0.009	O				0.39
15.000	0.00	0.02	0.009	O				0.38
15.083	0.00	0.02	0.009	O				0.38
15.167	0.00	0.02	0.009	O				0.37
15.250	0.00	0.02	0.009	O				0.37
15.333	0.00	0.02	0.009	O				0.36
15.417	0.00	0.02	0.009	O				0.36
15.500	0.00	0.02	0.009	O				0.36
15.583	0.00	0.02	0.008	O				0.35
15.667	0.00	0.02	0.008	O				0.35
15.750	0.00	0.02	0.008	O				0.34
15.833	0.00	0.02	0.008	O				0.34
15.917	0.00	0.01	0.008	O				0.33
16.000	0.00	0.01	0.008	O				0.33
16.083	0.00	0.01	0.008	O				0.32
16.167	0.00	0.01	0.008	O				0.32
16.250	0.00	0.01	0.008	O				0.32
16.333	0.00	0.01	0.007	O				0.31
16.417	0.00	0.01	0.007	O				0.31
16.500	0.00	0.01	0.007	O				0.30
16.583	0.00	0.01	0.007	O				0.30
16.667	0.00	0.01	0.007	O				0.30
16.750	0.00	0.01	0.007	O				0.29
16.833	0.00	0.01	0.007	O				0.29
16.917	0.00	0.01	0.007	O				0.29
17.000	0.00	0.01	0.007	O				0.28
17.083	0.00	0.01	0.007	O				0.28
17.167	0.00	0.01	0.007	O				0.27
17.250	0.00	0.01	0.006	O				0.27
17.333	0.00	0.01	0.006	O				0.27
17.417	0.00	0.01	0.006	O				0.26
17.500	0.00	0.01	0.006	O				0.26
17.583	0.00	0.01	0.006	O				0.26
17.667	0.00	0.01	0.006	O				0.25
17.750	0.00	0.01	0.006	O				0.25
17.833	0.00	0.01	0.006	O				0.25
17.917	0.00	0.01	0.006	O				0.24
18.000	0.00	0.01	0.006	O				0.24
18.083	0.00	0.01	0.006	O				0.24
18.167	0.00	0.01	0.006	O				0.23
18.250	0.00	0.01	0.006	O				0.23
18.333	0.00	0.01	0.005	O				0.23
18.417	0.00	0.01	0.005	O				0.23
18.500	0.00	0.01	0.005	O				0.22
18.583	0.00	0.01	0.005	O				0.22
18.667	0.00	0.01	0.005	O				0.22
18.750	0.00	0.01	0.005	O				0.21
18.833	0.00	0.01	0.005	O				0.21
18.917	0.00	0.01	0.005	O				0.21
19.000	0.00	0.01	0.005	O				0.21

19.083	0.00	0.01	0.005	O	|	|	|	0.20
19.167	0.00	0.01	0.005	O	|	|	|	0.20
19.250	0.00	0.01	0.005	O	|	|	|	0.20
19.333	0.00	0.01	0.005	O	|	|	|	0.20
19.417	0.00	0.01	0.005	O	|	|	|	0.19
19.500	0.00	0.01	0.005	O	|	|	|	0.19
19.583	0.00	0.01	0.005	O	|	|	|	0.19
19.667	0.00	0.01	0.004	O	|	|	|	0.19
19.750	0.00	0.01	0.004	O	|	|	|	0.18
19.833	0.00	0.01	0.004	O	|	|	|	0.18
19.917	0.00	0.01	0.004	O	|	|	|	0.18
20.000	0.00	0.01	0.004	O	|	|	|	0.18
20.083	0.00	0.01	0.004	O	|	|	|	0.17
20.167	0.00	0.01	0.004	O	|	|	|	0.17
20.250	0.00	0.01	0.004	O	|	|	|	0.17
20.333	0.00	0.01	0.004	O	|	|	|	0.17
20.417	0.00	0.01	0.004	O	|	|	|	0.17
20.500	0.00	0.01	0.004	O	|	|	|	0.16
20.583	0.00	0.01	0.004	O	|	|	|	0.16
20.667	0.00	0.01	0.004	O	|	|	|	0.16
20.750	0.00	0.01	0.004	O	|	|	|	0.16
20.833	0.00	0.01	0.004	O	|	|	|	0.16
20.917	0.00	0.01	0.004	O	|	|	|	0.15
21.000	0.00	0.01	0.004	O	|	|	|	0.15
21.083	0.00	0.01	0.004	O	|	|	|	0.15
21.167	0.00	0.01	0.004	O	|	|	|	0.15
21.250	0.00	0.01	0.003	O	|	|	|	0.15
21.333	0.00	0.01	0.003	O	|	|	|	0.14
21.417	0.00	0.01	0.003	O	|	|	|	0.14
21.500	0.00	0.01	0.003	O	|	|	|	0.14
21.583	0.00	0.01	0.003	O	|	|	|	0.14
21.667	0.00	0.01	0.003	O	|	|	|	0.14
21.750	0.00	0.01	0.003	O	|	|	|	0.13
21.833	0.00	0.01	0.003	O	|	|	|	0.13
21.917	0.00	0.01	0.003	O	|	|	|	0.13
22.000	0.00	0.01	0.003	O	|	|	|	0.13
22.083	0.00	0.01	0.003	O	|	|	|	0.13
22.167	0.00	0.01	0.003	O	|	|	|	0.13
22.250	0.00	0.01	0.003	O	|	|	|	0.12
22.333	0.00	0.01	0.003	O	|	|	|	0.12
22.417	0.00	0.01	0.003	O	|	|	|	0.12
22.500	0.00	0.01	0.003	O	|	|	|	0.12
22.583	0.00	0.01	0.003	O	|	|	|	0.12
22.667	0.00	0.01	0.003	O	|	|	|	0.12
22.750	0.00	0.01	0.003	O	|	|	|	0.12
22.833	0.00	0.01	0.003	O	|	|	|	0.11
22.917	0.00	0.01	0.003	O	|	|	|	0.11
23.000	0.00	0.00	0.003	O	|	|	|	0.11
23.083	0.00	0.00	0.003	O	|	|	|	0.11
23.167	0.00	0.00	0.003	O	|	|	|	0.11

23.250	0.00	0.00	0.003	O	|	|	|	0.11
23.333	0.00	0.00	0.003	O	|	|	|	0.11
23.417	0.00	0.00	0.002	O	|	|	|	0.10
23.500	0.00	0.00	0.002	O	|	|	|	0.10
23.583	0.00	0.00	0.002	O	|	|	|	0.10
23.667	0.00	0.00	0.002	O	|	|	|	0.10
23.750	0.00	0.00	0.002	O	|	|	|	0.10
23.833	0.00	0.00	0.002	O	|	|	|	0.10
23.917	0.00	0.00	0.002	O	|	|	|	0.10
24.000	0.00	0.00	0.002	O	|	|	|	0.10
24.083	0.00	0.00	0.002	O	|	|	|	0.09
24.167	0.00	0.00	0.002	O	|	|	|	0.09
24.250	0.00	0.00	0.002	O	|	|	|	0.09
24.333	0.00	0.00	0.002	O	|	|	|	0.09
24.417	0.00	0.00	0.002	O	|	|	|	0.09
24.500	0.00	0.00	0.002	O	|	|	|	0.09
24.583	0.00	0.00	0.002	O	|	|	|	0.09
24.667	0.00	0.00	0.002	O	|	|	|	0.09
24.750	0.00	0.00	0.002	O	|	|	|	0.08
24.833	0.00	0.00	0.002	O	|	|	|	0.08
24.917	0.00	0.00	0.002	O	|	|	|	0.08
25.000	0.00	0.00	0.002	O	|	|	|	0.08
25.083	0.00	0.00	0.002	O	|	|	|	0.08
25.167	0.00	0.00	0.002	O	|	|	|	0.08
25.250	0.00	0.00	0.002	O	|	|	|	0.08
25.333	0.00	0.00	0.002	O	|	|	|	0.08
25.417	0.00	0.00	0.002	O	|	|	|	0.08
25.500	0.00	0.00	0.002	O	|	|	|	0.08
25.583	0.00	0.00	0.002	O	|	|	|	0.07
25.667	0.00	0.00	0.002	O	|	|	|	0.07
25.750	0.00	0.00	0.002	O	|	|	|	0.07
25.833	0.00	0.00	0.002	O	|	|	|	0.07
25.917	0.00	0.00	0.002	O	|	|	|	0.07
26.000	0.00	0.00	0.002	O	|	|	|	0.07
26.083	0.00	0.00	0.002	O	|	|	|	0.07
26.167	0.00	0.00	0.002	O	|	|	|	0.07
26.250	0.00	0.00	0.002	O	|	|	|	0.07
26.333	0.00	0.00	0.002	O	|	|	|	0.07
26.417	0.00	0.00	0.002	O	|	|	|	0.07
26.500	0.00	0.00	0.002	O	|	|	|	0.06
26.583	0.00	0.00	0.002	O	|	|	|	0.06
26.667	0.00	0.00	0.002	O	|	|	|	0.06
26.750	0.00	0.00	0.001	O	|	|	|	0.06
26.833	0.00	0.00	0.001	O	|	|	|	0.06
26.917	0.00	0.00	0.001	O	|	|	|	0.06
27.000	0.00	0.00	0.001	O	|	|	|	0.06
27.083	0.00	0.00	0.001	O	|	|	|	0.06
27.167	0.00	0.00	0.001	O	|	|	|	0.06
27.250	0.00	0.00	0.001	O	|	|	|	0.06
27.333	0.00	0.00	0.001	O	|	|	|	0.06

27.417	0.00	0.00	0.001	O	|	|	|	0.06
27.500	0.00	0.00	0.001	O	|	|	|	0.06
27.583	0.00	0.00	0.001	O	|	|	|	0.05
27.667	0.00	0.00	0.001	O	|	|	|	0.05
27.750	0.00	0.00	0.001	O	|	|	|	0.05
27.833	0.00	0.00	0.001	O	|	|	|	0.05
27.917	0.00	0.00	0.001	O	|	|	|	0.05
28.000	0.00	0.00	0.001	O	|	|	|	0.05
28.083	0.00	0.00	0.001	O	|	|	|	0.05
28.167	0.00	0.00	0.001	O	|	|	|	0.05
28.250	0.00	0.00	0.001	O	|	|	|	0.05
28.333	0.00	0.00	0.001	O	|	|	|	0.05
28.417	0.00	0.00	0.001	O	|	|	|	0.05
28.500	0.00	0.00	0.001	O	|	|	|	0.05
28.583	0.00	0.00	0.001	O	|	|	|	0.05
28.667	0.00	0.00	0.001	O	|	|	|	0.05
28.750	0.00	0.00	0.001	O	|	|	|	0.05
28.833	0.00	0.00	0.001	O	|	|	|	0.04
28.917	0.00	0.00	0.001	O	|	|	|	0.04
29.000	0.00	0.00	0.001	O	|	|	|	0.04
29.083	0.00	0.00	0.001	O	|	|	|	0.04
29.167	0.00	0.00	0.001	O	|	|	|	0.04
29.250	0.00	0.00	0.001	O	|	|	|	0.04
29.333	0.00	0.00	0.001	O	|	|	|	0.04
29.417	0.00	0.00	0.001	O	|	|	|	0.04
29.500	0.00	0.00	0.001	O	|	|	|	0.04
29.583	0.00	0.00	0.001	O	|	|	|	0.04
29.667	0.00	0.00	0.001	O	|	|	|	0.04
29.750	0.00	0.00	0.001	O	|	|	|	0.04
29.833	0.00	0.00	0.001	O	|	|	|	0.04
29.917	0.00	0.00	0.001	O	|	|	|	0.04
30.000	0.00	0.00	0.001	O	|	|	|	0.04
30.083	0.00	0.00	0.001	O	|	|	|	0.04
30.167	0.00	0.00	0.001	O	|	|	|	0.04
30.250	0.00	0.00	0.001	O	|	|	|	0.04
30.333	0.00	0.00	0.001	O	|	|	|	0.04
30.417	0.00	0.00	0.001	O	|	|	|	0.04
30.500	0.00	0.00	0.001	O	|	|	|	0.03
30.583	0.00	0.00	0.001	O	|	|	|	0.03
30.667	0.00	0.00	0.001	O	|	|	|	0.03
30.750	0.00	0.00	0.001	O	|	|	|	0.03
30.833	0.00	0.00	0.001	O	|	|	|	0.03
30.917	0.00	0.00	0.001	O	|	|	|	0.03
31.000	0.00	0.00	0.001	O	|	|	|	0.03
31.083	0.00	0.00	0.001	O	|	|	|	0.03
31.167	0.00	0.00	0.001	O	|	|	|	0.03
31.250	0.00	0.00	0.001	O	|	|	|	0.03
31.333	0.00	0.00	0.001	O	|	|	|	0.03
31.417	0.00	0.00	0.001	O	|	|	|	0.03
31.500	0.00	0.00	0.001	O	|	|	|	0.03

31.583	0.00	0.00	0.001	O	|	|	|	|	0.03
31.667	0.00	0.00	0.001	O	|	|	|	|	0.03
31.750	0.00	0.00	0.001	O	|	|	|	|	0.03
31.833	0.00	0.00	0.001	O	|	|	|	|	0.03
31.917	0.00	0.00	0.001	O	|	|	|	|	0.03
32.000	0.00	0.00	0.001	O	|	|	|	|	0.03
32.083	0.00	0.00	0.001	O	|	|	|	|	0.03
32.167	0.00	0.00	0.001	O	|	|	|	|	0.03
32.250	0.00	0.00	0.001	O	|	|	|	|	0.03
32.333	0.00	0.00	0.001	O	|	|	|	|	0.03
32.417	0.00	0.00	0.001	O	|	|	|	|	0.03
32.500	0.00	0.00	0.001	O	|	|	|	|	0.03
32.583	0.00	0.00	0.001	O	|	|	|	|	0.03
32.667	0.00	0.00	0.001	O	|	|	|	|	0.02
32.750	0.00	0.00	0.001	O	|	|	|	|	0.02
32.833	0.00	0.00	0.001	O	|	|	|	|	0.02
32.917	0.00	0.00	0.001	O	|	|	|	|	0.02
33.000	0.00	0.00	0.001	O	|	|	|	|	0.02
33.083	0.00	0.00	0.001	O	|	|	|	|	0.02
33.167	0.00	0.00	0.001	O	|	|	|	|	0.02
33.250	0.00	0.00	0.001	O	|	|	|	|	0.02
33.333	0.00	0.00	0.001	O	|	|	|	|	0.02
33.417	0.00	0.00	0.001	O	|	|	|	|	0.02

**********HYDROGRAPH DATA**********

Number of intervals = 401
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.045 (CFS)
Total volume = 0.054 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
2 yr
3 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris32.rte
**********HYDROGRAPH DATA**********
Number of intervals = 44
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.966 (CFS)
Total volume = 0.094 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 44
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.2 0.48 0.72 0.97	Depth (Ft.)
0.083	0.03	0.00	0.000	OI | | | |	0.00
0.167	0.12	0.00	0.001	O I | | | |	0.03
0.250	0.14	0.00	0.001	O I | | | |	0.06
0.333	0.15	0.00	0.002	O I | | | |	0.10
0.417	0.18	0.01	0.004	O I | | | |	0.15
0.500	0.20	0.01	0.005	O I | | | |	0.20
0.583	0.22	0.01	0.006	O I| | | |	0.26
0.667	0.21	0.01	0.008	O I| | | |	0.32
0.750	0.23	0.02	0.009	O I| | | |	0.37
0.833	0.23	0.02	0.010	O I| | | |	0.44
0.917	0.22	0.02	0.012	O I| | | |	0.49
1.000	0.22	0.02	0.013	O I| | | |	0.55
1.083	0.25	0.03	0.015	O I | | |	0.61
1.167	0.28	0.03	0.016	|O |I | | |	0.68
1.250	0.29	0.03	0.018	|O |I | | |	0.75
1.333	0.29	0.04	0.020	|O |I | | |	0.82
1.417	0.29	0.04	0.021	|O |I | | |	0.89
1.500	0.33	0.04	0.023	|O | I | | |	0.97
1.583	0.34	0.04	0.025	|O | I | | |	1.03
1.667	0.34	0.04	0.027	|O | I | | |	1.08
1.750	0.37	0.04	0.029	|O | I | | |	1.14
1.833	0.41	0.04	0.032	|O | I | | |	1.20
1.917	0.41	0.04	0.034	|O | I | | |	1.26
2.000	0.40	0.04	0.037	|O | I | | |	1.32
2.083	0.41	0.04	0.039	|O | I | | |	1.38
2.167	0.44	0.04	0.042	|O | I | | |	1.45
2.250	0.54	0.04	0.045	|O | |I | |	1.53
2.333	0.58	0.04	0.049	|O | | I | |	1.61

```
2.417    0.59    0.04      0.052  |O      |        |  I    |        |     1.71
2.500    0.80    0.04      0.057  |O      |        |       | I      |     1.82
2.583    0.92    0.04      0.062  |O      |        |       |     I  |     1.96
2.667    0.97    0.04      0.069  |O      |        |       |      I|     2.11
2.750    0.76    0.04      0.074  |O      |        |       |I       |     2.26
2.833    0.47    0.04      0.078  |O      |       I|       |        |     2.35
2.917    0.36    0.04      0.081  |O      |   I    |       |        |     2.42
3.000    0.29    0.04      0.083  |O      |I       |       |        |     2.47
3.083    0.17    0.04      0.084  |O   I  |        |       |        |     2.50
3.167    0.08    0.04      0.084  |OI     |        |       |        |     2.51
3.250    0.05    0.04      0.085  |O      |        |       |        |     2.52
3.333    0.02    0.04      0.085  IO      |        |       |        |     2.51
3.417    0.01    0.04      0.084  IO      |        |       |        |     2.51
3.500    0.01    0.04      0.084  IO      |        |       |        |     2.50
3.583    0.00    0.04      0.084  IO      |        |       |        |     2.50
3.667    0.00    0.04      0.084  IO      |        |       |        |     2.49
3.750    0.00    0.04      0.083  IO      |        |       |        |     2.48
3.833    0.00    0.04      0.083  IO      |        |       |        |     2.47
3.917    0.00    0.04      0.083  IO      |        |       |        |     2.47
4.000    0.00    0.04      0.082  IO      |        |       |        |     2.46
4.083    0.00    0.04      0.082  IO      |        |       |        |     2.45
4.167    0.00    0.04      0.082  IO      |        |       |        |     2.44
4.250    0.00    0.04      0.081  IO      |        |       |        |     2.43
4.333    0.00    0.04      0.081  IO      |        |       |        |     2.43
4.417    0.00    0.04      0.081  IO      |        |       |        |     2.42
4.500    0.00    0.04      0.080  IO      |        |       |        |     2.41
4.583    0.00    0.04      0.080  IO      |        |       |        |     2.40
4.667    0.00    0.04      0.080  IO      |        |       |        |     2.40
4.750    0.00    0.04      0.080  IO      |        |       |        |     2.39
4.833    0.00    0.04      0.079  IO      |        |       |        |     2.38
4.917    0.00    0.04      0.079  IO      |        |       |        |     2.37
5.000    0.00    0.04      0.079  IO      |        |       |        |     2.36
5.083    0.00    0.04      0.078  IO      |        |       |        |     2.36
5.167    0.00    0.04      0.078  IO      |        |       |        |     2.35
5.250    0.00    0.04      0.078  IO      |        |       |        |     2.34
5.333    0.00    0.04      0.077  IO      |        |       |        |     2.33
5.417    0.00    0.04      0.077  IO      |        |       |        |     2.33
5.500    0.00    0.04      0.077  IO      |        |       |        |     2.32
5.583    0.00    0.04      0.076  IO      |        |       |        |     2.31
5.667    0.00    0.04      0.076  IO      |        |       |        |     2.30
5.750    0.00    0.04      0.076  IO      |        |       |        |     2.29
5.833    0.00    0.04      0.075  IO      |        |       |        |     2.29
5.917    0.00    0.04      0.075  IO      |        |       |        |     2.28
6.000    0.00    0.04      0.075  IO      |        |       |        |     2.27
6.083    0.00    0.04      0.075  IO      |        |       |        |     2.26
6.167    0.00    0.04      0.074  IO      |        |       |        |     2.26
6.250    0.00    0.04      0.074  IO      |        |       |        |     2.25
6.333    0.00    0.04      0.074  IO      |        |       |        |     2.24
6.417    0.00    0.04      0.073  IO      |        |       |        |     2.23
6.500    0.00    0.04      0.073  IO      |        |       |        |     2.22
```

6.583	0.00	0.04	0.073	IO				2.22
6.667	0.00	0.04	0.072	IO				2.21
6.750	0.00	0.04	0.072	IO				2.20
6.833	0.00	0.04	0.072	IO				2.19
6.917	0.00	0.04	0.071	IO				2.19
7.000	0.00	0.04	0.071	IO				2.18
7.083	0.00	0.04	0.071	IO				2.17
7.167	0.00	0.04	0.071	IO				2.16
7.250	0.00	0.04	0.070	IO				2.16
7.333	0.00	0.04	0.070	IO				2.15
7.417	0.00	0.04	0.070	IO				2.14
7.500	0.00	0.04	0.069	IO				2.13
7.583	0.00	0.04	0.069	IO				2.12
7.667	0.00	0.04	0.069	IO				2.12
7.750	0.00	0.04	0.068	IO				2.11
7.833	0.00	0.04	0.068	IO				2.10
7.917	0.00	0.04	0.068	IO				2.09
8.000	0.00	0.04	0.067	IO				2.09
8.083	0.00	0.04	0.067	IO				2.08
8.167	0.00	0.04	0.067	IO				2.07
8.250	0.00	0.04	0.066	IO				2.06
8.333	0.00	0.04	0.066	IO				2.05
8.417	0.00	0.04	0.066	IO				2.05
8.500	0.00	0.04	0.066	IO				2.04
8.583	0.00	0.04	0.065	IO				2.03
8.667	0.00	0.04	0.065	IO				2.02
8.750	0.00	0.04	0.065	IO				2.02
8.833	0.00	0.04	0.064	IO				2.01
8.917	0.00	0.04	0.064	IO				2.00
9.000	0.00	0.04	0.064	IO				1.99
9.083	0.00	0.04	0.063	IO				1.98
9.167	0.00	0.04	0.063	IO				1.98
9.250	0.00	0.04	0.063	IO				1.97
9.333	0.00	0.04	0.062	IO				1.96
9.417	0.00	0.04	0.062	IO				1.95
9.500	0.00	0.04	0.062	IO				1.95
9.583	0.00	0.04	0.062	IO				1.94
9.667	0.00	0.04	0.061	IO				1.93
9.750	0.00	0.04	0.061	IO				1.92
9.833	0.00	0.04	0.061	IO				1.91
9.917	0.00	0.04	0.060	IO				1.91
10.000	0.00	0.04	0.060	IO				1.90
10.083	0.00	0.04	0.060	IO				1.89
10.167	0.00	0.04	0.059	IO				1.88
10.250	0.00	0.04	0.059	IO				1.88
10.333	0.00	0.04	0.059	IO				1.87
10.417	0.00	0.04	0.058	IO				1.86
10.500	0.00	0.04	0.058	IO				1.85
10.583	0.00	0.04	0.058	IO				1.85
10.667	0.00	0.04	0.058	IO				1.84

10.750	0.00	0.04	0.057	IO				1.83
10.833	0.00	0.04	0.057	IO				1.82
10.917	0.00	0.04	0.057	IO				1.81
11.000	0.00	0.04	0.056	IO				1.81
11.083	0.00	0.04	0.056	IO				1.80
11.167	0.00	0.04	0.056	IO				1.79
11.250	0.00	0.04	0.055	IO				1.78
11.333	0.00	0.04	0.055	IO				1.78
11.417	0.00	0.04	0.055	IO				1.77
11.500	0.00	0.04	0.054	IO				1.76
11.583	0.00	0.04	0.054	IO				1.75
11.667	0.00	0.04	0.054	IO				1.74
11.750	0.00	0.04	0.053	IO				1.74
11.833	0.00	0.04	0.053	IO				1.73
11.917	0.00	0.04	0.053	IO				1.72
12.000	0.00	0.04	0.053	IO				1.71
12.083	0.00	0.04	0.052	IO				1.71
12.167	0.00	0.04	0.052	IO				1.70
12.250	0.00	0.04	0.052	IO				1.69
12.333	0.00	0.04	0.051	IO				1.68
12.417	0.00	0.04	0.051	IO				1.67
12.500	0.00	0.04	0.051	IO				1.67
12.583	0.00	0.04	0.050	IO				1.66
12.667	0.00	0.04	0.050	IO				1.65
12.750	0.00	0.04	0.050	IO				1.64
12.833	0.00	0.04	0.049	IO				1.64
12.917	0.00	0.04	0.049	IO				1.63
13.000	0.00	0.04	0.049	IO				1.62
13.083	0.00	0.04	0.049	IO				1.61
13.167	0.00	0.04	0.048	IO				1.61
13.250	0.00	0.04	0.048	IO				1.60
13.333	0.00	0.04	0.048	IO				1.59
13.417	0.00	0.04	0.047	IO				1.58
13.500	0.00	0.04	0.047	IO				1.57
13.583	0.00	0.04	0.047	IO				1.57
13.667	0.00	0.04	0.046	IO				1.56
13.750	0.00	0.04	0.046	IO				1.55
13.833	0.00	0.04	0.046	IO				1.54
13.917	0.00	0.04	0.045	IO				1.54
14.000	0.00	0.04	0.045	IO				1.53
14.083	0.00	0.04	0.045	IO				1.52
14.167	0.00	0.04	0.044	IO				1.51
14.250	0.00	0.04	0.044	IO				1.50
14.333	0.00	0.04	0.044	IO				1.50
14.417	0.00	0.04	0.044	IO				1.49
14.500	0.00	0.04	0.043	IO				1.48
14.583	0.00	0.04	0.043	IO				1.47
14.667	0.00	0.04	0.043	IO				1.47
14.750	0.00	0.04	0.042	IO				1.46
14.833	0.00	0.04	0.042	IO				1.45

14.917	0.00	0.04	0.042	IO				1.44
15.000	0.00	0.04	0.041	IO				1.43
15.083	0.00	0.04	0.041	IO				1.43
15.167	0.00	0.04	0.041	IO				1.42
15.250	0.00	0.04	0.040	IO				1.41
15.333	0.00	0.04	0.040	IO				1.40
15.417	0.00	0.04	0.040	IO				1.40
15.500	0.00	0.04	0.040	IO				1.39
15.583	0.00	0.04	0.039	IO				1.38
15.667	0.00	0.04	0.039	IO				1.37
15.750	0.00	0.04	0.039	IO				1.36
15.833	0.00	0.04	0.038	IO				1.36
15.917	0.00	0.04	0.038	IO				1.35
16.000	0.00	0.04	0.038	IO				1.34
16.083	0.00	0.04	0.037	IO				1.33
16.167	0.00	0.04	0.037	IO				1.33
16.250	0.00	0.04	0.037	IO				1.32
16.333	0.00	0.04	0.036	IO				1.31
16.417	0.00	0.04	0.036	IO				1.30
16.500	0.00	0.04	0.036	IO				1.30
16.583	0.00	0.04	0.035	IO				1.29
16.667	0.00	0.04	0.035	IO				1.28
16.750	0.00	0.04	0.035	IO				1.27
16.833	0.00	0.04	0.035	IO				1.26
16.917	0.00	0.04	0.034	IO				1.26
17.000	0.00	0.04	0.034	IO				1.25
17.083	0.00	0.04	0.034	IO				1.24
17.167	0.00	0.04	0.033	IO				1.23
17.250	0.00	0.04	0.033	IO				1.23
17.333	0.00	0.04	0.033	IO				1.22
17.417	0.00	0.04	0.032	IO				1.21
17.500	0.00	0.04	0.032	IO				1.20
17.583	0.00	0.04	0.032	IO				1.19
17.667	0.00	0.04	0.031	IO				1.19
17.750	0.00	0.04	0.031	IO				1.18
17.833	0.00	0.04	0.031	IO				1.17
17.917	0.00	0.04	0.031	IO				1.16
18.000	0.00	0.04	0.030	IO				1.16
18.083	0.00	0.04	0.030	IO				1.15
18.167	0.00	0.04	0.030	IO				1.14
18.250	0.00	0.04	0.029	IO				1.13
18.333	0.00	0.04	0.029	IO				1.12
18.417	0.00	0.04	0.029	IO				1.12
18.500	0.00	0.04	0.028	IO				1.11
18.583	0.00	0.04	0.028	IO				1.10
18.667	0.00	0.04	0.028	IO				1.09
18.750	0.00	0.04	0.027	IO				1.09
18.833	0.00	0.04	0.027	IO				1.08
18.917	0.00	0.04	0.027	IO				1.07
19.000	0.00	0.04	0.027	IO				1.06

19.083	0.00	0.04	0.026	IO				1.05
19.167	0.00	0.04	0.026	IO				1.05
19.250	0.00	0.04	0.026	IO				1.04
19.333	0.00	0.04	0.025	IO				1.03
19.417	0.00	0.04	0.025	IO				1.02
19.500	0.00	0.04	0.025	IO				1.02
19.583	0.00	0.04	0.024	IO				1.01
19.667	0.00	0.04	0.024	IO				1.00
19.750	0.00	0.04	0.024	IO				0.99
19.833	0.00	0.04	0.023	IO				0.98
19.917	0.00	0.04	0.023	IO				0.96
20.000	0.00	0.04	0.023	IO				0.95
20.083	0.00	0.04	0.023	IO				0.94
20.167	0.00	0.04	0.022	IO				0.93
20.250	0.00	0.04	0.022	IO				0.91
20.333	0.00	0.04	0.022	IO				0.90
20.417	0.00	0.04	0.021	IO				0.89
20.500	0.00	0.04	0.021	IO				0.88
20.583	0.00	0.04	0.021	IO				0.87
20.667	0.00	0.04	0.021	IO				0.86
20.750	0.00	0.04	0.020	IO				0.85
20.833	0.00	0.04	0.020	IO				0.84
20.917	0.00	0.04	0.020	IO				0.82
21.000	0.00	0.04	0.020	IO				0.81
21.083	0.00	0.04	0.019	IO				0.80
21.167	0.00	0.04	0.019	IO				0.79
21.250	0.00	0.04	0.019	IO				0.78
21.333	0.00	0.03	0.019	IO				0.77
21.417	0.00	0.03	0.018	IO				0.76
21.500	0.00	0.03	0.018	IO				0.75
21.583	0.00	0.03	0.018	IO				0.74
21.667	0.00	0.03	0.018	IO				0.73
21.750	0.00	0.03	0.017	IO				0.72
21.833	0.00	0.03	0.017	IO				0.72
21.917	0.00	0.03	0.017	IO				0.71
22.000	0.00	0.03	0.017	IO				0.70
22.083	0.00	0.03	0.017	IO				0.69
22.167	0.00	0.03	0.016	IO				0.68
22.250	0.00	0.03	0.016	IO				0.67
22.333	0.00	0.03	0.016	O				0.66
22.417	0.00	0.03	0.016	O				0.65
22.500	0.00	0.03	0.015	O				0.65
22.583	0.00	0.03	0.015	O				0.64
22.667	0.00	0.03	0.015	O				0.63
22.750	0.00	0.03	0.015	O				0.62
22.833	0.00	0.03	0.015	O				0.61
22.917	0.00	0.03	0.015	O				0.61
23.000	0.00	0.03	0.014	O				0.60
23.083	0.00	0.03	0.014	O				0.59
23.167	0.00	0.03	0.014	O				0.58

23.250	0.00	0.03	0.014	O				0.57
23.333	0.00	0.03	0.014	O				0.57
23.417	0.00	0.03	0.013	O				0.56
23.500	0.00	0.02	0.013	O				0.55
23.583	0.00	0.02	0.013	O				0.55
23.667	0.00	0.02	0.013	O				0.54
23.750	0.00	0.02	0.013	O				0.53
23.833	0.00	0.02	0.013	O				0.52
23.917	0.00	0.02	0.012	O				0.52
24.000	0.00	0.02	0.012	O				0.51
24.083	0.00	0.02	0.012	O				0.51
24.167	0.00	0.02	0.012	O				0.50
24.250	0.00	0.02	0.012	O				0.49
24.333	0.00	0.02	0.012	O				0.49
24.417	0.00	0.02	0.012	O				0.48
24.500	0.00	0.02	0.011	O				0.47
24.583	0.00	0.02	0.011	O				0.47
24.667	0.00	0.02	0.011	O				0.46
24.750	0.00	0.02	0.011	O				0.46
24.833	0.00	0.02	0.011	O				0.45
24.917	0.00	0.02	0.011	O				0.44
25.000	0.00	0.02	0.011	O				0.44
25.083	0.00	0.02	0.010	O				0.43
25.167	0.00	0.02	0.010	O				0.43
25.250	0.00	0.02	0.010	O				0.42
25.333	0.00	0.02	0.010	O				0.42
25.417	0.00	0.02	0.010	O				0.41
25.500	0.00	0.02	0.010	O				0.41
25.583	0.00	0.02	0.010	O				0.40
25.667	0.00	0.02	0.009	O				0.40
25.750	0.00	0.02	0.009	O				0.39
25.833	0.00	0.02	0.009	O				0.39
25.917	0.00	0.02	0.009	O				0.38
26.000	0.00	0.02	0.009	O				0.38
26.083	0.00	0.02	0.009	O				0.37
26.167	0.00	0.02	0.009	O				0.37
26.250	0.00	0.02	0.009	O				0.36
26.333	0.00	0.02	0.009	O				0.36
26.417	0.00	0.02	0.008	O				0.35
26.500	0.00	0.02	0.008	O				0.35
26.583	0.00	0.02	0.008	O				0.34
26.667	0.00	0.02	0.008	O				0.34
26.750	0.00	0.02	0.008	O				0.33
26.833	0.00	0.01	0.008	O				0.33
26.917	0.00	0.01	0.008	O				0.33
27.000	0.00	0.01	0.008	O				0.32
27.083	0.00	0.01	0.008	O				0.32
27.167	0.00	0.01	0.008	O				0.31
27.250	0.00	0.01	0.007	O				0.31
27.333	0.00	0.01	0.007	O				0.31

27.417	0.00	0.01	0.007	O	|	|	|	0.30
27.500	0.00	0.01	0.007	O	|	|	|	0.30
27.583	0.00	0.01	0.007	O	|	|	|	0.29
27.667	0.00	0.01	0.007	O	|	|	|	0.29
27.750	0.00	0.01	0.007	O	|	|	|	0.29
27.833	0.00	0.01	0.007	O	|	|	|	0.28
27.917	0.00	0.01	0.007	O	|	|	|	0.28
28.000	0.00	0.01	0.007	O	|	|	|	0.28
28.083	0.00	0.01	0.007	O	|	|	|	0.27
28.167	0.00	0.01	0.006	O	|	|	|	0.27
28.250	0.00	0.01	0.006	O	|	|	|	0.26
28.333	0.00	0.01	0.006	O	|	|	|	0.26
28.417	0.00	0.01	0.006	O	|	|	|	0.26
28.500	0.00	0.01	0.006	O	|	|	|	0.25
28.583	0.00	0.01	0.006	O	|	|	|	0.25
28.667	0.00	0.01	0.006	O	|	|	|	0.25
28.750	0.00	0.01	0.006	O	|	|	|	0.25
28.833	0.00	0.01	0.006	O	|	|	|	0.24
28.917	0.00	0.01	0.006	O	|	|	|	0.24
29.000	0.00	0.01	0.006	O	|	|	|	0.24
29.083	0.00	0.01	0.006	O	|	|	|	0.23
29.167	0.00	0.01	0.006	O	|	|	|	0.23
29.250	0.00	0.01	0.005	O	|	|	|	0.23
29.333	0.00	0.01	0.005	O	|	|	|	0.22
29.417	0.00	0.01	0.005	O	|	|	|	0.22
29.500	0.00	0.01	0.005	O	|	|	|	0.22
29.583	0.00	0.01	0.005	O	|	|	|	0.22
29.667	0.00	0.01	0.005	O	|	|	|	0.21
29.750	0.00	0.01	0.005	O	|	|	|	0.21
29.833	0.00	0.01	0.005	O	|	|	|	0.21
29.917	0.00	0.01	0.005	O	|	|	|	0.20
30.000	0.00	0.01	0.005	O	|	|	|	0.20
30.083	0.00	0.01	0.005	O	|	|	|	0.20
30.167	0.00	0.01	0.005	O	|	|	|	0.20
30.250	0.00	0.01	0.005	O	|	|	|	0.19
30.333	0.00	0.01	0.005	O	|	|	|	0.19
30.417	0.00	0.01	0.005	O	|	|	|	0.19
30.500	0.00	0.01	0.004	O	|	|	|	0.19
30.583	0.00	0.01	0.004	O	|	|	|	0.18
30.667	0.00	0.01	0.004	O	|	|	|	0.18
30.750	0.00	0.01	0.004	O	|	|	|	0.18
30.833	0.00	0.01	0.004	O	|	|	|	0.18
30.917	0.00	0.01	0.004	O	|	|	|	0.18
31.000	0.00	0.01	0.004	O	|	|	|	0.17
31.083	0.00	0.01	0.004	O	|	|	|	0.17
31.167	0.00	0.01	0.004	O	|	|	|	0.17
31.250	0.00	0.01	0.004	O	|	|	|	0.17
31.333	0.00	0.01	0.004	O	|	|	|	0.16
31.417	0.00	0.01	0.004	O	|	|	|	0.16
31.500	0.00	0.01	0.004	O	|	|	|	0.16

31.583	0.00	0.01	0.004	O	|	|	|	0.16
31.667	0.00	0.01	0.004	O	|	|	|	0.16
31.750	0.00	0.01	0.004	O	|	|	|	0.15
31.833	0.00	0.01	0.004	O	|	|	|	0.15
31.917	0.00	0.01	0.004	O	|	|	|	0.15
32.000	0.00	0.01	0.004	O	|	|	|	0.15
32.083	0.00	0.01	0.004	O	|	|	|	0.15
32.167	0.00	0.01	0.003	O	|	|	|	0.14
32.250	0.00	0.01	0.003	O	|	|	|	0.14
32.333	0.00	0.01	0.003	O	|	|	|	0.14
32.417	0.00	0.01	0.003	O	|	|	|	0.14
32.500	0.00	0.01	0.003	O	|	|	|	0.14
32.583	0.00	0.01	0.003	O	|	|	|	0.14
32.667	0.00	0.01	0.003	O	|	|	|	0.13
32.750	0.00	0.01	0.003	O	|	|	|	0.13
32.833	0.00	0.01	0.003	O	|	|	|	0.13
32.917	0.00	0.01	0.003	O	|	|	|	0.13
33.000	0.00	0.01	0.003	O	|	|	|	0.13
33.083	0.00	0.01	0.003	O	|	|	|	0.13
33.167	0.00	0.01	0.003	O	|	|	|	0.12
33.250	0.00	0.01	0.003	O	|	|	|	0.12
33.333	0.00	0.01	0.003	O	|	|	|	0.12
33.417	0.00	0.01	0.003	O	|	|	|	0.12
33.500	0.00	0.01	0.003	O	|	|	|	0.12
33.583	0.00	0.01	0.003	O	|	|	|	0.12
33.667	0.00	0.01	0.003	O	|	|	|	0.11
33.750	0.00	0.01	0.003	O	|	|	|	0.11
33.833	0.00	0.01	0.003	O	|	|	|	0.11
33.917	0.00	0.00	0.003	O	|	|	|	0.11
34.000	0.00	0.00	0.003	O	|	|	|	0.11
34.083	0.00	0.00	0.003	O	|	|	|	0.11
34.167	0.00	0.00	0.003	O	|	|	|	0.11
34.250	0.00	0.00	0.003	O	|	|	|	0.10
34.333	0.00	0.00	0.002	O	|	|	|	0.10
34.417	0.00	0.00	0.002	O	|	|	|	0.10
34.500	0.00	0.00	0.002	O	|	|	|	0.10
34.583	0.00	0.00	0.002	O	|	|	|	0.10
34.667	0.00	0.00	0.002	O	|	|	|	0.10
34.750	0.00	0.00	0.002	O	|	|	|	0.10
34.833	0.00	0.00	0.002	O	|	|	|	0.10
34.917	0.00	0.00	0.002	O	|	|	|	0.09
35.000	0.00	0.00	0.002	O	|	|	|	0.09
35.083	0.00	0.00	0.002	O	|	|	|	0.09
35.167	0.00	0.00	0.002	O	|	|	|	0.09
35.250	0.00	0.00	0.002	O	|	|	|	0.09
35.333	0.00	0.00	0.002	O	|	|	|	0.09
35.417	0.00	0.00	0.002	O	|	|	|	0.09
35.500	0.00	0.00	0.002	O	|	|	|	0.09
35.583	0.00	0.00	0.002	O	|	|	|	0.08
35.667	0.00	0.00	0.002	O	|	|	|	0.08

35.750	0.00	0.00	0.002	O				0.08
35.833	0.00	0.00	0.002	O				0.08
35.917	0.00	0.00	0.002	O				0.08
36.000	0.00	0.00	0.002	O				0.08
36.083	0.00	0.00	0.002	O				0.08
36.167	0.00	0.00	0.002	O				0.08
36.250	0.00	0.00	0.002	O				0.08
36.333	0.00	0.00	0.002	O				0.08
36.417	0.00	0.00	0.002	O				0.07
36.500	0.00	0.00	0.002	O				0.07
36.583	0.00	0.00	0.002	O				0.07
36.667	0.00	0.00	0.002	O				0.07
36.750	0.00	0.00	0.002	O				0.07
36.833	0.00	0.00	0.002	O				0.07
36.917	0.00	0.00	0.002	O				0.07
37.000	0.00	0.00	0.002	O				0.07
37.083	0.00	0.00	0.002	O				0.07
37.167	0.00	0.00	0.002	O				0.07
37.250	0.00	0.00	0.002	O				0.07
37.333	0.00	0.00	0.002	O				0.06
37.417	0.00	0.00	0.002	O				0.06
37.500	0.00	0.00	0.002	O				0.06
37.583	0.00	0.00	0.001	O				0.06
37.667	0.00	0.00	0.001	O				0.06
37.750	0.00	0.00	0.001	O				0.06
37.833	0.00	0.00	0.001	O				0.06
37.917	0.00	0.00	0.001	O				0.06
38.000	0.00	0.00	0.001	O				0.06
38.083	0.00	0.00	0.001	O				0.06
38.167	0.00	0.00	0.001	O				0.06
38.250	0.00	0.00	0.001	O				0.06
38.333	0.00	0.00	0.001	O				0.06
38.417	0.00	0.00	0.001	O				0.05
38.500	0.00	0.00	0.001	O				0.05
38.583	0.00	0.00	0.001	O				0.05
38.667	0.00	0.00	0.001	O				0.05
38.750	0.00	0.00	0.001	O				0.05
38.833	0.00	0.00	0.001	O				0.05
38.917	0.00	0.00	0.001	O				0.05
39.000	0.00	0.00	0.001	O				0.05
39.083	0.00	0.00	0.001	O				0.05
39.167	0.00	0.00	0.001	O				0.05
39.250	0.00	0.00	0.001	O				0.05
39.333	0.00	0.00	0.001	O				0.05
39.417	0.00	0.00	0.001	O				0.05
39.500	0.00	0.00	0.001	O				0.05
39.583	0.00	0.00	0.001	O				0.05
39.667	0.00	0.00	0.001	O				0.05
39.750	0.00	0.00	0.001	O				0.04
39.833	0.00	0.00	0.001	O				0.04

39.917	0.00	0.00	0.001	O	|	|	|	0.04
40.000	0.00	0.00	0.001	O	|	|	|	0.04
40.083	0.00	0.00	0.001	O	|	|	|	0.04
40.167	0.00	0.00	0.001	O	|	|	|	0.04
40.250	0.00	0.00	0.001	O	|	|	|	0.04
40.333	0.00	0.00	0.001	O	|	|	|	0.04
40.417	0.00	0.00	0.001	O	|	|	|	0.04
40.500	0.00	0.00	0.001	O	|	|	|	0.04
40.583	0.00	0.00	0.001	O	|	|	|	0.04
40.667	0.00	0.00	0.001	O	|	|	|	0.04
40.750	0.00	0.00	0.001	O	|	|	|	0.04
40.833	0.00	0.00	0.001	O	|	|	|	0.04
40.917	0.00	0.00	0.001	O	|	|	|	0.04
41.000	0.00	0.00	0.001	O	|	|	|	0.04
41.083	0.00	0.00	0.001	O	|	|	|	0.04
41.167	0.00	0.00	0.001	O	|	|	|	0.04
41.250	0.00	0.00	0.001	O	|	|	|	0.04
41.333	0.00	0.00	0.001	O	|	|	|	0.03
41.417	0.00	0.00	0.001	O	|	|	|	0.03
41.500	0.00	0.00	0.001	O	|	|	|	0.03
41.583	0.00	0.00	0.001	O	|	|	|	0.03
41.667	0.00	0.00	0.001	O	|	|	|	0.03
41.750	0.00	0.00	0.001	O	|	|	|	0.03
41.833	0.00	0.00	0.001	O	|	|	|	0.03
41.917	0.00	0.00	0.001	O	|	|	|	0.03
42.000	0.00	0.00	0.001	O	|	|	|	0.03
42.083	0.00	0.00	0.001	O	|	|	|	0.03
42.167	0.00	0.00	0.001	O	|	|	|	0.03
42.250	0.00	0.00	0.001	O	|	|	|	0.03
42.333	0.00	0.00	0.001	O	|	|	|	0.03
42.417	0.00	0.00	0.001	O	|	|	|	0.03
42.500	0.00	0.00	0.001	O	|	|	|	0.03
42.583	0.00	0.00	0.001	O	|	|	|	0.03
42.667	0.00	0.00	0.001	O	|	|	|	0.03
42.750	0.00	0.00	0.001	O	|	|	|	0.03
42.833	0.00	0.00	0.001	O	|	|	|	0.03
42.917	0.00	0.00	0.001	O	|	|	|	0.03
43.000	0.00	0.00	0.001	O	|	|	|	0.03
43.083	0.00	0.00	0.001	O	|	|	|	0.03
43.167	0.00	0.00	0.001	O	|	|	|	0.03
43.250	0.00	0.00	0.001	O	|	|	|	0.03
43.333	0.00	0.00	0.001	O	|	|	|	0.03
43.417	0.00	0.00	0.001	O	|	|	|	0.03
43.500	0.00	0.00	0.001	O	|	|	|	0.02
43.583	0.00	0.00	0.001	O	|	|	|	0.02
43.667	0.00	0.00	0.001	O	|	|	|	0.02
43.750	0.00	0.00	0.001	O	|	|	|	0.02
43.833	0.00	0.00	0.001	O	|	|	|	0.02
43.917	0.00	0.00	0.001	O	|	|	|	0.02
44.000	0.00	0.00	0.001	O	|	|	|	0.02

```
44.083    0.00    0.00      0.001  O       |       |       |       |     0.02
44.167    0.00    0.00      0.001  O       |       |       |       |     0.02
44.250    0.00    0.00      0.001  O       |       |       |       |     0.02

       ****************************HYDROGRAPH DATA****************************
                      Number of intervals =   531
                      Time interval =    5.0 (Min.)
                      Maximum/Peak flow rate =        0.045 (CFS)
                      Total volume =       0.093 (Ac.Ft)
              Status of hydrographs being held in storage
                         Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
       ************************************************************************

       ------------------------------------------------------------------------
```

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
2 yr
6 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris242.rte

**********HYDROGRAPH DATA**********

Number of intervals = 296
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.362 (CFS)
Total volume = 0.221 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++++++++++

Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 296
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.1	0.18	0.27	0.36	Depth (Ft.)
0.083	0.00	0.00	0.000	O	|	|	|	|	0.00
0.167	0.01	0.00	0.000	OI	|	|	|	|	0.00
0.250	0.02	0.00	0.000	OI	|	|	|	|	0.01
0.333	0.02	0.00	0.000	OI	|	|	|	|	0.01
0.417	0.03	0.00	0.000	O I	|	|	|	|	0.02
0.500	0.03	0.00	0.001	O I	|	|	|	|	0.03
0.583	0.03	0.00	0.001	O I	|	|	|	|	0.04
0.667	0.03	0.00	0.001	O I	|	|	|	|	0.04
0.750	0.03	0.00	0.001	O I	|	|	|	|	0.05
0.833	0.03	0.00	0.001	O I	|	|	|	|	0.06
0.917	0.04	0.00	0.002	O I	|	|	|	|	0.07
1.000	0.04	0.00	0.002	O I	|	|	|	|	0.08
1.083	0.04	0.00	0.002	O I	|	|	|	|	0.09
1.167	0.04	0.00	0.002	O I	|	|	|	|	0.10
1.250	0.03	0.00	0.003	O I	|	|	|	|	0.11
1.333	0.03	0.01	0.003	O I	|	|	|	|	0.12
1.417	0.03	0.01	0.003	O I	|	|	|	|	0.13
1.500	0.03	0.01	0.003	O I	|	|	|	|	0.13
1.583	0.03	0.01	0.003	O I	|	|	|	|	0.14
1.667	0.03	0.01	0.004	O I	|	|	|	|	0.15
1.750	0.03	0.01	0.004	O I	|	|	|	|	0.16
1.833	0.03	0.01	0.004	O I	|	|	|	|	0.16
1.917	0.04	0.01	0.004	O I	|	|	|	|	0.17
2.000	0.04	0.01	0.004	O I	|	|	|	|	0.18
2.083	0.04	0.01	0.005	O I	|	|	|	|	0.19
2.167	0.04	0.01	0.005	O I	|	|	|	|	0.20
2.250	0.04	0.01	0.005	O I	|	|	|	|	0.21
2.333	0.04	0.01	0.005	O I	|	|	|	|	0.22

2.417	0.04	0.01	0.005	O I |	|	|	|	0.23
2.500	0.04	0.01	0.006	O I |	|	|	|	0.24
2.583	0.04	0.01	0.006	O I |	|	|	|	0.25
2.667	0.05	0.01	0.006	|O I |	|	|	|	0.26
2.750	0.05	0.01	0.006	|O I |	|	|	|	0.27
2.833	0.05	0.01	0.007	|O I |	|	|	|	0.28
2.917	0.05	0.01	0.007	|O I |	|	|	|	0.29
3.000	0.05	0.01	0.007	|O I |	|	|	|	0.30
3.083	0.05	0.01	0.008	|O I |	|	|	|	0.31
3.167	0.05	0.01	0.008	|O I |	|	|	|	0.32
3.250	0.05	0.02	0.008	|O I |	|	|	|	0.34
3.333	0.05	0.02	0.008	|O I |	|	|	|	0.35
3.417	0.05	0.02	0.009	|O I |	|	|	|	0.36
3.500	0.05	0.02	0.009	|O I |	|	|	|	0.37
3.583	0.05	0.02	0.009	|O I |	|	|	|	0.38
3.667	0.05	0.02	0.009	|O I |	|	|	|	0.39
3.750	0.05	0.02	0.010	|O I |	|	|	|	0.40
3.833	0.06	0.02	0.010	|O I |	|	|	|	0.41
3.917	0.06	0.02	0.010	|O I |	|	|	|	0.42
4.000	0.06	0.02	0.010	|O I |	|	|	|	0.43
4.083	0.06	0.02	0.011	|O I |	|	|	|	0.45
4.167	0.06	0.02	0.011	|O I |	|	|	|	0.46
4.250	0.06	0.02	0.011	|O I |	|	|	|	0.47
4.333	0.07	0.02	0.012	|O I |	|	|	|	0.48
4.417	0.07	0.02	0.012	|O I |	|	|	|	0.50
4.500	0.07	0.02	0.012	| O I |	|	|	|	0.51
4.583	0.07	0.02	0.013	| O I |	|	|	|	0.52
4.667	0.07	0.02	0.013	| O I |	|	|	|	0.54
4.750	0.07	0.02	0.013	| O I |	|	|	|	0.55
4.833	0.08	0.03	0.014	| O I |	|	|	|	0.57
4.917	0.08	0.03	0.014	| O I|	|	|	|	0.58
5.000	0.08	0.03	0.014	| O I|	|	|	|	0.60
5.083	0.08	0.03	0.015	| O I|	|	|	|	0.62
5.167	0.07	0.03	0.015	| O I |	|	|	|	0.63
5.250	0.07	0.03	0.015	| O I |	|	|	|	0.64
5.333	0.07	0.03	0.016	| O I |	|	|	|	0.65
5.417	0.07	0.03	0.016	| O I |	|	|	|	0.66
5.500	0.07	0.03	0.016	| O I |	|	|	|	0.68
5.583	0.08	0.03	0.017	| O I |	|	|	|	0.69
5.667	0.08	0.03	0.017	| O I|	|	|	|	0.70
5.750	0.08	0.03	0.017	| O I|	|	|	|	0.72
5.833	0.08	0.03	0.018	| O I|	|	|	|	0.73
5.917	0.08	0.03	0.018	| O I|	|	|	|	0.75
6.000	0.09	0.03	0.018	| O I|	|	|	|	0.76
6.083	0.09	0.03	0.019	| O I|	|	|	|	0.78
6.167	0.09	0.04	0.019	| O I	|	|	|	0.79
6.250	0.09	0.04	0.019	| O I	|	|	|	0.81
6.333	0.10	0.04	0.020	| O I	|	|	|	0.82
6.417	0.10	0.04	0.020	| O I	|	|	|	0.84
6.500	0.10	0.04	0.021	| O I	|	|	|	0.86

6.583	0.10	0.04	0.021	O	I			0.87
6.667	0.10	0.04	0.021	O	I			0.89
6.750	0.11	0.04	0.022	O	I			0.91
6.833	0.11	0.04	0.022	O	I			0.93
6.917	0.11	0.04	0.023	O	I			0.95
7.000	0.11	0.04	0.023	O	I			0.97
7.083	0.11	0.04	0.024	O	I			0.98
7.167	0.11	0.04	0.024	O	I			1.00
7.250	0.11	0.04	0.024	O	I			1.01
7.333	0.11	0.04	0.025	O	I			1.02
7.417	0.11	0.04	0.025	O	I			1.03
7.500	0.12	0.04	0.026	O	I			1.05
7.583	0.12	0.04	0.026	O	I			1.06
7.667	0.12	0.04	0.027	O	I			1.07
7.750	0.13	0.04	0.027	O	I			1.09
7.833	0.13	0.04	0.028	O	I			1.10
7.917	0.13	0.04	0.029	O	I			1.11
8.000	0.14	0.04	0.029	O	I			1.13
8.083	0.14	0.04	0.030	O	I			1.15
8.167	0.15	0.04	0.031	O	I			1.16
8.250	0.16	0.04	0.031	O	I			1.18
8.333	0.16	0.04	0.032	O	I			1.20
8.417	0.16	0.04	0.033	O	I			1.22
8.500	0.16	0.04	0.034	O	I			1.24
8.583	0.16	0.04	0.034	O	I			1.26
8.667	0.17	0.04	0.035	O	I			1.28
8.750	0.17	0.04	0.036	O	I			1.30
8.833	0.17	0.04	0.037	O	I			1.33
8.917	0.18	0.04	0.038	O	I			1.35
9.000	0.18	0.04	0.039	O	I			1.37
9.083	0.18	0.04	0.040	O	I			1.39
9.167	0.20	0.04	0.041	O	I			1.42
9.250	0.20	0.04	0.042	O	I			1.45
9.333	0.20	0.04	0.043	O	I			1.47
9.417	0.21	0.04	0.044	O	I			1.50
9.500	0.21	0.04	0.045	O	I			1.53
9.583	0.21	0.04	0.046	O	I			1.56
9.667	0.22	0.04	0.047	O	I			1.59
9.750	0.22	0.04	0.049	O	I			1.62
9.833	0.23	0.04	0.050	O	I			1.65
9.917	0.23	0.04	0.051	O	I			1.68
10.000	0.23	0.04	0.052	O	I			1.71
10.083	0.22	0.04	0.054	O	I			1.74
10.167	0.19	0.04	0.055	O	I			1.77
10.250	0.17	0.04	0.056	O	I			1.79
10.333	0.17	0.04	0.057	O	I			1.82
10.417	0.17	0.04	0.057	O	I			1.84
10.500	0.16	0.04	0.058	O	I			1.86
10.583	0.17	0.04	0.059	O	I			1.88
10.667	0.20	0.04	0.060	O	I			1.90

10.750	0.20	0.04	0.061	O		I		1.93
10.833	0.21	0.04	0.062	O		I		1.96
10.917	0.21	0.04	0.063	O		I		1.99
11.000	0.21	0.04	0.065	O		I		2.01
11.083	0.21	0.04	0.066	O		I		2.04
11.167	0.21	0.04	0.067	O		I		2.07
11.250	0.21	0.04	0.068	O		I		2.10
11.333	0.20	0.04	0.069	O		I		2.13
11.417	0.20	0.04	0.070	O		I		2.15
11.500	0.20	0.04	0.071	O		I		2.18
11.583	0.20	0.04	0.072	O		I		2.21
11.667	0.19	0.04	0.073	O		I		2.23
11.750	0.19	0.04	0.074	O		I		2.26
11.833	0.19	0.04	0.075	O		I		2.28
11.917	0.19	0.04	0.076	O		I		2.31
12.000	0.19	0.04	0.077	O		I		2.33
12.083	0.21	0.04	0.078	O		I		2.36
12.167	0.24	0.04	0.080	O		I		2.39
12.250	0.25	0.04	0.081	O		I		2.42
12.333	0.26	0.04	0.082	O		I		2.46
12.417	0.27	0.04	0.084	O		I		2.50
12.500	0.27	0.04	0.086	O		I		2.54
12.583	0.28	0.04	0.087	O		I		2.58
12.667	0.29	0.04	0.089	O		I		2.62
12.750	0.30	0.04	0.091	O		I		2.66
12.833	0.30	0.04	0.092	O		I		2.71
12.917	0.31	0.04	0.094	O		I		2.75
13.000	0.31	0.04	0.096	O		I		2.80
13.083	0.32	0.04	0.098	O		I		2.84
13.167	0.35	0.04	0.100	O		I		2.89
13.250	0.35	0.04	0.102	O		I		2.94
13.333	0.36	0.04	0.104	O		I		3.00
13.417	0.36	0.04	0.106	O		I		3.05
13.500	0.36	0.04	0.108	O		I		3.11
13.583	0.34	0.04	0.110	O		I		3.16
13.667	0.29	0.04	0.112	O		I		3.21
13.750	0.27	0.04	0.114	O		I		3.25
13.833	0.26	0.04	0.115	O		I		3.28
13.917	0.25	0.04	0.117	O		I		3.32
14.000	0.25	0.04	0.118	O		I		3.35
14.083	0.26	0.04	0.120	O		I		3.39
14.167	0.28	0.04	0.121	O		I		3.43
14.250	0.28	0.04	0.123	O		I		3.47
14.333	0.28	0.04	0.124	O		I		3.51
14.417	0.28	0.04	0.126	O		I		3.55
14.500	0.28	0.04	0.128	O		I		3.59
14.583	0.28	0.04	0.129	O		I		3.63
14.667	0.28	0.04	0.131	O		I		3.67
14.750	0.28	0.04	0.132	O		I		3.71
14.833	0.28	0.04	0.134	O		I		3.75

14.917	0.27	0.04	0.136	O			I	3.79
15.000	0.27	0.04	0.137	O			I	3.83
15.083	0.27	0.04	0.139	O			I	3.87
15.167	0.26	0.04	0.140	O			I	3.91
15.250	0.26	0.04	0.142	O			I	3.94
15.333	0.26	0.04	0.143	O			I	3.98
15.417	0.25	0.04	0.145	O			I	4.02
15.500	0.25	0.04	0.146	O			I	4.05
15.583	0.24	0.04	0.147	O			I	4.09
15.667	0.22	0.04	0.149	O		I		4.12
15.750	0.21	0.04	0.150	O		I		4.15
15.833	0.21	0.04	0.151	O		I		4.17
15.917	0.21	0.04	0.152	O		I		4.20
16.000	0.21	0.04	0.153	O		I		4.23
16.083	0.18	0.04	0.154	O	I			4.26
16.167	0.10	0.04	0.155	O	I			4.27
16.250	0.07	0.04	0.155	O I				4.28
16.333	0.06	0.04	0.155	O I				4.28
16.417	0.05	0.04	0.155	OI				4.28
16.500	0.05	0.04	0.155	OI				4.28
16.583	0.04	0.04	0.155	O				4.28
16.667	0.04	0.04	0.155	O				4.28
16.750	0.03	0.04	0.155	O				4.28
16.833	0.03	0.04	0.155	IO				4.28
16.917	0.03	0.04	0.155	IO				4.28
17.000	0.03	0.04	0.155	IO				4.28
17.083	0.04	0.04	0.155	O				4.27
17.167	0.05	0.04	0.155	OI				4.27
17.250	0.05	0.04	0.155	OI				4.27
17.333	0.05	0.04	0.155	OI				4.28
17.417	0.05	0.04	0.155	OI				4.28
17.500	0.05	0.04	0.155	OI				4.28
17.583	0.05	0.04	0.155	OI				4.28
17.667	0.05	0.04	0.155	OI				4.28
17.750	0.05	0.04	0.155	OI				4.28
17.833	0.05	0.04	0.155	OI				4.28
17.917	0.05	0.04	0.155	OI				4.28
18.000	0.04	0.04	0.155	O				4.28
18.083	0.04	0.04	0.155	O				4.28
18.167	0.04	0.04	0.155	O				4.28
18.250	0.04	0.04	0.155	O				4.28
18.333	0.04	0.04	0.155	O				4.28
18.417	0.04	0.04	0.155	O				4.28
18.500	0.04	0.04	0.155	O				4.28
18.583	0.04	0.04	0.155	O				4.28
18.667	0.04	0.04	0.155	O				4.28
18.750	0.03	0.04	0.155	O				4.28
18.833	0.03	0.04	0.155	IO				4.28
18.917	0.03	0.04	0.155	IO				4.27
19.000	0.02	0.04	0.155	IO				4.27

19.083	0.02	0.04	0.155	IO				4.27
19.167	0.03	0.04	0.155	IO				4.26
19.250	0.03	0.04	0.154	IO				4.26
19.333	0.03	0.04	0.154	IO				4.26
19.417	0.04	0.04	0.154	O				4.26
19.500	0.04	0.04	0.154	O				4.26
19.583	0.04	0.04	0.154	O				4.26
19.667	0.04	0.04	0.154	O				4.25
19.750	0.03	0.04	0.154	IO				4.25
19.833	0.03	0.04	0.154	IO				4.25
19.917	0.03	0.04	0.154	IO				4.25
20.000	0.02	0.04	0.154	IO				4.24
20.083	0.02	0.04	0.154	IO				4.24
20.167	0.03	0.04	0.153	IO				4.24
20.250	0.03	0.04	0.153	IO				4.23
20.333	0.03	0.04	0.153	IO				4.23
20.417	0.03	0.04	0.153	IO				4.23
20.500	0.03	0.04	0.153	IO				4.23
20.583	0.03	0.04	0.153	IO				4.23
20.667	0.03	0.04	0.153	IO				4.22
20.750	0.03	0.04	0.153	IO				4.22
20.833	0.03	0.04	0.153	IO				4.22
20.917	0.03	0.04	0.153	IO				4.22
21.000	0.02	0.04	0.152	IO				4.21
21.083	0.02	0.04	0.152	IO				4.21
21.167	0.03	0.04	0.152	IO				4.21
21.250	0.03	0.04	0.152	IO				4.20
21.333	0.03	0.04	0.152	IO				4.20
21.417	0.02	0.04	0.152	IO				4.20
21.500	0.02	0.04	0.152	IO				4.19
21.583	0.02	0.04	0.152	IO				4.19
21.667	0.03	0.04	0.151	IO				4.19
21.750	0.03	0.04	0.151	IO				4.18
21.833	0.03	0.04	0.151	IO				4.18
21.917	0.02	0.04	0.151	IO				4.18
22.000	0.02	0.04	0.151	IO				4.17
22.083	0.02	0.04	0.151	IO				4.17
22.167	0.03	0.04	0.151	IO				4.17
22.250	0.03	0.04	0.151	IO				4.16
22.333	0.03	0.04	0.150	IO				4.16
22.417	0.02	0.04	0.150	IO				4.16
22.500	0.02	0.04	0.150	IO				4.16
22.583	0.02	0.04	0.150	I O				4.15
22.667	0.02	0.04	0.150	I O				4.15
22.750	0.02	0.04	0.150	I O				4.14
22.833	0.02	0.04	0.150	I O				4.14
22.917	0.02	0.04	0.149	I O				4.14
23.000	0.02	0.04	0.149	I O				4.13
23.083	0.02	0.04	0.149	I O				4.13
23.167	0.02	0.04	0.149	I O				4.12

23.250	0.02	0.04	0.149	|I O	|	|	|	4.12
23.333	0.02	0.04	0.149	|I O	|	|	|	4.12
23.417	0.02	0.04	0.148	|I O	|	|	|	4.11
23.500	0.02	0.04	0.148	|I O	|	|	|	4.11
23.583	0.02	0.04	0.148	|I O	|	|	|	4.10
23.667	0.02	0.04	0.148	|I O	|	|	|	4.10
23.750	0.02	0.04	0.148	|I O	|	|	|	4.10
23.833	0.02	0.04	0.148	|I O	|	|	|	4.09
23.917	0.02	0.04	0.147	|I O	|	|	|	4.09
24.000	0.02	0.04	0.147	|I O	|	|	|	4.08
24.083	0.02	0.04	0.147	|I O	|	|	|	4.08
24.167	0.01	0.04	0.147	I O	|	|	|	4.07
24.250	0.00	0.04	0.147	I O	|	|	|	4.07
24.333	0.00	0.04	0.146	I O	|	|	|	4.06
24.417	0.00	0.04	0.146	I O	|	|	|	4.05
24.500	0.00	0.04	0.146	I O	|	|	|	4.04
24.583	0.00	0.04	0.145	I O	|	|	|	4.04
24.667	0.00	0.04	0.145	I O	|	|	|	4.03
24.750	0.00	0.04	0.145	I O	|	|	|	4.02
24.833	0.00	0.04	0.145	I O	|	|	|	4.01
24.917	0.00	0.04	0.144	I O	|	|	|	4.01
25.000	0.00	0.04	0.144	I O	|	|	|	4.00
25.083	0.00	0.04	0.144	I O	|	|	|	3.99
25.167	0.00	0.04	0.143	I O	|	|	|	3.98
25.250	0.00	0.04	0.143	I O	|	|	|	3.97
25.333	0.00	0.04	0.143	I O	|	|	|	3.97
25.417	0.00	0.04	0.142	I O	|	|	|	3.96
25.500	0.00	0.04	0.142	I O	|	|	|	3.95
25.583	0.00	0.04	0.142	I O	|	|	|	3.94
25.667	0.00	0.04	0.141	I O	|	|	|	3.94
25.750	0.00	0.04	0.141	I O	|	|	|	3.93
25.833	0.00	0.04	0.141	I O	|	|	|	3.92
25.917	0.00	0.04	0.140	I O	|	|	|	3.91
26.000	0.00	0.04	0.140	I O	|	|	|	3.90
26.083	0.00	0.04	0.140	I O	|	|	|	3.90
26.167	0.00	0.04	0.140	I O	|	|	|	3.89
26.250	0.00	0.04	0.139	I O	|	|	|	3.88
26.333	0.00	0.04	0.139	I O	|	|	|	3.87
26.417	0.00	0.04	0.139	I O	|	|	|	3.87
26.500	0.00	0.04	0.138	I O	|	|	|	3.86
26.583	0.00	0.04	0.138	I O	|	|	|	3.85
26.667	0.00	0.04	0.138	I O	|	|	|	3.84
26.750	0.00	0.04	0.137	I O	|	|	|	3.83
26.833	0.00	0.04	0.137	I O	|	|	|	3.83
26.917	0.00	0.04	0.137	I O	|	|	|	3.82
27.000	0.00	0.04	0.136	I O	|	|	|	3.81
27.083	0.00	0.04	0.136	I O	|	|	|	3.80
27.167	0.00	0.04	0.136	I O	|	|	|	3.80
27.250	0.00	0.04	0.136	I O	|	|	|	3.79
27.333	0.00	0.04	0.135	I O	|	|	|	3.78

27.417	0.00	0.04	0.135	I	O					3.77
27.500	0.00	0.04	0.135	I	O					3.77
27.583	0.00	0.04	0.134	I	O					3.76
27.667	0.00	0.04	0.134	I	O					3.75
27.750	0.00	0.04	0.134	I	O					3.74
27.833	0.00	0.04	0.133	I	O					3.73
27.917	0.00	0.04	0.133	I	O					3.73
28.000	0.00	0.04	0.133	I	O					3.72
28.083	0.00	0.04	0.132	I	O					3.71
28.167	0.00	0.04	0.132	I	O					3.70
28.250	0.00	0.04	0.132	I	O					3.70
28.333	0.00	0.04	0.132	I	O					3.69
28.417	0.00	0.04	0.131	I	O					3.68
28.500	0.00	0.04	0.131	I	O					3.67
28.583	0.00	0.04	0.131	I	O					3.66
28.667	0.00	0.04	0.130	I	O					3.66
28.750	0.00	0.04	0.130	I	O					3.65
28.833	0.00	0.04	0.130	I	O					3.64
28.917	0.00	0.04	0.129	I	O					3.63
29.000	0.00	0.04	0.129	I	O					3.63
29.083	0.00	0.04	0.129	I	O					3.62
29.167	0.00	0.04	0.128	I	O					3.61
29.250	0.00	0.04	0.128	I	O					3.60
29.333	0.00	0.04	0.128	I	O					3.59
29.417	0.00	0.04	0.127	I	O					3.59
29.500	0.00	0.04	0.127	I	O					3.58
29.583	0.00	0.04	0.127	I	O					3.57
29.667	0.00	0.04	0.127	I	O					3.56
29.750	0.00	0.04	0.126	I	O					3.56
29.833	0.00	0.04	0.126	I	O					3.55
29.917	0.00	0.04	0.126	I	O					3.54
30.000	0.00	0.04	0.125	I	O					3.53
30.083	0.00	0.04	0.125	I	O					3.52
30.167	0.00	0.04	0.125	I	O					3.52
30.250	0.00	0.04	0.124	I	O					3.51
30.333	0.00	0.04	0.124	I	O					3.50
30.417	0.00	0.04	0.124	I	O					3.49
30.500	0.00	0.04	0.123	I	O					3.49
30.583	0.00	0.04	0.123	I	O					3.48
30.667	0.00	0.04	0.123	I	O					3.47
30.750	0.00	0.04	0.123	I	O					3.46
30.833	0.00	0.04	0.122	I	O					3.46
30.917	0.00	0.04	0.122	I	O					3.45
31.000	0.00	0.04	0.122	I	O					3.44
31.083	0.00	0.04	0.121	I	O					3.43
31.167	0.00	0.04	0.121	I	O					3.42
31.250	0.00	0.04	0.121	I	O					3.42
31.333	0.00	0.04	0.120	I	O					3.41
31.417	0.00	0.04	0.120	I	O					3.40
31.500	0.00	0.04	0.120	I	O					3.39

31.583	0.00	0.04	0.119	I	O					3.39
31.667	0.00	0.04	0.119	I	O					3.38
31.750	0.00	0.04	0.119	I	O					3.37
31.833	0.00	0.04	0.118	I	O					3.36
31.917	0.00	0.04	0.118	I	O					3.35
32.000	0.00	0.04	0.118	I	O					3.35
32.083	0.00	0.04	0.118	I	O					3.34
32.167	0.00	0.04	0.117	I	O					3.33
32.250	0.00	0.04	0.117	I	O					3.32
32.333	0.00	0.04	0.117	I	O					3.32
32.417	0.00	0.04	0.116	I	O					3.31
32.500	0.00	0.04	0.116	I	O					3.30
32.583	0.00	0.04	0.116	I	O					3.29
32.667	0.00	0.04	0.115	I	O					3.28
32.750	0.00	0.04	0.115	I	O					3.28
32.833	0.00	0.04	0.115	I	O					3.27
32.917	0.00	0.04	0.114	I	O					3.26
33.000	0.00	0.04	0.114	I	O					3.25
33.083	0.00	0.04	0.114	I	O					3.25
33.167	0.00	0.04	0.114	I	O					3.24
33.250	0.00	0.04	0.113	I	O					3.23
33.333	0.00	0.04	0.113	I	O					3.22
33.417	0.00	0.04	0.113	I	O					3.22
33.500	0.00	0.04	0.112	I	O					3.21
33.583	0.00	0.04	0.112	I	O					3.20
33.667	0.00	0.04	0.112	I	O					3.19
33.750	0.00	0.04	0.111	I	O					3.18
33.833	0.00	0.04	0.111	I	O					3.18
33.917	0.00	0.04	0.111	I	O					3.17
34.000	0.00	0.04	0.110	I	O					3.16
34.083	0.00	0.04	0.110	I	O					3.15
34.167	0.00	0.04	0.110	I	O					3.15
34.250	0.00	0.04	0.110	I	O					3.14
34.333	0.00	0.04	0.109	I	O					3.13
34.417	0.00	0.04	0.109	I	O					3.12
34.500	0.00	0.04	0.109	I	O					3.11
34.583	0.00	0.04	0.108	I	O					3.11
34.667	0.00	0.04	0.108	I	O					3.10
34.750	0.00	0.04	0.108	I	O					3.09
34.833	0.00	0.04	0.107	I	O					3.08
34.917	0.00	0.04	0.107	I	O					3.08
35.000	0.00	0.04	0.107	I	O					3.07
35.083	0.00	0.04	0.106	I	O					3.06
35.167	0.00	0.04	0.106	I	O					3.05
35.250	0.00	0.04	0.106	I	O					3.04
35.333	0.00	0.04	0.105	I	O					3.04
35.417	0.00	0.04	0.105	I	O					3.03
35.500	0.00	0.04	0.105	I	O					3.02
35.583	0.00	0.04	0.105	I	O					3.01
35.667	0.00	0.04	0.104	I	O					3.01

35.750	0.00	0.04	0.104	I	O					3.00
35.833	0.00	0.04	0.104	I	O					2.99
35.917	0.00	0.04	0.103	I	O					2.98
36.000	0.00	0.04	0.103	I	O					2.97
36.083	0.00	0.04	0.103	I	O					2.97
36.167	0.00	0.04	0.102	I	O					2.96
36.250	0.00	0.04	0.102	I	O					2.95
36.333	0.00	0.04	0.102	I	O					2.94
36.417	0.00	0.04	0.101	I	O					2.94
36.500	0.00	0.04	0.101	I	O					2.93
36.583	0.00	0.04	0.101	I	O					2.92
36.667	0.00	0.04	0.101	I	O					2.91
36.750	0.00	0.04	0.100	I	O					2.91
36.833	0.00	0.04	0.100	I	O					2.90
36.917	0.00	0.04	0.100	I	O					2.89
37.000	0.00	0.04	0.099	I	O					2.88
37.083	0.00	0.04	0.099	I	O					2.87
37.167	0.00	0.04	0.099	I	O					2.87
37.250	0.00	0.04	0.098	I	O					2.86
37.333	0.00	0.04	0.098	I	O					2.85
37.417	0.00	0.04	0.098	I	O					2.84
37.500	0.00	0.04	0.097	I	O					2.84
37.583	0.00	0.04	0.097	I	O					2.83
37.667	0.00	0.04	0.097	I	O					2.82
37.750	0.00	0.04	0.096	I	O					2.81
37.833	0.00	0.04	0.096	I	O					2.80
37.917	0.00	0.04	0.096	I	O					2.80
38.000	0.00	0.04	0.096	I	O					2.79
38.083	0.00	0.04	0.095	I	O					2.78
38.167	0.00	0.04	0.095	I	O					2.77
38.250	0.00	0.04	0.095	I	O					2.77
38.333	0.00	0.04	0.094	I	O					2.76
38.417	0.00	0.04	0.094	I	O					2.75
38.500	0.00	0.04	0.094	I	O					2.74
38.583	0.00	0.04	0.093	I	O					2.73
38.667	0.00	0.04	0.093	I	O					2.73
38.750	0.00	0.04	0.093	I	O					2.72
38.833	0.00	0.04	0.092	I	O					2.71
38.917	0.00	0.04	0.092	I	O					2.70
39.000	0.00	0.04	0.092	I	O					2.70
39.083	0.00	0.04	0.092	I	O					2.69
39.167	0.00	0.04	0.091	I	O					2.68
39.250	0.00	0.04	0.091	I	O					2.67
39.333	0.00	0.04	0.091	I	O					2.66
39.417	0.00	0.04	0.090	I	O					2.66
39.500	0.00	0.04	0.090	I	O					2.65
39.583	0.00	0.04	0.090	I	O					2.64
39.667	0.00	0.04	0.089	I	O					2.63
39.750	0.00	0.04	0.089	I	O					2.63
39.833	0.00	0.04	0.089	I	O					2.62

39.917	0.00	0.04	0.088	I	O					2.61
40.000	0.00	0.04	0.088	I	O					2.60
40.083	0.00	0.04	0.088	I	O					2.60
40.167	0.00	0.04	0.087	I	O					2.59
40.250	0.00	0.04	0.087	I	O					2.58
40.333	0.00	0.04	0.087	I	O					2.57
40.417	0.00	0.04	0.087	I	O					2.56
40.500	0.00	0.04	0.086	I	O					2.56
40.583	0.00	0.04	0.086	I	O					2.55
40.667	0.00	0.04	0.086	I	O					2.54
40.750	0.00	0.04	0.085	I	O					2.53
40.833	0.00	0.04	0.085	I	O					2.53
40.917	0.00	0.04	0.085	I	O					2.52
41.000	0.00	0.04	0.084	I	O					2.51
41.083	0.00	0.04	0.084	I	O					2.50
41.167	0.00	0.04	0.084	I	O					2.49
41.250	0.00	0.04	0.083	I	O					2.49
41.333	0.00	0.04	0.083	I	O					2.48
41.417	0.00	0.04	0.083	I	O					2.47
41.500	0.00	0.04	0.083	I	O					2.46
41.583	0.00	0.04	0.082	I	O					2.46
41.667	0.00	0.04	0.082	I	O					2.45
41.750	0.00	0.04	0.082	I	O					2.44
41.833	0.00	0.04	0.081	I	O					2.43
41.917	0.00	0.04	0.081	I	O					2.42
42.000	0.00	0.04	0.081	I	O					2.42
42.083	0.00	0.04	0.080	I	O					2.41
42.167	0.00	0.04	0.080	I	O					2.40
42.250	0.00	0.04	0.080	I	O					2.39
42.333	0.00	0.04	0.079	I	O					2.39
42.417	0.00	0.04	0.079	I	O					2.38
42.500	0.00	0.04	0.079	I	O					2.37
42.583	0.00	0.04	0.079	I	O					2.36
42.667	0.00	0.04	0.078	I	O					2.36
42.750	0.00	0.04	0.078	I	O					2.35
42.833	0.00	0.04	0.078	I	O					2.34
42.917	0.00	0.04	0.077	I	O					2.33
43.000	0.00	0.04	0.077	I	O					2.32
43.083	0.00	0.04	0.077	I	O					2.32
43.167	0.00	0.04	0.076	I	O					2.31
43.250	0.00	0.04	0.076	I	O					2.30
43.333	0.00	0.04	0.076	I	O					2.29
43.417	0.00	0.04	0.075	I	O					2.29
43.500	0.00	0.04	0.075	I	O					2.28
43.583	0.00	0.04	0.075	I	O					2.27
43.667	0.00	0.04	0.074	I	O					2.26
43.750	0.00	0.04	0.074	I	O					2.25
43.833	0.00	0.04	0.074	I	O					2.25
43.917	0.00	0.04	0.074	I	O					2.24
44.000	0.00	0.04	0.073	I	O					2.23

44.083	0.00	0.04	0.073	I	O	|	|	|	|	2.22
44.167	0.00	0.04	0.073	I	O	|	|	|	|	2.22
44.250	0.00	0.04	0.072	I	O	|	|	|	|	2.21
44.333	0.00	0.04	0.072	I	O	|	|	|	|	2.20
44.417	0.00	0.04	0.072	I	O	|	|	|	|	2.19
44.500	0.00	0.04	0.071	I	O	|	|	|	|	2.18
44.583	0.00	0.04	0.071	I	O	|	|	|	|	2.18
44.667	0.00	0.04	0.071	I	O	|	|	|	|	2.17
44.750	0.00	0.04	0.070	I	O	|	|	|	|	2.16
44.833	0.00	0.04	0.070	I	O	|	|	|	|	2.15
44.917	0.00	0.04	0.070	I	O	|	|	|	|	2.15
45.000	0.00	0.04	0.070	I	O	|	|	|	|	2.14
45.083	0.00	0.04	0.069	I	O	|	|	|	|	2.13
45.167	0.00	0.04	0.069	I	O	|	|	|	|	2.12
45.250	0.00	0.04	0.069	I	O	|	|	|	|	2.11
45.333	0.00	0.04	0.068	I	O	|	|	|	|	2.11
45.417	0.00	0.04	0.068	I	O	|	|	|	|	2.10
45.500	0.00	0.04	0.068	I	O	|	|	|	|	2.09
45.583	0.00	0.04	0.067	I	O	|	|	|	|	2.08
45.667	0.00	0.04	0.067	I	O	|	|	|	|	2.08
45.750	0.00	0.04	0.067	I	O	|	|	|	|	2.07
45.833	0.00	0.04	0.066	I	O	|	|	|	|	2.06
45.917	0.00	0.04	0.066	I	O	|	|	|	|	2.05
46.000	0.00	0.04	0.066	I	O	|	|	|	|	2.05
46.083	0.00	0.04	0.065	I	O	|	|	|	|	2.04
46.167	0.00	0.04	0.065	I	O	|	|	|	|	2.03
46.250	0.00	0.04	0.065	I	O	|	|	|	|	2.02
46.333	0.00	0.04	0.065	I	O	|	|	|	|	2.01
46.417	0.00	0.04	0.064	I	O	|	|	|	|	2.01
46.500	0.00	0.04	0.064	I	O	|	|	|	|	2.00
46.583	0.00	0.04	0.064	I	O	|	|	|	|	1.99
46.667	0.00	0.04	0.063	I	O	|	|	|	|	1.98
46.750	0.00	0.04	0.063	I	O	|	|	|	|	1.98
46.833	0.00	0.04	0.063	I	O	|	|	|	|	1.97
46.917	0.00	0.04	0.062	I	O	|	|	|	|	1.96
47.000	0.00	0.04	0.062	I	O	|	|	|	|	1.95
47.083	0.00	0.04	0.062	I	O	|	|	|	|	1.94
47.167	0.00	0.04	0.061	I	O	|	|	|	|	1.94
47.250	0.00	0.04	0.061	I	O	|	|	|	|	1.93
47.333	0.00	0.04	0.061	I	O	|	|	|	|	1.92
47.417	0.00	0.04	0.061	I	O	|	|	|	|	1.91
47.500	0.00	0.04	0.060	I	O	|	|	|	|	1.91
47.583	0.00	0.04	0.060	I	O	|	|	|	|	1.90
47.667	0.00	0.04	0.060	I	O	|	|	|	|	1.89
47.750	0.00	0.04	0.059	I	O	|	|	|	|	1.88
47.833	0.00	0.04	0.059	I	O	|	|	|	|	1.87
47.917	0.00	0.04	0.059	I	O	|	|	|	|	1.87
48.000	0.00	0.04	0.058	I	O	|	|	|	|	1.86
48.083	0.00	0.04	0.058	I	O	|	|	|	|	1.85
48.167	0.00	0.04	0.058	I	O	|	|	|	|	1.84

48.250	0.00	0.04	0.057	I	O	|	|	|	|	1.84
48.333	0.00	0.04	0.057	I	O	|	|	|	|	1.83
48.417	0.00	0.04	0.057	I	O	|	|	|	|	1.82
48.500	0.00	0.04	0.057	I	O	|	|	|	|	1.81
48.583	0.00	0.04	0.056	I	O	|	|	|	|	1.80
48.667	0.00	0.04	0.056	I	O	|	|	|	|	1.80
48.750	0.00	0.04	0.056	I	O	|	|	|	|	1.79
48.833	0.00	0.04	0.055	I	O	|	|	|	|	1.78
48.917	0.00	0.04	0.055	I	O	|	|	|	|	1.77
49.000	0.00	0.04	0.055	I	O	|	|	|	|	1.77
49.083	0.00	0.04	0.054	I	O	|	|	|	|	1.76
49.167	0.00	0.04	0.054	I	O	|	|	|	|	1.75
49.250	0.00	0.04	0.054	I	O	|	|	|	|	1.74
49.333	0.00	0.04	0.053	I	O	|	|	|	|	1.74
49.417	0.00	0.04	0.053	I	O	|	|	|	|	1.73
49.500	0.00	0.04	0.053	I	O	|	|	|	|	1.72
49.583	0.00	0.04	0.052	I	O	|	|	|	|	1.71
49.667	0.00	0.04	0.052	I	O	|	|	|	|	1.70
49.750	0.00	0.04	0.052	I	O	|	|	|	|	1.70
49.833	0.00	0.04	0.052	I	O	|	|	|	|	1.69
49.917	0.00	0.04	0.051	I	O	|	|	|	|	1.68
50.000	0.00	0.04	0.051	I	O	|	|	|	|	1.67
50.083	0.00	0.04	0.051	I	O	|	|	|	|	1.67
50.167	0.00	0.04	0.050	I	O	|	|	|	|	1.66
50.250	0.00	0.04	0.050	I	O	|	|	|	|	1.65
50.333	0.00	0.04	0.050	I	O	|	|	|	|	1.64
50.417	0.00	0.04	0.049	I	O	|	|	|	|	1.63
50.500	0.00	0.04	0.049	I	O	|	|	|	|	1.63
50.583	0.00	0.04	0.049	I	O	|	|	|	|	1.62
50.667	0.00	0.04	0.048	I	O	|	|	|	|	1.61
50.750	0.00	0.04	0.048	I	O	|	|	|	|	1.60
50.833	0.00	0.04	0.048	I	O	|	|	|	|	1.60
50.917	0.00	0.04	0.048	I	O	|	|	|	|	1.59
51.000	0.00	0.04	0.047	I	O	|	|	|	|	1.58
51.083	0.00	0.04	0.047	I	O	|	|	|	|	1.57
51.167	0.00	0.04	0.047	I	O	|	|	|	|	1.56
51.250	0.00	0.04	0.046	I	O	|	|	|	|	1.56
51.333	0.00	0.04	0.046	I	O	|	|	|	|	1.55
51.417	0.00	0.04	0.046	I	O	|	|	|	|	1.54
51.500	0.00	0.04	0.045	I	O	|	|	|	|	1.53
51.583	0.00	0.04	0.045	I	O	|	|	|	|	1.53
51.667	0.00	0.04	0.045	I	O	|	|	|	|	1.52
51.750	0.00	0.04	0.044	I	O	|	|	|	|	1.51
51.833	0.00	0.04	0.044	I	O	|	|	|	|	1.50
51.917	0.00	0.04	0.044	I	O	|	|	|	|	1.50
52.000	0.00	0.04	0.043	I	O	|	|	|	|	1.49
52.083	0.00	0.04	0.043	I	O	|	|	|	|	1.48
52.167	0.00	0.04	0.043	I	O	|	|	|	|	1.47
52.250	0.00	0.04	0.043	I	O	|	|	|	|	1.46
52.333	0.00	0.04	0.042	I	O	|	|	|	|	1.46

52.417	0.00	0.04	0.042	I	O	|	|	|	|	1.45
52.500	0.00	0.04	0.042	I	O	|	|	|	|	1.44
52.583	0.00	0.04	0.041	I	O	|	|	|	|	1.43
52.667	0.00	0.04	0.041	I	O	|	|	|	|	1.43
52.750	0.00	0.04	0.041	I	O	|	|	|	|	1.42
52.833	0.00	0.04	0.040	I	O	|	|	|	|	1.41
52.917	0.00	0.04	0.040	I	O	|	|	|	|	1.40
53.000	0.00	0.04	0.040	I	O	|	|	|	|	1.39
53.083	0.00	0.04	0.039	I	O	|	|	|	|	1.39
53.167	0.00	0.04	0.039	I	O	|	|	|	|	1.38
53.250	0.00	0.04	0.039	I	O	|	|	|	|	1.37
53.333	0.00	0.04	0.039	I	O	|	|	|	|	1.36
53.417	0.00	0.04	0.038	I	O	|	|	|	|	1.36
53.500	0.00	0.04	0.038	I	O	|	|	|	|	1.35
53.583	0.00	0.04	0.038	I	O	|	|	|	|	1.34
53.667	0.00	0.04	0.037	I	O	|	|	|	|	1.33
53.750	0.00	0.04	0.037	I	O	|	|	|	|	1.32
53.833	0.00	0.04	0.037	I	O	|	|	|	|	1.32
53.917	0.00	0.04	0.036	I	O	|	|	|	|	1.31
54.000	0.00	0.04	0.036	I	O	|	|	|	|	1.30
54.083	0.00	0.04	0.036	I	O	|	|	|	|	1.29
54.167	0.00	0.04	0.035	I	O	|	|	|	|	1.29
54.250	0.00	0.04	0.035	I	O	|	|	|	|	1.28
54.333	0.00	0.04	0.035	I	O	|	|	|	|	1.27
54.417	0.00	0.04	0.035	I	O	|	|	|	|	1.26
54.500	0.00	0.04	0.034	I	O	|	|	|	|	1.25
54.583	0.00	0.04	0.034	I	O	|	|	|	|	1.25
54.667	0.00	0.04	0.034	I	O	|	|	|	|	1.24
54.750	0.00	0.04	0.033	I	O	|	|	|	|	1.23
54.833	0.00	0.04	0.033	I	O	|	|	|	|	1.22
54.917	0.00	0.04	0.033	I	O	|	|	|	|	1.22
55.000	0.00	0.04	0.032	I	O	|	|	|	|	1.21
55.083	0.00	0.04	0.032	I	O	|	|	|	|	1.20
55.167	0.00	0.04	0.032	I	O	|	|	|	|	1.19
55.250	0.00	0.04	0.031	I	O	|	|	|	|	1.19
55.333	0.00	0.04	0.031	I	O	|	|	|	|	1.18
55.417	0.00	0.04	0.031	I	O	|	|	|	|	1.17
55.500	0.00	0.04	0.030	I	O	|	|	|	|	1.16
55.583	0.00	0.04	0.030	I	O	|	|	|	|	1.15
55.667	0.00	0.04	0.030	I	O	|	|	|	|	1.15
55.750	0.00	0.04	0.030	I	O	|	|	|	|	1.14
55.833	0.00	0.04	0.029	I	O	|	|	|	|	1.13
55.917	0.00	0.04	0.029	I	O	|	|	|	|	1.12
56.000	0.00	0.04	0.029	I	O	|	|	|	|	1.12
56.083	0.00	0.04	0.028	I	O	|	|	|	|	1.11
56.167	0.00	0.04	0.028	I	O	|	|	|	|	1.10
56.250	0.00	0.04	0.028	I	O	|	|	|	|	1.09
56.333	0.00	0.04	0.027	I	O	|	|	|	|	1.08
56.417	0.00	0.04	0.027	I	O	|	|	|	|	1.08
56.500	0.00	0.04	0.027	I	O	|	|	|	|	1.07

56.583	0.00	0.04	0.026	I	O				1.06
56.667	0.00	0.04	0.026	I	O				1.05
56.750	0.00	0.04	0.026	I	O				1.05
56.833	0.00	0.04	0.026	I	O				1.04
56.917	0.00	0.04	0.025	I	O				1.03
57.000	0.00	0.04	0.025	I	O				1.02
57.083	0.00	0.04	0.025	I	O				1.01
57.167	0.00	0.04	0.024	I	O				1.01
57.250	0.00	0.04	0.024	I	O				1.00
57.333	0.00	0.04	0.024	I	O				0.99
57.417	0.00	0.04	0.023	I	O				0.97
57.500	0.00	0.04	0.023	I	O				0.96
57.583	0.00	0.04	0.023	I	O				0.95
57.667	0.00	0.04	0.022	I	O				0.94
57.750	0.00	0.04	0.022	I	O				0.92
57.833	0.00	0.04	0.022	I	O				0.91
57.917	0.00	0.04	0.022	I	O				0.90
58.000	0.00	0.04	0.021	I	O				0.89
58.083	0.00	0.04	0.021	I	O				0.88
58.167	0.00	0.04	0.021	I	O				0.87
58.250	0.00	0.04	0.021	I	O				0.86
58.333	0.00	0.04	0.020	I	O				0.84
58.417	0.00	0.04	0.020	I	O				0.83
58.500	0.00	0.04	0.020	I	O				0.82
58.583	0.00	0.04	0.019	I	O				0.81
58.667	0.00	0.04	0.019	I	O				0.80
58.750	0.00	0.04	0.019	I	O				0.79
58.833	0.00	0.04	0.019	I	O				0.78
58.917	0.00	0.03	0.019	I	O				0.77
59.000	0.00	0.03	0.018	I	O				0.76
59.083	0.00	0.03	0.018	I	O				0.75
59.167	0.00	0.03	0.018	I	O				0.74
59.250	0.00	0.03	0.018	I	O				0.73
59.333	0.00	0.03	0.017	I	O				0.72
59.417	0.00	0.03	0.017	I	O				0.71
59.500	0.00	0.03	0.017	I	O				0.70
59.583	0.00	0.03	0.017	I	O				0.70
59.667	0.00	0.03	0.016	I	O				0.69
59.750	0.00	0.03	0.016	I	O				0.68
59.833	0.00	0.03	0.016	I	O				0.67
59.917	0.00	0.03	0.016	I	O				0.66
60.000	0.00	0.03	0.016	I	O				0.65
60.083	0.00	0.03	0.015	I	O				0.64
60.167	0.00	0.03	0.015	I	O				0.64
60.250	0.00	0.03	0.015	I	O				0.63
60.333	0.00	0.03	0.015	I	O				0.62
60.417	0.00	0.03	0.015	I	O				0.61
60.500	0.00	0.03	0.014	I	O				0.60
60.583	0.00	0.03	0.014	I	O				0.60
60.667	0.00	0.03	0.014	I	O				0.59

60.750	0.00	0.03	0.014	I O				0.58
60.833	0.00	0.03	0.014	I O				0.57
60.917	0.00	0.03	0.014	I O				0.57
61.000	0.00	0.03	0.013	I O				0.56
61.083	0.00	0.02	0.013	I O				0.55
61.167	0.00	0.02	0.013	I O				0.54
61.250	0.00	0.02	0.013	I O				0.54
61.333	0.00	0.02	0.013	I O				0.53
61.417	0.00	0.02	0.013	I O				0.52
61.500	0.00	0.02	0.012	I O				0.52
61.583	0.00	0.02	0.012	I O				0.51
61.667	0.00	0.02	0.012	I O				0.50
61.750	0.00	0.02	0.012	IO				0.50
61.833	0.00	0.02	0.012	IO				0.49
61.917	0.00	0.02	0.012	IO				0.48
62.000	0.00	0.02	0.011	IO				0.48
62.083	0.00	0.02	0.011	IO				0.47
62.167	0.00	0.02	0.011	IO				0.47
62.250	0.00	0.02	0.011	IO				0.46
62.333	0.00	0.02	0.011	IO				0.45
62.417	0.00	0.02	0.011	IO				0.45
62.500	0.00	0.02	0.011	IO				0.44
62.583	0.00	0.02	0.010	IO				0.44
62.667	0.00	0.02	0.010	IO				0.43
62.750	0.00	0.02	0.010	IO				0.43
62.833	0.00	0.02	0.010	IO				0.42
62.917	0.00	0.02	0.010	IO				0.41
63.000	0.00	0.02	0.010	IO				0.41
63.083	0.00	0.02	0.010	IO				0.40
63.167	0.00	0.02	0.010	IO				0.40
63.250	0.00	0.02	0.009	IO				0.39
63.333	0.00	0.02	0.009	IO				0.39
63.417	0.00	0.02	0.009	IO				0.38
63.500	0.00	0.02	0.009	IO				0.38
63.583	0.00	0.02	0.009	IO				0.37
63.667	0.00	0.02	0.009	IO				0.37
63.750	0.00	0.02	0.009	IO				0.36
63.833	0.00	0.02	0.009	IO				0.36
63.917	0.00	0.02	0.009	IO				0.36
64.000	0.00	0.02	0.008	IO				0.35
64.083	0.00	0.02	0.008	IO				0.35
64.167	0.00	0.02	0.008	IO				0.34
64.250	0.00	0.02	0.008	IO				0.34
64.333	0.00	0.01	0.008	IO				0.33
64.417	0.00	0.01	0.008	IO				0.33
64.500	0.00	0.01	0.008	IO				0.32
64.583	0.00	0.01	0.008	IO				0.32
64.667	0.00	0.01	0.008	IO				0.32
64.750	0.00	0.01	0.007	IO				0.31
64.833	0.00	0.01	0.007	IO				0.31

64.917	0.00	0.01	0.007	IO				0.30
65.000	0.00	0.01	0.007	IO				0.30
65.083	0.00	0.01	0.007	IO				0.30
65.167	0.00	0.01	0.007	IO				0.29
65.250	0.00	0.01	0.007	IO				0.29
65.333	0.00	0.01	0.007	IO				0.29
65.417	0.00	0.01	0.007	IO				0.28
65.500	0.00	0.01	0.007	IO				0.28
65.583	0.00	0.01	0.007	IO				0.27
65.667	0.00	0.01	0.007	IO				0.27
65.750	0.00	0.01	0.006	IO				0.27
65.833	0.00	0.01	0.006	IO				0.26
65.917	0.00	0.01	0.006	IO				0.26
66.000	0.00	0.01	0.006	IO				0.26
66.083	0.00	0.01	0.006	IO				0.25
66.167	0.00	0.01	0.006	O				0.25
66.250	0.00	0.01	0.006	O				0.25
66.333	0.00	0.01	0.006	O				0.24
66.417	0.00	0.01	0.006	O				0.24
66.500	0.00	0.01	0.006	O				0.24
66.583	0.00	0.01	0.006	O				0.24
66.667	0.00	0.01	0.006	O				0.23
66.750	0.00	0.01	0.005	O				0.23
66.833	0.00	0.01	0.005	O				0.23
66.917	0.00	0.01	0.005	O				0.22
67.000	0.00	0.01	0.005	O				0.22
67.083	0.00	0.01	0.005	O				0.22
67.167	0.00	0.01	0.005	O				0.21
67.250	0.00	0.01	0.005	O				0.21
67.333	0.00	0.01	0.005	O				0.21
67.417	0.00	0.01	0.005	O				0.21
67.500	0.00	0.01	0.005	O				0.20
67.583	0.00	0.01	0.005	O				0.20
67.667	0.00	0.01	0.005	O				0.20
67.750	0.00	0.01	0.005	O				0.20
67.833	0.00	0.01	0.005	O				0.19
67.917	0.00	0.01	0.005	O				0.19
68.000	0.00	0.01	0.005	O				0.19
68.083	0.00	0.01	0.004	O				0.19
68.167	0.00	0.01	0.004	O				0.18
68.250	0.00	0.01	0.004	O				0.18
68.333	0.00	0.01	0.004	O				0.18
68.417	0.00	0.01	0.004	O				0.18
68.500	0.00	0.01	0.004	O				0.17
68.583	0.00	0.01	0.004	O				0.17
68.667	0.00	0.01	0.004	O				0.17
68.750	0.00	0.01	0.004	O				0.17
68.833	0.00	0.01	0.004	O				0.17
68.917	0.00	0.01	0.004	O				0.16
69.000	0.00	0.01	0.004	O				0.16

69.083	0.00	0.01	0.004	O	|	|	|	0.16
69.167	0.00	0.01	0.004	O	|	|	|	0.16
69.250	0.00	0.01	0.004	O	|	|	|	0.16
69.333	0.00	0.01	0.004	O	|	|	|	0.15
69.417	0.00	0.01	0.004	O	|	|	|	0.15
69.500	0.00	0.01	0.004	O	|	|	|	0.15
69.583	0.00	0.01	0.004	O	|	|	|	0.15
69.667	0.00	0.01	0.003	O	|	|	|	0.15
69.750	0.00	0.01	0.003	O	|	|	|	0.14
69.833	0.00	0.01	0.003	O	|	|	|	0.14
69.917	0.00	0.01	0.003	O	|	|	|	0.14
70.000	0.00	0.01	0.003	O	|	|	|	0.14
70.083	0.00	0.01	0.003	O	|	|	|	0.14
70.167	0.00	0.01	0.003	O	|	|	|	0.13
70.250	0.00	0.01	0.003	O	|	|	|	0.13
70.333	0.00	0.01	0.003	O	|	|	|	0.13
70.417	0.00	0.01	0.003	O	|	|	|	0.13
70.500	0.00	0.01	0.003	O	|	|	|	0.13
70.583	0.00	0.01	0.003	O	|	|	|	0.13
70.667	0.00	0.01	0.003	O	|	|	|	0.12
70.750	0.00	0.01	0.003	O	|	|	|	0.12
70.833	0.00	0.01	0.003	O	|	|	|	0.12
70.917	0.00	0.01	0.003	O	|	|	|	0.12
71.000	0.00	0.01	0.003	O	|	|	|	0.12
71.083	0.00	0.01	0.003	O	|	|	|	0.12
71.167	0.00	0.01	0.003	O	|	|	|	0.12
71.250	0.00	0.01	0.003	O	|	|	|	0.11
71.333	0.00	0.01	0.003	O	|	|	|	0.11
71.417	0.00	0.01	0.003	O	|	|	|	0.11
71.500	0.00	0.00	0.003	O	|	|	|	0.11
71.583	0.00	0.00	0.003	O	|	|	|	0.11
71.667	0.00	0.00	0.003	O	|	|	|	0.11
71.750	0.00	0.00	0.003	O	|	|	|	0.11
71.833	0.00	0.00	0.003	O	|	|	|	0.10
71.917	0.00	0.00	0.002	O	|	|	|	0.10
72.000	0.00	0.00	0.002	O	|	|	|	0.10
72.083	0.00	0.00	0.002	O	|	|	|	0.10
72.167	0.00	0.00	0.002	O	|	|	|	0.10
72.250	0.00	0.00	0.002	O	|	|	|	0.10
72.333	0.00	0.00	0.002	O	|	|	|	0.10
72.417	0.00	0.00	0.002	O	|	|	|	0.10
72.500	0.00	0.00	0.002	O	|	|	|	0.09
72.583	0.00	0.00	0.002	O	|	|	|	0.09
72.667	0.00	0.00	0.002	O	|	|	|	0.09
72.750	0.00	0.00	0.002	O	|	|	|	0.09
72.833	0.00	0.00	0.002	O	|	|	|	0.09
72.917	0.00	0.00	0.002	O	|	|	|	0.09
73.000	0.00	0.00	0.002	O	|	|	|	0.09
73.083	0.00	0.00	0.002	O	|	|	|	0.09
73.167	0.00	0.00	0.002	O	|	|	|	0.08

73.250	0.00	0.00	0.002	O				0.08
73.333	0.00	0.00	0.002	O				0.08
73.417	0.00	0.00	0.002	O				0.08
73.500	0.00	0.00	0.002	O				0.08
73.583	0.00	0.00	0.002	O				0.08
73.667	0.00	0.00	0.002	O				0.08
73.750	0.00	0.00	0.002	O				0.08
73.833	0.00	0.00	0.002	O				0.08
73.917	0.00	0.00	0.002	O				0.08
74.000	0.00	0.00	0.002	O				0.07
74.083	0.00	0.00	0.002	O				0.07
74.167	0.00	0.00	0.002	O				0.07
74.250	0.00	0.00	0.002	O				0.07
74.333	0.00	0.00	0.002	O				0.07
74.417	0.00	0.00	0.002	O				0.07
74.500	0.00	0.00	0.002	O				0.07
74.583	0.00	0.00	0.002	O				0.07
74.667	0.00	0.00	0.002	O				0.07
74.750	0.00	0.00	0.002	O				0.07
74.833	0.00	0.00	0.002	O				0.07
74.917	0.00	0.00	0.002	O				0.06
75.000	0.00	0.00	0.002	O				0.06
75.083	0.00	0.00	0.002	O				0.06
75.167	0.00	0.00	0.001	O				0.06
75.250	0.00	0.00	0.001	O				0.06
75.333	0.00	0.00	0.001	O				0.06
75.417	0.00	0.00	0.001	O				0.06
75.500	0.00	0.00	0.001	O				0.06
75.583	0.00	0.00	0.001	O				0.06
75.667	0.00	0.00	0.001	O				0.06
75.750	0.00	0.00	0.001	O				0.06
75.833	0.00	0.00	0.001	O				0.06
75.917	0.00	0.00	0.001	O				0.06
76.000	0.00	0.00	0.001	O				0.05
76.083	0.00	0.00	0.001	O				0.05
76.167	0.00	0.00	0.001	O				0.05
76.250	0.00	0.00	0.001	O				0.05
76.333	0.00	0.00	0.001	O				0.05
76.417	0.00	0.00	0.001	O				0.05
76.500	0.00	0.00	0.001	O				0.05
76.583	0.00	0.00	0.001	O				0.05
76.667	0.00	0.00	0.001	O				0.05
76.750	0.00	0.00	0.001	O				0.05
76.833	0.00	0.00	0.001	O				0.05
76.917	0.00	0.00	0.001	O				0.05
77.000	0.00	0.00	0.001	O				0.05
77.083	0.00	0.00	0.001	O				0.05
77.167	0.00	0.00	0.001	O				0.05
77.250	0.00	0.00	0.001	O				0.05
77.333	0.00	0.00	0.001	O				0.04

77.417	0.00	0.00	0.001	O	|	|	|	0.04
77.500	0.00	0.00	0.001	O	|	|	|	0.04
77.583	0.00	0.00	0.001	O	|	|	|	0.04
77.667	0.00	0.00	0.001	O	|	|	|	0.04
77.750	0.00	0.00	0.001	O	|	|	|	0.04
77.833	0.00	0.00	0.001	O	|	|	|	0.04
77.917	0.00	0.00	0.001	O	|	|	|	0.04
78.000	0.00	0.00	0.001	O	|	|	|	0.04
78.083	0.00	0.00	0.001	O	|	|	|	0.04
78.167	0.00	0.00	0.001	O	|	|	|	0.04
78.250	0.00	0.00	0.001	O	|	|	|	0.04
78.333	0.00	0.00	0.001	O	|	|	|	0.04
78.417	0.00	0.00	0.001	O	|	|	|	0.04
78.500	0.00	0.00	0.001	O	|	|	|	0.04
78.583	0.00	0.00	0.001	O	|	|	|	0.04
78.667	0.00	0.00	0.001	O	|	|	|	0.04
78.750	0.00	0.00	0.001	O	|	|	|	0.04
78.833	0.00	0.00	0.001	O	|	|	|	0.04
78.917	0.00	0.00	0.001	O	|	|	|	0.03
79.000	0.00	0.00	0.001	O	|	|	|	0.03
79.083	0.00	0.00	0.001	O	|	|	|	0.03
79.167	0.00	0.00	0.001	O	|	|	|	0.03
79.250	0.00	0.00	0.001	O	|	|	|	0.03
79.333	0.00	0.00	0.001	O	|	|	|	0.03
79.417	0.00	0.00	0.001	O	|	|	|	0.03
79.500	0.00	0.00	0.001	O	|	|	|	0.03
79.583	0.00	0.00	0.001	O	|	|	|	0.03
79.667	0.00	0.00	0.001	O	|	|	|	0.03
79.750	0.00	0.00	0.001	O	|	|	|	0.03
79.833	0.00	0.00	0.001	O	|	|	|	0.03
79.917	0.00	0.00	0.001	O	|	|	|	0.03
80.000	0.00	0.00	0.001	O	|	|	|	0.03
80.083	0.00	0.00	0.001	O	|	|	|	0.03
80.167	0.00	0.00	0.001	O	|	|	|	0.03
80.250	0.00	0.00	0.001	O	|	|	|	0.03
80.333	0.00	0.00	0.001	O	|	|	|	0.03
80.417	0.00	0.00	0.001	O	|	|	|	0.03
80.500	0.00	0.00	0.001	O	|	|	|	0.03
80.583	0.00	0.00	0.001	O	|	|	|	0.03
80.667	0.00	0.00	0.001	O	|	|	|	0.03
80.750	0.00	0.00	0.001	O	|	|	|	0.03
80.833	0.00	0.00	0.001	O	|	|	|	0.03
80.917	0.00	0.00	0.001	O	|	|	|	0.03
81.000	0.00	0.00	0.001	O	|	|	|	0.03
81.083	0.00	0.00	0.001	O	|	|	|	0.02
81.167	0.00	0.00	0.001	O	|	|	|	0.02
81.250	0.00	0.00	0.001	O	|	|	|	0.02
81.333	0.00	0.00	0.001	O	|	|	|	0.02
81.417	0.00	0.00	0.001	O	|	|	|	0.02
81.500	0.00	0.00	0.001	O	|	|	|	0.02

```
81.583    0.00    0.00      0.001  O       |       |       |       |     0.02
81.667    0.00    0.00      0.001  O       |       |       |       |     0.02
81.750    0.00    0.00      0.001  O       |       |       |       |     0.02
81.833    0.00    0.00      0.001  O       |       |       |       |     0.02

        ****************************HYDROGRAPH DATA****************************
                       Number of intervals =   982
                       Time interval =    5.0 (Min.)
                       Maximum/Peak flow rate =        0.045 (CFS)
                       Total volume =       0.221 (Ac.Ft)
                Status of hydrographs being held in storage
                           Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
                Peak (CFS)      0.000     0.000     0.000     0.000     0.000
                Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
        ***********************************************************************

        ---------------------------------------------------------------------
```

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
5 yr
24 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris242.rte
**********HYDROGRAPH DATA**********
Number of intervals = 296
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.362 (CFS)
Total volume = 0.221 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 296
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.1	0.18	0.27	0.36	Depth (Ft.)
0.083	0.00	0.00	0.000	O	|	|	|	|	0.00
0.167	0.01	0.00	0.000	OI	|	|	|	|	0.00
0.250	0.02	0.00	0.000	OI	|	|	|	|	0.01
0.333	0.02	0.00	0.000	OI	|	|	|	|	0.01
0.417	0.03	0.00	0.000	O I	|	|	|	|	0.02
0.500	0.03	0.00	0.001	O I	|	|	|	|	0.03
0.583	0.03	0.00	0.001	O I	|	|	|	|	0.04
0.667	0.03	0.00	0.001	O I	|	|	|	|	0.04
0.750	0.03	0.00	0.001	O I	|	|	|	|	0.05
0.833	0.03	0.00	0.001	O I	|	|	|	|	0.06
0.917	0.04	0.00	0.002	O I	|	|	|	|	0.07
1.000	0.04	0.00	0.002	O I	|	|	|	|	0.08
1.083	0.04	0.00	0.002	O I	|	|	|	|	0.09
1.167	0.04	0.00	0.002	O I	|	|	|	|	0.10
1.250	0.03	0.00	0.003	O I	|	|	|	|	0.11
1.333	0.03	0.01	0.003	O I	|	|	|	|	0.12
1.417	0.03	0.01	0.003	O I	|	|	|	|	0.13
1.500	0.03	0.01	0.003	O I	|	|	|	|	0.13
1.583	0.03	0.01	0.003	O I	|	|	|	|	0.14
1.667	0.03	0.01	0.004	O I	|	|	|	|	0.15
1.750	0.03	0.01	0.004	O I	|	|	|	|	0.16
1.833	0.03	0.01	0.004	O I	|	|	|	|	0.16
1.917	0.04	0.01	0.004	O I	|	|	|	|	0.17
2.000	0.04	0.01	0.004	O I	|	|	|	|	0.18
2.083	0.04	0.01	0.005	O I	|	|	|	|	0.19
2.167	0.04	0.01	0.005	O I	|	|	|	|	0.20
2.250	0.04	0.01	0.005	O I	|	|	|	|	0.21
2.333	0.04	0.01	0.005	O I	|	|	|	|	0.22

2.417	0.04	0.01	0.005	O I |	|	|	|	0.23
2.500	0.04	0.01	0.006	O I |	|	|	|	0.24
2.583	0.04	0.01	0.006	O I |	|	|	|	0.25
2.667	0.05	0.01	0.006	|O I |	|	|	|	0.26
2.750	0.05	0.01	0.006	|O I |	|	|	|	0.27
2.833	0.05	0.01	0.007	|O I |	|	|	|	0.28
2.917	0.05	0.01	0.007	|O I |	|	|	|	0.29
3.000	0.05	0.01	0.007	|O I |	|	|	|	0.30
3.083	0.05	0.01	0.008	|O I |	|	|	|	0.31
3.167	0.05	0.01	0.008	|O I |	|	|	|	0.32
3.250	0.05	0.02	0.008	|O I |	|	|	|	0.34
3.333	0.05	0.02	0.008	|O I |	|	|	|	0.35
3.417	0.05	0.02	0.009	|O I |	|	|	|	0.36
3.500	0.05	0.02	0.009	|O I |	|	|	|	0.37
3.583	0.05	0.02	0.009	|O I |	|	|	|	0.38
3.667	0.05	0.02	0.009	|O I |	|	|	|	0.39
3.750	0.05	0.02	0.010	|O I |	|	|	|	0.40
3.833	0.06	0.02	0.010	|O I |	|	|	|	0.41
3.917	0.06	0.02	0.010	|O I |	|	|	|	0.42
4.000	0.06	0.02	0.010	|O I |	|	|	|	0.43
4.083	0.06	0.02	0.011	|O I |	|	|	|	0.45
4.167	0.06	0.02	0.011	|O I |	|	|	|	0.46
4.250	0.06	0.02	0.011	|O I |	|	|	|	0.47
4.333	0.07	0.02	0.012	|O I |	|	|	|	0.48
4.417	0.07	0.02	0.012	|O I |	|	|	|	0.50
4.500	0.07	0.02	0.012	| O I |	|	|	|	0.51
4.583	0.07	0.02	0.013	| O I |	|	|	|	0.52
4.667	0.07	0.02	0.013	| O I |	|	|	|	0.54
4.750	0.07	0.02	0.013	| O I |	|	|	|	0.55
4.833	0.08	0.03	0.014	| O I |	|	|	|	0.57
4.917	0.08	0.03	0.014	| O I|	|	|	|	0.58
5.000	0.08	0.03	0.014	| O I|	|	|	|	0.60
5.083	0.08	0.03	0.015	| O I|	|	|	|	0.62
5.167	0.07	0.03	0.015	| O I |	|	|	|	0.63
5.250	0.07	0.03	0.015	| O I |	|	|	|	0.64
5.333	0.07	0.03	0.016	| O I |	|	|	|	0.65
5.417	0.07	0.03	0.016	| O I |	|	|	|	0.66
5.500	0.07	0.03	0.016	| O I |	|	|	|	0.68
5.583	0.08	0.03	0.017	| O I |	|	|	|	0.69
5.667	0.08	0.03	0.017	| O I|	|	|	|	0.70
5.750	0.08	0.03	0.017	| O I|	|	|	|	0.72
5.833	0.08	0.03	0.018	| O I|	|	|	|	0.73
5.917	0.08	0.03	0.018	| O I|	|	|	|	0.75
6.000	0.09	0.03	0.018	| O I|	|	|	|	0.76
6.083	0.09	0.03	0.019	| O I|	|	|	|	0.78
6.167	0.09	0.04	0.019	| O I	|	|	|	0.79
6.250	0.09	0.04	0.019	| O I	|	|	|	0.81
6.333	0.10	0.04	0.020	| O I	|	|	|	0.82
6.417	0.10	0.04	0.020	| O I	|	|	|	0.84
6.500	0.10	0.04	0.021	| O I	|	|	|	0.86

6.583	0.10	0.04	0.021	O	I			0.87
6.667	0.10	0.04	0.021	O	I			0.89
6.750	0.11	0.04	0.022	O	I			0.91
6.833	0.11	0.04	0.022	O	I			0.93
6.917	0.11	0.04	0.023	O	I			0.95
7.000	0.11	0.04	0.023	O	I			0.97
7.083	0.11	0.04	0.024	O	I			0.98
7.167	0.11	0.04	0.024	O	I			1.00
7.250	0.11	0.04	0.024	O	I			1.01
7.333	0.11	0.04	0.025	O	I			1.02
7.417	0.11	0.04	0.025	O	I			1.03
7.500	0.12	0.04	0.026	O	I			1.05
7.583	0.12	0.04	0.026	O	I			1.06
7.667	0.12	0.04	0.027	O	I			1.07
7.750	0.13	0.04	0.027	O	I			1.09
7.833	0.13	0.04	0.028	O	I			1.10
7.917	0.13	0.04	0.029	O	I			1.11
8.000	0.14	0.04	0.029	O	I			1.13
8.083	0.14	0.04	0.030	O	I			1.15
8.167	0.15	0.04	0.031	O	I			1.16
8.250	0.16	0.04	0.031	O	I			1.18
8.333	0.16	0.04	0.032	O	I			1.20
8.417	0.16	0.04	0.033	O	I			1.22
8.500	0.16	0.04	0.034	O	I			1.24
8.583	0.16	0.04	0.034	O	I			1.26
8.667	0.17	0.04	0.035	O	I			1.28
8.750	0.17	0.04	0.036	O	I			1.30
8.833	0.17	0.04	0.037	O	I			1.33
8.917	0.18	0.04	0.038	O	I			1.35
9.000	0.18	0.04	0.039	O	I			1.37
9.083	0.18	0.04	0.040	O	I			1.39
9.167	0.20	0.04	0.041	O	I			1.42
9.250	0.20	0.04	0.042	O	I			1.45
9.333	0.20	0.04	0.043	O	I			1.47
9.417	0.21	0.04	0.044	O	I			1.50
9.500	0.21	0.04	0.045	O	I			1.53
9.583	0.21	0.04	0.046	O	I			1.56
9.667	0.22	0.04	0.047	O	I			1.59
9.750	0.22	0.04	0.049	O	I			1.62
9.833	0.23	0.04	0.050	O	I			1.65
9.917	0.23	0.04	0.051	O	I			1.68
10.000	0.23	0.04	0.052	O	I			1.71
10.083	0.22	0.04	0.054	O	I			1.74
10.167	0.19	0.04	0.055	O	I			1.77
10.250	0.17	0.04	0.056	O	I			1.79
10.333	0.17	0.04	0.057	O	I			1.82
10.417	0.17	0.04	0.057	O	I			1.84
10.500	0.16	0.04	0.058	O	I			1.86
10.583	0.17	0.04	0.059	O	I			1.88
10.667	0.20	0.04	0.060	O	I			1.90

10.750	0.20	0.04	0.061	O		I		1.93
10.833	0.21	0.04	0.062	O		I		1.96
10.917	0.21	0.04	0.063	O		I		1.99
11.000	0.21	0.04	0.065	O		I		2.01
11.083	0.21	0.04	0.066	O		I		2.04
11.167	0.21	0.04	0.067	O		I		2.07
11.250	0.21	0.04	0.068	O		I		2.10
11.333	0.20	0.04	0.069	O		I		2.13
11.417	0.20	0.04	0.070	O		I		2.15
11.500	0.20	0.04	0.071	O		I		2.18
11.583	0.20	0.04	0.072	O		I		2.21
11.667	0.19	0.04	0.073	O		I		2.23
11.750	0.19	0.04	0.074	O		I		2.26
11.833	0.19	0.04	0.075	O		I		2.28
11.917	0.19	0.04	0.076	O		I		2.31
12.000	0.19	0.04	0.077	O		I		2.33
12.083	0.21	0.04	0.078	O		I		2.36
12.167	0.24	0.04	0.080	O		I		2.39
12.250	0.25	0.04	0.081	O		I		2.42
12.333	0.26	0.04	0.082	O		I		2.46
12.417	0.27	0.04	0.084	O		I		2.50
12.500	0.27	0.04	0.086	O		I		2.54
12.583	0.28	0.04	0.087	O		I		2.58
12.667	0.29	0.04	0.089	O		I		2.62
12.750	0.30	0.04	0.091	O		I		2.66
12.833	0.30	0.04	0.092	O		I		2.71
12.917	0.31	0.04	0.094	O		I		2.75
13.000	0.31	0.04	0.096	O		I		2.80
13.083	0.32	0.04	0.098	O		I		2.84
13.167	0.35	0.04	0.100	O		I		2.89
13.250	0.35	0.04	0.102	O		I		2.94
13.333	0.36	0.04	0.104	O		I		3.00
13.417	0.36	0.04	0.106	O		I		3.05
13.500	0.36	0.04	0.108	O		I		3.11
13.583	0.34	0.04	0.110	O		I		3.16
13.667	0.29	0.04	0.112	O		I		3.21
13.750	0.27	0.04	0.114	O		I		3.25
13.833	0.26	0.04	0.115	O		I		3.28
13.917	0.25	0.04	0.117	O		I		3.32
14.000	0.25	0.04	0.118	O		I		3.35
14.083	0.26	0.04	0.120	O		I		3.39
14.167	0.28	0.04	0.121	O		I		3.43
14.250	0.28	0.04	0.123	O		I		3.47
14.333	0.28	0.04	0.124	O		I		3.51
14.417	0.28	0.04	0.126	O		I		3.55
14.500	0.28	0.04	0.128	O		I		3.59
14.583	0.28	0.04	0.129	O		I		3.63
14.667	0.28	0.04	0.131	O		I		3.67
14.750	0.28	0.04	0.132	O		I		3.71
14.833	0.28	0.04	0.134	O		I		3.75

14.917	0.27	0.04	0.136	O			I	3.79
15.000	0.27	0.04	0.137	O			I	3.83
15.083	0.27	0.04	0.139	O			I	3.87
15.167	0.26	0.04	0.140	O			I	3.91
15.250	0.26	0.04	0.142	O			I	3.94
15.333	0.26	0.04	0.143	O			I	3.98
15.417	0.25	0.04	0.145	O			I	4.02
15.500	0.25	0.04	0.146	O			I	4.05
15.583	0.24	0.04	0.147	O			I	4.09
15.667	0.22	0.04	0.149	O		I		4.12
15.750	0.21	0.04	0.150	O		I		4.15
15.833	0.21	0.04	0.151	O		I		4.17
15.917	0.21	0.04	0.152	O		I		4.20
16.000	0.21	0.04	0.153	O		I		4.23
16.083	0.18	0.04	0.154	O	I			4.26
16.167	0.10	0.04	0.155	O	I			4.27
16.250	0.07	0.04	0.155	O I				4.28
16.333	0.06	0.04	0.155	O I				4.28
16.417	0.05	0.04	0.155	OI				4.28
16.500	0.05	0.04	0.155	OI				4.28
16.583	0.04	0.04	0.155	O				4.28
16.667	0.04	0.04	0.155	O				4.28
16.750	0.03	0.04	0.155	O				4.28
16.833	0.03	0.04	0.155	IO				4.28
16.917	0.03	0.04	0.155	IO				4.28
17.000	0.03	0.04	0.155	IO				4.28
17.083	0.04	0.04	0.155	O				4.27
17.167	0.05	0.04	0.155	OI				4.27
17.250	0.05	0.04	0.155	OI				4.27
17.333	0.05	0.04	0.155	OI				4.28
17.417	0.05	0.04	0.155	OI				4.28
17.500	0.05	0.04	0.155	OI				4.28
17.583	0.05	0.04	0.155	OI				4.28
17.667	0.05	0.04	0.155	OI				4.28
17.750	0.05	0.04	0.155	OI				4.28
17.833	0.05	0.04	0.155	OI				4.28
17.917	0.05	0.04	0.155	OI				4.28
18.000	0.04	0.04	0.155	O				4.28
18.083	0.04	0.04	0.155	O				4.28
18.167	0.04	0.04	0.155	O				4.28
18.250	0.04	0.04	0.155	O				4.28
18.333	0.04	0.04	0.155	O				4.28
18.417	0.04	0.04	0.155	O				4.28
18.500	0.04	0.04	0.155	O				4.28
18.583	0.04	0.04	0.155	O				4.28
18.667	0.04	0.04	0.155	O				4.28
18.750	0.03	0.04	0.155	O				4.28
18.833	0.03	0.04	0.155	IO				4.28
18.917	0.03	0.04	0.155	IO				4.27
19.000	0.02	0.04	0.155	IO				4.27

19.083	0.02	0.04	0.155	IO				4.27
19.167	0.03	0.04	0.155	IO				4.26
19.250	0.03	0.04	0.154	IO				4.26
19.333	0.03	0.04	0.154	IO				4.26
19.417	0.04	0.04	0.154	O				4.26
19.500	0.04	0.04	0.154	O				4.26
19.583	0.04	0.04	0.154	O				4.26
19.667	0.04	0.04	0.154	O				4.25
19.750	0.03	0.04	0.154	IO				4.25
19.833	0.03	0.04	0.154	IO				4.25
19.917	0.03	0.04	0.154	IO				4.25
20.000	0.02	0.04	0.154	IO				4.24
20.083	0.02	0.04	0.154	IO				4.24
20.167	0.03	0.04	0.153	IO				4.24
20.250	0.03	0.04	0.153	IO				4.23
20.333	0.03	0.04	0.153	IO				4.23
20.417	0.03	0.04	0.153	IO				4.23
20.500	0.03	0.04	0.153	IO				4.23
20.583	0.03	0.04	0.153	IO				4.23
20.667	0.03	0.04	0.153	IO				4.22
20.750	0.03	0.04	0.153	IO				4.22
20.833	0.03	0.04	0.153	IO				4.22
20.917	0.03	0.04	0.153	IO				4.22
21.000	0.02	0.04	0.152	IO				4.21
21.083	0.02	0.04	0.152	IO				4.21
21.167	0.03	0.04	0.152	IO				4.21
21.250	0.03	0.04	0.152	IO				4.20
21.333	0.03	0.04	0.152	IO				4.20
21.417	0.02	0.04	0.152	IO				4.20
21.500	0.02	0.04	0.152	IO				4.19
21.583	0.02	0.04	0.152	IO				4.19
21.667	0.03	0.04	0.151	IO				4.19
21.750	0.03	0.04	0.151	IO				4.18
21.833	0.03	0.04	0.151	IO				4.18
21.917	0.02	0.04	0.151	IO				4.18
22.000	0.02	0.04	0.151	IO				4.17
22.083	0.02	0.04	0.151	IO				4.17
22.167	0.03	0.04	0.151	IO				4.17
22.250	0.03	0.04	0.151	IO				4.16
22.333	0.03	0.04	0.150	IO				4.16
22.417	0.02	0.04	0.150	IO				4.16
22.500	0.02	0.04	0.150	IO				4.16
22.583	0.02	0.04	0.150	I O				4.15
22.667	0.02	0.04	0.150	I O				4.15
22.750	0.02	0.04	0.150	I O				4.14
22.833	0.02	0.04	0.150	I O				4.14
22.917	0.02	0.04	0.149	I O				4.14
23.000	0.02	0.04	0.149	I O				4.13
23.083	0.02	0.04	0.149	I O				4.13
23.167	0.02	0.04	0.149	I O				4.12

23.250	0.02	0.04	0.149	|I O	|	|	|	4.12
23.333	0.02	0.04	0.149	|I O	|	|	|	4.12
23.417	0.02	0.04	0.148	|I O	|	|	|	4.11
23.500	0.02	0.04	0.148	|I O	|	|	|	4.11
23.583	0.02	0.04	0.148	|I O	|	|	|	4.10
23.667	0.02	0.04	0.148	|I O	|	|	|	4.10
23.750	0.02	0.04	0.148	|I O	|	|	|	4.10
23.833	0.02	0.04	0.148	|I O	|	|	|	4.09
23.917	0.02	0.04	0.147	|I O	|	|	|	4.09
24.000	0.02	0.04	0.147	|I O	|	|	|	4.08
24.083	0.02	0.04	0.147	|I O	|	|	|	4.08
24.167	0.01	0.04	0.147	I O	|	|	|	4.07
24.250	0.00	0.04	0.147	I O	|	|	|	4.07
24.333	0.00	0.04	0.146	I O	|	|	|	4.06
24.417	0.00	0.04	0.146	I O	|	|	|	4.05
24.500	0.00	0.04	0.146	I O	|	|	|	4.04
24.583	0.00	0.04	0.145	I O	|	|	|	4.04
24.667	0.00	0.04	0.145	I O	|	|	|	4.03
24.750	0.00	0.04	0.145	I O	|	|	|	4.02
24.833	0.00	0.04	0.145	I O	|	|	|	4.01
24.917	0.00	0.04	0.144	I O	|	|	|	4.01
25.000	0.00	0.04	0.144	I O	|	|	|	4.00
25.083	0.00	0.04	0.144	I O	|	|	|	3.99
25.167	0.00	0.04	0.143	I O	|	|	|	3.98
25.250	0.00	0.04	0.143	I O	|	|	|	3.97
25.333	0.00	0.04	0.143	I O	|	|	|	3.97
25.417	0.00	0.04	0.142	I O	|	|	|	3.96
25.500	0.00	0.04	0.142	I O	|	|	|	3.95
25.583	0.00	0.04	0.142	I O	|	|	|	3.94
25.667	0.00	0.04	0.141	I O	|	|	|	3.94
25.750	0.00	0.04	0.141	I O	|	|	|	3.93
25.833	0.00	0.04	0.141	I O	|	|	|	3.92
25.917	0.00	0.04	0.140	I O	|	|	|	3.91
26.000	0.00	0.04	0.140	I O	|	|	|	3.90
26.083	0.00	0.04	0.140	I O	|	|	|	3.90
26.167	0.00	0.04	0.140	I O	|	|	|	3.89
26.250	0.00	0.04	0.139	I O	|	|	|	3.88
26.333	0.00	0.04	0.139	I O	|	|	|	3.87
26.417	0.00	0.04	0.139	I O	|	|	|	3.87
26.500	0.00	0.04	0.138	I O	|	|	|	3.86
26.583	0.00	0.04	0.138	I O	|	|	|	3.85
26.667	0.00	0.04	0.138	I O	|	|	|	3.84
26.750	0.00	0.04	0.137	I O	|	|	|	3.83
26.833	0.00	0.04	0.137	I O	|	|	|	3.83
26.917	0.00	0.04	0.137	I O	|	|	|	3.82
27.000	0.00	0.04	0.136	I O	|	|	|	3.81
27.083	0.00	0.04	0.136	I O	|	|	|	3.80
27.167	0.00	0.04	0.136	I O	|	|	|	3.80
27.250	0.00	0.04	0.136	I O	|	|	|	3.79
27.333	0.00	0.04	0.135	I O	|	|	|	3.78

27.417	0.00	0.04	0.135	I	O					3.77
27.500	0.00	0.04	0.135	I	O					3.77
27.583	0.00	0.04	0.134	I	O					3.76
27.667	0.00	0.04	0.134	I	O					3.75
27.750	0.00	0.04	0.134	I	O					3.74
27.833	0.00	0.04	0.133	I	O					3.73
27.917	0.00	0.04	0.133	I	O					3.73
28.000	0.00	0.04	0.133	I	O					3.72
28.083	0.00	0.04	0.132	I	O					3.71
28.167	0.00	0.04	0.132	I	O					3.70
28.250	0.00	0.04	0.132	I	O					3.70
28.333	0.00	0.04	0.132	I	O					3.69
28.417	0.00	0.04	0.131	I	O					3.68
28.500	0.00	0.04	0.131	I	O					3.67
28.583	0.00	0.04	0.131	I	O					3.66
28.667	0.00	0.04	0.130	I	O					3.66
28.750	0.00	0.04	0.130	I	O					3.65
28.833	0.00	0.04	0.130	I	O					3.64
28.917	0.00	0.04	0.129	I	O					3.63
29.000	0.00	0.04	0.129	I	O					3.63
29.083	0.00	0.04	0.129	I	O					3.62
29.167	0.00	0.04	0.128	I	O					3.61
29.250	0.00	0.04	0.128	I	O					3.60
29.333	0.00	0.04	0.128	I	O					3.59
29.417	0.00	0.04	0.127	I	O					3.59
29.500	0.00	0.04	0.127	I	O					3.58
29.583	0.00	0.04	0.127	I	O					3.57
29.667	0.00	0.04	0.127	I	O					3.56
29.750	0.00	0.04	0.126	I	O					3.56
29.833	0.00	0.04	0.126	I	O					3.55
29.917	0.00	0.04	0.126	I	O					3.54
30.000	0.00	0.04	0.125	I	O					3.53
30.083	0.00	0.04	0.125	I	O					3.52
30.167	0.00	0.04	0.125	I	O					3.52
30.250	0.00	0.04	0.124	I	O					3.51
30.333	0.00	0.04	0.124	I	O					3.50
30.417	0.00	0.04	0.124	I	O					3.49
30.500	0.00	0.04	0.123	I	O					3.49
30.583	0.00	0.04	0.123	I	O					3.48
30.667	0.00	0.04	0.123	I	O					3.47
30.750	0.00	0.04	0.123	I	O					3.46
30.833	0.00	0.04	0.122	I	O					3.46
30.917	0.00	0.04	0.122	I	O					3.45
31.000	0.00	0.04	0.122	I	O					3.44
31.083	0.00	0.04	0.121	I	O					3.43
31.167	0.00	0.04	0.121	I	O					3.42
31.250	0.00	0.04	0.121	I	O					3.42
31.333	0.00	0.04	0.120	I	O					3.41
31.417	0.00	0.04	0.120	I	O					3.40
31.500	0.00	0.04	0.120	I	O					3.39

31.583	0.00	0.04	0.119	I	O					3.39
31.667	0.00	0.04	0.119	I	O					3.38
31.750	0.00	0.04	0.119	I	O					3.37
31.833	0.00	0.04	0.118	I	O					3.36
31.917	0.00	0.04	0.118	I	O					3.35
32.000	0.00	0.04	0.118	I	O					3.35
32.083	0.00	0.04	0.118	I	O					3.34
32.167	0.00	0.04	0.117	I	O					3.33
32.250	0.00	0.04	0.117	I	O					3.32
32.333	0.00	0.04	0.117	I	O					3.32
32.417	0.00	0.04	0.116	I	O					3.31
32.500	0.00	0.04	0.116	I	O					3.30
32.583	0.00	0.04	0.116	I	O					3.29
32.667	0.00	0.04	0.115	I	O					3.28
32.750	0.00	0.04	0.115	I	O					3.28
32.833	0.00	0.04	0.115	I	O					3.27
32.917	0.00	0.04	0.114	I	O					3.26
33.000	0.00	0.04	0.114	I	O					3.25
33.083	0.00	0.04	0.114	I	O					3.25
33.167	0.00	0.04	0.114	I	O					3.24
33.250	0.00	0.04	0.113	I	O					3.23
33.333	0.00	0.04	0.113	I	O					3.22
33.417	0.00	0.04	0.113	I	O					3.22
33.500	0.00	0.04	0.112	I	O					3.21
33.583	0.00	0.04	0.112	I	O					3.20
33.667	0.00	0.04	0.112	I	O					3.19
33.750	0.00	0.04	0.111	I	O					3.18
33.833	0.00	0.04	0.111	I	O					3.18
33.917	0.00	0.04	0.111	I	O					3.17
34.000	0.00	0.04	0.110	I	O					3.16
34.083	0.00	0.04	0.110	I	O					3.15
34.167	0.00	0.04	0.110	I	O					3.15
34.250	0.00	0.04	0.110	I	O					3.14
34.333	0.00	0.04	0.109	I	O					3.13
34.417	0.00	0.04	0.109	I	O					3.12
34.500	0.00	0.04	0.109	I	O					3.11
34.583	0.00	0.04	0.108	I	O					3.11
34.667	0.00	0.04	0.108	I	O					3.10
34.750	0.00	0.04	0.108	I	O					3.09
34.833	0.00	0.04	0.107	I	O					3.08
34.917	0.00	0.04	0.107	I	O					3.08
35.000	0.00	0.04	0.107	I	O					3.07
35.083	0.00	0.04	0.106	I	O					3.06
35.167	0.00	0.04	0.106	I	O					3.05
35.250	0.00	0.04	0.106	I	O					3.04
35.333	0.00	0.04	0.105	I	O					3.04
35.417	0.00	0.04	0.105	I	O					3.03
35.500	0.00	0.04	0.105	I	O					3.02
35.583	0.00	0.04	0.105	I	O					3.01
35.667	0.00	0.04	0.104	I	O					3.01

35.750	0.00	0.04	0.104	I	O					3.00
35.833	0.00	0.04	0.104	I	O					2.99
35.917	0.00	0.04	0.103	I	O					2.98
36.000	0.00	0.04	0.103	I	O					2.97
36.083	0.00	0.04	0.103	I	O					2.97
36.167	0.00	0.04	0.102	I	O					2.96
36.250	0.00	0.04	0.102	I	O					2.95
36.333	0.00	0.04	0.102	I	O					2.94
36.417	0.00	0.04	0.101	I	O					2.94
36.500	0.00	0.04	0.101	I	O					2.93
36.583	0.00	0.04	0.101	I	O					2.92
36.667	0.00	0.04	0.101	I	O					2.91
36.750	0.00	0.04	0.100	I	O					2.91
36.833	0.00	0.04	0.100	I	O					2.90
36.917	0.00	0.04	0.100	I	O					2.89
37.000	0.00	0.04	0.099	I	O					2.88
37.083	0.00	0.04	0.099	I	O					2.87
37.167	0.00	0.04	0.099	I	O					2.87
37.250	0.00	0.04	0.098	I	O					2.86
37.333	0.00	0.04	0.098	I	O					2.85
37.417	0.00	0.04	0.098	I	O					2.84
37.500	0.00	0.04	0.097	I	O					2.84
37.583	0.00	0.04	0.097	I	O					2.83
37.667	0.00	0.04	0.097	I	O					2.82
37.750	0.00	0.04	0.096	I	O					2.81
37.833	0.00	0.04	0.096	I	O					2.80
37.917	0.00	0.04	0.096	I	O					2.80
38.000	0.00	0.04	0.096	I	O					2.79
38.083	0.00	0.04	0.095	I	O					2.78
38.167	0.00	0.04	0.095	I	O					2.77
38.250	0.00	0.04	0.095	I	O					2.77
38.333	0.00	0.04	0.094	I	O					2.76
38.417	0.00	0.04	0.094	I	O					2.75
38.500	0.00	0.04	0.094	I	O					2.74
38.583	0.00	0.04	0.093	I	O					2.73
38.667	0.00	0.04	0.093	I	O					2.73
38.750	0.00	0.04	0.093	I	O					2.72
38.833	0.00	0.04	0.092	I	O					2.71
38.917	0.00	0.04	0.092	I	O					2.70
39.000	0.00	0.04	0.092	I	O					2.70
39.083	0.00	0.04	0.092	I	O					2.69
39.167	0.00	0.04	0.091	I	O					2.68
39.250	0.00	0.04	0.091	I	O					2.67
39.333	0.00	0.04	0.091	I	O					2.66
39.417	0.00	0.04	0.090	I	O					2.66
39.500	0.00	0.04	0.090	I	O					2.65
39.583	0.00	0.04	0.090	I	O					2.64
39.667	0.00	0.04	0.089	I	O					2.63
39.750	0.00	0.04	0.089	I	O					2.63
39.833	0.00	0.04	0.089	I	O					2.62

39.917	0.00	0.04	0.088	I	O					2.61
40.000	0.00	0.04	0.088	I	O					2.60
40.083	0.00	0.04	0.088	I	O					2.60
40.167	0.00	0.04	0.087	I	O					2.59
40.250	0.00	0.04	0.087	I	O					2.58
40.333	0.00	0.04	0.087	I	O					2.57
40.417	0.00	0.04	0.087	I	O					2.56
40.500	0.00	0.04	0.086	I	O					2.56
40.583	0.00	0.04	0.086	I	O					2.55
40.667	0.00	0.04	0.086	I	O					2.54
40.750	0.00	0.04	0.085	I	O					2.53
40.833	0.00	0.04	0.085	I	O					2.53
40.917	0.00	0.04	0.085	I	O					2.52
41.000	0.00	0.04	0.084	I	O					2.51
41.083	0.00	0.04	0.084	I	O					2.50
41.167	0.00	0.04	0.084	I	O					2.49
41.250	0.00	0.04	0.083	I	O					2.49
41.333	0.00	0.04	0.083	I	O					2.48
41.417	0.00	0.04	0.083	I	O					2.47
41.500	0.00	0.04	0.083	I	O					2.46
41.583	0.00	0.04	0.082	I	O					2.46
41.667	0.00	0.04	0.082	I	O					2.45
41.750	0.00	0.04	0.082	I	O					2.44
41.833	0.00	0.04	0.081	I	O					2.43
41.917	0.00	0.04	0.081	I	O					2.42
42.000	0.00	0.04	0.081	I	O					2.42
42.083	0.00	0.04	0.080	I	O					2.41
42.167	0.00	0.04	0.080	I	O					2.40
42.250	0.00	0.04	0.080	I	O					2.39
42.333	0.00	0.04	0.079	I	O					2.39
42.417	0.00	0.04	0.079	I	O					2.38
42.500	0.00	0.04	0.079	I	O					2.37
42.583	0.00	0.04	0.079	I	O					2.36
42.667	0.00	0.04	0.078	I	O					2.36
42.750	0.00	0.04	0.078	I	O					2.35
42.833	0.00	0.04	0.078	I	O					2.34
42.917	0.00	0.04	0.077	I	O					2.33
43.000	0.00	0.04	0.077	I	O					2.32
43.083	0.00	0.04	0.077	I	O					2.32
43.167	0.00	0.04	0.076	I	O					2.31
43.250	0.00	0.04	0.076	I	O					2.30
43.333	0.00	0.04	0.076	I	O					2.29
43.417	0.00	0.04	0.075	I	O					2.29
43.500	0.00	0.04	0.075	I	O					2.28
43.583	0.00	0.04	0.075	I	O					2.27
43.667	0.00	0.04	0.074	I	O					2.26
43.750	0.00	0.04	0.074	I	O					2.25
43.833	0.00	0.04	0.074	I	O					2.25
43.917	0.00	0.04	0.074	I	O					2.24
44.000	0.00	0.04	0.073	I	O					2.23

44.083	0.00	0.04	0.073	I	O	|	|	|	|	2.22
44.167	0.00	0.04	0.073	I	O	|	|	|	|	2.22
44.250	0.00	0.04	0.072	I	O	|	|	|	|	2.21
44.333	0.00	0.04	0.072	I	O	|	|	|	|	2.20
44.417	0.00	0.04	0.072	I	O	|	|	|	|	2.19
44.500	0.00	0.04	0.071	I	O	|	|	|	|	2.18
44.583	0.00	0.04	0.071	I	O	|	|	|	|	2.18
44.667	0.00	0.04	0.071	I	O	|	|	|	|	2.17
44.750	0.00	0.04	0.070	I	O	|	|	|	|	2.16
44.833	0.00	0.04	0.070	I	O	|	|	|	|	2.15
44.917	0.00	0.04	0.070	I	O	|	|	|	|	2.15
45.000	0.00	0.04	0.070	I	O	|	|	|	|	2.14
45.083	0.00	0.04	0.069	I	O	|	|	|	|	2.13
45.167	0.00	0.04	0.069	I	O	|	|	|	|	2.12
45.250	0.00	0.04	0.069	I	O	|	|	|	|	2.11
45.333	0.00	0.04	0.068	I	O	|	|	|	|	2.11
45.417	0.00	0.04	0.068	I	O	|	|	|	|	2.10
45.500	0.00	0.04	0.068	I	O	|	|	|	|	2.09
45.583	0.00	0.04	0.067	I	O	|	|	|	|	2.08
45.667	0.00	0.04	0.067	I	O	|	|	|	|	2.08
45.750	0.00	0.04	0.067	I	O	|	|	|	|	2.07
45.833	0.00	0.04	0.066	I	O	|	|	|	|	2.06
45.917	0.00	0.04	0.066	I	O	|	|	|	|	2.05
46.000	0.00	0.04	0.066	I	O	|	|	|	|	2.05
46.083	0.00	0.04	0.065	I	O	|	|	|	|	2.04
46.167	0.00	0.04	0.065	I	O	|	|	|	|	2.03
46.250	0.00	0.04	0.065	I	O	|	|	|	|	2.02
46.333	0.00	0.04	0.065	I	O	|	|	|	|	2.01
46.417	0.00	0.04	0.064	I	O	|	|	|	|	2.01
46.500	0.00	0.04	0.064	I	O	|	|	|	|	2.00
46.583	0.00	0.04	0.064	I	O	|	|	|	|	1.99
46.667	0.00	0.04	0.063	I	O	|	|	|	|	1.98
46.750	0.00	0.04	0.063	I	O	|	|	|	|	1.98
46.833	0.00	0.04	0.063	I	O	|	|	|	|	1.97
46.917	0.00	0.04	0.062	I	O	|	|	|	|	1.96
47.000	0.00	0.04	0.062	I	O	|	|	|	|	1.95
47.083	0.00	0.04	0.062	I	O	|	|	|	|	1.94
47.167	0.00	0.04	0.061	I	O	|	|	|	|	1.94
47.250	0.00	0.04	0.061	I	O	|	|	|	|	1.93
47.333	0.00	0.04	0.061	I	O	|	|	|	|	1.92
47.417	0.00	0.04	0.061	I	O	|	|	|	|	1.91
47.500	0.00	0.04	0.060	I	O	|	|	|	|	1.91
47.583	0.00	0.04	0.060	I	O	|	|	|	|	1.90
47.667	0.00	0.04	0.060	I	O	|	|	|	|	1.89
47.750	0.00	0.04	0.059	I	O	|	|	|	|	1.88
47.833	0.00	0.04	0.059	I	O	|	|	|	|	1.87
47.917	0.00	0.04	0.059	I	O	|	|	|	|	1.87
48.000	0.00	0.04	0.058	I	O	|	|	|	|	1.86
48.083	0.00	0.04	0.058	I	O	|	|	|	|	1.85
48.167	0.00	0.04	0.058	I	O	|	|	|	|	1.84

48.250	0.00	0.04	0.057	I	O	|	|	|	|	1.84
48.333	0.00	0.04	0.057	I	O	|	|	|	|	1.83
48.417	0.00	0.04	0.057	I	O	|	|	|	|	1.82
48.500	0.00	0.04	0.057	I	O	|	|	|	|	1.81
48.583	0.00	0.04	0.056	I	O	|	|	|	|	1.80
48.667	0.00	0.04	0.056	I	O	|	|	|	|	1.80
48.750	0.00	0.04	0.056	I	O	|	|	|	|	1.79
48.833	0.00	0.04	0.055	I	O	|	|	|	|	1.78
48.917	0.00	0.04	0.055	I	O	|	|	|	|	1.77
49.000	0.00	0.04	0.055	I	O	|	|	|	|	1.77
49.083	0.00	0.04	0.054	I	O	|	|	|	|	1.76
49.167	0.00	0.04	0.054	I	O	|	|	|	|	1.75
49.250	0.00	0.04	0.054	I	O	|	|	|	|	1.74
49.333	0.00	0.04	0.053	I	O	|	|	|	|	1.74
49.417	0.00	0.04	0.053	I	O	|	|	|	|	1.73
49.500	0.00	0.04	0.053	I	O	|	|	|	|	1.72
49.583	0.00	0.04	0.052	I	O	|	|	|	|	1.71
49.667	0.00	0.04	0.052	I	O	|	|	|	|	1.70
49.750	0.00	0.04	0.052	I	O	|	|	|	|	1.70
49.833	0.00	0.04	0.052	I	O	|	|	|	|	1.69
49.917	0.00	0.04	0.051	I	O	|	|	|	|	1.68
50.000	0.00	0.04	0.051	I	O	|	|	|	|	1.67
50.083	0.00	0.04	0.051	I	O	|	|	|	|	1.67
50.167	0.00	0.04	0.050	I	O	|	|	|	|	1.66
50.250	0.00	0.04	0.050	I	O	|	|	|	|	1.65
50.333	0.00	0.04	0.050	I	O	|	|	|	|	1.64
50.417	0.00	0.04	0.049	I	O	|	|	|	|	1.63
50.500	0.00	0.04	0.049	I	O	|	|	|	|	1.63
50.583	0.00	0.04	0.049	I	O	|	|	|	|	1.62
50.667	0.00	0.04	0.048	I	O	|	|	|	|	1.61
50.750	0.00	0.04	0.048	I	O	|	|	|	|	1.60
50.833	0.00	0.04	0.048	I	O	|	|	|	|	1.60
50.917	0.00	0.04	0.048	I	O	|	|	|	|	1.59
51.000	0.00	0.04	0.047	I	O	|	|	|	|	1.58
51.083	0.00	0.04	0.047	I	O	|	|	|	|	1.57
51.167	0.00	0.04	0.047	I	O	|	|	|	|	1.56
51.250	0.00	0.04	0.046	I	O	|	|	|	|	1.56
51.333	0.00	0.04	0.046	I	O	|	|	|	|	1.55
51.417	0.00	0.04	0.046	I	O	|	|	|	|	1.54
51.500	0.00	0.04	0.045	I	O	|	|	|	|	1.53
51.583	0.00	0.04	0.045	I	O	|	|	|	|	1.53
51.667	0.00	0.04	0.045	I	O	|	|	|	|	1.52
51.750	0.00	0.04	0.044	I	O	|	|	|	|	1.51
51.833	0.00	0.04	0.044	I	O	|	|	|	|	1.50
51.917	0.00	0.04	0.044	I	O	|	|	|	|	1.50
52.000	0.00	0.04	0.043	I	O	|	|	|	|	1.49
52.083	0.00	0.04	0.043	I	O	|	|	|	|	1.48
52.167	0.00	0.04	0.043	I	O	|	|	|	|	1.47
52.250	0.00	0.04	0.043	I	O	|	|	|	|	1.46
52.333	0.00	0.04	0.042	I	O	|	|	|	|	1.46

52.417	0.00	0.04	0.042	I	O	|	|	|	|	1.45
52.500	0.00	0.04	0.042	I	O	|	|	|	|	1.44
52.583	0.00	0.04	0.041	I	O	|	|	|	|	1.43
52.667	0.00	0.04	0.041	I	O	|	|	|	|	1.43
52.750	0.00	0.04	0.041	I	O	|	|	|	|	1.42
52.833	0.00	0.04	0.040	I	O	|	|	|	|	1.41
52.917	0.00	0.04	0.040	I	O	|	|	|	|	1.40
53.000	0.00	0.04	0.040	I	O	|	|	|	|	1.39
53.083	0.00	0.04	0.039	I	O	|	|	|	|	1.39
53.167	0.00	0.04	0.039	I	O	|	|	|	|	1.38
53.250	0.00	0.04	0.039	I	O	|	|	|	|	1.37
53.333	0.00	0.04	0.039	I	O	|	|	|	|	1.36
53.417	0.00	0.04	0.038	I	O	|	|	|	|	1.36
53.500	0.00	0.04	0.038	I	O	|	|	|	|	1.35
53.583	0.00	0.04	0.038	I	O	|	|	|	|	1.34
53.667	0.00	0.04	0.037	I	O	|	|	|	|	1.33
53.750	0.00	0.04	0.037	I	O	|	|	|	|	1.32
53.833	0.00	0.04	0.037	I	O	|	|	|	|	1.32
53.917	0.00	0.04	0.036	I	O	|	|	|	|	1.31
54.000	0.00	0.04	0.036	I	O	|	|	|	|	1.30
54.083	0.00	0.04	0.036	I	O	|	|	|	|	1.29
54.167	0.00	0.04	0.035	I	O	|	|	|	|	1.29
54.250	0.00	0.04	0.035	I	O	|	|	|	|	1.28
54.333	0.00	0.04	0.035	I	O	|	|	|	|	1.27
54.417	0.00	0.04	0.035	I	O	|	|	|	|	1.26
54.500	0.00	0.04	0.034	I	O	|	|	|	|	1.25
54.583	0.00	0.04	0.034	I	O	|	|	|	|	1.25
54.667	0.00	0.04	0.034	I	O	|	|	|	|	1.24
54.750	0.00	0.04	0.033	I	O	|	|	|	|	1.23
54.833	0.00	0.04	0.033	I	O	|	|	|	|	1.22
54.917	0.00	0.04	0.033	I	O	|	|	|	|	1.22
55.000	0.00	0.04	0.032	I	O	|	|	|	|	1.21
55.083	0.00	0.04	0.032	I	O	|	|	|	|	1.20
55.167	0.00	0.04	0.032	I	O	|	|	|	|	1.19
55.250	0.00	0.04	0.031	I	O	|	|	|	|	1.19
55.333	0.00	0.04	0.031	I	O	|	|	|	|	1.18
55.417	0.00	0.04	0.031	I	O	|	|	|	|	1.17
55.500	0.00	0.04	0.030	I	O	|	|	|	|	1.16
55.583	0.00	0.04	0.030	I	O	|	|	|	|	1.15
55.667	0.00	0.04	0.030	I	O	|	|	|	|	1.15
55.750	0.00	0.04	0.030	I	O	|	|	|	|	1.14
55.833	0.00	0.04	0.029	I	O	|	|	|	|	1.13
55.917	0.00	0.04	0.029	I	O	|	|	|	|	1.12
56.000	0.00	0.04	0.029	I	O	|	|	|	|	1.12
56.083	0.00	0.04	0.028	I	O	|	|	|	|	1.11
56.167	0.00	0.04	0.028	I	O	|	|	|	|	1.10
56.250	0.00	0.04	0.028	I	O	|	|	|	|	1.09
56.333	0.00	0.04	0.027	I	O	|	|	|	|	1.08
56.417	0.00	0.04	0.027	I	O	|	|	|	|	1.08
56.500	0.00	0.04	0.027	I	O	|	|	|	|	1.07

56.583	0.00	0.04	0.026	I	O				1.06
56.667	0.00	0.04	0.026	I	O				1.05
56.750	0.00	0.04	0.026	I	O				1.05
56.833	0.00	0.04	0.026	I	O				1.04
56.917	0.00	0.04	0.025	I	O				1.03
57.000	0.00	0.04	0.025	I	O				1.02
57.083	0.00	0.04	0.025	I	O				1.01
57.167	0.00	0.04	0.024	I	O				1.01
57.250	0.00	0.04	0.024	I	O				1.00
57.333	0.00	0.04	0.024	I	O				0.99
57.417	0.00	0.04	0.023	I	O				0.97
57.500	0.00	0.04	0.023	I	O				0.96
57.583	0.00	0.04	0.023	I	O				0.95
57.667	0.00	0.04	0.022	I	O				0.94
57.750	0.00	0.04	0.022	I	O				0.92
57.833	0.00	0.04	0.022	I	O				0.91
57.917	0.00	0.04	0.022	I	O				0.90
58.000	0.00	0.04	0.021	I	O				0.89
58.083	0.00	0.04	0.021	I	O				0.88
58.167	0.00	0.04	0.021	I	O				0.87
58.250	0.00	0.04	0.021	I	O				0.86
58.333	0.00	0.04	0.020	I	O				0.84
58.417	0.00	0.04	0.020	I	O				0.83
58.500	0.00	0.04	0.020	I	O				0.82
58.583	0.00	0.04	0.019	I	O				0.81
58.667	0.00	0.04	0.019	I	O				0.80
58.750	0.00	0.04	0.019	I	O				0.79
58.833	0.00	0.04	0.019	I	O				0.78
58.917	0.00	0.03	0.019	I	O				0.77
59.000	0.00	0.03	0.018	I	O				0.76
59.083	0.00	0.03	0.018	I	O				0.75
59.167	0.00	0.03	0.018	I	O				0.74
59.250	0.00	0.03	0.018	I	O				0.73
59.333	0.00	0.03	0.017	I	O				0.72
59.417	0.00	0.03	0.017	I	O				0.71
59.500	0.00	0.03	0.017	I	O				0.70
59.583	0.00	0.03	0.017	I	O				0.70
59.667	0.00	0.03	0.016	I	O				0.69
59.750	0.00	0.03	0.016	I	O				0.68
59.833	0.00	0.03	0.016	I	O				0.67
59.917	0.00	0.03	0.016	I	O				0.66
60.000	0.00	0.03	0.016	I	O				0.65
60.083	0.00	0.03	0.015	I	O				0.64
60.167	0.00	0.03	0.015	I	O				0.64
60.250	0.00	0.03	0.015	I	O				0.63
60.333	0.00	0.03	0.015	I	O				0.62
60.417	0.00	0.03	0.015	I	O				0.61
60.500	0.00	0.03	0.014	I	O				0.60
60.583	0.00	0.03	0.014	I	O				0.60
60.667	0.00	0.03	0.014	I	O				0.59

60.750	0.00	0.03	0.014	I O				0.58
60.833	0.00	0.03	0.014	I O				0.57
60.917	0.00	0.03	0.014	I O				0.57
61.000	0.00	0.03	0.013	I O				0.56
61.083	0.00	0.02	0.013	I O				0.55
61.167	0.00	0.02	0.013	I O				0.54
61.250	0.00	0.02	0.013	I O				0.54
61.333	0.00	0.02	0.013	I O				0.53
61.417	0.00	0.02	0.013	I O				0.52
61.500	0.00	0.02	0.012	I O				0.52
61.583	0.00	0.02	0.012	I O				0.51
61.667	0.00	0.02	0.012	I O				0.50
61.750	0.00	0.02	0.012	IO				0.50
61.833	0.00	0.02	0.012	IO				0.49
61.917	0.00	0.02	0.012	IO				0.48
62.000	0.00	0.02	0.011	IO				0.48
62.083	0.00	0.02	0.011	IO				0.47
62.167	0.00	0.02	0.011	IO				0.47
62.250	0.00	0.02	0.011	IO				0.46
62.333	0.00	0.02	0.011	IO				0.45
62.417	0.00	0.02	0.011	IO				0.45
62.500	0.00	0.02	0.011	IO				0.44
62.583	0.00	0.02	0.010	IO				0.44
62.667	0.00	0.02	0.010	IO				0.43
62.750	0.00	0.02	0.010	IO				0.43
62.833	0.00	0.02	0.010	IO				0.42
62.917	0.00	0.02	0.010	IO				0.41
63.000	0.00	0.02	0.010	IO				0.41
63.083	0.00	0.02	0.010	IO				0.40
63.167	0.00	0.02	0.010	IO				0.40
63.250	0.00	0.02	0.009	IO				0.39
63.333	0.00	0.02	0.009	IO				0.39
63.417	0.00	0.02	0.009	IO				0.38
63.500	0.00	0.02	0.009	IO				0.38
63.583	0.00	0.02	0.009	IO				0.37
63.667	0.00	0.02	0.009	IO				0.37
63.750	0.00	0.02	0.009	IO				0.36
63.833	0.00	0.02	0.009	IO				0.36
63.917	0.00	0.02	0.009	IO				0.36
64.000	0.00	0.02	0.008	IO				0.35
64.083	0.00	0.02	0.008	IO				0.35
64.167	0.00	0.02	0.008	IO				0.34
64.250	0.00	0.02	0.008	IO				0.34
64.333	0.00	0.01	0.008	IO				0.33
64.417	0.00	0.01	0.008	IO				0.33
64.500	0.00	0.01	0.008	IO				0.32
64.583	0.00	0.01	0.008	IO				0.32
64.667	0.00	0.01	0.008	IO				0.32
64.750	0.00	0.01	0.007	IO				0.31
64.833	0.00	0.01	0.007	IO				0.31

64.917	0.00	0.01	0.007	IO				0.30
65.000	0.00	0.01	0.007	IO				0.30
65.083	0.00	0.01	0.007	IO				0.30
65.167	0.00	0.01	0.007	IO				0.29
65.250	0.00	0.01	0.007	IO				0.29
65.333	0.00	0.01	0.007	IO				0.29
65.417	0.00	0.01	0.007	IO				0.28
65.500	0.00	0.01	0.007	IO				0.28
65.583	0.00	0.01	0.007	IO				0.27
65.667	0.00	0.01	0.007	IO				0.27
65.750	0.00	0.01	0.006	IO				0.27
65.833	0.00	0.01	0.006	IO				0.26
65.917	0.00	0.01	0.006	IO				0.26
66.000	0.00	0.01	0.006	IO				0.26
66.083	0.00	0.01	0.006	IO				0.25
66.167	0.00	0.01	0.006	O				0.25
66.250	0.00	0.01	0.006	O				0.25
66.333	0.00	0.01	0.006	O				0.24
66.417	0.00	0.01	0.006	O				0.24
66.500	0.00	0.01	0.006	O				0.24
66.583	0.00	0.01	0.006	O				0.24
66.667	0.00	0.01	0.006	O				0.23
66.750	0.00	0.01	0.005	O				0.23
66.833	0.00	0.01	0.005	O				0.23
66.917	0.00	0.01	0.005	O				0.22
67.000	0.00	0.01	0.005	O				0.22
67.083	0.00	0.01	0.005	O				0.22
67.167	0.00	0.01	0.005	O				0.21
67.250	0.00	0.01	0.005	O				0.21
67.333	0.00	0.01	0.005	O				0.21
67.417	0.00	0.01	0.005	O				0.21
67.500	0.00	0.01	0.005	O				0.20
67.583	0.00	0.01	0.005	O				0.20
67.667	0.00	0.01	0.005	O				0.20
67.750	0.00	0.01	0.005	O				0.20
67.833	0.00	0.01	0.005	O				0.19
67.917	0.00	0.01	0.005	O				0.19
68.000	0.00	0.01	0.005	O				0.19
68.083	0.00	0.01	0.004	O				0.19
68.167	0.00	0.01	0.004	O				0.18
68.250	0.00	0.01	0.004	O				0.18
68.333	0.00	0.01	0.004	O				0.18
68.417	0.00	0.01	0.004	O				0.18
68.500	0.00	0.01	0.004	O				0.17
68.583	0.00	0.01	0.004	O				0.17
68.667	0.00	0.01	0.004	O				0.17
68.750	0.00	0.01	0.004	O				0.17
68.833	0.00	0.01	0.004	O				0.17
68.917	0.00	0.01	0.004	O				0.16
69.000	0.00	0.01	0.004	O				0.16

69.083	0.00	0.01	0.004	O	|	|	|	0.16
69.167	0.00	0.01	0.004	O	|	|	|	0.16
69.250	0.00	0.01	0.004	O	|	|	|	0.16
69.333	0.00	0.01	0.004	O	|	|	|	0.15
69.417	0.00	0.01	0.004	O	|	|	|	0.15
69.500	0.00	0.01	0.004	O	|	|	|	0.15
69.583	0.00	0.01	0.004	O	|	|	|	0.15
69.667	0.00	0.01	0.003	O	|	|	|	0.15
69.750	0.00	0.01	0.003	O	|	|	|	0.14
69.833	0.00	0.01	0.003	O	|	|	|	0.14
69.917	0.00	0.01	0.003	O	|	|	|	0.14
70.000	0.00	0.01	0.003	O	|	|	|	0.14
70.083	0.00	0.01	0.003	O	|	|	|	0.14
70.167	0.00	0.01	0.003	O	|	|	|	0.13
70.250	0.00	0.01	0.003	O	|	|	|	0.13
70.333	0.00	0.01	0.003	O	|	|	|	0.13
70.417	0.00	0.01	0.003	O	|	|	|	0.13
70.500	0.00	0.01	0.003	O	|	|	|	0.13
70.583	0.00	0.01	0.003	O	|	|	|	0.13
70.667	0.00	0.01	0.003	O	|	|	|	0.12
70.750	0.00	0.01	0.003	O	|	|	|	0.12
70.833	0.00	0.01	0.003	O	|	|	|	0.12
70.917	0.00	0.01	0.003	O	|	|	|	0.12
71.000	0.00	0.01	0.003	O	|	|	|	0.12
71.083	0.00	0.01	0.003	O	|	|	|	0.12
71.167	0.00	0.01	0.003	O	|	|	|	0.12
71.250	0.00	0.01	0.003	O	|	|	|	0.11
71.333	0.00	0.01	0.003	O	|	|	|	0.11
71.417	0.00	0.01	0.003	O	|	|	|	0.11
71.500	0.00	0.00	0.003	O	|	|	|	0.11
71.583	0.00	0.00	0.003	O	|	|	|	0.11
71.667	0.00	0.00	0.003	O	|	|	|	0.11
71.750	0.00	0.00	0.003	O	|	|	|	0.11
71.833	0.00	0.00	0.003	O	|	|	|	0.10
71.917	0.00	0.00	0.002	O	|	|	|	0.10
72.000	0.00	0.00	0.002	O	|	|	|	0.10
72.083	0.00	0.00	0.002	O	|	|	|	0.10
72.167	0.00	0.00	0.002	O	|	|	|	0.10
72.250	0.00	0.00	0.002	O	|	|	|	0.10
72.333	0.00	0.00	0.002	O	|	|	|	0.10
72.417	0.00	0.00	0.002	O	|	|	|	0.10
72.500	0.00	0.00	0.002	O	|	|	|	0.09
72.583	0.00	0.00	0.002	O	|	|	|	0.09
72.667	0.00	0.00	0.002	O	|	|	|	0.09
72.750	0.00	0.00	0.002	O	|	|	|	0.09
72.833	0.00	0.00	0.002	O	|	|	|	0.09
72.917	0.00	0.00	0.002	O	|	|	|	0.09
73.000	0.00	0.00	0.002	O	|	|	|	0.09
73.083	0.00	0.00	0.002	O	|	|	|	0.09
73.167	0.00	0.00	0.002	O	|	|	|	0.08

73.250	0.00	0.00	0.002	O				0.08
73.333	0.00	0.00	0.002	O				0.08
73.417	0.00	0.00	0.002	O				0.08
73.500	0.00	0.00	0.002	O				0.08
73.583	0.00	0.00	0.002	O				0.08
73.667	0.00	0.00	0.002	O				0.08
73.750	0.00	0.00	0.002	O				0.08
73.833	0.00	0.00	0.002	O				0.08
73.917	0.00	0.00	0.002	O				0.08
74.000	0.00	0.00	0.002	O				0.07
74.083	0.00	0.00	0.002	O				0.07
74.167	0.00	0.00	0.002	O				0.07
74.250	0.00	0.00	0.002	O				0.07
74.333	0.00	0.00	0.002	O				0.07
74.417	0.00	0.00	0.002	O				0.07
74.500	0.00	0.00	0.002	O				0.07
74.583	0.00	0.00	0.002	O				0.07
74.667	0.00	0.00	0.002	O				0.07
74.750	0.00	0.00	0.002	O				0.07
74.833	0.00	0.00	0.002	O				0.07
74.917	0.00	0.00	0.002	O				0.06
75.000	0.00	0.00	0.002	O				0.06
75.083	0.00	0.00	0.002	O				0.06
75.167	0.00	0.00	0.001	O				0.06
75.250	0.00	0.00	0.001	O				0.06
75.333	0.00	0.00	0.001	O				0.06
75.417	0.00	0.00	0.001	O				0.06
75.500	0.00	0.00	0.001	O				0.06
75.583	0.00	0.00	0.001	O				0.06
75.667	0.00	0.00	0.001	O				0.06
75.750	0.00	0.00	0.001	O				0.06
75.833	0.00	0.00	0.001	O				0.06
75.917	0.00	0.00	0.001	O				0.06
76.000	0.00	0.00	0.001	O				0.05
76.083	0.00	0.00	0.001	O				0.05
76.167	0.00	0.00	0.001	O				0.05
76.250	0.00	0.00	0.001	O				0.05
76.333	0.00	0.00	0.001	O				0.05
76.417	0.00	0.00	0.001	O				0.05
76.500	0.00	0.00	0.001	O				0.05
76.583	0.00	0.00	0.001	O				0.05
76.667	0.00	0.00	0.001	O				0.05
76.750	0.00	0.00	0.001	O				0.05
76.833	0.00	0.00	0.001	O				0.05
76.917	0.00	0.00	0.001	O				0.05
77.000	0.00	0.00	0.001	O				0.05
77.083	0.00	0.00	0.001	O				0.05
77.167	0.00	0.00	0.001	O				0.05
77.250	0.00	0.00	0.001	O				0.05
77.333	0.00	0.00	0.001	O				0.04

77.417	0.00	0.00	0.001	O	|	|	|	0.04
77.500	0.00	0.00	0.001	O	|	|	|	0.04
77.583	0.00	0.00	0.001	O	|	|	|	0.04
77.667	0.00	0.00	0.001	O	|	|	|	0.04
77.750	0.00	0.00	0.001	O	|	|	|	0.04
77.833	0.00	0.00	0.001	O	|	|	|	0.04
77.917	0.00	0.00	0.001	O	|	|	|	0.04
78.000	0.00	0.00	0.001	O	|	|	|	0.04
78.083	0.00	0.00	0.001	O	|	|	|	0.04
78.167	0.00	0.00	0.001	O	|	|	|	0.04
78.250	0.00	0.00	0.001	O	|	|	|	0.04
78.333	0.00	0.00	0.001	O	|	|	|	0.04
78.417	0.00	0.00	0.001	O	|	|	|	0.04
78.500	0.00	0.00	0.001	O	|	|	|	0.04
78.583	0.00	0.00	0.001	O	|	|	|	0.04
78.667	0.00	0.00	0.001	O	|	|	|	0.04
78.750	0.00	0.00	0.001	O	|	|	|	0.04
78.833	0.00	0.00	0.001	O	|	|	|	0.04
78.917	0.00	0.00	0.001	O	|	|	|	0.03
79.000	0.00	0.00	0.001	O	|	|	|	0.03
79.083	0.00	0.00	0.001	O	|	|	|	0.03
79.167	0.00	0.00	0.001	O	|	|	|	0.03
79.250	0.00	0.00	0.001	O	|	|	|	0.03
79.333	0.00	0.00	0.001	O	|	|	|	0.03
79.417	0.00	0.00	0.001	O	|	|	|	0.03
79.500	0.00	0.00	0.001	O	|	|	|	0.03
79.583	0.00	0.00	0.001	O	|	|	|	0.03
79.667	0.00	0.00	0.001	O	|	|	|	0.03
79.750	0.00	0.00	0.001	O	|	|	|	0.03
79.833	0.00	0.00	0.001	O	|	|	|	0.03
79.917	0.00	0.00	0.001	O	|	|	|	0.03
80.000	0.00	0.00	0.001	O	|	|	|	0.03
80.083	0.00	0.00	0.001	O	|	|	|	0.03
80.167	0.00	0.00	0.001	O	|	|	|	0.03
80.250	0.00	0.00	0.001	O	|	|	|	0.03
80.333	0.00	0.00	0.001	O	|	|	|	0.03
80.417	0.00	0.00	0.001	O	|	|	|	0.03
80.500	0.00	0.00	0.001	O	|	|	|	0.03
80.583	0.00	0.00	0.001	O	|	|	|	0.03
80.667	0.00	0.00	0.001	O	|	|	|	0.03
80.750	0.00	0.00	0.001	O	|	|	|	0.03
80.833	0.00	0.00	0.001	O	|	|	|	0.03
80.917	0.00	0.00	0.001	O	|	|	|	0.03
81.000	0.00	0.00	0.001	O	|	|	|	0.03
81.083	0.00	0.00	0.001	O	|	|	|	0.02
81.167	0.00	0.00	0.001	O	|	|	|	0.02
81.250	0.00	0.00	0.001	O	|	|	|	0.02
81.333	0.00	0.00	0.001	O	|	|	|	0.02
81.417	0.00	0.00	0.001	O	|	|	|	0.02
81.500	0.00	0.00	0.001	O	|	|	|	0.02

```
81.583    0.00    0.00      0.001  O       |       |       |       |     0.02
81.667    0.00    0.00      0.001  O       |       |       |       |     0.02
81.750    0.00    0.00      0.001  O       |       |       |       |     0.02
81.833    0.00    0.00      0.001  O       |       |       |       |     0.02

        ****************************HYDROGRAPH DATA****************************
                       Number of intervals =   982
                       Time interval =    5.0 (Min.)
                       Maximum/Peak flow rate =        0.045 (CFS)
                       Total volume =       0.221 (Ac.Ft)
                Status of hydrographs being held in storage
                           Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
                Peak (CFS)      0.000     0.000     0.000     0.000     0.000
                Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
        ***********************************************************************

        ---------------------------------------------------------------------
```

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
5 yr
1 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris15.rte

**********HYDROGRAPH DATA**********

Number of intervals = 20
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 2.224 (CFS)
Total volume = 0.078 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++++++++++

Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 20
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.6 1.11 1.67 2.22	Depth (Ft.)
0.083	0.08	0.00	0.000	OI	0.01
0.167	0.30	0.00	0.002	O I	0.07
0.250	0.40	0.01	0.004	O I	0.17
0.333	0.47	0.01	0.007	O I	0.29
0.417	0.52	0.02	0.010	O I	0.42
0.500	0.59	0.03	0.014	O I	0.58
0.583	0.67	0.03	0.018	O I	0.75
0.667	0.77	0.04	0.023	O I	0.94
0.750	0.94	0.04	0.028	O I	1.10
0.833	1.58	0.04	0.037	O I	1.31
0.917	2.22	0.04	0.049	O I	1.63
1.000	1.22	0.04	0.061	O I	1.92
1.083	0.75	0.04	0.067	O I	2.08
1.167	0.36	0.04	0.071	O I	2.17
1.250	0.21	0.04	0.073	O I	2.21
1.333	0.13	0.04	0.073	OI	2.23
1.417	0.08	0.04	0.074	OI	2.24
1.500	0.05	0.04	0.074	O	2.25
1.583	0.01	0.04	0.074	O	2.24
1.667	0.00	0.04	0.073	O	2.24
1.750	0.00	0.04	0.073	O	2.23
1.833	0.00	0.04	0.073	O	2.22
1.917	0.00	0.04	0.073	O	2.21
2.000	0.00	0.04	0.072	O	2.21
2.083	0.00	0.04	0.072	O	2.20
2.167	0.00	0.04	0.072	O	2.19
2.250	0.00	0.04	0.071	O	2.18
2.333	0.00	0.04	0.071	O	2.18

2.417	0.00	0.04	0.071	O				2.17
2.500	0.00	0.04	0.070	O				2.16
2.583	0.00	0.04	0.070	O				2.15
2.667	0.00	0.04	0.070	O				2.14
2.750	0.00	0.04	0.069	O				2.14
2.833	0.00	0.04	0.069	O				2.13
2.917	0.00	0.04	0.069	O				2.12
3.000	0.00	0.04	0.069	O				2.11
3.083	0.00	0.04	0.068	O				2.11
3.167	0.00	0.04	0.068	O				2.10
3.250	0.00	0.04	0.068	O				2.09
3.333	0.00	0.04	0.067	O				2.08
3.417	0.00	0.04	0.067	O				2.08
3.500	0.00	0.04	0.067	O				2.07
3.583	0.00	0.04	0.066	O				2.06
3.667	0.00	0.04	0.066	O				2.05
3.750	0.00	0.04	0.066	O				2.04
3.833	0.00	0.04	0.065	O				2.04
3.917	0.00	0.04	0.065	O				2.03
4.000	0.00	0.04	0.065	O				2.02
4.083	0.00	0.04	0.065	O				2.01
4.167	0.00	0.04	0.064	O				2.01
4.250	0.00	0.04	0.064	O				2.00
4.333	0.00	0.04	0.064	O				1.99
4.417	0.00	0.04	0.063	O				1.98
4.500	0.00	0.04	0.063	O				1.97
4.583	0.00	0.04	0.063	O				1.97
4.667	0.00	0.04	0.062	O				1.96
4.750	0.00	0.04	0.062	O				1.95
4.833	0.00	0.04	0.062	O				1.94
4.917	0.00	0.04	0.061	O				1.94
5.000	0.00	0.04	0.061	O				1.93
5.083	0.00	0.04	0.061	O				1.92
5.167	0.00	0.04	0.060	O				1.91
5.250	0.00	0.04	0.060	O				1.90
5.333	0.00	0.04	0.060	O				1.90
5.417	0.00	0.04	0.060	O				1.89
5.500	0.00	0.04	0.059	O				1.88
5.583	0.00	0.04	0.059	O				1.87
5.667	0.00	0.04	0.059	O				1.87
5.750	0.00	0.04	0.058	O				1.86
5.833	0.00	0.04	0.058	O				1.85
5.917	0.00	0.04	0.058	O				1.84
6.000	0.00	0.04	0.057	O				1.83
6.083	0.00	0.04	0.057	O				1.83
6.167	0.00	0.04	0.057	O				1.82
6.250	0.00	0.04	0.056	O				1.81
6.333	0.00	0.04	0.056	O				1.80
6.417	0.00	0.04	0.056	O				1.80
6.500	0.00	0.04	0.056	O				1.79

6.583	0.00	0.04	0.055	O				1.78
6.667	0.00	0.04	0.055	O				1.77
6.750	0.00	0.04	0.055	O				1.77
6.833	0.00	0.04	0.054	O				1.76
6.917	0.00	0.04	0.054	O				1.75
7.000	0.00	0.04	0.054	O				1.74
7.083	0.00	0.04	0.053	O				1.73
7.167	0.00	0.04	0.053	O				1.73
7.250	0.00	0.04	0.053	O				1.72
7.333	0.00	0.04	0.052	O				1.71
7.417	0.00	0.04	0.052	O				1.70
7.500	0.00	0.04	0.052	O				1.70
7.583	0.00	0.04	0.052	O				1.69
7.667	0.00	0.04	0.051	O				1.68
7.750	0.00	0.04	0.051	O				1.67
7.833	0.00	0.04	0.051	O				1.66
7.917	0.00	0.04	0.050	O				1.66
8.000	0.00	0.04	0.050	O				1.65
8.083	0.00	0.04	0.050	O				1.64
8.167	0.00	0.04	0.049	O				1.63
8.250	0.00	0.04	0.049	O				1.63
8.333	0.00	0.04	0.049	O				1.62
8.417	0.00	0.04	0.048	O				1.61
8.500	0.00	0.04	0.048	O				1.60
8.583	0.00	0.04	0.048	O				1.59
8.667	0.00	0.04	0.047	O				1.59
8.750	0.00	0.04	0.047	O				1.58
8.833	0.00	0.04	0.047	O				1.57
8.917	0.00	0.04	0.047	O				1.56
9.000	0.00	0.04	0.046	O				1.56
9.083	0.00	0.04	0.046	O				1.55
9.167	0.00	0.04	0.046	O				1.54
9.250	0.00	0.04	0.045	O				1.53
9.333	0.00	0.04	0.045	O				1.53
9.417	0.00	0.04	0.045	O				1.52
9.500	0.00	0.04	0.044	O				1.51
9.583	0.00	0.04	0.044	O				1.50
9.667	0.00	0.04	0.044	O				1.49
9.750	0.00	0.04	0.043	O				1.49
9.833	0.00	0.04	0.043	O				1.48
9.917	0.00	0.04	0.043	O				1.47
10.000	0.00	0.04	0.043	O				1.46
10.083	0.00	0.04	0.042	O				1.46
10.167	0.00	0.04	0.042	O				1.45
10.250	0.00	0.04	0.042	O				1.44
10.333	0.00	0.04	0.041	O				1.43
10.417	0.00	0.04	0.041	O				1.42
10.500	0.00	0.04	0.041	O				1.42
10.583	0.00	0.04	0.040	O				1.41
10.667	0.00	0.04	0.040	O				1.40

10.750	0.00	0.04	0.040	O				1.39
10.833	0.00	0.04	0.039	O				1.39
10.917	0.00	0.04	0.039	O				1.38
11.000	0.00	0.04	0.039	O				1.37
11.083	0.00	0.04	0.038	O				1.36
11.167	0.00	0.04	0.038	O				1.35
11.250	0.00	0.04	0.038	O				1.35
11.333	0.00	0.04	0.038	O				1.34
11.417	0.00	0.04	0.037	O				1.33
11.500	0.00	0.04	0.037	O				1.32
11.583	0.00	0.04	0.037	O				1.32
11.667	0.00	0.04	0.036	O				1.31
11.750	0.00	0.04	0.036	O				1.30
11.833	0.00	0.04	0.036	O				1.29
11.917	0.00	0.04	0.035	O				1.28
12.000	0.00	0.04	0.035	O				1.28
12.083	0.00	0.04	0.035	O				1.27
12.167	0.00	0.04	0.034	O				1.26
12.250	0.00	0.04	0.034	O				1.25
12.333	0.00	0.04	0.034	O				1.25
12.417	0.00	0.04	0.034	O				1.24
12.500	0.00	0.04	0.033	O				1.23
12.583	0.00	0.04	0.033	O				1.22
12.667	0.00	0.04	0.033	O				1.22
12.750	0.00	0.04	0.032	O				1.21
12.833	0.00	0.04	0.032	O				1.20
12.917	0.00	0.04	0.032	O				1.19
13.000	0.00	0.04	0.031	O				1.18
13.083	0.00	0.04	0.031	O				1.18
13.167	0.00	0.04	0.031	O				1.17
13.250	0.00	0.04	0.030	O				1.16
13.333	0.00	0.04	0.030	O				1.15
13.417	0.00	0.04	0.030	O				1.15
13.500	0.00	0.04	0.030	O				1.14
13.583	0.00	0.04	0.029	O				1.13
13.667	0.00	0.04	0.029	O				1.12
13.750	0.00	0.04	0.029	O				1.11
13.833	0.00	0.04	0.028	O				1.11
13.917	0.00	0.04	0.028	O				1.10
14.000	0.00	0.04	0.028	O				1.09
14.083	0.00	0.04	0.027	O				1.08
14.167	0.00	0.04	0.027	O				1.08
14.250	0.00	0.04	0.027	O				1.07
14.333	0.00	0.04	0.026	O				1.06
14.417	0.00	0.04	0.026	O				1.05
14.500	0.00	0.04	0.026	O				1.04
14.583	0.00	0.04	0.025	O				1.04
14.667	0.00	0.04	0.025	O				1.03
14.750	0.00	0.04	0.025	O				1.02
14.833	0.00	0.04	0.025	O				1.01

14.917	0.00	0.04	0.024	O				1.01
15.000	0.00	0.04	0.024	O				1.00
15.083	0.00	0.04	0.024	O				0.98
15.167	0.00	0.04	0.023	O				0.97
15.250	0.00	0.04	0.023	O				0.96
15.333	0.00	0.04	0.023	O				0.95
15.417	0.00	0.04	0.022	O				0.93
15.500	0.00	0.04	0.022	O				0.92
15.583	0.00	0.04	0.022	O				0.91
15.667	0.00	0.04	0.022	O				0.90
15.750	0.00	0.04	0.021	O				0.89
15.833	0.00	0.04	0.021	O				0.88
15.917	0.00	0.04	0.021	O				0.86
16.000	0.00	0.04	0.020	O				0.85
16.083	0.00	0.04	0.020	O				0.84
16.167	0.00	0.04	0.020	O				0.83
16.250	0.00	0.04	0.020	O				0.82
16.333	0.00	0.04	0.019	O				0.81
16.417	0.00	0.04	0.019	O				0.80
16.500	0.00	0.04	0.019	O				0.79
16.583	0.00	0.04	0.019	O				0.78
16.667	0.00	0.03	0.018	O				0.77
16.750	0.00	0.03	0.018	O				0.76
16.833	0.00	0.03	0.018	O				0.75
16.917	0.00	0.03	0.018	O				0.74
17.000	0.00	0.03	0.018	O				0.73
17.083	0.00	0.03	0.017	O				0.72
17.167	0.00	0.03	0.017	O				0.71
17.250	0.00	0.03	0.017	O				0.70
17.333	0.00	0.03	0.017	O				0.69
17.417	0.00	0.03	0.016	O				0.69
17.500	0.00	0.03	0.016	O				0.68
17.583	0.00	0.03	0.016	O				0.67
17.667	0.00	0.03	0.016	O				0.66
17.750	0.00	0.03	0.016	O				0.65
17.833	0.00	0.03	0.015	O				0.64
17.917	0.00	0.03	0.015	O				0.63
18.000	0.00	0.03	0.015	O				0.63
18.083	0.00	0.03	0.015	O				0.62
18.167	0.00	0.03	0.015	O				0.61
18.250	0.00	0.03	0.014	O				0.60
18.333	0.00	0.03	0.014	O				0.59
18.417	0.00	0.03	0.014	O				0.59
18.500	0.00	0.03	0.014	O				0.58
18.583	0.00	0.03	0.014	O				0.57
18.667	0.00	0.03	0.014	O				0.56
18.750	0.00	0.03	0.013	O				0.56
18.833	0.00	0.02	0.013	O				0.55
18.917	0.00	0.02	0.013	O				0.54
19.000	0.00	0.02	0.013	O				0.54

19.083	0.00	0.02	0.013	O	|	|	|	0.53
19.167	0.00	0.02	0.013	O	|	|	|	0.52
19.250	0.00	0.02	0.012	O	|	|	|	0.52
19.333	0.00	0.02	0.012	O	|	|	|	0.51
19.417	0.00	0.02	0.012	O	|	|	|	0.50
19.500	0.00	0.02	0.012	O	|	|	|	0.50
19.583	0.00	0.02	0.012	O	|	|	|	0.49
19.667	0.00	0.02	0.012	O	|	|	|	0.48
19.750	0.00	0.02	0.011	O	|	|	|	0.48
19.833	0.00	0.02	0.011	O	|	|	|	0.47
19.917	0.00	0.02	0.011	O	|	|	|	0.47
20.000	0.00	0.02	0.011	O	|	|	|	0.46
20.083	0.00	0.02	0.011	O	|	|	|	0.45
20.167	0.00	0.02	0.011	O	|	|	|	0.45
20.250	0.00	0.02	0.011	O	|	|	|	0.44
20.333	0.00	0.02	0.010	O	|	|	|	0.44
20.417	0.00	0.02	0.010	O	|	|	|	0.43
20.500	0.00	0.02	0.010	O	|	|	|	0.43
20.583	0.00	0.02	0.010	O	|	|	|	0.42
20.667	0.00	0.02	0.010	O	|	|	|	0.41
20.750	0.00	0.02	0.010	O	|	|	|	0.41
20.833	0.00	0.02	0.010	O	|	|	|	0.40
20.917	0.00	0.02	0.010	O	|	|	|	0.40
21.000	0.00	0.02	0.009	O	|	|	|	0.39
21.083	0.00	0.02	0.009	O	|	|	|	0.39
21.167	0.00	0.02	0.009	O	|	|	|	0.38
21.250	0.00	0.02	0.009	O	|	|	|	0.38
21.333	0.00	0.02	0.009	O	|	|	|	0.37
21.417	0.00	0.02	0.009	O	|	|	|	0.37
21.500	0.00	0.02	0.009	O	|	|	|	0.36
21.583	0.00	0.02	0.009	O	|	|	|	0.36
21.667	0.00	0.02	0.009	O	|	|	|	0.35
21.750	0.00	0.02	0.008	O	|	|	|	0.35
21.833	0.00	0.02	0.008	O	|	|	|	0.35
21.917	0.00	0.02	0.008	O	|	|	|	0.34
22.000	0.00	0.02	0.008	O	|	|	|	0.34
22.083	0.00	0.01	0.008	O	|	|	|	0.33
22.167	0.00	0.01	0.008	O	|	|	|	0.33
22.250	0.00	0.01	0.008	O	|	|	|	0.32
22.333	0.00	0.01	0.008	O	|	|	|	0.32
22.417	0.00	0.01	0.008	O	|	|	|	0.32
22.500	0.00	0.01	0.007	O	|	|	|	0.31
22.583	0.00	0.01	0.007	O	|	|	|	0.31
22.667	0.00	0.01	0.007	O	|	|	|	0.30
22.750	0.00	0.01	0.007	O	|	|	|	0.30
22.833	0.00	0.01	0.007	O	|	|	|	0.30
22.917	0.00	0.01	0.007	O	|	|	|	0.29
23.000	0.00	0.01	0.007	O	|	|	|	0.29
23.083	0.00	0.01	0.007	O	|	|	|	0.28
23.167	0.00	0.01	0.007	O	|	|	|	0.28

23.250	0.00	0.01	0.007	O	|	|	|	0.28
23.333	0.00	0.01	0.007	O	|	|	|	0.27
23.417	0.00	0.01	0.006	O	|	|	|	0.27
23.500	0.00	0.01	0.006	O	|	|	|	0.27
23.583	0.00	0.01	0.006	O	|	|	|	0.26
23.667	0.00	0.01	0.006	O	|	|	|	0.26
23.750	0.00	0.01	0.006	O	|	|	|	0.26
23.833	0.00	0.01	0.006	O	|	|	|	0.25
23.917	0.00	0.01	0.006	O	|	|	|	0.25
24.000	0.00	0.01	0.006	O	|	|	|	0.25
24.083	0.00	0.01	0.006	O	|	|	|	0.24
24.167	0.00	0.01	0.006	O	|	|	|	0.24
24.250	0.00	0.01	0.006	O	|	|	|	0.24
24.333	0.00	0.01	0.006	O	|	|	|	0.23
24.417	0.00	0.01	0.006	O	|	|	|	0.23
24.500	0.00	0.01	0.005	O	|	|	|	0.23
24.583	0.00	0.01	0.005	O	|	|	|	0.23
24.667	0.00	0.01	0.005	O	|	|	|	0.22
24.750	0.00	0.01	0.005	O	|	|	|	0.22
24.833	0.00	0.01	0.005	O	|	|	|	0.22
24.917	0.00	0.01	0.005	O	|	|	|	0.21
25.000	0.00	0.01	0.005	O	|	|	|	0.21
25.083	0.00	0.01	0.005	O	|	|	|	0.21
25.167	0.00	0.01	0.005	O	|	|	|	0.21
25.250	0.00	0.01	0.005	O	|	|	|	0.20
25.333	0.00	0.01	0.005	O	|	|	|	0.20
25.417	0.00	0.01	0.005	O	|	|	|	0.20
25.500	0.00	0.01	0.005	O	|	|	|	0.20
25.583	0.00	0.01	0.005	O	|	|	|	0.19
25.667	0.00	0.01	0.005	O	|	|	|	0.19
25.750	0.00	0.01	0.005	O	|	|	|	0.19
25.833	0.00	0.01	0.004	O	|	|	|	0.19
25.917	0.00	0.01	0.004	O	|	|	|	0.18
26.000	0.00	0.01	0.004	O	|	|	|	0.18
26.083	0.00	0.01	0.004	O	|	|	|	0.18
26.167	0.00	0.01	0.004	O	|	|	|	0.18
26.250	0.00	0.01	0.004	O	|	|	|	0.17
26.333	0.00	0.01	0.004	O	|	|	|	0.17
26.417	0.00	0.01	0.004	O	|	|	|	0.17
26.500	0.00	0.01	0.004	O	|	|	|	0.17
26.583	0.00	0.01	0.004	O	|	|	|	0.17
26.667	0.00	0.01	0.004	O	|	|	|	0.16
26.750	0.00	0.01	0.004	O	|	|	|	0.16
26.833	0.00	0.01	0.004	O	|	|	|	0.16
26.917	0.00	0.01	0.004	O	|	|	|	0.16
27.000	0.00	0.01	0.004	O	|	|	|	0.16
27.083	0.00	0.01	0.004	O	|	|	|	0.15
27.167	0.00	0.01	0.004	O	|	|	|	0.15
27.250	0.00	0.01	0.004	O	|	|	|	0.15
27.333	0.00	0.01	0.004	O	|	|	|	0.15

27.417	0.00	0.01	0.003	O	|	|	|	0.15
27.500	0.00	0.01	0.003	O	|	|	|	0.14
27.583	0.00	0.01	0.003	O	|	|	|	0.14
27.667	0.00	0.01	0.003	O	|	|	|	0.14
27.750	0.00	0.01	0.003	O	|	|	|	0.14
27.833	0.00	0.01	0.003	O	|	|	|	0.14
27.917	0.00	0.01	0.003	O	|	|	|	0.13
28.000	0.00	0.01	0.003	O	|	|	|	0.13
28.083	0.00	0.01	0.003	O	|	|	|	0.13
28.167	0.00	0.01	0.003	O	|	|	|	0.13
28.250	0.00	0.01	0.003	O	|	|	|	0.13
28.333	0.00	0.01	0.003	O	|	|	|	0.13
28.417	0.00	0.01	0.003	O	|	|	|	0.12
28.500	0.00	0.01	0.003	O	|	|	|	0.12
28.583	0.00	0.01	0.003	O	|	|	|	0.12
28.667	0.00	0.01	0.003	O	|	|	|	0.12
28.750	0.00	0.01	0.003	O	|	|	|	0.12
28.833	0.00	0.01	0.003	O	|	|	|	0.12
28.917	0.00	0.01	0.003	O	|	|	|	0.12
29.000	0.00	0.01	0.003	O	|	|	|	0.11
29.083	0.00	0.01	0.003	O	|	|	|	0.11
29.167	0.00	0.00	0.003	O	|	|	|	0.11
29.250	0.00	0.00	0.003	O	|	|	|	0.11
29.333	0.00	0.00	0.003	O	|	|	|	0.11
29.417	0.00	0.00	0.003	O	|	|	|	0.11
29.500	0.00	0.00	0.003	O	|	|	|	0.11
29.583	0.00	0.00	0.002	O	|	|	|	0.10
29.667	0.00	0.00	0.002	O	|	|	|	0.10
29.750	0.00	0.00	0.002	O	|	|	|	0.10
29.833	0.00	0.00	0.002	O	|	|	|	0.10
29.917	0.00	0.00	0.002	O	|	|	|	0.10
30.000	0.00	0.00	0.002	O	|	|	|	0.10
30.083	0.00	0.00	0.002	O	|	|	|	0.10
30.167	0.00	0.00	0.002	O	|	|	|	0.10
30.250	0.00	0.00	0.002	O	|	|	|	0.09
30.333	0.00	0.00	0.002	O	|	|	|	0.09
30.417	0.00	0.00	0.002	O	|	|	|	0.09
30.500	0.00	0.00	0.002	O	|	|	|	0.09
30.583	0.00	0.00	0.002	O	|	|	|	0.09
30.667	0.00	0.00	0.002	O	|	|	|	0.09
30.750	0.00	0.00	0.002	O	|	|	|	0.09
30.833	0.00	0.00	0.002	O	|	|	|	0.09
30.917	0.00	0.00	0.002	O	|	|	|	0.08
31.000	0.00	0.00	0.002	O	|	|	|	0.08
31.083	0.00	0.00	0.002	O	|	|	|	0.08
31.167	0.00	0.00	0.002	O	|	|	|	0.08
31.250	0.00	0.00	0.002	O	|	|	|	0.08
31.333	0.00	0.00	0.002	O	|	|	|	0.08
31.417	0.00	0.00	0.002	O	|	|	|	0.08
31.500	0.00	0.00	0.002	O	|	|	|	0.08

31.583	0.00	0.00	0.002	O	|	|	|	0.08
31.667	0.00	0.00	0.002	O	|	|	|	0.08
31.750	0.00	0.00	0.002	O	|	|	|	0.07
31.833	0.00	0.00	0.002	O	|	|	|	0.07
31.917	0.00	0.00	0.002	O	|	|	|	0.07
32.000	0.00	0.00	0.002	O	|	|	|	0.07
32.083	0.00	0.00	0.002	O	|	|	|	0.07
32.167	0.00	0.00	0.002	O	|	|	|	0.07
32.250	0.00	0.00	0.002	O	|	|	|	0.07
32.333	0.00	0.00	0.002	O	|	|	|	0.07
32.417	0.00	0.00	0.002	O	|	|	|	0.07
32.500	0.00	0.00	0.002	O	|	|	|	0.07
32.583	0.00	0.00	0.002	O	|	|	|	0.07
32.667	0.00	0.00	0.002	O	|	|	|	0.06
32.750	0.00	0.00	0.002	O	|	|	|	0.06
32.833	0.00	0.00	0.002	O	|	|	|	0.06
32.917	0.00	0.00	0.001	O	|	|	|	0.06
33.000	0.00	0.00	0.001	O	|	|	|	0.06
33.083	0.00	0.00	0.001	O	|	|	|	0.06
33.167	0.00	0.00	0.001	O	|	|	|	0.06
33.250	0.00	0.00	0.001	O	|	|	|	0.06
33.333	0.00	0.00	0.001	O	|	|	|	0.06
33.417	0.00	0.00	0.001	O	|	|	|	0.06
33.500	0.00	0.00	0.001	O	|	|	|	0.06
33.583	0.00	0.00	0.001	O	|	|	|	0.06
33.667	0.00	0.00	0.001	O	|	|	|	0.06
33.750	0.00	0.00	0.001	O	|	|	|	0.05
33.833	0.00	0.00	0.001	O	|	|	|	0.05
33.917	0.00	0.00	0.001	O	|	|	|	0.05
34.000	0.00	0.00	0.001	O	|	|	|	0.05
34.083	0.00	0.00	0.001	O	|	|	|	0.05
34.167	0.00	0.00	0.001	O	|	|	|	0.05
34.250	0.00	0.00	0.001	O	|	|	|	0.05
34.333	0.00	0.00	0.001	O	|	|	|	0.05
34.417	0.00	0.00	0.001	O	|	|	|	0.05
34.500	0.00	0.00	0.001	O	|	|	|	0.05
34.583	0.00	0.00	0.001	O	|	|	|	0.05
34.667	0.00	0.00	0.001	O	|	|	|	0.05
34.750	0.00	0.00	0.001	O	|	|	|	0.05
34.833	0.00	0.00	0.001	O	|	|	|	0.05
34.917	0.00	0.00	0.001	O	|	|	|	0.05
35.000	0.00	0.00	0.001	O	|	|	|	0.04
35.083	0.00	0.00	0.001	O	|	|	|	0.04
35.167	0.00	0.00	0.001	O	|	|	|	0.04
35.250	0.00	0.00	0.001	O	|	|	|	0.04
35.333	0.00	0.00	0.001	O	|	|	|	0.04
35.417	0.00	0.00	0.001	O	|	|	|	0.04
35.500	0.00	0.00	0.001	O	|	|	|	0.04
35.583	0.00	0.00	0.001	O	|	|	|	0.04
35.667	0.00	0.00	0.001	O	|	|	|	0.04

35.750	0.00	0.00	0.001	O	|	|	|	0.04
35.833	0.00	0.00	0.001	O	|	|	|	0.04
35.917	0.00	0.00	0.001	O	|	|	|	0.04
36.000	0.00	0.00	0.001	O	|	|	|	0.04
36.083	0.00	0.00	0.001	O	|	|	|	0.04
36.167	0.00	0.00	0.001	O	|	|	|	0.04
36.250	0.00	0.00	0.001	O	|	|	|	0.04
36.333	0.00	0.00	0.001	O	|	|	|	0.04
36.417	0.00	0.00	0.001	O	|	|	|	0.04
36.500	0.00	0.00	0.001	O	|	|	|	0.04
36.583	0.00	0.00	0.001	O	|	|	|	0.04
36.667	0.00	0.00	0.001	O	|	|	|	0.03
36.750	0.00	0.00	0.001	O	|	|	|	0.03
36.833	0.00	0.00	0.001	O	|	|	|	0.03
36.917	0.00	0.00	0.001	O	|	|	|	0.03
37.000	0.00	0.00	0.001	O	|	|	|	0.03
37.083	0.00	0.00	0.001	O	|	|	|	0.03
37.167	0.00	0.00	0.001	O	|	|	|	0.03
37.250	0.00	0.00	0.001	O	|	|	|	0.03
37.333	0.00	0.00	0.001	O	|	|	|	0.03
37.417	0.00	0.00	0.001	O	|	|	|	0.03
37.500	0.00	0.00	0.001	O	|	|	|	0.03
37.583	0.00	0.00	0.001	O	|	|	|	0.03
37.667	0.00	0.00	0.001	O	|	|	|	0.03
37.750	0.00	0.00	0.001	O	|	|	|	0.03
37.833	0.00	0.00	0.001	O	|	|	|	0.03
37.917	0.00	0.00	0.001	O	|	|	|	0.03
38.000	0.00	0.00	0.001	O	|	|	|	0.03
38.083	0.00	0.00	0.001	O	|	|	|	0.03
38.167	0.00	0.00	0.001	O	|	|	|	0.03
38.250	0.00	0.00	0.001	O	|	|	|	0.03
38.333	0.00	0.00	0.001	O	|	|	|	0.03
38.417	0.00	0.00	0.001	O	|	|	|	0.03
38.500	0.00	0.00	0.001	O	|	|	|	0.03
38.583	0.00	0.00	0.001	O	|	|	|	0.03
38.667	0.00	0.00	0.001	O	|	|	|	0.03
38.750	0.00	0.00	0.001	O	|	|	|	0.03
38.833	0.00	0.00	0.001	O	|	|	|	0.02
38.917	0.00	0.00	0.001	O	|	|	|	0.02
39.000	0.00	0.00	0.001	O	|	|	|	0.02
39.083	0.00	0.00	0.001	O	|	|	|	0.02
39.167	0.00	0.00	0.001	O	|	|	|	0.02
39.250	0.00	0.00	0.001	O	|	|	|	0.02
39.333	0.00	0.00	0.001	O	|	|	|	0.02
39.417	0.00	0.00	0.001	O	|	|	|	0.02
39.500	0.00	0.00	0.001	O	|	|	|	0.02
39.583	0.00	0.00	0.001	O	|	|	|	0.02

**********HYDROGRAPH DATA**********

Number of intervals = 475

```
                Time interval =    5.0 (Min.)
                Maximum/Peak flow rate =        0.045 (CFS)
                Total volume =       0.078 (Ac.Ft)
        Status of hydrographs being held in storage
                    Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
        Peak (CFS)      0.000     0.000     0.000     0.000     0.000
        Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
****************************************************************************

----------------------------------------------------------------------
```

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
5 yr
3 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris35.rte
**********HYDROGRAPH DATA**********
Number of intervals = 44
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.322 (CFS)
Total volume = 0.126 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 44
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.3 0.66 0.99 1.32	Depth (Ft.)
0.083	0.04	0.00	0.000	OI | | | |	0.01
0.167	0.16	0.00	0.001	O I | | | |	0.03
0.250	0.19	0.00	0.002	O I | | | |	0.08
0.333	0.20	0.01	0.003	O I | | | |	0.14
0.417	0.24	0.01	0.005	O I | | | |	0.20
0.500	0.26	0.01	0.006	O I | | | |	0.27
0.583	0.29	0.02	0.008	O I | | | |	0.34
0.667	0.29	0.02	0.010	O I | | | |	0.42
0.750	0.31	0.02	0.012	O I| | | |	0.50
0.833	0.31	0.03	0.014	O I| | | |	0.58
0.917	0.29	0.03	0.016	O I | | | |	0.66
1.000	0.30	0.03	0.018	O I| | | |	0.73
1.083	0.33	0.04	0.020	O I| | | |	0.81
1.167	0.37	0.04	0.022	O I | | |	0.90
1.250	0.38	0.04	0.024	|O |I | | |	1.00
1.333	0.38	0.04	0.026	|O |I | | |	1.06
1.417	0.39	0.04	0.029	|O |I | | |	1.12
1.500	0.44	0.04	0.031	|O | I | | |	1.18
1.583	0.46	0.04	0.034	|O | I | | |	1.25
1.667	0.45	0.04	0.037	|O | I | | |	1.32
1.750	0.49	0.04	0.040	|O | I | | |	1.39
1.833	0.55	0.04	0.043	|O | I | | |	1.47
1.917	0.54	0.04	0.046	|O | I | | |	1.56
2.000	0.53	0.04	0.050	|O | I | | |	1.65
2.083	0.54	0.04	0.053	|O | I | | |	1.73
2.167	0.59	0.04	0.057	|O | I | | |	1.82
2.250	0.72	0.04	0.061	|O | |I | |	1.93
2.333	0.77	0.04	0.066	|O | | I | |	2.05

```
2.417    0.79    0.04      0.071  |O      |        |  I    |        |     2.17
2.500    1.07    0.04      0.077  |O      |        |       | I      |     2.33
2.583    1.25    0.04      0.085  |O      |        |       |     I  |     2.52
2.667    1.32    0.04      0.093  |O      |        |       |       I|     2.73
2.750    1.03    0.04      0.101  |O      |        |       I        |     2.93
2.833    0.64    0.04      0.106  |O      |       I|       |        |     3.06
2.917    0.49    0.04      0.110  |O      |  I     |       |        |     3.15
3.000    0.38    0.04      0.113  |O     |I       |       |        |     3.22
3.083    0.22    0.04      0.115  |O   I  |        |       |        |     3.26
3.167    0.11    0.04      0.115  |OI     |        |       |        |     3.28
3.250    0.06    0.04      0.116  |O      |        |       |        |     3.29
3.333    0.03    0.04      0.116  IO      |        |       |        |     3.29
3.417    0.02    0.04      0.116  IO      |        |       |        |     3.29
3.500    0.01    0.04      0.115  IO      |        |       |        |     3.28
3.583    0.00    0.04      0.115  IO      |        |       |        |     3.28
3.667    0.00    0.04      0.115  IO      |        |       |        |     3.27
3.750    0.00    0.04      0.114  IO      |        |       |        |     3.26
3.833    0.00    0.04      0.114  IO      |        |       |        |     3.25
3.917    0.00    0.04      0.114  IO      |        |       |        |     3.24
4.000    0.00    0.04      0.113  IO      |        |       |        |     3.24
4.083    0.00    0.04      0.113  IO      |        |       |        |     3.23
4.167    0.00    0.04      0.113  IO      |        |       |        |     3.22
4.250    0.00    0.04      0.113  IO      |        |       |        |     3.21
4.333    0.00    0.04      0.112  IO      |        |       |        |     3.21
4.417    0.00    0.04      0.112  IO      |        |       |        |     3.20
4.500    0.00    0.04      0.112  IO      |        |       |        |     3.19
4.583    0.00    0.04      0.111  IO      |        |       |        |     3.18
4.667    0.00    0.04      0.111  IO      |        |       |        |     3.18
4.750    0.00    0.04      0.111  IO      |        |       |        |     3.17
4.833    0.00    0.04      0.110  IO      |        |       |        |     3.16
4.917    0.00    0.04      0.110  IO      |        |       |        |     3.15
5.000    0.00    0.04      0.110  IO      |        |       |        |     3.14
5.083    0.00    0.04      0.109  IO      |        |       |        |     3.14
5.167    0.00    0.04      0.109  IO      |        |       |        |     3.13
5.250    0.00    0.04      0.109  IO      |        |       |        |     3.12
5.333    0.00    0.04      0.109  IO      |        |       |        |     3.11
5.417    0.00    0.04      0.108  IO      |        |       |        |     3.11
5.500    0.00    0.04      0.108  IO      |        |       |        |     3.10
5.583    0.00    0.04      0.108  IO      |        |       |        |     3.09
5.667    0.00    0.04      0.107  IO      |        |       |        |     3.08
5.750    0.00    0.04      0.107  IO      |        |       |        |     3.07
5.833    0.00    0.04      0.107  IO      |        |       |        |     3.07
5.917    0.00    0.04      0.106  IO      |        |       |        |     3.06
6.000    0.00    0.04      0.106  IO      |        |       |        |     3.05
6.083    0.00    0.04      0.106  IO      |        |       |        |     3.04
6.167    0.00    0.04      0.105  IO      |        |       |        |     3.04
6.250    0.00    0.04      0.105  IO      |        |       |        |     3.03
6.333    0.00    0.04      0.105  IO      |        |       |        |     3.02
6.417    0.00    0.04      0.104  IO      |        |       |        |     3.01
6.500    0.00    0.04      0.104  IO      |        |       |        |     3.00
```

6.583	0.00	0.04	0.104	IO				3.00
6.667	0.00	0.04	0.104	IO				2.99
6.750	0.00	0.04	0.103	IO				2.98
6.833	0.00	0.04	0.103	IO				2.97
6.917	0.00	0.04	0.103	IO				2.97
7.000	0.00	0.04	0.102	IO				2.96
7.083	0.00	0.04	0.102	IO				2.95
7.167	0.00	0.04	0.102	IO				2.94
7.250	0.00	0.04	0.101	IO				2.93
7.333	0.00	0.04	0.101	IO				2.93
7.417	0.00	0.04	0.101	IO				2.92
7.500	0.00	0.04	0.100	IO				2.91
7.583	0.00	0.04	0.100	IO				2.90
7.667	0.00	0.04	0.100	IO				2.90
7.750	0.00	0.04	0.100	IO				2.89
7.833	0.00	0.04	0.099	IO				2.88
7.917	0.00	0.04	0.099	IO				2.87
8.000	0.00	0.04	0.099	IO				2.87
8.083	0.00	0.04	0.098	IO				2.86
8.167	0.00	0.04	0.098	IO				2.85
8.250	0.00	0.04	0.098	IO				2.84
8.333	0.00	0.04	0.097	IO				2.83
8.417	0.00	0.04	0.097	IO				2.83
8.500	0.00	0.04	0.097	IO				2.82
8.583	0.00	0.04	0.096	IO				2.81
8.667	0.00	0.04	0.096	IO				2.80
8.750	0.00	0.04	0.096	IO				2.80
8.833	0.00	0.04	0.096	IO				2.79
8.917	0.00	0.04	0.095	IO				2.78
9.000	0.00	0.04	0.095	IO				2.77
9.083	0.00	0.04	0.095	IO				2.76
9.167	0.00	0.04	0.094	IO				2.76
9.250	0.00	0.04	0.094	IO				2.75
9.333	0.00	0.04	0.094	IO				2.74
9.417	0.00	0.04	0.093	IO				2.73
9.500	0.00	0.04	0.093	IO				2.73
9.583	0.00	0.04	0.093	IO				2.72
9.667	0.00	0.04	0.092	IO				2.71
9.750	0.00	0.04	0.092	IO				2.70
9.833	0.00	0.04	0.092	IO				2.69
9.917	0.00	0.04	0.091	IO				2.69
10.000	0.00	0.04	0.091	IO				2.68
10.083	0.00	0.04	0.091	IO				2.67
10.167	0.00	0.04	0.091	IO				2.66
10.250	0.00	0.04	0.090	IO				2.66
10.333	0.00	0.04	0.090	IO				2.65
10.417	0.00	0.04	0.090	IO				2.64
10.500	0.00	0.04	0.089	IO				2.63
10.583	0.00	0.04	0.089	IO				2.63
10.667	0.00	0.04	0.089	IO				2.62

10.750	0.00	0.04	0.088	IO				2.61
10.833	0.00	0.04	0.088	IO				2.60
10.917	0.00	0.04	0.088	IO				2.59
11.000	0.00	0.04	0.087	IO				2.59
11.083	0.00	0.04	0.087	IO				2.58
11.167	0.00	0.04	0.087	IO				2.57
11.250	0.00	0.04	0.087	IO				2.56
11.333	0.00	0.04	0.086	IO				2.56
11.417	0.00	0.04	0.086	IO				2.55
11.500	0.00	0.04	0.086	IO				2.54
11.583	0.00	0.04	0.085	IO				2.53
11.667	0.00	0.04	0.085	IO				2.52
11.750	0.00	0.04	0.085	IO				2.52
11.833	0.00	0.04	0.084	IO				2.51
11.917	0.00	0.04	0.084	IO				2.50
12.000	0.00	0.04	0.084	IO				2.49
12.083	0.00	0.04	0.083	IO				2.49
12.167	0.00	0.04	0.083	IO				2.48
12.250	0.00	0.04	0.083	IO				2.47
12.333	0.00	0.04	0.082	IO				2.46
12.417	0.00	0.04	0.082	IO				2.45
12.500	0.00	0.04	0.082	IO				2.45
12.583	0.00	0.04	0.082	IO				2.44
12.667	0.00	0.04	0.081	IO				2.43
12.750	0.00	0.04	0.081	IO				2.42
12.833	0.00	0.04	0.081	IO				2.42
12.917	0.00	0.04	0.080	IO				2.41
13.000	0.00	0.04	0.080	IO				2.40
13.083	0.00	0.04	0.080	IO				2.39
13.167	0.00	0.04	0.079	IO				2.38
13.250	0.00	0.04	0.079	IO				2.38
13.333	0.00	0.04	0.079	IO				2.37
13.417	0.00	0.04	0.078	IO				2.36
13.500	0.00	0.04	0.078	IO				2.35
13.583	0.00	0.04	0.078	IO				2.35
13.667	0.00	0.04	0.078	IO				2.34
13.750	0.00	0.04	0.077	IO				2.33
13.833	0.00	0.04	0.077	IO				2.32
13.917	0.00	0.04	0.077	IO				2.32
14.000	0.00	0.04	0.076	IO				2.31
14.083	0.00	0.04	0.076	IO				2.30
14.167	0.00	0.04	0.076	IO				2.29
14.250	0.00	0.04	0.075	IO				2.28
14.333	0.00	0.04	0.075	IO				2.28
14.417	0.00	0.04	0.075	IO				2.27
14.500	0.00	0.04	0.074	IO				2.26
14.583	0.00	0.04	0.074	IO				2.25
14.667	0.00	0.04	0.074	IO				2.25
14.750	0.00	0.04	0.074	IO				2.24
14.833	0.00	0.04	0.073	IO				2.23

14.917	0.00	0.04	0.073	IO				2.22
15.000	0.00	0.04	0.073	IO				2.21
15.083	0.00	0.04	0.072	IO				2.21
15.167	0.00	0.04	0.072	IO				2.20
15.250	0.00	0.04	0.072	IO				2.19
15.333	0.00	0.04	0.071	IO				2.18
15.417	0.00	0.04	0.071	IO				2.18
15.500	0.00	0.04	0.071	IO				2.17
15.583	0.00	0.04	0.070	IO				2.16
15.667	0.00	0.04	0.070	IO				2.15
15.750	0.00	0.04	0.070	IO				2.14
15.833	0.00	0.04	0.069	IO				2.14
15.917	0.00	0.04	0.069	IO				2.13
16.000	0.00	0.04	0.069	IO				2.12
16.083	0.00	0.04	0.069	IO				2.11
16.167	0.00	0.04	0.068	IO				2.11
16.250	0.00	0.04	0.068	IO				2.10
16.333	0.00	0.04	0.068	IO				2.09
16.417	0.00	0.04	0.067	IO				2.08
16.500	0.00	0.04	0.067	IO				2.07
16.583	0.00	0.04	0.067	IO				2.07
16.667	0.00	0.04	0.066	IO				2.06
16.750	0.00	0.04	0.066	IO				2.05
16.833	0.00	0.04	0.066	IO				2.04
16.917	0.00	0.04	0.065	IO				2.04
17.000	0.00	0.04	0.065	IO				2.03
17.083	0.00	0.04	0.065	IO				2.02
17.167	0.00	0.04	0.065	IO				2.01
17.250	0.00	0.04	0.064	IO				2.01
17.333	0.00	0.04	0.064	IO				2.00
17.417	0.00	0.04	0.064	IO				1.99
17.500	0.00	0.04	0.063	IO				1.98
17.583	0.00	0.04	0.063	IO				1.97
17.667	0.00	0.04	0.063	IO				1.97
17.750	0.00	0.04	0.062	IO				1.96
17.833	0.00	0.04	0.062	IO				1.95
17.917	0.00	0.04	0.062	IO				1.94
18.000	0.00	0.04	0.061	IO				1.94
18.083	0.00	0.04	0.061	IO				1.93
18.167	0.00	0.04	0.061	IO				1.92
18.250	0.00	0.04	0.060	IO				1.91
18.333	0.00	0.04	0.060	IO				1.90
18.417	0.00	0.04	0.060	IO				1.90
18.500	0.00	0.04	0.060	IO				1.89
18.583	0.00	0.04	0.059	IO				1.88
18.667	0.00	0.04	0.059	IO				1.87
18.750	0.00	0.04	0.059	IO				1.87
18.833	0.00	0.04	0.058	IO				1.86
18.917	0.00	0.04	0.058	IO				1.85
19.000	0.00	0.04	0.058	IO				1.84

19.083	0.00	0.04	0.057	IO				1.83
19.167	0.00	0.04	0.057	IO				1.83
19.250	0.00	0.04	0.057	IO				1.82
19.333	0.00	0.04	0.056	IO				1.81
19.417	0.00	0.04	0.056	IO				1.80
19.500	0.00	0.04	0.056	IO				1.80
19.583	0.00	0.04	0.056	IO				1.79
19.667	0.00	0.04	0.055	IO				1.78
19.750	0.00	0.04	0.055	IO				1.77
19.833	0.00	0.04	0.055	IO				1.77
19.917	0.00	0.04	0.054	IO				1.76
20.000	0.00	0.04	0.054	IO				1.75
20.083	0.00	0.04	0.054	IO				1.74
20.167	0.00	0.04	0.053	IO				1.73
20.250	0.00	0.04	0.053	IO				1.73
20.333	0.00	0.04	0.053	IO				1.72
20.417	0.00	0.04	0.052	IO				1.71
20.500	0.00	0.04	0.052	IO				1.70
20.583	0.00	0.04	0.052	IO				1.70
20.667	0.00	0.04	0.052	IO				1.69
20.750	0.00	0.04	0.051	IO				1.68
20.833	0.00	0.04	0.051	IO				1.67
20.917	0.00	0.04	0.051	IO				1.66
21.000	0.00	0.04	0.050	IO				1.66
21.083	0.00	0.04	0.050	IO				1.65
21.167	0.00	0.04	0.050	IO				1.64
21.250	0.00	0.04	0.049	IO				1.63
21.333	0.00	0.04	0.049	IO				1.63
21.417	0.00	0.04	0.049	IO				1.62
21.500	0.00	0.04	0.048	IO				1.61
21.583	0.00	0.04	0.048	IO				1.60
21.667	0.00	0.04	0.048	IO				1.59
21.750	0.00	0.04	0.047	IO				1.59
21.833	0.00	0.04	0.047	IO				1.58
21.917	0.00	0.04	0.047	IO				1.57
22.000	0.00	0.04	0.047	IO				1.56
22.083	0.00	0.04	0.046	IO				1.56
22.167	0.00	0.04	0.046	IO				1.55
22.250	0.00	0.04	0.046	IO				1.54
22.333	0.00	0.04	0.045	IO				1.53
22.417	0.00	0.04	0.045	IO				1.52
22.500	0.00	0.04	0.045	IO				1.52
22.583	0.00	0.04	0.044	IO				1.51
22.667	0.00	0.04	0.044	IO				1.50
22.750	0.00	0.04	0.044	IO				1.49
22.833	0.00	0.04	0.043	IO				1.49
22.917	0.00	0.04	0.043	IO				1.48
23.000	0.00	0.04	0.043	IO				1.47
23.083	0.00	0.04	0.043	IO				1.46
23.167	0.00	0.04	0.042	IO				1.46

23.250	0.00	0.04	0.042	IO				1.45
23.333	0.00	0.04	0.042	IO				1.44
23.417	0.00	0.04	0.041	IO				1.43
23.500	0.00	0.04	0.041	IO				1.42
23.583	0.00	0.04	0.041	IO				1.42
23.667	0.00	0.04	0.040	IO				1.41
23.750	0.00	0.04	0.040	IO				1.40
23.833	0.00	0.04	0.040	IO				1.39
23.917	0.00	0.04	0.039	IO				1.39
24.000	0.00	0.04	0.039	IO				1.38
24.083	0.00	0.04	0.039	IO				1.37
24.167	0.00	0.04	0.038	IO				1.36
24.250	0.00	0.04	0.038	IO				1.35
24.333	0.00	0.04	0.038	IO				1.35
24.417	0.00	0.04	0.038	IO				1.34
24.500	0.00	0.04	0.037	IO				1.33
24.583	0.00	0.04	0.037	IO				1.32
24.667	0.00	0.04	0.037	IO				1.32
24.750	0.00	0.04	0.036	IO				1.31
24.833	0.00	0.04	0.036	IO				1.30
24.917	0.00	0.04	0.036	IO				1.29
25.000	0.00	0.04	0.035	IO				1.28
25.083	0.00	0.04	0.035	IO				1.28
25.167	0.00	0.04	0.035	IO				1.27
25.250	0.00	0.04	0.034	IO				1.26
25.333	0.00	0.04	0.034	IO				1.25
25.417	0.00	0.04	0.034	IO				1.25
25.500	0.00	0.04	0.034	IO				1.24
25.583	0.00	0.04	0.033	IO				1.23
25.667	0.00	0.04	0.033	IO				1.22
25.750	0.00	0.04	0.033	IO				1.21
25.833	0.00	0.04	0.032	IO				1.21
25.917	0.00	0.04	0.032	IO				1.20
26.000	0.00	0.04	0.032	IO				1.19
26.083	0.00	0.04	0.031	IO				1.18
26.167	0.00	0.04	0.031	IO				1.18
26.250	0.00	0.04	0.031	IO				1.17
26.333	0.00	0.04	0.030	IO				1.16
26.417	0.00	0.04	0.030	IO				1.15
26.500	0.00	0.04	0.030	IO				1.15
26.583	0.00	0.04	0.029	IO				1.14
26.667	0.00	0.04	0.029	IO				1.13
26.750	0.00	0.04	0.029	IO				1.12
26.833	0.00	0.04	0.029	IO				1.11
26.917	0.00	0.04	0.028	IO				1.11
27.000	0.00	0.04	0.028	IO				1.10
27.083	0.00	0.04	0.028	IO				1.09
27.167	0.00	0.04	0.027	IO				1.08
27.250	0.00	0.04	0.027	IO				1.08
27.333	0.00	0.04	0.027	IO				1.07

27.417	0.00	0.04	0.026	IO				1.06
27.500	0.00	0.04	0.026	IO				1.05
27.583	0.00	0.04	0.026	IO				1.04
27.667	0.00	0.04	0.025	IO				1.04
27.750	0.00	0.04	0.025	IO				1.03
27.833	0.00	0.04	0.025	IO				1.02
27.917	0.00	0.04	0.025	IO				1.01
28.000	0.00	0.04	0.024	IO				1.01
28.083	0.00	0.04	0.024	IO				1.00
28.167	0.00	0.04	0.024	IO				0.98
28.250	0.00	0.04	0.023	IO				0.97
28.333	0.00	0.04	0.023	IO				0.96
28.417	0.00	0.04	0.023	IO				0.95
28.500	0.00	0.04	0.022	IO				0.93
28.583	0.00	0.04	0.022	IO				0.92
28.667	0.00	0.04	0.022	O				0.91
28.750	0.00	0.04	0.022	O				0.90
28.833	0.00	0.04	0.021	O				0.89
28.917	0.00	0.04	0.021	O				0.88
29.000	0.00	0.04	0.021	O				0.86
29.083	0.00	0.04	0.020	O				0.85
29.167	0.00	0.04	0.020	O				0.84
29.250	0.00	0.04	0.020	O				0.83
29.333	0.00	0.04	0.020	O				0.82
29.417	0.00	0.04	0.019	O				0.81
29.500	0.00	0.04	0.019	O				0.80
29.583	0.00	0.04	0.019	O				0.79
29.667	0.00	0.04	0.019	O				0.78
29.750	0.00	0.03	0.018	O				0.77
29.833	0.00	0.03	0.018	O				0.76
29.917	0.00	0.03	0.018	O				0.75
30.000	0.00	0.03	0.018	O				0.74
30.083	0.00	0.03	0.018	O				0.73
30.167	0.00	0.03	0.017	O				0.72
30.250	0.00	0.03	0.017	O				0.71
30.333	0.00	0.03	0.017	O				0.70
30.417	0.00	0.03	0.017	O				0.69
30.500	0.00	0.03	0.016	O				0.69
30.583	0.00	0.03	0.016	O				0.68
30.667	0.00	0.03	0.016	O				0.67
30.750	0.00	0.03	0.016	O				0.66
30.833	0.00	0.03	0.016	O				0.65
30.917	0.00	0.03	0.015	O				0.64
31.000	0.00	0.03	0.015	O				0.63
31.083	0.00	0.03	0.015	O				0.63
31.167	0.00	0.03	0.015	O				0.62
31.250	0.00	0.03	0.015	O				0.61
31.333	0.00	0.03	0.014	O				0.60
31.417	0.00	0.03	0.014	O				0.59
31.500	0.00	0.03	0.014	O				0.59

31.583	0.00	0.03	0.014	O	|	|	|	0.58
31.667	0.00	0.03	0.014	O	|	|	|	0.57
31.750	0.00	0.03	0.014	O	|	|	|	0.56
31.833	0.00	0.03	0.013	O	|	|	|	0.56
31.917	0.00	0.02	0.013	O	|	|	|	0.55
32.000	0.00	0.02	0.013	O	|	|	|	0.54
32.083	0.00	0.02	0.013	O	|	|	|	0.54
32.167	0.00	0.02	0.013	O	|	|	|	0.53
32.250	0.00	0.02	0.013	O	|	|	|	0.52
32.333	0.00	0.02	0.012	O	|	|	|	0.52
32.417	0.00	0.02	0.012	O	|	|	|	0.51
32.500	0.00	0.02	0.012	O	|	|	|	0.50
32.583	0.00	0.02	0.012	O	|	|	|	0.50
32.667	0.00	0.02	0.012	O	|	|	|	0.49
32.750	0.00	0.02	0.012	O	|	|	|	0.48
32.833	0.00	0.02	0.011	O	|	|	|	0.48
32.917	0.00	0.02	0.011	O	|	|	|	0.47
33.000	0.00	0.02	0.011	O	|	|	|	0.47
33.083	0.00	0.02	0.011	O	|	|	|	0.46
33.167	0.00	0.02	0.011	O	|	|	|	0.45
33.250	0.00	0.02	0.011	O	|	|	|	0.45
33.333	0.00	0.02	0.011	O	|	|	|	0.44
33.417	0.00	0.02	0.010	O	|	|	|	0.44
33.500	0.00	0.02	0.010	O	|	|	|	0.43
33.583	0.00	0.02	0.010	O	|	|	|	0.42
33.667	0.00	0.02	0.010	O	|	|	|	0.42
33.750	0.00	0.02	0.010	O	|	|	|	0.41
33.833	0.00	0.02	0.010	O	|	|	|	0.41
33.917	0.00	0.02	0.010	O	|	|	|	0.40
34.000	0.00	0.02	0.010	O	|	|	|	0.40
34.083	0.00	0.02	0.009	O	|	|	|	0.39
34.167	0.00	0.02	0.009	O	|	|	|	0.39
34.250	0.00	0.02	0.009	O	|	|	|	0.38
34.333	0.00	0.02	0.009	O	|	|	|	0.38
34.417	0.00	0.02	0.009	O	|	|	|	0.37
34.500	0.00	0.02	0.009	O	|	|	|	0.37
34.583	0.00	0.02	0.009	O	|	|	|	0.36
34.667	0.00	0.02	0.009	O	|	|	|	0.36
34.750	0.00	0.02	0.009	O	|	|	|	0.35
34.833	0.00	0.02	0.008	O	|	|	|	0.35
34.917	0.00	0.02	0.008	O	|	|	|	0.35
35.000	0.00	0.02	0.008	O	|	|	|	0.34
35.083	0.00	0.02	0.008	O	|	|	|	0.34
35.167	0.00	0.01	0.008	O	|	|	|	0.33
35.250	0.00	0.01	0.008	O	|	|	|	0.33
35.333	0.00	0.01	0.008	O	|	|	|	0.32
35.417	0.00	0.01	0.008	O	|	|	|	0.32
35.500	0.00	0.01	0.008	O	|	|	|	0.32
35.583	0.00	0.01	0.007	O	|	|	|	0.31
35.667	0.00	0.01	0.007	O	|	|	|	0.31

35.750	0.00	0.01	0.007	O	|	|	|	0.30
35.833	0.00	0.01	0.007	O	|	|	|	0.30
35.917	0.00	0.01	0.007	O	|	|	|	0.30
36.000	0.00	0.01	0.007	O	|	|	|	0.29
36.083	0.00	0.01	0.007	O	|	|	|	0.29
36.167	0.00	0.01	0.007	O	|	|	|	0.28
36.250	0.00	0.01	0.007	O	|	|	|	0.28
36.333	0.00	0.01	0.007	O	|	|	|	0.28
36.417	0.00	0.01	0.007	O	|	|	|	0.27
36.500	0.00	0.01	0.006	O	|	|	|	0.27
36.583	0.00	0.01	0.006	O	|	|	|	0.27
36.667	0.00	0.01	0.006	O	|	|	|	0.26
36.750	0.00	0.01	0.006	O	|	|	|	0.26
36.833	0.00	0.01	0.006	O	|	|	|	0.26
36.917	0.00	0.01	0.006	O	|	|	|	0.25
37.000	0.00	0.01	0.006	O	|	|	|	0.25
37.083	0.00	0.01	0.006	O	|	|	|	0.25
37.167	0.00	0.01	0.006	O	|	|	|	0.24
37.250	0.00	0.01	0.006	O	|	|	|	0.24
37.333	0.00	0.01	0.006	O	|	|	|	0.24
37.417	0.00	0.01	0.006	O	|	|	|	0.23
37.500	0.00	0.01	0.006	O	|	|	|	0.23
37.583	0.00	0.01	0.005	O	|	|	|	0.23
37.667	0.00	0.01	0.005	O	|	|	|	0.23
37.750	0.00	0.01	0.005	O	|	|	|	0.22
37.833	0.00	0.01	0.005	O	|	|	|	0.22
37.917	0.00	0.01	0.005	O	|	|	|	0.22
38.000	0.00	0.01	0.005	O	|	|	|	0.21
38.083	0.00	0.01	0.005	O	|	|	|	0.21
38.167	0.00	0.01	0.005	O	|	|	|	0.21
38.250	0.00	0.01	0.005	O	|	|	|	0.21
38.333	0.00	0.01	0.005	O	|	|	|	0.20
38.417	0.00	0.01	0.005	O	|	|	|	0.20
38.500	0.00	0.01	0.005	O	|	|	|	0.20
38.583	0.00	0.01	0.005	O	|	|	|	0.20
38.667	0.00	0.01	0.005	O	|	|	|	0.19
38.750	0.00	0.01	0.005	O	|	|	|	0.19
38.833	0.00	0.01	0.005	O	|	|	|	0.19
38.917	0.00	0.01	0.004	O	|	|	|	0.19
39.000	0.00	0.01	0.004	O	|	|	|	0.18
39.083	0.00	0.01	0.004	O	|	|	|	0.18
39.167	0.00	0.01	0.004	O	|	|	|	0.18
39.250	0.00	0.01	0.004	O	|	|	|	0.18
39.333	0.00	0.01	0.004	O	|	|	|	0.17
39.417	0.00	0.01	0.004	O	|	|	|	0.17
39.500	0.00	0.01	0.004	O	|	|	|	0.17
39.583	0.00	0.01	0.004	O	|	|	|	0.17
39.667	0.00	0.01	0.004	O	|	|	|	0.17
39.750	0.00	0.01	0.004	O	|	|	|	0.16
39.833	0.00	0.01	0.004	O	|	|	|	0.16

39.917	0.00	0.01	0.004	O				0.16
40.000	0.00	0.01	0.004	O				0.16
40.083	0.00	0.01	0.004	O				0.16
40.167	0.00	0.01	0.004	O				0.15
40.250	0.00	0.01	0.004	O				0.15
40.333	0.00	0.01	0.004	O				0.15
40.417	0.00	0.01	0.004	O				0.15
40.500	0.00	0.01	0.003	O				0.15
40.583	0.00	0.01	0.003	O				0.14
40.667	0.00	0.01	0.003	O				0.14
40.750	0.00	0.01	0.003	O				0.14
40.833	0.00	0.01	0.003	O				0.14
40.917	0.00	0.01	0.003	O				0.14
41.000	0.00	0.01	0.003	O				0.13
41.083	0.00	0.01	0.003	O				0.13
41.167	0.00	0.01	0.003	O				0.13
41.250	0.00	0.01	0.003	O				0.13
41.333	0.00	0.01	0.003	O				0.13
41.417	0.00	0.01	0.003	O				0.13
41.500	0.00	0.01	0.003	O				0.12
41.583	0.00	0.01	0.003	O				0.12
41.667	0.00	0.01	0.003	O				0.12
41.750	0.00	0.01	0.003	O				0.12
41.833	0.00	0.01	0.003	O				0.12
41.917	0.00	0.01	0.003	O				0.12
42.000	0.00	0.01	0.003	O				0.12
42.083	0.00	0.01	0.003	O				0.11
42.167	0.00	0.01	0.003	O				0.11
42.250	0.00	0.00	0.003	O				0.11
42.333	0.00	0.00	0.003	O				0.11
42.417	0.00	0.00	0.003	O				0.11
42.500	0.00	0.00	0.003	O				0.11
42.583	0.00	0.00	0.003	O				0.11
42.667	0.00	0.00	0.002	O				0.10
42.750	0.00	0.00	0.002	O				0.10
42.833	0.00	0.00	0.002	O				0.10
42.917	0.00	0.00	0.002	O				0.10
43.000	0.00	0.00	0.002	O				0.10
43.083	0.00	0.00	0.002	O				0.10
43.167	0.00	0.00	0.002	O				0.10
43.250	0.00	0.00	0.002	O				0.10
43.333	0.00	0.00	0.002	O				0.09
43.417	0.00	0.00	0.002	O				0.09
43.500	0.00	0.00	0.002	O				0.09
43.583	0.00	0.00	0.002	O				0.09
43.667	0.00	0.00	0.002	O				0.09
43.750	0.00	0.00	0.002	O				0.09
43.833	0.00	0.00	0.002	O				0.09
43.917	0.00	0.00	0.002	O				0.09
44.000	0.00	0.00	0.002	O				0.08

44.083	0.00	0.00	0.002	O	|	|	|	0.08
44.167	0.00	0.00	0.002	O	|	|	|	0.08
44.250	0.00	0.00	0.002	O	|	|	|	0.08
44.333	0.00	0.00	0.002	O	|	|	|	0.08
44.417	0.00	0.00	0.002	O	|	|	|	0.08
44.500	0.00	0.00	0.002	O	|	|	|	0.08
44.583	0.00	0.00	0.002	O	|	|	|	0.08
44.667	0.00	0.00	0.002	O	|	|	|	0.08
44.750	0.00	0.00	0.002	O	|	|	|	0.08
44.833	0.00	0.00	0.002	O	|	|	|	0.07
44.917	0.00	0.00	0.002	O	|	|	|	0.07
45.000	0.00	0.00	0.002	O	|	|	|	0.07
45.083	0.00	0.00	0.002	O	|	|	|	0.07
45.167	0.00	0.00	0.002	O	|	|	|	0.07
45.250	0.00	0.00	0.002	O	|	|	|	0.07
45.333	0.00	0.00	0.002	O	|	|	|	0.07
45.417	0.00	0.00	0.002	O	|	|	|	0.07
45.500	0.00	0.00	0.002	O	|	|	|	0.07
45.583	0.00	0.00	0.002	O	|	|	|	0.07
45.667	0.00	0.00	0.002	O	|	|	|	0.07
45.750	0.00	0.00	0.002	O	|	|	|	0.06
45.833	0.00	0.00	0.002	O	|	|	|	0.06
45.917	0.00	0.00	0.002	O	|	|	|	0.06
46.000	0.00	0.00	0.001	O	|	|	|	0.06
46.083	0.00	0.00	0.001	O	|	|	|	0.06
46.167	0.00	0.00	0.001	O	|	|	|	0.06
46.250	0.00	0.00	0.001	O	|	|	|	0.06
46.333	0.00	0.00	0.001	O	|	|	|	0.06
46.417	0.00	0.00	0.001	O	|	|	|	0.06
46.500	0.00	0.00	0.001	O	|	|	|	0.06
46.583	0.00	0.00	0.001	O	|	|	|	0.06
46.667	0.00	0.00	0.001	O	|	|	|	0.06
46.750	0.00	0.00	0.001	O	|	|	|	0.06
46.833	0.00	0.00	0.001	O	|	|	|	0.05
46.917	0.00	0.00	0.001	O	|	|	|	0.05
47.000	0.00	0.00	0.001	O	|	|	|	0.05
47.083	0.00	0.00	0.001	O	|	|	|	0.05
47.167	0.00	0.00	0.001	O	|	|	|	0.05
47.250	0.00	0.00	0.001	O	|	|	|	0.05
47.333	0.00	0.00	0.001	O	|	|	|	0.05
47.417	0.00	0.00	0.001	O	|	|	|	0.05
47.500	0.00	0.00	0.001	O	|	|	|	0.05
47.583	0.00	0.00	0.001	O	|	|	|	0.05
47.667	0.00	0.00	0.001	O	|	|	|	0.05
47.750	0.00	0.00	0.001	O	|	|	|	0.05
47.833	0.00	0.00	0.001	O	|	|	|	0.05
47.917	0.00	0.00	0.001	O	|	|	|	0.05
48.000	0.00	0.00	0.001	O	|	|	|	0.05
48.083	0.00	0.00	0.001	O	|	|	|	0.04
48.167	0.00	0.00	0.001	O	|	|	|	0.04

48.250	0.00	0.00	0.001	O	|	|	|	0.04
48.333	0.00	0.00	0.001	O	|	|	|	0.04
48.417	0.00	0.00	0.001	O	|	|	|	0.04
48.500	0.00	0.00	0.001	O	|	|	|	0.04
48.583	0.00	0.00	0.001	O	|	|	|	0.04
48.667	0.00	0.00	0.001	O	|	|	|	0.04
48.750	0.00	0.00	0.001	O	|	|	|	0.04
48.833	0.00	0.00	0.001	O	|	|	|	0.04
48.917	0.00	0.00	0.001	O	|	|	|	0.04
49.000	0.00	0.00	0.001	O	|	|	|	0.04
49.083	0.00	0.00	0.001	O	|	|	|	0.04
49.167	0.00	0.00	0.001	O	|	|	|	0.04
49.250	0.00	0.00	0.001	O	|	|	|	0.04
49.333	0.00	0.00	0.001	O	|	|	|	0.04
49.417	0.00	0.00	0.001	O	|	|	|	0.04
49.500	0.00	0.00	0.001	O	|	|	|	0.04
49.583	0.00	0.00	0.001	O	|	|	|	0.04
49.667	0.00	0.00	0.001	O	|	|	|	0.04
49.750	0.00	0.00	0.001	O	|	|	|	0.03
49.833	0.00	0.00	0.001	O	|	|	|	0.03
49.917	0.00	0.00	0.001	O	|	|	|	0.03
50.000	0.00	0.00	0.001	O	|	|	|	0.03
50.083	0.00	0.00	0.001	O	|	|	|	0.03
50.167	0.00	0.00	0.001	O	|	|	|	0.03
50.250	0.00	0.00	0.001	O	|	|	|	0.03
50.333	0.00	0.00	0.001	O	|	|	|	0.03
50.417	0.00	0.00	0.001	O	|	|	|	0.03
50.500	0.00	0.00	0.001	O	|	|	|	0.03
50.583	0.00	0.00	0.001	O	|	|	|	0.03
50.667	0.00	0.00	0.001	O	|	|	|	0.03
50.750	0.00	0.00	0.001	O	|	|	|	0.03
50.833	0.00	0.00	0.001	O	|	|	|	0.03
50.917	0.00	0.00	0.001	O	|	|	|	0.03
51.000	0.00	0.00	0.001	O	|	|	|	0.03
51.083	0.00	0.00	0.001	O	|	|	|	0.03
51.167	0.00	0.00	0.001	O	|	|	|	0.03
51.250	0.00	0.00	0.001	O	|	|	|	0.03
51.333	0.00	0.00	0.001	O	|	|	|	0.03
51.417	0.00	0.00	0.001	O	|	|	|	0.03
51.500	0.00	0.00	0.001	O	|	|	|	0.03
51.583	0.00	0.00	0.001	O	|	|	|	0.03
51.667	0.00	0.00	0.001	O	|	|	|	0.03
51.750	0.00	0.00	0.001	O	|	|	|	0.03
51.833	0.00	0.00	0.001	O	|	|	|	0.03
51.917	0.00	0.00	0.001	O	|	|	|	0.02
52.000	0.00	0.00	0.001	O	|	|	|	0.02
52.083	0.00	0.00	0.001	O	|	|	|	0.02
52.167	0.00	0.00	0.001	O	|	|	|	0.02
52.250	0.00	0.00	0.001	O	|	|	|	0.02
52.333	0.00	0.00	0.001	O	|	|	|	0.02

```
52.417    0.00    0.00      0.001  O       |       |       |       |     0.02
52.500    0.00    0.00      0.001  O       |       |       |       |     0.02
52.583    0.00    0.00      0.001  O       |       |       |       |     0.02
52.667    0.00    0.00      0.001  O       |       |       |       |     0.02

        ****************************HYDROGRAPH DATA****************************
                       Number of intervals =   632
                       Time interval =    5.0 (Min.)
                       Maximum/Peak flow rate =        0.045 (CFS)
                       Total volume =       0.125 (Ac.Ft)
              Status of hydrographs being held in storage
                          Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
        ***********************************************************************

        ---------------------------------------------------------------------
```

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
5 yr
6 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris65.rte
**********HYDROGRAPH DATA**********
Number of intervals = 80
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.155 (CFS)
Total volume = 0.174 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 80
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.3 0.58 0.87 1.16	Depth (Ft.)
0.083	0.02	0.00	0.000	O | | | |	0.00
0.167	0.09	0.00	0.000	O I | | | |	0.02
0.250	0.12	0.00	0.001	O I | | | |	0.05
0.333	0.13	0.00	0.002	O I | | | |	0.08
0.417	0.14	0.01	0.003	O I | | | |	0.12
0.500	0.15	0.01	0.004	O I | | | |	0.16
0.583	0.16	0.01	0.005	O I | | | |	0.20
0.667	0.17	0.01	0.006	O I | | | |	0.25
0.750	0.17	0.01	0.007	O I | | | |	0.30
0.833	0.17	0.02	0.008	O I | | | |	0.34
0.917	0.18	0.02	0.009	O I | | | |	0.39
1.000	0.18	0.02	0.010	O I | | | |	0.43
1.083	0.19	0.02	0.012	O I | | | |	0.48
1.167	0.20	0.02	0.013	O I | | | |	0.53
1.250	0.20	0.03	0.014	O I | | | |	0.58
1.333	0.20	0.03	0.015	O I | | | |	0.63
1.417	0.20	0.03	0.016	O I | | | |	0.68
1.500	0.20	0.03	0.017	O I | | | |	0.73
1.583	0.20	0.03	0.019	O I | | | |	0.77
1.667	0.20	0.04	0.020	|O I | | | |	0.82
1.750	0.20	0.04	0.021	|O I | | | |	0.87
1.833	0.20	0.04	0.022	|O I | | | |	0.91
1.917	0.20	0.04	0.023	|O I | | | |	0.96
2.000	0.21	0.04	0.024	|O I | | | |	1.00
2.083	0.21	0.04	0.025	|O I | | | |	1.03
2.167	0.21	0.04	0.026	|O I | | | |	1.06
2.250	0.22	0.04	0.028	|O I | | | |	1.09
2.333	0.22	0.04	0.029	|O I | | | |	1.12

```
2.417    0.22    0.04      0.030  |O    I |       |       |       |     1.15
2.500    0.23    0.04      0.031  |O    I |       |       |       |     1.18
2.583    0.23    0.04      0.033  |O    I |       |       |       |     1.21
2.667    0.23    0.04      0.034  |O    I |       |       |       |     1.24
2.750    0.23    0.04      0.035  |O    I |       |       |       |     1.28
2.833    0.24    0.04      0.036  |O    I |       |       |       |     1.31
2.917    0.25    0.04      0.038  |O    I |       |       |       |     1.34
3.000    0.25    0.04      0.039  |O    I |       |       |       |     1.38
3.083    0.25    0.04      0.041  |O    I |       |       |       |     1.41
3.167    0.26    0.04      0.042  |O     I|       |       |       |     1.45
3.250    0.27    0.04      0.043  |O     I|       |       |       |     1.49
3.333    0.27    0.04      0.045  |O     I|       |       |       |     1.53
3.417    0.28    0.04      0.047  |O     I|       |       |       |     1.57
3.500    0.30    0.04      0.048  |O      I       |       |       |     1.61
3.583    0.32    0.04      0.050  |O      I       |       |       |     1.65
3.667    0.34    0.04      0.052  |O      |I      |       |       |     1.70
3.750    0.35    0.04      0.054  |O      |I      |       |       |     1.75
3.833    0.36    0.04      0.056  |O      | I     |       |       |     1.81
3.917    0.37    0.04      0.058  |O      | I     |       |       |     1.86
4.000    0.39    0.04      0.061  |O      | I     |       |       |     1.92
4.083    0.40    0.04      0.063  |O      |  I    |       |       |     1.98
4.167    0.42    0.04      0.066  |O      |  I    |       |       |     2.04
4.250    0.44    0.04      0.068  |O      |   I   |       |       |     2.11
4.333    0.47    0.04      0.071  |O      |   I   |       |       |     2.18
4.417    0.49    0.04      0.074  |O      |    I  |       |       |     2.25
4.500    0.51    0.04      0.077  |O      |     I |       |       |     2.33
4.583    0.52    0.04      0.081  |O      |     I |       |       |     2.41
4.667    0.54    0.04      0.084  |O      |      I|       |       |     2.50
4.750    0.57    0.04      0.087  |O      |      I|       |       |     2.59
4.833    0.59    0.04      0.091  |O      |       I       |       |     2.68
4.917    0.60    0.04      0.095  |O      |       I       |       |     2.77
5.000    0.62    0.04      0.099  |O      |       |I      |       |     2.87
5.083    0.66    0.04      0.103  |O      |       | I     |       |     2.97
5.167    0.75    0.04      0.107  |O      |       |   I   |       |     3.09
5.250    0.85    0.04      0.113  |O      |       |      I|       |     3.22
5.333    0.93    0.04      0.118  |O      |       |       |I      |     3.36
5.417    1.02    0.04      0.125  |O      |       |       |   I   |     3.52
5.500    1.16    0.04      0.132  |O      |       |       |      I|     3.70
5.583    1.15    0.04      0.140  |O      |       |       |     I|      3.89
5.667    0.69    0.04      0.146  |O      |       |  I    |       |     4.04
5.750    0.43    0.04      0.149  |O      |  I    |       |       |     4.13
5.833    0.30    0.04      0.151  |O      I       |       |       |     4.19
5.917    0.21    0.04      0.153  |O   I  |       |       |       |     4.22
6.000    0.15    0.04      0.154  |O  I   |       |       |       |     4.25
6.083    0.09    0.04      0.154  |OI     |       |       |       |     4.26
6.167    0.04    0.04      0.155  |O      |       |       |       |     4.26
6.250    0.02    0.04      0.154  IO      |       |       |       |     4.26
6.333    0.01    0.04      0.154  IO      |       |       |       |     4.25
6.417    0.01    0.04      0.154  IO      |       |       |       |     4.25
6.500    0.00    0.04      0.154  IO      |       |       |       |     4.24
```

6.583	0.00	0.04	0.153	IO				4.23
6.667	0.00	0.04	0.153	IO				4.23
6.750	0.00	0.04	0.153	IO				4.22
6.833	0.00	0.04	0.152	IO				4.21
6.917	0.00	0.04	0.152	IO				4.20
7.000	0.00	0.04	0.152	IO				4.20
7.083	0.00	0.04	0.152	IO				4.19
7.167	0.00	0.04	0.151	IO				4.18
7.250	0.00	0.04	0.151	IO				4.17
7.333	0.00	0.04	0.151	IO				4.16
7.417	0.00	0.04	0.150	IO				4.16
7.500	0.00	0.04	0.150	IO				4.15
7.583	0.00	0.04	0.150	IO				4.14
7.667	0.00	0.04	0.149	IO				4.13
7.750	0.00	0.04	0.149	IO				4.13
7.833	0.00	0.04	0.149	IO				4.12
7.917	0.00	0.04	0.148	IO				4.11
8.000	0.00	0.04	0.148	IO				4.10
8.083	0.00	0.04	0.148	IO				4.09
8.167	0.00	0.04	0.147	IO				4.09
8.250	0.00	0.04	0.147	IO				4.08
8.333	0.00	0.04	0.147	IO				4.07
8.417	0.00	0.04	0.147	IO				4.06
8.500	0.00	0.04	0.146	IO				4.06
8.583	0.00	0.04	0.146	IO				4.05
8.667	0.00	0.04	0.146	IO				4.04
8.750	0.00	0.04	0.145	IO				4.03
8.833	0.00	0.04	0.145	IO				4.03
8.917	0.00	0.04	0.145	IO				4.02
9.000	0.00	0.04	0.144	IO				4.01
9.083	0.00	0.04	0.144	IO				4.00
9.167	0.00	0.04	0.144	IO				3.99
9.250	0.00	0.04	0.143	IO				3.99
9.333	0.00	0.04	0.143	IO				3.98
9.417	0.00	0.04	0.143	IO				3.97
9.500	0.00	0.04	0.143	IO				3.96
9.583	0.00	0.04	0.142	IO				3.96
9.667	0.00	0.04	0.142	IO				3.95
9.750	0.00	0.04	0.142	IO				3.94
9.833	0.00	0.04	0.141	IO				3.93
9.917	0.00	0.04	0.141	IO				3.92
10.000	0.00	0.04	0.141	IO				3.92
10.083	0.00	0.04	0.140	IO				3.91
10.167	0.00	0.04	0.140	IO				3.90
10.250	0.00	0.04	0.140	IO				3.89
10.333	0.00	0.04	0.139	IO				3.89
10.417	0.00	0.04	0.139	IO				3.88
10.500	0.00	0.04	0.139	IO				3.87
10.583	0.00	0.04	0.138	IO				3.86
10.667	0.00	0.04	0.138	IO				3.85

10.750	0.00	0.04	0.138	IO				3.85
10.833	0.00	0.04	0.138	IO				3.84
10.917	0.00	0.04	0.137	IO				3.83
11.000	0.00	0.04	0.137	IO				3.82
11.083	0.00	0.04	0.137	IO				3.82
11.167	0.00	0.04	0.136	IO				3.81
11.250	0.00	0.04	0.136	IO				3.80
11.333	0.00	0.04	0.136	IO				3.79
11.417	0.00	0.04	0.135	IO				3.78
11.500	0.00	0.04	0.135	IO				3.78
11.583	0.00	0.04	0.135	IO				3.77
11.667	0.00	0.04	0.134	IO				3.76
11.750	0.00	0.04	0.134	IO				3.75
11.833	0.00	0.04	0.134	IO				3.75
11.917	0.00	0.04	0.134	IO				3.74
12.000	0.00	0.04	0.133	IO				3.73
12.083	0.00	0.04	0.133	IO				3.72
12.167	0.00	0.04	0.133	IO				3.72
12.250	0.00	0.04	0.132	IO				3.71
12.333	0.00	0.04	0.132	IO				3.70
12.417	0.00	0.04	0.132	IO				3.69
12.500	0.00	0.04	0.131	IO				3.68
12.583	0.00	0.04	0.131	IO				3.68
12.667	0.00	0.04	0.131	IO				3.67
12.750	0.00	0.04	0.130	IO				3.66
12.833	0.00	0.04	0.130	IO				3.65
12.917	0.00	0.04	0.130	IO				3.65
13.000	0.00	0.04	0.130	IO				3.64
13.083	0.00	0.04	0.129	IO				3.63
13.167	0.00	0.04	0.129	IO				3.62
13.250	0.00	0.04	0.129	IO				3.61
13.333	0.00	0.04	0.128	IO				3.61
13.417	0.00	0.04	0.128	IO				3.60
13.500	0.00	0.04	0.128	IO				3.59
13.583	0.00	0.04	0.127	IO				3.58
13.667	0.00	0.04	0.127	IO				3.58
13.750	0.00	0.04	0.127	IO				3.57
13.833	0.00	0.04	0.126	IO				3.56
13.917	0.00	0.04	0.126	IO				3.55
14.000	0.00	0.04	0.126	IO				3.54
14.083	0.00	0.04	0.125	IO				3.54
14.167	0.00	0.04	0.125	IO				3.53
14.250	0.00	0.04	0.125	IO				3.52
14.333	0.00	0.04	0.125	IO				3.51
14.417	0.00	0.04	0.124	IO				3.51
14.500	0.00	0.04	0.124	IO				3.50
14.583	0.00	0.04	0.124	IO				3.49
14.667	0.00	0.04	0.123	IO				3.48
14.750	0.00	0.04	0.123	IO				3.47
14.833	0.00	0.04	0.123	IO				3.47

14.917	0.00	0.04	0.122	IO				3.46
15.000	0.00	0.04	0.122	IO				3.45
15.083	0.00	0.04	0.122	IO				3.44
15.167	0.00	0.04	0.121	IO				3.44
15.250	0.00	0.04	0.121	IO				3.43
15.333	0.00	0.04	0.121	IO				3.42
15.417	0.00	0.04	0.121	IO				3.41
15.500	0.00	0.04	0.120	IO				3.41
15.583	0.00	0.04	0.120	IO				3.40
15.667	0.00	0.04	0.120	IO				3.39
15.750	0.00	0.04	0.119	IO				3.38
15.833	0.00	0.04	0.119	IO				3.37
15.917	0.00	0.04	0.119	IO				3.37
16.000	0.00	0.04	0.118	IO				3.36
16.083	0.00	0.04	0.118	IO				3.35
16.167	0.00	0.04	0.118	IO				3.34
16.250	0.00	0.04	0.117	IO				3.34
16.333	0.00	0.04	0.117	IO				3.33
16.417	0.00	0.04	0.117	IO				3.32
16.500	0.00	0.04	0.116	IO				3.31
16.583	0.00	0.04	0.116	IO				3.30
16.667	0.00	0.04	0.116	IO				3.30
16.750	0.00	0.04	0.116	IO				3.29
16.833	0.00	0.04	0.115	IO				3.28
16.917	0.00	0.04	0.115	IO				3.27
17.000	0.00	0.04	0.115	IO				3.27
17.083	0.00	0.04	0.114	IO				3.26
17.167	0.00	0.04	0.114	IO				3.25
17.250	0.00	0.04	0.114	IO				3.24
17.333	0.00	0.04	0.113	IO				3.23
17.417	0.00	0.04	0.113	IO				3.23
17.500	0.00	0.04	0.113	IO				3.22
17.583	0.00	0.04	0.112	IO				3.21
17.667	0.00	0.04	0.112	IO				3.20
17.750	0.00	0.04	0.112	IO				3.20
17.833	0.00	0.04	0.112	IO				3.19
17.917	0.00	0.04	0.111	IO				3.18
18.000	0.00	0.04	0.111	IO				3.17
18.083	0.00	0.04	0.111	IO				3.16
18.167	0.00	0.04	0.110	IO				3.16
18.250	0.00	0.04	0.110	IO				3.15
18.333	0.00	0.04	0.110	IO				3.14
18.417	0.00	0.04	0.109	IO				3.13
18.500	0.00	0.04	0.109	IO				3.13
18.583	0.00	0.04	0.109	IO				3.12
18.667	0.00	0.04	0.108	IO				3.11
18.750	0.00	0.04	0.108	IO				3.10
18.833	0.00	0.04	0.108	IO				3.10
18.917	0.00	0.04	0.108	IO				3.09
19.000	0.00	0.04	0.107	IO				3.08

19.083	0.00	0.04	0.107	IO				3.07
19.167	0.00	0.04	0.107	IO				3.06
19.250	0.00	0.04	0.106	IO				3.06
19.333	0.00	0.04	0.106	IO				3.05
19.417	0.00	0.04	0.106	IO				3.04
19.500	0.00	0.04	0.105	IO				3.03
19.583	0.00	0.04	0.105	IO				3.03
19.667	0.00	0.04	0.105	IO				3.02
19.750	0.00	0.04	0.104	IO				3.01
19.833	0.00	0.04	0.104	IO				3.00
19.917	0.00	0.04	0.104	IO				2.99
20.000	0.00	0.04	0.103	IO				2.99
20.083	0.00	0.04	0.103	IO				2.98
20.167	0.00	0.04	0.103	IO				2.97
20.250	0.00	0.04	0.103	IO				2.96
20.333	0.00	0.04	0.102	IO				2.96
20.417	0.00	0.04	0.102	IO				2.95
20.500	0.00	0.04	0.102	IO				2.94
20.583	0.00	0.04	0.101	IO				2.93
20.667	0.00	0.04	0.101	IO				2.92
20.750	0.00	0.04	0.101	IO				2.92
20.833	0.00	0.04	0.100	IO				2.91
20.917	0.00	0.04	0.100	IO				2.90
21.000	0.00	0.04	0.100	IO				2.89
21.083	0.00	0.04	0.099	IO				2.89
21.167	0.00	0.04	0.099	IO				2.88
21.250	0.00	0.04	0.099	IO				2.87
21.333	0.00	0.04	0.099	IO				2.86
21.417	0.00	0.04	0.098	IO				2.86
21.500	0.00	0.04	0.098	IO				2.85
21.583	0.00	0.04	0.098	IO				2.84
21.667	0.00	0.04	0.097	IO				2.83
21.750	0.00	0.04	0.097	IO				2.82
21.833	0.00	0.04	0.097	IO				2.82
21.917	0.00	0.04	0.096	IO				2.81
22.000	0.00	0.04	0.096	IO				2.80
22.083	0.00	0.04	0.096	IO				2.79
22.167	0.00	0.04	0.095	IO				2.79
22.250	0.00	0.04	0.095	IO				2.78
22.333	0.00	0.04	0.095	IO				2.77
22.417	0.00	0.04	0.094	IO				2.76
22.500	0.00	0.04	0.094	IO				2.75
22.583	0.00	0.04	0.094	IO				2.75
22.667	0.00	0.04	0.094	IO				2.74
22.750	0.00	0.04	0.093	IO				2.73
22.833	0.00	0.04	0.093	IO				2.72
22.917	0.00	0.04	0.093	IO				2.72
23.000	0.00	0.04	0.092	IO				2.71
23.083	0.00	0.04	0.092	IO				2.70
23.167	0.00	0.04	0.092	IO				2.69

23.250	0.00	0.04	0.091	IO				2.68
23.333	0.00	0.04	0.091	IO				2.68
23.417	0.00	0.04	0.091	IO				2.67
23.500	0.00	0.04	0.090	IO				2.66
23.583	0.00	0.04	0.090	IO				2.65
23.667	0.00	0.04	0.090	IO				2.65
23.750	0.00	0.04	0.090	IO				2.64
23.833	0.00	0.04	0.089	IO				2.63
23.917	0.00	0.04	0.089	IO				2.62
24.000	0.00	0.04	0.089	IO				2.61
24.083	0.00	0.04	0.088	IO				2.61
24.167	0.00	0.04	0.088	IO				2.60
24.250	0.00	0.04	0.088	IO				2.59
24.333	0.00	0.04	0.087	IO				2.58
24.417	0.00	0.04	0.087	IO				2.58
24.500	0.00	0.04	0.087	IO				2.57
24.583	0.00	0.04	0.086	IO				2.56
24.667	0.00	0.04	0.086	IO				2.55
24.750	0.00	0.04	0.086	IO				2.55
24.833	0.00	0.04	0.085	IO				2.54
24.917	0.00	0.04	0.085	IO				2.53
25.000	0.00	0.04	0.085	IO				2.52
25.083	0.00	0.04	0.085	IO				2.51
25.167	0.00	0.04	0.084	IO				2.51
25.250	0.00	0.04	0.084	IO				2.50
25.333	0.00	0.04	0.084	IO				2.49
25.417	0.00	0.04	0.083	IO				2.48
25.500	0.00	0.04	0.083	IO				2.48
25.583	0.00	0.04	0.083	IO				2.47
25.667	0.00	0.04	0.082	IO				2.46
25.750	0.00	0.04	0.082	IO				2.45
25.833	0.00	0.04	0.082	IO				2.44
25.917	0.00	0.04	0.081	IO				2.44
26.000	0.00	0.04	0.081	IO				2.43
26.083	0.00	0.04	0.081	IO				2.42
26.167	0.00	0.04	0.081	IO				2.41
26.250	0.00	0.04	0.080	IO				2.41
26.333	0.00	0.04	0.080	IO				2.40
26.417	0.00	0.04	0.080	IO				2.39
26.500	0.00	0.04	0.079	IO				2.38
26.583	0.00	0.04	0.079	IO				2.37
26.667	0.00	0.04	0.079	IO				2.37
26.750	0.00	0.04	0.078	IO				2.36
26.833	0.00	0.04	0.078	IO				2.35
26.917	0.00	0.04	0.078	IO				2.34
27.000	0.00	0.04	0.077	IO				2.34
27.083	0.00	0.04	0.077	IO				2.33
27.167	0.00	0.04	0.077	IO				2.32
27.250	0.00	0.04	0.077	IO				2.31
27.333	0.00	0.04	0.076	IO				2.30

27.417	0.00	0.04	0.076	IO				2.30
27.500	0.00	0.04	0.076	IO				2.29
27.583	0.00	0.04	0.075	IO				2.28
27.667	0.00	0.04	0.075	IO				2.27
27.750	0.00	0.04	0.075	IO				2.27
27.833	0.00	0.04	0.074	IO				2.26
27.917	0.00	0.04	0.074	IO				2.25
28.000	0.00	0.04	0.074	IO				2.24
28.083	0.00	0.04	0.073	IO				2.24
28.167	0.00	0.04	0.073	IO				2.23
28.250	0.00	0.04	0.073	IO				2.22
28.333	0.00	0.04	0.072	IO				2.21
28.417	0.00	0.04	0.072	IO				2.20
28.500	0.00	0.04	0.072	IO				2.20
28.583	0.00	0.04	0.072	IO				2.19
28.667	0.00	0.04	0.071	IO				2.18
28.750	0.00	0.04	0.071	IO				2.17
28.833	0.00	0.04	0.071	IO				2.17
28.917	0.00	0.04	0.070	IO				2.16
29.000	0.00	0.04	0.070	IO				2.15
29.083	0.00	0.04	0.070	IO				2.14
29.167	0.00	0.04	0.069	IO				2.13
29.250	0.00	0.04	0.069	IO				2.13
29.333	0.00	0.04	0.069	IO				2.12
29.417	0.00	0.04	0.068	IO				2.11
29.500	0.00	0.04	0.068	IO				2.10
29.583	0.00	0.04	0.068	IO				2.10
29.667	0.00	0.04	0.068	IO				2.09
29.750	0.00	0.04	0.067	IO				2.08
29.833	0.00	0.04	0.067	IO				2.07
29.917	0.00	0.04	0.067	IO				2.06
30.000	0.00	0.04	0.066	IO				2.06
30.083	0.00	0.04	0.066	IO				2.05
30.167	0.00	0.04	0.066	IO				2.04
30.250	0.00	0.04	0.065	IO				2.03
30.333	0.00	0.04	0.065	IO				2.03
30.417	0.00	0.04	0.065	IO				2.02
30.500	0.00	0.04	0.064	IO				2.01
30.583	0.00	0.04	0.064	IO				2.00
30.667	0.00	0.04	0.064	IO				2.00
30.750	0.00	0.04	0.063	IO				1.99
30.833	0.00	0.04	0.063	IO				1.98
30.917	0.00	0.04	0.063	IO				1.97
31.000	0.00	0.04	0.063	IO				1.96
31.083	0.00	0.04	0.062	IO				1.96
31.167	0.00	0.04	0.062	IO				1.95
31.250	0.00	0.04	0.062	IO				1.94
31.333	0.00	0.04	0.061	IO				1.93
31.417	0.00	0.04	0.061	IO				1.93
31.500	0.00	0.04	0.061	IO				1.92

31.583	0.00	0.04	0.060	IO				1.91
31.667	0.00	0.04	0.060	IO				1.90
31.750	0.00	0.04	0.060	IO				1.89
31.833	0.00	0.04	0.059	IO				1.89
31.917	0.00	0.04	0.059	IO				1.88
32.000	0.00	0.04	0.059	IO				1.87
32.083	0.00	0.04	0.059	IO				1.86
32.167	0.00	0.04	0.058	IO				1.86
32.250	0.00	0.04	0.058	IO				1.85
32.333	0.00	0.04	0.058	IO				1.84
32.417	0.00	0.04	0.057	IO				1.83
32.500	0.00	0.04	0.057	IO				1.82
32.583	0.00	0.04	0.057	IO				1.82
32.667	0.00	0.04	0.056	IO				1.81
32.750	0.00	0.04	0.056	IO				1.80
32.833	0.00	0.04	0.056	IO				1.79
32.917	0.00	0.04	0.055	IO				1.79
33.000	0.00	0.04	0.055	IO				1.78
33.083	0.00	0.04	0.055	IO				1.77
33.167	0.00	0.04	0.055	IO				1.76
33.250	0.00	0.04	0.054	IO				1.75
33.333	0.00	0.04	0.054	IO				1.75
33.417	0.00	0.04	0.054	IO				1.74
33.500	0.00	0.04	0.053	IO				1.73
33.583	0.00	0.04	0.053	IO				1.72
33.667	0.00	0.04	0.053	IO				1.72
33.750	0.00	0.04	0.052	IO				1.71
33.833	0.00	0.04	0.052	IO				1.70
33.917	0.00	0.04	0.052	IO				1.69
34.000	0.00	0.04	0.051	IO				1.69
34.083	0.00	0.04	0.051	IO				1.68
34.167	0.00	0.04	0.051	IO				1.67
34.250	0.00	0.04	0.050	IO				1.66
34.333	0.00	0.04	0.050	IO				1.65
34.417	0.00	0.04	0.050	IO				1.65
34.500	0.00	0.04	0.050	IO				1.64
34.583	0.00	0.04	0.049	IO				1.63
34.667	0.00	0.04	0.049	IO				1.62
34.750	0.00	0.04	0.049	IO				1.62
34.833	0.00	0.04	0.048	IO				1.61
34.917	0.00	0.04	0.048	IO				1.60
35.000	0.00	0.04	0.048	IO				1.59
35.083	0.00	0.04	0.047	IO				1.58
35.167	0.00	0.04	0.047	IO				1.58
35.250	0.00	0.04	0.047	IO				1.57
35.333	0.00	0.04	0.046	IO				1.56
35.417	0.00	0.04	0.046	IO				1.55
35.500	0.00	0.04	0.046	IO				1.55
35.583	0.00	0.04	0.046	IO				1.54
35.667	0.00	0.04	0.045	IO				1.53

35.750	0.00	0.04	0.045	IO				1.52
35.833	0.00	0.04	0.045	IO				1.51
35.917	0.00	0.04	0.044	IO				1.51
36.000	0.00	0.04	0.044	IO				1.50
36.083	0.00	0.04	0.044	IO				1.49
36.167	0.00	0.04	0.043	IO				1.48
36.250	0.00	0.04	0.043	IO				1.48
36.333	0.00	0.04	0.043	IO				1.47
36.417	0.00	0.04	0.042	IO				1.46
36.500	0.00	0.04	0.042	IO				1.45
36.583	0.00	0.04	0.042	IO				1.44
36.667	0.00	0.04	0.041	IO				1.44
36.750	0.00	0.04	0.041	IO				1.43
36.833	0.00	0.04	0.041	IO				1.42
36.917	0.00	0.04	0.041	IO				1.41
37.000	0.00	0.04	0.040	IO				1.41
37.083	0.00	0.04	0.040	IO				1.40
37.167	0.00	0.04	0.040	IO				1.39
37.250	0.00	0.04	0.039	IO				1.38
37.333	0.00	0.04	0.039	IO				1.38
37.417	0.00	0.04	0.039	IO				1.37
37.500	0.00	0.04	0.038	IO				1.36
37.583	0.00	0.04	0.038	IO				1.35
37.667	0.00	0.04	0.038	IO				1.34
37.750	0.00	0.04	0.037	IO				1.34
37.833	0.00	0.04	0.037	IO				1.33
37.917	0.00	0.04	0.037	IO				1.32
38.000	0.00	0.04	0.037	IO				1.31
38.083	0.00	0.04	0.036	IO				1.31
38.167	0.00	0.04	0.036	IO				1.30
38.250	0.00	0.04	0.036	IO				1.29
38.333	0.00	0.04	0.035	IO				1.28
38.417	0.00	0.04	0.035	IO				1.27
38.500	0.00	0.04	0.035	IO				1.27
38.583	0.00	0.04	0.034	IO				1.26
38.667	0.00	0.04	0.034	IO				1.25
38.750	0.00	0.04	0.034	IO				1.24
38.833	0.00	0.04	0.033	IO				1.24
38.917	0.00	0.04	0.033	IO				1.23
39.000	0.00	0.04	0.033	IO				1.22
39.083	0.00	0.04	0.033	IO				1.21
39.167	0.00	0.04	0.032	IO				1.20
39.250	0.00	0.04	0.032	IO				1.20
39.333	0.00	0.04	0.032	IO				1.19
39.417	0.00	0.04	0.031	IO				1.18
39.500	0.00	0.04	0.031	IO				1.17
39.583	0.00	0.04	0.031	IO				1.17
39.667	0.00	0.04	0.030	IO				1.16
39.750	0.00	0.04	0.030	IO				1.15
39.833	0.00	0.04	0.030	IO				1.14

39.917	0.00	0.04	0.029	IO				1.14
40.000	0.00	0.04	0.029	IO				1.13
40.083	0.00	0.04	0.029	IO				1.12
40.167	0.00	0.04	0.028	IO				1.11
40.250	0.00	0.04	0.028	IO				1.10
40.333	0.00	0.04	0.028	IO				1.10
40.417	0.00	0.04	0.028	IO				1.09
40.500	0.00	0.04	0.027	IO				1.08
40.583	0.00	0.04	0.027	IO				1.07
40.667	0.00	0.04	0.027	IO				1.07
40.750	0.00	0.04	0.026	IO				1.06
40.833	0.00	0.04	0.026	IO				1.05
40.917	0.00	0.04	0.026	IO				1.04
41.000	0.00	0.04	0.025	IO				1.03
41.083	0.00	0.04	0.025	IO				1.03
41.167	0.00	0.04	0.025	IO				1.02
41.250	0.00	0.04	0.024	IO				1.01
41.333	0.00	0.04	0.024	IO				1.00
41.417	0.00	0.04	0.024	IO				0.99
41.500	0.00	0.04	0.024	IO				0.98
41.583	0.00	0.04	0.023	IO				0.97
41.667	0.00	0.04	0.023	IO				0.95
41.750	0.00	0.04	0.023	IO				0.94
41.833	0.00	0.04	0.022	IO				0.93
41.917	0.00	0.04	0.022	IO				0.92
42.000	0.00	0.04	0.022	IO				0.91
42.083	0.00	0.04	0.021	IO				0.90
42.167	0.00	0.04	0.021	IO				0.88
42.250	0.00	0.04	0.021	IO				0.87
42.333	0.00	0.04	0.021	IO				0.86
42.417	0.00	0.04	0.020	IO				0.85
42.500	0.00	0.04	0.020	IO				0.84
42.583	0.00	0.04	0.020	IO				0.83
42.667	0.00	0.04	0.020	IO				0.82
42.750	0.00	0.04	0.019	IO				0.81
42.833	0.00	0.04	0.019	O				0.80
42.917	0.00	0.04	0.019	O				0.79
43.000	0.00	0.03	0.019	O				0.78
43.083	0.00	0.03	0.018	O				0.77
43.167	0.00	0.03	0.018	O				0.76
43.250	0.00	0.03	0.018	O				0.75
43.333	0.00	0.03	0.018	O				0.74
43.417	0.00	0.03	0.017	O				0.73
43.500	0.00	0.03	0.017	O				0.72
43.583	0.00	0.03	0.017	O				0.71
43.667	0.00	0.03	0.017	O				0.70
43.750	0.00	0.03	0.017	O				0.69
43.833	0.00	0.03	0.016	O				0.68
43.917	0.00	0.03	0.016	O				0.67
44.000	0.00	0.03	0.016	O				0.67

44.083	0.00	0.03	0.016	O				0.66
44.167	0.00	0.03	0.016	O				0.65
44.250	0.00	0.03	0.015	O				0.64
44.333	0.00	0.03	0.015	O				0.63
44.417	0.00	0.03	0.015	O				0.62
44.500	0.00	0.03	0.015	O				0.62
44.583	0.00	0.03	0.015	O				0.61
44.667	0.00	0.03	0.014	O				0.60
44.750	0.00	0.03	0.014	O				0.59
44.833	0.00	0.03	0.014	O				0.58
44.917	0.00	0.03	0.014	O				0.58
45.000	0.00	0.03	0.014	O				0.57
45.083	0.00	0.03	0.013	O				0.56
45.167	0.00	0.02	0.013	O				0.56
45.250	0.00	0.02	0.013	O				0.55
45.333	0.00	0.02	0.013	O				0.54
45.417	0.00	0.02	0.013	O				0.53
45.500	0.00	0.02	0.013	O				0.53
45.583	0.00	0.02	0.012	O				0.52
45.667	0.00	0.02	0.012	O				0.51
45.750	0.00	0.02	0.012	O				0.51
45.833	0.00	0.02	0.012	O				0.50
45.917	0.00	0.02	0.012	O				0.49
46.000	0.00	0.02	0.012	O				0.49
46.083	0.00	0.02	0.012	O				0.48
46.167	0.00	0.02	0.011	O				0.48
46.250	0.00	0.02	0.011	O				0.47
46.333	0.00	0.02	0.011	O				0.46
46.417	0.00	0.02	0.011	O				0.46
46.500	0.00	0.02	0.011	O				0.45
46.583	0.00	0.02	0.011	O				0.45
46.667	0.00	0.02	0.011	O				0.44
46.750	0.00	0.02	0.010	O				0.43
46.833	0.00	0.02	0.010	O				0.43
46.917	0.00	0.02	0.010	O				0.42
47.000	0.00	0.02	0.010	O				0.42
47.083	0.00	0.02	0.010	O				0.41
47.167	0.00	0.02	0.010	O				0.41
47.250	0.00	0.02	0.010	O				0.40
47.333	0.00	0.02	0.010	O				0.40
47.417	0.00	0.02	0.009	O				0.39
47.500	0.00	0.02	0.009	O				0.39
47.583	0.00	0.02	0.009	O				0.38
47.667	0.00	0.02	0.009	O				0.38
47.750	0.00	0.02	0.009	O				0.37
47.833	0.00	0.02	0.009	O				0.37
47.917	0.00	0.02	0.009	O				0.36
48.000	0.00	0.02	0.009	O				0.36
48.083	0.00	0.02	0.008	O				0.35
48.167	0.00	0.02	0.008	O				0.35

48.250	0.00	0.02	0.008	O	|	|	|	0.34
48.333	0.00	0.02	0.008	O	|	|	|	0.34
48.417	0.00	0.02	0.008	O	|	|	|	0.34
48.500	0.00	0.01	0.008	O	|	|	|	0.33
48.583	0.00	0.01	0.008	O	|	|	|	0.33
48.667	0.00	0.01	0.008	O	|	|	|	0.32
48.750	0.00	0.01	0.008	O	|	|	|	0.32
48.833	0.00	0.01	0.008	O	|	|	|	0.31
48.917	0.00	0.01	0.007	O	|	|	|	0.31
49.000	0.00	0.01	0.007	O	|	|	|	0.31
49.083	0.00	0.01	0.007	O	|	|	|	0.30
49.167	0.00	0.01	0.007	O	|	|	|	0.30
49.250	0.00	0.01	0.007	O	|	|	|	0.29
49.333	0.00	0.01	0.007	O	|	|	|	0.29
49.417	0.00	0.01	0.007	O	|	|	|	0.29
49.500	0.00	0.01	0.007	O	|	|	|	0.28
49.583	0.00	0.01	0.007	O	|	|	|	0.28
49.667	0.00	0.01	0.007	O	|	|	|	0.28
49.750	0.00	0.01	0.007	O	|	|	|	0.27
49.833	0.00	0.01	0.006	O	|	|	|	0.27
49.917	0.00	0.01	0.006	O	|	|	|	0.27
50.000	0.00	0.01	0.006	O	|	|	|	0.26
50.083	0.00	0.01	0.006	O	|	|	|	0.26
50.167	0.00	0.01	0.006	O	|	|	|	0.26
50.250	0.00	0.01	0.006	O	|	|	|	0.25
50.333	0.00	0.01	0.006	O	|	|	|	0.25
50.417	0.00	0.01	0.006	O	|	|	|	0.25
50.500	0.00	0.01	0.006	O	|	|	|	0.24
50.583	0.00	0.01	0.006	O	|	|	|	0.24
50.667	0.00	0.01	0.006	O	|	|	|	0.24
50.750	0.00	0.01	0.006	O	|	|	|	0.23
50.833	0.00	0.01	0.006	O	|	|	|	0.23
50.917	0.00	0.01	0.005	O	|	|	|	0.23
51.000	0.00	0.01	0.005	O	|	|	|	0.22
51.083	0.00	0.01	0.005	O	|	|	|	0.22
51.167	0.00	0.01	0.005	O	|	|	|	0.22
51.250	0.00	0.01	0.005	O	|	|	|	0.22
51.333	0.00	0.01	0.005	O	|	|	|	0.21
51.417	0.00	0.01	0.005	O	|	|	|	0.21
51.500	0.00	0.01	0.005	O	|	|	|	0.21
51.583	0.00	0.01	0.005	O	|	|	|	0.21
51.667	0.00	0.01	0.005	O	|	|	|	0.20
51.750	0.00	0.01	0.005	O	|	|	|	0.20
51.833	0.00	0.01	0.005	O	|	|	|	0.20
51.917	0.00	0.01	0.005	O	|	|	|	0.20
52.000	0.00	0.01	0.005	O	|	|	|	0.19
52.083	0.00	0.01	0.005	O	|	|	|	0.19
52.167	0.00	0.01	0.005	O	|	|	|	0.19
52.250	0.00	0.01	0.004	O	|	|	|	0.19
52.333	0.00	0.01	0.004	O	|	|	|	0.18

52.417	0.00	0.01	0.004	O	|	|	|	0.18
52.500	0.00	0.01	0.004	O	|	|	|	0.18
52.583	0.00	0.01	0.004	O	|	|	|	0.18
52.667	0.00	0.01	0.004	O	|	|	|	0.17
52.750	0.00	0.01	0.004	O	|	|	|	0.17
52.833	0.00	0.01	0.004	O	|	|	|	0.17
52.917	0.00	0.01	0.004	O	|	|	|	0.17
53.000	0.00	0.01	0.004	O	|	|	|	0.16
53.083	0.00	0.01	0.004	O	|	|	|	0.16
53.167	0.00	0.01	0.004	O	|	|	|	0.16
53.250	0.00	0.01	0.004	O	|	|	|	0.16
53.333	0.00	0.01	0.004	O	|	|	|	0.16
53.417	0.00	0.01	0.004	O	|	|	|	0.15
53.500	0.00	0.01	0.004	O	|	|	|	0.15
53.583	0.00	0.01	0.004	O	|	|	|	0.15
53.667	0.00	0.01	0.004	O	|	|	|	0.15
53.750	0.00	0.01	0.004	O	|	|	|	0.15
53.833	0.00	0.01	0.003	O	|	|	|	0.14
53.917	0.00	0.01	0.003	O	|	|	|	0.14
54.000	0.00	0.01	0.003	O	|	|	|	0.14
54.083	0.00	0.01	0.003	O	|	|	|	0.14
54.167	0.00	0.01	0.003	O	|	|	|	0.14
54.250	0.00	0.01	0.003	O	|	|	|	0.14
54.333	0.00	0.01	0.003	O	|	|	|	0.13
54.417	0.00	0.01	0.003	O	|	|	|	0.13
54.500	0.00	0.01	0.003	O	|	|	|	0.13
54.583	0.00	0.01	0.003	O	|	|	|	0.13
54.667	0.00	0.01	0.003	O	|	|	|	0.13
54.750	0.00	0.01	0.003	O	|	|	|	0.13
54.833	0.00	0.01	0.003	O	|	|	|	0.12
54.917	0.00	0.01	0.003	O	|	|	|	0.12
55.000	0.00	0.01	0.003	O	|	|	|	0.12
55.083	0.00	0.01	0.003	O	|	|	|	0.12
55.167	0.00	0.01	0.003	O	|	|	|	0.12
55.250	0.00	0.01	0.003	O	|	|	|	0.12
55.333	0.00	0.01	0.003	O	|	|	|	0.11
55.417	0.00	0.01	0.003	O	|	|	|	0.11
55.500	0.00	0.01	0.003	O	|	|	|	0.11
55.583	0.00	0.00	0.003	O	|	|	|	0.11
55.667	0.00	0.00	0.003	O	|	|	|	0.11
55.750	0.00	0.00	0.003	O	|	|	|	0.11
55.833	0.00	0.00	0.003	O	|	|	|	0.11
55.917	0.00	0.00	0.003	O	|	|	|	0.10
56.000	0.00	0.00	0.002	O	|	|	|	0.10
56.083	0.00	0.00	0.002	O	|	|	|	0.10
56.167	0.00	0.00	0.002	O	|	|	|	0.10
56.250	0.00	0.00	0.002	O	|	|	|	0.10
56.333	0.00	0.00	0.002	O	|	|	|	0.10
56.417	0.00	0.00	0.002	O	|	|	|	0.10
56.500	0.00	0.00	0.002	O	|	|	|	0.10

56.583	0.00	0.00	0.002	O	|	|	|	0.09
56.667	0.00	0.00	0.002	O	|	|	|	0.09
56.750	0.00	0.00	0.002	O	|	|	|	0.09
56.833	0.00	0.00	0.002	O	|	|	|	0.09
56.917	0.00	0.00	0.002	O	|	|	|	0.09
57.000	0.00	0.00	0.002	O	|	|	|	0.09
57.083	0.00	0.00	0.002	O	|	|	|	0.09
57.167	0.00	0.00	0.002	O	|	|	|	0.09
57.250	0.00	0.00	0.002	O	|	|	|	0.09
57.333	0.00	0.00	0.002	O	|	|	|	0.08
57.417	0.00	0.00	0.002	O	|	|	|	0.08
57.500	0.00	0.00	0.002	O	|	|	|	0.08
57.583	0.00	0.00	0.002	O	|	|	|	0.08
57.667	0.00	0.00	0.002	O	|	|	|	0.08
57.750	0.00	0.00	0.002	O	|	|	|	0.08
57.833	0.00	0.00	0.002	O	|	|	|	0.08
57.917	0.00	0.00	0.002	O	|	|	|	0.08
58.000	0.00	0.00	0.002	O	|	|	|	0.08
58.083	0.00	0.00	0.002	O	|	|	|	0.08
58.167	0.00	0.00	0.002	O	|	|	|	0.07
58.250	0.00	0.00	0.002	O	|	|	|	0.07
58.333	0.00	0.00	0.002	O	|	|	|	0.07
58.417	0.00	0.00	0.002	O	|	|	|	0.07
58.500	0.00	0.00	0.002	O	|	|	|	0.07
58.583	0.00	0.00	0.002	O	|	|	|	0.07
58.667	0.00	0.00	0.002	O	|	|	|	0.07
58.750	0.00	0.00	0.002	O	|	|	|	0.07
58.833	0.00	0.00	0.002	O	|	|	|	0.07
58.917	0.00	0.00	0.002	O	|	|	|	0.07
59.000	0.00	0.00	0.002	O	|	|	|	0.07
59.083	0.00	0.00	0.002	O	|	|	|	0.06
59.167	0.00	0.00	0.002	O	|	|	|	0.06
59.250	0.00	0.00	0.002	O	|	|	|	0.06
59.333	0.00	0.00	0.001	O	|	|	|	0.06
59.417	0.00	0.00	0.001	O	|	|	|	0.06
59.500	0.00	0.00	0.001	O	|	|	|	0.06
59.583	0.00	0.00	0.001	O	|	|	|	0.06
59.667	0.00	0.00	0.001	O	|	|	|	0.06
59.750	0.00	0.00	0.001	O	|	|	|	0.06
59.833	0.00	0.00	0.001	O	|	|	|	0.06
59.917	0.00	0.00	0.001	O	|	|	|	0.06
60.000	0.00	0.00	0.001	O	|	|	|	0.06
60.083	0.00	0.00	0.001	O	|	|	|	0.06
60.167	0.00	0.00	0.001	O	|	|	|	0.05
60.250	0.00	0.00	0.001	O	|	|	|	0.05
60.333	0.00	0.00	0.001	O	|	|	|	0.05
60.417	0.00	0.00	0.001	O	|	|	|	0.05
60.500	0.00	0.00	0.001	O	|	|	|	0.05
60.583	0.00	0.00	0.001	O	|	|	|	0.05
60.667	0.00	0.00	0.001	O	|	|	|	0.05

60.750	0.00	0.00	0.001	O	|	|	|	0.05
60.833	0.00	0.00	0.001	O	|	|	|	0.05
60.917	0.00	0.00	0.001	O	|	|	|	0.05
61.000	0.00	0.00	0.001	O	|	|	|	0.05
61.083	0.00	0.00	0.001	O	|	|	|	0.05
61.167	0.00	0.00	0.001	O	|	|	|	0.05
61.250	0.00	0.00	0.001	O	|	|	|	0.05
61.333	0.00	0.00	0.001	O	|	|	|	0.05
61.417	0.00	0.00	0.001	O	|	|	|	0.04
61.500	0.00	0.00	0.001	O	|	|	|	0.04
61.583	0.00	0.00	0.001	O	|	|	|	0.04
61.667	0.00	0.00	0.001	O	|	|	|	0.04
61.750	0.00	0.00	0.001	O	|	|	|	0.04
61.833	0.00	0.00	0.001	O	|	|	|	0.04
61.917	0.00	0.00	0.001	O	|	|	|	0.04
62.000	0.00	0.00	0.001	O	|	|	|	0.04
62.083	0.00	0.00	0.001	O	|	|	|	0.04
62.167	0.00	0.00	0.001	O	|	|	|	0.04
62.250	0.00	0.00	0.001	O	|	|	|	0.04
62.333	0.00	0.00	0.001	O	|	|	|	0.04
62.417	0.00	0.00	0.001	O	|	|	|	0.04
62.500	0.00	0.00	0.001	O	|	|	|	0.04
62.583	0.00	0.00	0.001	O	|	|	|	0.04
62.667	0.00	0.00	0.001	O	|	|	|	0.04
62.750	0.00	0.00	0.001	O	|	|	|	0.04
62.833	0.00	0.00	0.001	O	|	|	|	0.04
62.917	0.00	0.00	0.001	O	|	|	|	0.04
63.000	0.00	0.00	0.001	O	|	|	|	0.04
63.083	0.00	0.00	0.001	O	|	|	|	0.03
63.167	0.00	0.00	0.001	O	|	|	|	0.03
63.250	0.00	0.00	0.001	O	|	|	|	0.03
63.333	0.00	0.00	0.001	O	|	|	|	0.03
63.417	0.00	0.00	0.001	O	|	|	|	0.03
63.500	0.00	0.00	0.001	O	|	|	|	0.03
63.583	0.00	0.00	0.001	O	|	|	|	0.03
63.667	0.00	0.00	0.001	O	|	|	|	0.03
63.750	0.00	0.00	0.001	O	|	|	|	0.03
63.833	0.00	0.00	0.001	O	|	|	|	0.03
63.917	0.00	0.00	0.001	O	|	|	|	0.03
64.000	0.00	0.00	0.001	O	|	|	|	0.03
64.083	0.00	0.00	0.001	O	|	|	|	0.03
64.167	0.00	0.00	0.001	O	|	|	|	0.03
64.250	0.00	0.00	0.001	O	|	|	|	0.03
64.333	0.00	0.00	0.001	O	|	|	|	0.03
64.417	0.00	0.00	0.001	O	|	|	|	0.03
64.500	0.00	0.00	0.001	O	|	|	|	0.03
64.583	0.00	0.00	0.001	O	|	|	|	0.03
64.667	0.00	0.00	0.001	O	|	|	|	0.03
64.750	0.00	0.00	0.001	O	|	|	|	0.03
64.833	0.00	0.00	0.001	O	|	|	|	0.03

64.917	0.00	0.00	0.001	O	|	|	|	|	0.03
65.000	0.00	0.00	0.001	O	|	|	|	|	0.03
65.083	0.00	0.00	0.001	O	|	|	|	|	0.03
65.167	0.00	0.00	0.001	O	|	|	|	|	0.03
65.250	0.00	0.00	0.001	O	|	|	|	|	0.02
65.333	0.00	0.00	0.001	O	|	|	|	|	0.02
65.417	0.00	0.00	0.001	O	|	|	|	|	0.02
65.500	0.00	0.00	0.001	O	|	|	|	|	0.02
65.583	0.00	0.00	0.001	O	|	|	|	|	0.02
65.667	0.00	0.00	0.001	O	|	|	|	|	0.02
65.750	0.00	0.00	0.001	O	|	|	|	|	0.02
65.833	0.00	0.00	0.001	O	|	|	|	|	0.02
65.917	0.00	0.00	0.001	O	|	|	|	|	0.02
66.000	0.00	0.00	0.001	O	|	|	|	|	0.02

**********HYDROGRAPH DATA**********

Number of intervals = 792
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.045 (CFS)
Total volume = 0.173 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
5 yr
24 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris245.rte
**********HYDROGRAPH DATA**********
Number of intervals = 296
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.495 (CFS)
Total volume = 0.302 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 296
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.1 0.25 0.37 0.49	Depth (Ft.)
0.083	0.01	0.00	0.000	O	0.00
0.167	0.02	0.00	0.000	OI	0.00
0.250	0.02	0.00	0.000	OI	0.01
0.333	0.03	0.00	0.000	OI	0.02
0.417	0.04	0.00	0.001	O I	0.03
0.500	0.04	0.00	0.001	O I	0.04
0.583	0.04	0.00	0.001	O I	0.05
0.667	0.04	0.00	0.001	O I	0.06
0.750	0.04	0.00	0.002	O I	0.07
0.833	0.05	0.00	0.002	O I	0.08
0.917	0.05	0.00	0.002	O I	0.10
1.000	0.06	0.00	0.003	O I	0.11
1.083	0.05	0.01	0.003	O I	0.13
1.167	0.05	0.01	0.003	O I	0.14
1.250	0.05	0.01	0.004	O I	0.15
1.333	0.05	0.01	0.004	O I	0.16
1.417	0.04	0.01	0.004	O I	0.17
1.500	0.04	0.01	0.004	O I	0.18
1.583	0.04	0.01	0.005	O I	0.19
1.667	0.04	0.01	0.005	O I	0.20
1.750	0.04	0.01	0.005	O I	0.21
1.833	0.05	0.01	0.005	O I	0.22
1.917	0.05	0.01	0.006	O I	0.23
2.000	0.06	0.01	0.006	O I	0.25
2.083	0.06	0.01	0.006	O I	0.26
2.167	0.06	0.01	0.007	O I	0.27
2.250	0.06	0.01	0.007	O I	0.29
2.333	0.06	0.01	0.007	O I	0.30

2.417	0.06	0.01	0.007	O I |	|	|	|	0.31
2.500	0.06	0.01	0.008	O I |	|	|	|	0.32
2.583	0.06	0.02	0.008	O I |	|	|	|	0.34
2.667	0.07	0.02	0.008	|O I |	|	|	|	0.35
2.750	0.07	0.02	0.009	|O I |	|	|	|	0.37
2.833	0.07	0.02	0.009	|O I |	|	|	|	0.38
2.917	0.07	0.02	0.010	|O I |	|	|	|	0.40
3.000	0.07	0.02	0.010	|O I |	|	|	|	0.41
3.083	0.07	0.02	0.010	|O I |	|	|	|	0.43
3.167	0.07	0.02	0.011	|O I |	|	|	|	0.44
3.250	0.07	0.02	0.011	|O I |	|	|	|	0.46
3.333	0.07	0.02	0.011	|O I |	|	|	|	0.47
3.417	0.07	0.02	0.012	|O I |	|	|	|	0.49
3.500	0.07	0.02	0.012	|O I |	|	|	|	0.50
3.583	0.07	0.02	0.012	|O I |	|	|	|	0.52
3.667	0.07	0.02	0.013	|O I |	|	|	|	0.53
3.750	0.07	0.02	0.013	|O I |	|	|	|	0.55
3.833	0.08	0.03	0.013	|O I |	|	|	|	0.56
3.917	0.08	0.03	0.014	|O I |	|	|	|	0.58
4.000	0.09	0.03	0.014	|O I |	|	|	|	0.59
4.083	0.09	0.03	0.015	|O I |	|	|	|	0.61
4.167	0.09	0.03	0.015	|O I |	|	|	|	0.63
4.250	0.09	0.03	0.015	|O I |	|	|	|	0.64
4.333	0.09	0.03	0.016	|O I |	|	|	|	0.66
4.417	0.10	0.03	0.016	|O I |	|	|	|	0.68
4.500	0.10	0.03	0.017	| O I |	|	|	|	0.70
4.583	0.10	0.03	0.017	| O I |	|	|	|	0.72
4.667	0.10	0.03	0.018	| O I |	|	|	|	0.74
4.750	0.10	0.03	0.018	| O I |	|	|	|	0.76
4.833	0.10	0.03	0.019	| O I |	|	|	|	0.78
4.917	0.11	0.04	0.019	| O I|	|	|	|	0.80
5.000	0.11	0.04	0.020	| O I|	|	|	|	0.82
5.083	0.11	0.04	0.020	| O I|	|	|	|	0.84
5.167	0.10	0.04	0.021	| O I |	|	|	|	0.86
5.250	0.09	0.04	0.021	| O I |	|	|	|	0.88
5.333	0.09	0.04	0.021	| O I |	|	|	|	0.89
5.417	0.10	0.04	0.022	| O I |	|	|	|	0.91
5.500	0.10	0.04	0.022	| O I |	|	|	|	0.92
5.583	0.10	0.04	0.023	| O I |	|	|	|	0.94
5.667	0.11	0.04	0.023	| O I|	|	|	|	0.96
5.750	0.11	0.04	0.023	| O I|	|	|	|	0.98
5.833	0.12	0.04	0.024	| O I|	|	|	|	1.00
5.917	0.12	0.04	0.024	| O I|	|	|	|	1.01
6.000	0.12	0.04	0.025	| O I|	|	|	|	1.02
6.083	0.12	0.04	0.025	| O I|	|	|	|	1.04
6.167	0.13	0.04	0.026	| O I	|	|	|	1.05
6.250	0.13	0.04	0.027	| O I	|	|	|	1.06
6.333	0.13	0.04	0.027	| O I	|	|	|	1.08
6.417	0.13	0.04	0.028	| O I	|	|	|	1.09
6.500	0.13	0.04	0.028	| O I	|	|	|	1.11

6.583	0.13	0.04	0.029	O	I			1.12
6.667	0.14	0.04	0.030	O	I			1.14
6.750	0.14	0.04	0.030	O	I			1.16
6.833	0.14	0.04	0.031	O	I			1.17
6.917	0.15	0.04	0.032	O	I			1.19
7.000	0.15	0.04	0.032	O	I			1.21
7.083	0.15	0.04	0.033	O	I			1.23
7.167	0.15	0.04	0.034	O	I			1.24
7.250	0.15	0.04	0.034	O	I			1.26
7.333	0.15	0.04	0.035	O	I			1.28
7.417	0.16	0.04	0.036	O	I			1.30
7.500	0.16	0.04	0.037	O	I			1.32
7.583	0.16	0.04	0.037	O	I			1.34
7.667	0.17	0.04	0.038	O	I			1.36
7.750	0.17	0.04	0.039	O	I			1.38
7.833	0.18	0.04	0.040	O	I			1.40
7.917	0.18	0.04	0.041	O	I			1.42
8.000	0.19	0.04	0.042	O	I			1.45
8.083	0.19	0.04	0.043	O	I			1.47
8.167	0.21	0.04	0.044	O	I			1.50
8.250	0.21	0.04	0.045	O	I			1.53
8.333	0.22	0.04	0.046	O	I			1.56
8.417	0.22	0.04	0.047	O	I			1.59
8.500	0.22	0.04	0.049	O	I			1.62
8.583	0.22	0.04	0.050	O	I			1.65
8.667	0.23	0.04	0.051	O	I			1.68
8.750	0.23	0.04	0.052	O	I			1.71
8.833	0.24	0.04	0.054	O	I			1.74
8.917	0.24	0.04	0.055	O	I			1.78
9.000	0.25	0.04	0.056	O	I			1.81
9.083	0.25	0.04	0.058	O	I			1.84
9.167	0.27	0.04	0.059	O	I			1.88
9.250	0.27	0.04	0.061	O	I			1.92
9.333	0.28	0.04	0.062	O	I			1.96
9.417	0.29	0.04	0.064	O	I			2.00
9.500	0.29	0.04	0.066	O	I			2.04
9.583	0.29	0.04	0.067	O	I			2.08
9.667	0.30	0.04	0.069	O	I			2.13
9.750	0.30	0.04	0.071	O	I			2.17
9.833	0.31	0.04	0.073	O	I			2.22
9.917	0.32	0.04	0.075	O	I			2.26
10.000	0.32	0.04	0.076	O	I			2.31
10.083	0.30	0.04	0.078	O	I			2.36
10.167	0.25	0.04	0.080	O	I			2.40
10.250	0.24	0.04	0.081	O	I			2.43
10.333	0.23	0.04	0.083	O	I			2.46
10.417	0.23	0.04	0.084	O	I			2.49
10.500	0.22	0.04	0.085	O	I			2.53
10.583	0.23	0.04	0.086	O	I			2.56
10.667	0.27	0.04	0.088	O	I			2.59

```
10.750    0.28    0.04      0.089   | O     |        | I     |        |     2.63
10.833    0.28    0.04      0.091   | O     |        | I     |        |     2.67
10.917    0.29    0.04      0.093   | O     |        | I     |        |     2.71
11.000    0.29    0.04      0.094   | O     |        | I     |        |     2.76
11.083    0.29    0.04      0.096   | O     |        | I     |        |     2.80
11.167    0.28    0.04      0.098   | O     |        | I     |        |     2.84
11.250    0.28    0.04      0.099   | O     |        | I     |        |     2.88
11.333    0.28    0.04      0.101   | O     |        | I     |        |     2.92
11.417    0.28    0.04      0.102   | O     |        | I     |        |     2.96
11.500    0.28    0.04      0.104   | O     |        | I     |        |     3.00
11.583    0.27    0.04      0.106   | O     |        |I      |        |     3.04
11.667    0.26    0.04      0.107   | O     |        I       |        |     3.08
11.750    0.25    0.04      0.109   | O     |        I       |        |     3.12
11.833    0.25    0.04      0.110   | O     |        I       |        |     3.15
11.917    0.26    0.04      0.112   | O     |        I       |        |     3.19
12.000    0.26    0.04      0.113   | O     |        I       |        |     3.23
12.083    0.28    0.04      0.115   | O     |        | I     |        |     3.26
12.167    0.33    0.04      0.116   | O     |        |    I  |        |     3.31
12.250    0.35    0.04      0.118   | O     |        |     I |        |     3.36
12.333    0.36    0.04      0.121   | O     |        |      I|        |     3.41
12.417    0.37    0.04      0.123   | O     |        |      I|        |     3.47
12.500    0.37    0.04      0.125   | O     |        |       I        |     3.52
12.583    0.38    0.04      0.127   | O     |        |       I        |     3.58
12.667    0.40    0.04      0.130   | O     |        |       |I       |     3.64
12.750    0.40    0.04      0.132   | O     |        |       | I      |     3.70
12.833    0.41    0.04      0.135   | O     |        |       | I      |     3.76
12.917    0.42    0.04      0.137   | O     |        |       | I      |     3.83
13.000    0.42    0.04      0.140   | O     |        |       |  I     |     3.89
13.083    0.44    0.04      0.142   | O     |        |       |   I    |     3.96
13.167    0.47    0.04      0.145   | O     |        |       |     I  |     4.03
13.250    0.48    0.04      0.148   | O     |        |       |      I|     4.10
13.333    0.49    0.04      0.151   | O     |        |       |      I|     4.18
13.417    0.49    0.04      0.154   | O     |        |       |      I|     4.26
13.500    0.49    0.04      0.157   | O     |        |       |       I     4.33
13.583    0.47    0.04      0.160   | O     |        |       |     I  |     4.41
13.667    0.39    0.04      0.163   | O     |        |       |I       |     4.47
13.750    0.37    0.04      0.165   | O     |        |      I|        |     4.53
13.833    0.35    0.04      0.167   | O     |        |     I |        |     4.58
13.917    0.35    0.04      0.169   | O     |        |     I |        |     4.64
14.000    0.34    0.04      0.172   | O     |        |     I |        |     4.69
14.083    0.35    0.04      0.174   | O     |        |     I |        |     4.74
14.167    0.38    0.04      0.176   | O     |        |       I        |     4.79
14.250    0.38    0.04      0.178   | O     |        |       I        |     4.85
14.333    0.39    0.04      0.180   | O     |        |       I        |     4.91
14.417    0.38    0.04      0.183   | O     |        |       I        |     4.96
14.500    0.38    0.04      0.185   | O     |        |       I        |     5.02
14.583    0.38    0.04      0.187   | O     |        |       I        |     5.08
14.667    0.38    0.04      0.190   | O     |        |       I        |     5.14
14.750    0.38    0.04      0.192   | O     |        |       I        |     5.19
14.833    0.38    0.04      0.194   | O     |        |       I        |     5.25
```

14.917	0.37	0.04	0.197	O			I	5.31
15.000	0.37	0.04	0.199	O			I	5.36
15.083	0.36	0.04	0.201	O			I	5.42
15.167	0.36	0.04	0.203	O			I	5.47
15.250	0.35	0.04	0.205	O			I	5.52
15.333	0.35	0.04	0.208	O			I	5.57
15.417	0.34	0.04	0.210	O			I	5.63
15.500	0.34	0.04	0.212	O			I	5.68
15.583	0.33	0.04	0.214	O			I	5.73
15.667	0.30	0.04	0.215	O		I		5.77
15.750	0.29	0.04	0.217	O		I		5.81
15.833	0.28	0.04	0.219	O		I		5.85
15.917	0.28	0.04	0.220	O		I		5.89
16.000	0.28	0.04	0.222	O		I		5.93
16.083	0.24	0.04	0.224	O	I			5.97
16.167	0.13	0.04	0.225	O	I			6.00
16.250	0.10	0.04	0.225	O	I			6.01
16.333	0.08	0.04	0.225	O	I			6.02
16.417	0.07	0.04	0.226	O	I			6.02
16.500	0.07	0.04	0.226	O	I			6.02
16.583	0.06	0.04	0.226	O	I			6.03
16.667	0.05	0.04	0.226	O	I			6.03
16.750	0.05	0.04	0.226	O	I			6.03
16.833	0.05	0.04	0.226	O				6.03
16.917	0.04	0.04	0.226	O				6.03
17.000	0.04	0.04	0.226	O				6.03
17.083	0.05	0.04	0.226	O	I			6.03
17.167	0.06	0.04	0.226	O	I			6.03
17.250	0.07	0.04	0.226	O	I			6.04
17.333	0.07	0.04	0.226	O	I			6.04
17.417	0.07	0.04	0.227	O	I			6.04
17.500	0.07	0.04	0.227	O	I			6.05
17.583	0.07	0.04	0.227	O	I			6.05
17.667	0.07	0.04	0.227	O	I			6.06
17.750	0.07	0.04	0.227	O	I			6.06
17.833	0.07	0.04	0.227	O	I			6.07
17.917	0.06	0.04	0.228	O	I			6.07
18.000	0.06	0.04	0.228	O	I			6.07
18.083	0.06	0.04	0.228	O	I			6.08
18.167	0.06	0.04	0.228	O	I			6.08
18.250	0.06	0.04	0.228	O	I			6.08
18.333	0.06	0.04	0.228	O	I			6.08
18.417	0.06	0.04	0.228	O	I			6.09
18.500	0.06	0.04	0.228	O	I			6.09
18.583	0.06	0.04	0.228	O	I			6.09
18.667	0.05	0.04	0.228	O	I			6.09
18.750	0.05	0.04	0.229	O	I			6.09
18.833	0.04	0.04	0.229	O				6.09
18.917	0.04	0.04	0.228	O				6.09
19.000	0.03	0.04	0.228	O				6.09

19.083	0.03	0.04	0.228	O				6.09
19.167	0.04	0.04	0.228	O				6.09
19.250	0.04	0.04	0.228	O				6.09
19.333	0.05	0.04	0.228	O				6.09
19.417	0.05	0.04	0.228	OI				6.09
19.500	0.06	0.04	0.228	OI				6.09
19.583	0.05	0.04	0.228	OI				6.09
19.667	0.05	0.04	0.228	OI				6.09
19.750	0.05	0.04	0.228	O				6.09
19.833	0.04	0.04	0.228	O				6.09
19.917	0.04	0.04	0.228	O				6.09
20.000	0.03	0.04	0.228	O				6.09
20.083	0.03	0.04	0.228	O				6.09
20.167	0.04	0.04	0.228	O				6.08
20.250	0.04	0.04	0.228	O				6.08
20.333	0.04	0.04	0.228	O				6.08
20.417	0.04	0.04	0.228	O				6.08
20.500	0.04	0.04	0.228	O				6.08
20.583	0.04	0.04	0.228	O				6.08
20.667	0.04	0.04	0.228	O				6.08
20.750	0.04	0.04	0.228	O				6.08
20.833	0.04	0.04	0.228	O				6.08
20.917	0.03	0.04	0.228	O				6.08
21.000	0.03	0.04	0.228	O				6.08
21.083	0.03	0.04	0.228	O				6.08
21.167	0.04	0.04	0.228	O				6.07
21.250	0.04	0.04	0.228	O				6.07
21.333	0.04	0.04	0.228	O				6.07
21.417	0.03	0.04	0.228	O				6.07
21.500	0.03	0.04	0.228	O				6.07
21.583	0.03	0.04	0.227	O				6.07
21.667	0.04	0.04	0.227	O				6.07
21.750	0.04	0.04	0.227	O				6.07
21.833	0.04	0.04	0.227	O				6.06
21.917	0.03	0.04	0.227	O				6.06
22.000	0.03	0.04	0.227	O				6.06
22.083	0.03	0.04	0.227	O				6.06
22.167	0.04	0.04	0.227	O				6.06
22.250	0.04	0.04	0.227	O				6.06
22.333	0.04	0.04	0.227	O				6.06
22.417	0.03	0.04	0.227	O				6.05
22.500	0.03	0.04	0.227	O				6.05
22.583	0.03	0.04	0.227	IO				6.05
22.667	0.03	0.04	0.227	IO				6.05
22.750	0.03	0.04	0.227	IO				6.04
22.833	0.03	0.04	0.226	IO				6.04
22.917	0.03	0.04	0.226	IO				6.04
23.000	0.03	0.04	0.226	IO				6.04
23.083	0.03	0.04	0.226	IO				6.03
23.167	0.03	0.04	0.226	IO				6.03

23.250	0.03	0.04	0.226	IO				6.03
23.333	0.03	0.04	0.226	IO				6.03
23.417	0.03	0.04	0.226	IO				6.02
23.500	0.03	0.04	0.226	IO				6.02
23.583	0.03	0.04	0.225	IO				6.02
23.667	0.03	0.04	0.225	IO				6.02
23.750	0.03	0.04	0.225	IO				6.01
23.833	0.03	0.04	0.225	IO				6.01
23.917	0.03	0.04	0.225	IO				6.01
24.000	0.03	0.04	0.225	IO				6.00
24.083	0.02	0.04	0.225	IO				6.00
24.167	0.01	0.04	0.225	I O				6.00
24.250	0.01	0.04	0.224	I O				5.99
24.333	0.00	0.04	0.224	I O				5.98
24.417	0.00	0.04	0.224	I O				5.98
24.500	0.00	0.04	0.223	I O				5.97
24.583	0.00	0.04	0.223	I O				5.96
24.667	0.00	0.04	0.223	I O				5.95
24.750	0.00	0.04	0.223	I O				5.95
24.833	0.00	0.04	0.222	I O				5.94
24.917	0.00	0.04	0.222	I O				5.93
25.000	0.00	0.04	0.222	I O				5.92
25.083	0.00	0.04	0.221	I O				5.92
25.167	0.00	0.04	0.221	I O				5.91
25.250	0.00	0.04	0.221	I O				5.90
25.333	0.00	0.04	0.220	I O				5.89
25.417	0.00	0.04	0.220	I O				5.88
25.500	0.00	0.04	0.220	I O				5.88
25.583	0.00	0.04	0.219	I O				5.87
25.667	0.00	0.04	0.219	I O				5.86
25.750	0.00	0.04	0.219	I O				5.85
25.833	0.00	0.04	0.219	I O				5.85
25.917	0.00	0.04	0.218	I O				5.84
26.000	0.00	0.04	0.218	I O				5.83
26.083	0.00	0.04	0.218	I O				5.82
26.167	0.00	0.04	0.217	I O				5.82
26.250	0.00	0.04	0.217	I O				5.81
26.333	0.00	0.04	0.217	I O				5.80
26.417	0.00	0.04	0.216	I O				5.79
26.500	0.00	0.04	0.216	I O				5.79
26.583	0.00	0.04	0.216	I O				5.78
26.667	0.00	0.04	0.215	I O				5.77
26.750	0.00	0.04	0.215	I O				5.76
26.833	0.00	0.04	0.215	I O				5.75
26.917	0.00	0.04	0.215	I O				5.75
27.000	0.00	0.04	0.214	I O				5.74
27.083	0.00	0.04	0.214	I O				5.73
27.167	0.00	0.04	0.214	I O				5.72
27.250	0.00	0.04	0.213	I O				5.72
27.333	0.00	0.04	0.213	I O				5.71

27.417	0.00	0.04	0.213	I O				5.70
27.500	0.00	0.04	0.212	I O				5.69
27.583	0.00	0.04	0.212	I O				5.69
27.667	0.00	0.04	0.212	I O				5.68
27.750	0.00	0.04	0.211	I O				5.67
27.833	0.00	0.04	0.211	I O				5.66
27.917	0.00	0.04	0.211	I O				5.66
28.000	0.00	0.04	0.210	I O				5.65
28.083	0.00	0.04	0.210	I O				5.64
28.167	0.00	0.04	0.210	I O				5.63
28.250	0.00	0.04	0.210	I O				5.62
28.333	0.00	0.04	0.209	I O				5.62
28.417	0.00	0.04	0.209	I O				5.61
28.500	0.00	0.04	0.209	I O				5.60
28.583	0.00	0.04	0.208	I O				5.59
28.667	0.00	0.04	0.208	I O				5.59
28.750	0.00	0.04	0.208	I O				5.58
28.833	0.00	0.04	0.207	I O				5.57
28.917	0.00	0.04	0.207	I O				5.56
29.000	0.00	0.04	0.207	I O				5.56
29.083	0.00	0.04	0.206	I O				5.55
29.167	0.00	0.04	0.206	I O				5.54
29.250	0.00	0.04	0.206	I O				5.53
29.333	0.00	0.04	0.206	I O				5.53
29.417	0.00	0.04	0.205	I O				5.52
29.500	0.00	0.04	0.205	I O				5.51
29.583	0.00	0.04	0.205	I O				5.50
29.667	0.00	0.04	0.204	I O				5.49
29.750	0.00	0.04	0.204	I O				5.49
29.833	0.00	0.04	0.204	I O				5.48
29.917	0.00	0.04	0.203	I O				5.47
30.000	0.00	0.04	0.203	I O				5.46
30.083	0.00	0.04	0.203	I O				5.46
30.167	0.00	0.04	0.202	I O				5.45
30.250	0.00	0.04	0.202	I O				5.44
30.333	0.00	0.04	0.202	I O				5.43
30.417	0.00	0.04	0.201	I O				5.43
30.500	0.00	0.04	0.201	I O				5.42
30.583	0.00	0.04	0.201	I O				5.41
30.667	0.00	0.04	0.201	I O				5.40
30.750	0.00	0.04	0.200	I O				5.40
30.833	0.00	0.04	0.200	I O				5.39
30.917	0.00	0.04	0.200	I O				5.38
31.000	0.00	0.04	0.199	I O				5.37
31.083	0.00	0.04	0.199	I O				5.36
31.167	0.00	0.04	0.199	I O				5.36
31.250	0.00	0.04	0.198	I O				5.35
31.333	0.00	0.04	0.198	I O				5.34
31.417	0.00	0.04	0.198	I O				5.33
31.500	0.00	0.04	0.197	I O				5.33

31.583	0.00	0.04	0.197	I	O	|	|	|	5.32
31.667	0.00	0.04	0.197	I	O	|	|	|	5.31
31.750	0.00	0.04	0.197	I	O	|	|	|	5.30
31.833	0.00	0.04	0.196	I	O	|	|	|	5.30
31.917	0.00	0.04	0.196	I	O	|	|	|	5.29
32.000	0.00	0.04	0.196	I	O	|	|	|	5.28
32.083	0.00	0.04	0.195	I	O	|	|	|	5.27
32.167	0.00	0.04	0.195	I	O	|	|	|	5.27
32.250	0.00	0.04	0.195	I	O	|	|	|	5.26
32.333	0.00	0.04	0.194	I	O	|	|	|	5.25
32.417	0.00	0.04	0.194	I	O	|	|	|	5.24
32.500	0.00	0.04	0.194	I	O	|	|	|	5.23
32.583	0.00	0.04	0.193	I	O	|	|	|	5.23
32.667	0.00	0.04	0.193	I	O	|	|	|	5.22
32.750	0.00	0.04	0.193	I	O	|	|	|	5.21
32.833	0.00	0.04	0.193	I	O	|	|	|	5.20
32.917	0.00	0.04	0.192	I	O	|	|	|	5.20
33.000	0.00	0.04	0.192	I	O	|	|	|	5.19
33.083	0.00	0.04	0.192	I	O	|	|	|	5.18
33.167	0.00	0.04	0.191	I	O	|	|	|	5.17
33.250	0.00	0.04	0.191	I	O	|	|	|	5.17
33.333	0.00	0.04	0.191	I	O	|	|	|	5.16
33.417	0.00	0.04	0.190	I	O	|	|	|	5.15
33.500	0.00	0.04	0.190	I	O	|	|	|	5.14
33.583	0.00	0.04	0.190	I	O	|	|	|	5.14
33.667	0.00	0.04	0.189	I	O	|	|	|	5.13
33.750	0.00	0.04	0.189	I	O	|	|	|	5.12
33.833	0.00	0.04	0.189	I	O	|	|	|	5.11
33.917	0.00	0.04	0.188	I	O	|	|	|	5.10
34.000	0.00	0.04	0.188	I	O	|	|	|	5.10
34.083	0.00	0.04	0.188	I	O	|	|	|	5.09
34.167	0.00	0.04	0.188	I	O	|	|	|	5.08
34.250	0.00	0.04	0.187	I	O	|	|	|	5.07
34.333	0.00	0.04	0.187	I	O	|	|	|	5.07
34.417	0.00	0.04	0.187	I	O	|	|	|	5.06
34.500	0.00	0.04	0.186	I	O	|	|	|	5.05
34.583	0.00	0.04	0.186	I	O	|	|	|	5.04
34.667	0.00	0.04	0.186	I	O	|	|	|	5.04
34.750	0.00	0.04	0.185	I	O	|	|	|	5.03
34.833	0.00	0.04	0.185	I	O	|	|	|	5.02
34.917	0.00	0.04	0.185	I	O	|	|	|	5.01
35.000	0.00	0.04	0.184	I	O	|	|	|	5.00
35.083	0.00	0.04	0.184	I	O	|	|	|	5.00
35.167	0.00	0.04	0.184	I	O	|	|	|	4.99
35.250	0.00	0.04	0.184	I	O	|	|	|	4.98
35.333	0.00	0.04	0.183	I	O	|	|	|	4.97
35.417	0.00	0.04	0.183	I	O	|	|	|	4.97
35.500	0.00	0.04	0.183	I	O	|	|	|	4.96
35.583	0.00	0.04	0.182	I	O	|	|	|	4.95
35.667	0.00	0.04	0.182	I	O	|	|	|	4.94

35.750	0.00	0.04	0.182	I O				4.94
35.833	0.00	0.04	0.181	I O				4.93
35.917	0.00	0.04	0.181	I O				4.92
36.000	0.00	0.04	0.181	I O				4.91
36.083	0.00	0.04	0.180	I O				4.91
36.167	0.00	0.04	0.180	I O				4.90
36.250	0.00	0.04	0.180	I O				4.89
36.333	0.00	0.04	0.179	I O				4.88
36.417	0.00	0.04	0.179	I O				4.87
36.500	0.00	0.04	0.179	I O				4.87
36.583	0.00	0.04	0.179	I O				4.86
36.667	0.00	0.04	0.178	I O				4.85
36.750	0.00	0.04	0.178	I O				4.84
36.833	0.00	0.04	0.178	I O				4.84
36.917	0.00	0.04	0.177	I O				4.83
37.000	0.00	0.04	0.177	I O				4.82
37.083	0.00	0.04	0.177	I O				4.81
37.167	0.00	0.04	0.176	I O				4.81
37.250	0.00	0.04	0.176	I O				4.80
37.333	0.00	0.04	0.176	I O				4.79
37.417	0.00	0.04	0.175	I O				4.78
37.500	0.00	0.04	0.175	I O				4.78
37.583	0.00	0.04	0.175	I O				4.77
37.667	0.00	0.04	0.175	I O				4.76
37.750	0.00	0.04	0.174	I O				4.75
37.833	0.00	0.04	0.174	I O				4.74
37.917	0.00	0.04	0.174	I O				4.74
38.000	0.00	0.04	0.173	I O				4.73
38.083	0.00	0.04	0.173	I O				4.72
38.167	0.00	0.04	0.173	I O				4.71
38.250	0.00	0.04	0.172	I O				4.71
38.333	0.00	0.04	0.172	I O				4.70
38.417	0.00	0.04	0.172	I O				4.69
38.500	0.00	0.04	0.171	I O				4.68
38.583	0.00	0.04	0.171	I O				4.68
38.667	0.00	0.04	0.171	I O				4.67
38.750	0.00	0.04	0.171	I O				4.66
38.833	0.00	0.04	0.170	I O				4.65
38.917	0.00	0.04	0.170	I O				4.65
39.000	0.00	0.04	0.170	I O				4.64
39.083	0.00	0.04	0.169	I O				4.63
39.167	0.00	0.04	0.169	I O				4.62
39.250	0.00	0.04	0.169	I O				4.61
39.333	0.00	0.04	0.168	I O				4.61
39.417	0.00	0.04	0.168	I O				4.60
39.500	0.00	0.04	0.168	I O				4.59
39.583	0.00	0.04	0.167	I O				4.58
39.667	0.00	0.04	0.167	I O				4.58
39.750	0.00	0.04	0.167	I O				4.57
39.833	0.00	0.04	0.166	I O				4.56

39.917	0.00	0.04	0.166	I	O				4.55
40.000	0.00	0.04	0.166	I	O				4.55
40.083	0.00	0.04	0.166	I	O				4.54
40.167	0.00	0.04	0.165	I	O				4.53
40.250	0.00	0.04	0.165	I	O				4.52
40.333	0.00	0.04	0.165	I	O				4.52
40.417	0.00	0.04	0.164	I	O				4.51
40.500	0.00	0.04	0.164	I	O				4.50
40.583	0.00	0.04	0.164	I	O				4.49
40.667	0.00	0.04	0.163	I	O				4.48
40.750	0.00	0.04	0.163	I	O				4.48
40.833	0.00	0.04	0.163	I	O				4.47
40.917	0.00	0.04	0.162	I	O				4.46
41.000	0.00	0.04	0.162	I	O				4.45
41.083	0.00	0.04	0.162	I	O				4.45
41.167	0.00	0.04	0.162	I	O				4.44
41.250	0.00	0.04	0.161	I	O				4.43
41.333	0.00	0.04	0.161	I	O				4.42
41.417	0.00	0.04	0.161	I	O				4.41
41.500	0.00	0.04	0.160	I	O				4.41
41.583	0.00	0.04	0.160	I	O				4.40
41.667	0.00	0.04	0.160	I	O				4.39
41.750	0.00	0.04	0.159	I	O				4.38
41.833	0.00	0.04	0.159	I	O				4.38
41.917	0.00	0.04	0.159	I	O				4.37
42.000	0.00	0.04	0.158	I	O				4.36
42.083	0.00	0.04	0.158	I	O				4.35
42.167	0.00	0.04	0.158	I	O				4.34
42.250	0.00	0.04	0.157	I	O				4.34
42.333	0.00	0.04	0.157	I	O				4.33
42.417	0.00	0.04	0.157	I	O				4.32
42.500	0.00	0.04	0.157	I	O				4.31
42.583	0.00	0.04	0.156	I	O				4.31
42.667	0.00	0.04	0.156	I	O				4.30
42.750	0.00	0.04	0.156	I	O				4.29
42.833	0.00	0.04	0.155	I	O				4.28
42.917	0.00	0.04	0.155	I	O				4.28
43.000	0.00	0.04	0.155	I	O				4.27
43.083	0.00	0.04	0.154	I	O				4.26
43.167	0.00	0.04	0.154	I	O				4.25
43.250	0.00	0.04	0.154	I	O				4.24
43.333	0.00	0.04	0.153	I	O				4.24
43.417	0.00	0.04	0.153	I	O				4.23
43.500	0.00	0.04	0.153	I	O				4.22
43.583	0.00	0.04	0.153	I	O				4.21
43.667	0.00	0.04	0.152	I	O				4.21
43.750	0.00	0.04	0.152	I	O				4.20
43.833	0.00	0.04	0.152	I	O				4.19
43.917	0.00	0.04	0.151	I	O				4.18
44.000	0.00	0.04	0.151	I	O				4.17

44.083	0.00	0.04	0.151	I O				4.17
44.167	0.00	0.04	0.150	I O				4.16
44.250	0.00	0.04	0.150	I O				4.15
44.333	0.00	0.04	0.150	I O				4.14
44.417	0.00	0.04	0.149	I O				4.14
44.500	0.00	0.04	0.149	I O				4.13
44.583	0.00	0.04	0.149	I O				4.12
44.667	0.00	0.04	0.148	I O				4.11
44.750	0.00	0.04	0.148	I O				4.10
44.833	0.00	0.04	0.148	I O				4.10
44.917	0.00	0.04	0.148	I O				4.09
45.000	0.00	0.04	0.147	I O				4.08
45.083	0.00	0.04	0.147	I O				4.07
45.167	0.00	0.04	0.147	I O				4.07
45.250	0.00	0.04	0.146	I O				4.06
45.333	0.00	0.04	0.146	I O				4.05
45.417	0.00	0.04	0.146	I O				4.04
45.500	0.00	0.04	0.145	I O				4.03
45.583	0.00	0.04	0.145	I O				4.03
45.667	0.00	0.04	0.145	I O				4.02
45.750	0.00	0.04	0.144	I O				4.01
45.833	0.00	0.04	0.144	I O				4.00
45.917	0.00	0.04	0.144	I O				4.00
46.000	0.00	0.04	0.144	I O				3.99
46.083	0.00	0.04	0.143	I O				3.98
46.167	0.00	0.04	0.143	I O				3.97
46.250	0.00	0.04	0.143	I O				3.97
46.333	0.00	0.04	0.142	I O				3.96
46.417	0.00	0.04	0.142	I O				3.95
46.500	0.00	0.04	0.142	I O				3.94
46.583	0.00	0.04	0.141	I O				3.93
46.667	0.00	0.04	0.141	I O				3.93
46.750	0.00	0.04	0.141	I O				3.92
46.833	0.00	0.04	0.140	I O				3.91
46.917	0.00	0.04	0.140	I O				3.90
47.000	0.00	0.04	0.140	I O				3.90
47.083	0.00	0.04	0.140	I O				3.89
47.167	0.00	0.04	0.139	I O				3.88
47.250	0.00	0.04	0.139	I O				3.87
47.333	0.00	0.04	0.139	I O				3.86
47.417	0.00	0.04	0.138	I O				3.86
47.500	0.00	0.04	0.138	I O				3.85
47.583	0.00	0.04	0.138	I O				3.84
47.667	0.00	0.04	0.137	I O				3.83
47.750	0.00	0.04	0.137	I O				3.83
47.833	0.00	0.04	0.137	I O				3.82
47.917	0.00	0.04	0.136	I O				3.81
48.000	0.00	0.04	0.136	I O				3.80
48.083	0.00	0.04	0.136	I O				3.79
48.167	0.00	0.04	0.135	I O				3.79

48.250	0.00	0.04	0.135	I O				3.78
48.333	0.00	0.04	0.135	I O				3.77
48.417	0.00	0.04	0.135	I O				3.76
48.500	0.00	0.04	0.134	I O				3.76
48.583	0.00	0.04	0.134	I O				3.75
48.667	0.00	0.04	0.134	I O				3.74
48.750	0.00	0.04	0.133	I O				3.73
48.833	0.00	0.04	0.133	I O				3.73
48.917	0.00	0.04	0.133	I O				3.72
49.000	0.00	0.04	0.132	I O				3.71
49.083	0.00	0.04	0.132	I O				3.70
49.167	0.00	0.04	0.132	I O				3.69
49.250	0.00	0.04	0.131	I O				3.69
49.333	0.00	0.04	0.131	I O				3.68
49.417	0.00	0.04	0.131	I O				3.67
49.500	0.00	0.04	0.131	I O				3.66
49.583	0.00	0.04	0.130	I O				3.66
49.667	0.00	0.04	0.130	I O				3.65
49.750	0.00	0.04	0.130	I O				3.64
49.833	0.00	0.04	0.129	I O				3.63
49.917	0.00	0.04	0.129	I O				3.62
50.000	0.00	0.04	0.129	I O				3.62
50.083	0.00	0.04	0.128	I O				3.61
50.167	0.00	0.04	0.128	I O				3.60
50.250	0.00	0.04	0.128	I O				3.59
50.333	0.00	0.04	0.127	I O				3.59
50.417	0.00	0.04	0.127	I O				3.58
50.500	0.00	0.04	0.127	I O				3.57
50.583	0.00	0.04	0.126	I O				3.56
50.667	0.00	0.04	0.126	I O				3.55
50.750	0.00	0.04	0.126	I O				3.55
50.833	0.00	0.04	0.126	I O				3.54
50.917	0.00	0.04	0.125	I O				3.53
51.000	0.00	0.04	0.125	I O				3.52
51.083	0.00	0.04	0.125	I O				3.52
51.167	0.00	0.04	0.124	I O				3.51
51.250	0.00	0.04	0.124	I O				3.50
51.333	0.00	0.04	0.124	I O				3.49
51.417	0.00	0.04	0.123	I O				3.48
51.500	0.00	0.04	0.123	I O				3.48
51.583	0.00	0.04	0.123	I O				3.47
51.667	0.00	0.04	0.122	I O				3.46
51.750	0.00	0.04	0.122	I O				3.45
51.833	0.00	0.04	0.122	I O				3.45
51.917	0.00	0.04	0.122	I O				3.44
52.000	0.00	0.04	0.121	I O				3.43
52.083	0.00	0.04	0.121	I O				3.42
52.167	0.00	0.04	0.121	I O				3.42
52.250	0.00	0.04	0.120	I O				3.41
52.333	0.00	0.04	0.120	I O				3.40

52.417	0.00	0.04	0.120	I O				3.39
52.500	0.00	0.04	0.119	I O				3.38
52.583	0.00	0.04	0.119	I O				3.38
52.667	0.00	0.04	0.119	I O				3.37
52.750	0.00	0.04	0.118	I O				3.36
52.833	0.00	0.04	0.118	I O				3.35
52.917	0.00	0.04	0.118	I O				3.35
53.000	0.00	0.04	0.118	I O				3.34
53.083	0.00	0.04	0.117	I O				3.33
53.167	0.00	0.04	0.117	I O				3.32
53.250	0.00	0.04	0.117	I O				3.31
53.333	0.00	0.04	0.116	I O				3.31
53.417	0.00	0.04	0.116	I O				3.30
53.500	0.00	0.04	0.116	I O				3.29
53.583	0.00	0.04	0.115	I O				3.28
53.667	0.00	0.04	0.115	I O				3.28
53.750	0.00	0.04	0.115	I O				3.27
53.833	0.00	0.04	0.114	I O				3.26
53.917	0.00	0.04	0.114	I O				3.25
54.000	0.00	0.04	0.114	I O				3.24
54.083	0.00	0.04	0.113	I O				3.24
54.167	0.00	0.04	0.113	I O				3.23
54.250	0.00	0.04	0.113	I O				3.22
54.333	0.00	0.04	0.113	I O				3.21
54.417	0.00	0.04	0.112	I O				3.21
54.500	0.00	0.04	0.112	I O				3.20
54.583	0.00	0.04	0.112	I O				3.19
54.667	0.00	0.04	0.111	I O				3.18
54.750	0.00	0.04	0.111	I O				3.17
54.833	0.00	0.04	0.111	I O				3.17
54.917	0.00	0.04	0.110	I O				3.16
55.000	0.00	0.04	0.110	I O				3.15
55.083	0.00	0.04	0.110	I O				3.14
55.167	0.00	0.04	0.109	I O				3.14
55.250	0.00	0.04	0.109	I O				3.13
55.333	0.00	0.04	0.109	I O				3.12
55.417	0.00	0.04	0.109	I O				3.11
55.500	0.00	0.04	0.108	I O				3.11
55.583	0.00	0.04	0.108	I O				3.10
55.667	0.00	0.04	0.108	I O				3.09
55.750	0.00	0.04	0.107	I O				3.08
55.833	0.00	0.04	0.107	I O				3.07
55.917	0.00	0.04	0.107	I O				3.07
56.000	0.00	0.04	0.106	I O				3.06
56.083	0.00	0.04	0.106	I O				3.05
56.167	0.00	0.04	0.106	I O				3.04
56.250	0.00	0.04	0.105	I O				3.04
56.333	0.00	0.04	0.105	I O				3.03
56.417	0.00	0.04	0.105	I O				3.02
56.500	0.00	0.04	0.104	I O				3.01

56.583	0.00	0.04	0.104	I	O	|	|	|	3.00
56.667	0.00	0.04	0.104	I	O	|	|	|	3.00
56.750	0.00	0.04	0.104	I	O	|	|	|	2.99
56.833	0.00	0.04	0.103	I	O	|	|	|	2.98
56.917	0.00	0.04	0.103	I	O	|	|	|	2.97
57.000	0.00	0.04	0.103	I	O	|	|	|	2.97
57.083	0.00	0.04	0.102	I	O	|	|	|	2.96
57.167	0.00	0.04	0.102	I	O	|	|	|	2.95
57.250	0.00	0.04	0.102	I	O	|	|	|	2.94
57.333	0.00	0.04	0.101	I	O	|	|	|	2.93
57.417	0.00	0.04	0.101	I	O	|	|	|	2.93
57.500	0.00	0.04	0.101	I	O	|	|	|	2.92
57.583	0.00	0.04	0.100	I	O	|	|	|	2.91
57.667	0.00	0.04	0.100	I	O	|	|	|	2.90
57.750	0.00	0.04	0.100	I	O	|	|	|	2.90
57.833	0.00	0.04	0.100	I	O	|	|	|	2.89
57.917	0.00	0.04	0.099	I	O	|	|	|	2.88
58.000	0.00	0.04	0.099	I	O	|	|	|	2.87
58.083	0.00	0.04	0.099	I	O	|	|	|	2.87
58.167	0.00	0.04	0.098	I	O	|	|	|	2.86
58.250	0.00	0.04	0.098	I	O	|	|	|	2.85
58.333	0.00	0.04	0.098	I	O	|	|	|	2.84
58.417	0.00	0.04	0.097	I	O	|	|	|	2.83
58.500	0.00	0.04	0.097	I	O	|	|	|	2.83
58.583	0.00	0.04	0.097	I	O	|	|	|	2.82
58.667	0.00	0.04	0.096	I	O	|	|	|	2.81
58.750	0.00	0.04	0.096	I	O	|	|	|	2.80
58.833	0.00	0.04	0.096	I	O	|	|	|	2.80
58.917	0.00	0.04	0.096	I	O	|	|	|	2.79
59.000	0.00	0.04	0.095	I	O	|	|	|	2.78
59.083	0.00	0.04	0.095	I	O	|	|	|	2.77
59.167	0.00	0.04	0.095	I	O	|	|	|	2.76
59.250	0.00	0.04	0.094	I	O	|	|	|	2.76
59.333	0.00	0.04	0.094	I	O	|	|	|	2.75
59.417	0.00	0.04	0.094	I	O	|	|	|	2.74
59.500	0.00	0.04	0.093	I	O	|	|	|	2.73
59.583	0.00	0.04	0.093	I	O	|	|	|	2.73
59.667	0.00	0.04	0.093	I	O	|	|	|	2.72
59.750	0.00	0.04	0.092	I	O	|	|	|	2.71
59.833	0.00	0.04	0.092	I	O	|	|	|	2.70
59.917	0.00	0.04	0.092	I	O	|	|	|	2.69
60.000	0.00	0.04	0.091	I	O	|	|	|	2.69
60.083	0.00	0.04	0.091	I	O	|	|	|	2.68
60.167	0.00	0.04	0.091	I	O	|	|	|	2.67
60.250	0.00	0.04	0.091	I	O	|	|	|	2.66
60.333	0.00	0.04	0.090	I	O	|	|	|	2.66
60.417	0.00	0.04	0.090	I	O	|	|	|	2.65
60.500	0.00	0.04	0.090	I	O	|	|	|	2.64
60.583	0.00	0.04	0.089	I	O	|	|	|	2.63
60.667	0.00	0.04	0.089	I	O	|	|	|	2.62

60.750	0.00	0.04	0.089	I	O	|	|	|	2.62
60.833	0.00	0.04	0.088	I	O	|	|	|	2.61
60.917	0.00	0.04	0.088	I	O	|	|	|	2.60
61.000	0.00	0.04	0.088	I	O	|	|	|	2.59
61.083	0.00	0.04	0.087	I	O	|	|	|	2.59
61.167	0.00	0.04	0.087	I	O	|	|	|	2.58
61.250	0.00	0.04	0.087	I	O	|	|	|	2.57
61.333	0.00	0.04	0.087	I	O	|	|	|	2.56
61.417	0.00	0.04	0.086	I	O	|	|	|	2.56
61.500	0.00	0.04	0.086	I	O	|	|	|	2.55
61.583	0.00	0.04	0.086	I	O	|	|	|	2.54
61.667	0.00	0.04	0.085	I	O	|	|	|	2.53
61.750	0.00	0.04	0.085	I	O	|	|	|	2.52
61.833	0.00	0.04	0.085	I	O	|	|	|	2.52
61.917	0.00	0.04	0.084	I	O	|	|	|	2.51
62.000	0.00	0.04	0.084	I	O	|	|	|	2.50
62.083	0.00	0.04	0.084	I	O	|	|	|	2.49
62.167	0.00	0.04	0.083	I	O	|	|	|	2.49
62.250	0.00	0.04	0.083	I	O	|	|	|	2.48
62.333	0.00	0.04	0.083	I	O	|	|	|	2.47
62.417	0.00	0.04	0.082	I	O	|	|	|	2.46
62.500	0.00	0.04	0.082	I	O	|	|	|	2.45
62.583	0.00	0.04	0.082	I	O	|	|	|	2.45
62.667	0.00	0.04	0.082	I	O	|	|	|	2.44
62.750	0.00	0.04	0.081	I	O	|	|	|	2.43
62.833	0.00	0.04	0.081	I	O	|	|	|	2.42
62.917	0.00	0.04	0.081	I	O	|	|	|	2.42
63.000	0.00	0.04	0.080	I	O	|	|	|	2.41
63.083	0.00	0.04	0.080	I	O	|	|	|	2.40
63.167	0.00	0.04	0.080	I	O	|	|	|	2.39
63.250	0.00	0.04	0.079	I	O	|	|	|	2.38
63.333	0.00	0.04	0.079	I	O	|	|	|	2.38
63.417	0.00	0.04	0.079	I	O	|	|	|	2.37
63.500	0.00	0.04	0.078	I	O	|	|	|	2.36
63.583	0.00	0.04	0.078	I	O	|	|	|	2.35
63.667	0.00	0.04	0.078	I	O	|	|	|	2.35
63.750	0.00	0.04	0.078	I	O	|	|	|	2.34
63.833	0.00	0.04	0.077	I	O	|	|	|	2.33
63.917	0.00	0.04	0.077	I	O	|	|	|	2.32
64.000	0.00	0.04	0.077	I	O	|	|	|	2.31
64.083	0.00	0.04	0.076	I	O	|	|	|	2.31
64.167	0.00	0.04	0.076	I	O	|	|	|	2.30
64.250	0.00	0.04	0.076	I	O	|	|	|	2.29
64.333	0.00	0.04	0.075	I	O	|	|	|	2.28
64.417	0.00	0.04	0.075	I	O	|	|	|	2.28
64.500	0.00	0.04	0.075	I	O	|	|	|	2.27
64.583	0.00	0.04	0.074	I	O	|	|	|	2.26
64.667	0.00	0.04	0.074	I	O	|	|	|	2.25
64.750	0.00	0.04	0.074	I	O	|	|	|	2.25
64.833	0.00	0.04	0.073	I	O	|	|	|	2.24

64.917	0.00	0.04	0.073	I	O	|	|	|	2.23
65.000	0.00	0.04	0.073	I	O	|	|	|	2.22
65.083	0.00	0.04	0.073	I	O	|	|	|	2.21
65.167	0.00	0.04	0.072	I	O	|	|	|	2.21
65.250	0.00	0.04	0.072	I	O	|	|	|	2.20
65.333	0.00	0.04	0.072	I	O	|	|	|	2.19
65.417	0.00	0.04	0.071	I	O	|	|	|	2.18
65.500	0.00	0.04	0.071	I	O	|	|	|	2.18
65.583	0.00	0.04	0.071	I	O	|	|	|	2.17
65.667	0.00	0.04	0.070	I	O	|	|	|	2.16
65.750	0.00	0.04	0.070	I	O	|	|	|	2.15
65.833	0.00	0.04	0.070	I	O	|	|	|	2.14
65.917	0.00	0.04	0.069	I	O	|	|	|	2.14
66.000	0.00	0.04	0.069	I	O	|	|	|	2.13
66.083	0.00	0.04	0.069	I	O	|	|	|	2.12
66.167	0.00	0.04	0.069	I	O	|	|	|	2.11
66.250	0.00	0.04	0.068	I	O	|	|	|	2.11
66.333	0.00	0.04	0.068	I	O	|	|	|	2.10
66.417	0.00	0.04	0.068	I	O	|	|	|	2.09
66.500	0.00	0.04	0.067	I	O	|	|	|	2.08
66.583	0.00	0.04	0.067	I	O	|	|	|	2.07
66.667	0.00	0.04	0.067	I	O	|	|	|	2.07
66.750	0.00	0.04	0.066	I	O	|	|	|	2.06
66.833	0.00	0.04	0.066	I	O	|	|	|	2.05
66.917	0.00	0.04	0.066	I	O	|	|	|	2.04
67.000	0.00	0.04	0.065	I	O	|	|	|	2.04
67.083	0.00	0.04	0.065	I	O	|	|	|	2.03
67.167	0.00	0.04	0.065	I	O	|	|	|	2.02
67.250	0.00	0.04	0.065	I	O	|	|	|	2.01
67.333	0.00	0.04	0.064	I	O	|	|	|	2.01
67.417	0.00	0.04	0.064	I	O	|	|	|	2.00
67.500	0.00	0.04	0.064	I	O	|	|	|	1.99
67.583	0.00	0.04	0.063	I	O	|	|	|	1.98
67.667	0.00	0.04	0.063	I	O	|	|	|	1.97
67.750	0.00	0.04	0.063	I	O	|	|	|	1.97
67.833	0.00	0.04	0.062	I	O	|	|	|	1.96
67.917	0.00	0.04	0.062	I	O	|	|	|	1.95
68.000	0.00	0.04	0.062	I	O	|	|	|	1.94
68.083	0.00	0.04	0.061	I	O	|	|	|	1.94
68.167	0.00	0.04	0.061	I	O	|	|	|	1.93
68.250	0.00	0.04	0.061	I	O	|	|	|	1.92
68.333	0.00	0.04	0.060	I	O	|	|	|	1.91
68.417	0.00	0.04	0.060	I	O	|	|	|	1.90
68.500	0.00	0.04	0.060	I	O	|	|	|	1.90
68.583	0.00	0.04	0.060	I	O	|	|	|	1.89
68.667	0.00	0.04	0.059	I	O	|	|	|	1.88
68.750	0.00	0.04	0.059	I	O	|	|	|	1.87
68.833	0.00	0.04	0.059	I	O	|	|	|	1.87
68.917	0.00	0.04	0.058	I	O	|	|	|	1.86
69.000	0.00	0.04	0.058	I	O	|	|	|	1.85

69.083	0.00	0.04	0.058	I O				1.84
69.167	0.00	0.04	0.057	I O				1.83
69.250	0.00	0.04	0.057	I O				1.83
69.333	0.00	0.04	0.057	I O				1.82
69.417	0.00	0.04	0.056	I O				1.81
69.500	0.00	0.04	0.056	I O				1.80
69.583	0.00	0.04	0.056	I O				1.80
69.667	0.00	0.04	0.056	I O				1.79
69.750	0.00	0.04	0.055	I O				1.78
69.833	0.00	0.04	0.055	I O				1.77
69.917	0.00	0.04	0.055	I O				1.76
70.000	0.00	0.04	0.054	I O				1.76
70.083	0.00	0.04	0.054	I O				1.75
70.167	0.00	0.04	0.054	I O				1.74
70.250	0.00	0.04	0.053	I O				1.73
70.333	0.00	0.04	0.053	I O				1.73
70.417	0.00	0.04	0.053	I O				1.72
70.500	0.00	0.04	0.052	I O				1.71
70.583	0.00	0.04	0.052	I O				1.70
70.667	0.00	0.04	0.052	I O				1.70
70.750	0.00	0.04	0.051	I O				1.69
70.833	0.00	0.04	0.051	I O				1.68
70.917	0.00	0.04	0.051	I O				1.67
71.000	0.00	0.04	0.051	I O				1.66
71.083	0.00	0.04	0.050	I O				1.66
71.167	0.00	0.04	0.050	I O				1.65
71.250	0.00	0.04	0.050	I O				1.64
71.333	0.00	0.04	0.049	I O				1.63
71.417	0.00	0.04	0.049	I O				1.63
71.500	0.00	0.04	0.049	I O				1.62
71.583	0.00	0.04	0.048	I O				1.61
71.667	0.00	0.04	0.048	I O				1.60
71.750	0.00	0.04	0.048	I O				1.59
71.833	0.00	0.04	0.047	I O				1.59
71.917	0.00	0.04	0.047	I O				1.58
72.000	0.00	0.04	0.047	I O				1.57
72.083	0.00	0.04	0.047	I O				1.56
72.167	0.00	0.04	0.046	I O				1.56
72.250	0.00	0.04	0.046	I O				1.55
72.333	0.00	0.04	0.046	I O				1.54
72.417	0.00	0.04	0.045	I O				1.53
72.500	0.00	0.04	0.045	I O				1.52
72.583	0.00	0.04	0.045	I O				1.52
72.667	0.00	0.04	0.044	I O				1.51
72.750	0.00	0.04	0.044	I O				1.50
72.833	0.00	0.04	0.044	I O				1.49
72.917	0.00	0.04	0.043	I O				1.49
73.000	0.00	0.04	0.043	I O				1.48
73.083	0.00	0.04	0.043	I O				1.47
73.167	0.00	0.04	0.043	I O				1.46

73.250	0.00	0.04	0.042	I O				1.45
73.333	0.00	0.04	0.042	I O				1.45
73.417	0.00	0.04	0.042	I O				1.44
73.500	0.00	0.04	0.041	I O				1.43
73.583	0.00	0.04	0.041	I O				1.42
73.667	0.00	0.04	0.041	I O				1.42
73.750	0.00	0.04	0.040	I O				1.41
73.833	0.00	0.04	0.040	I O				1.40
73.917	0.00	0.04	0.040	I O				1.39
74.000	0.00	0.04	0.039	I O				1.39
74.083	0.00	0.04	0.039	I O				1.38
74.167	0.00	0.04	0.039	I O				1.37
74.250	0.00	0.04	0.038	I O				1.36
74.333	0.00	0.04	0.038	I O				1.35
74.417	0.00	0.04	0.038	I O				1.35
74.500	0.00	0.04	0.038	I O				1.34
74.583	0.00	0.04	0.037	I O				1.33
74.667	0.00	0.04	0.037	I O				1.32
74.750	0.00	0.04	0.037	I O				1.32
74.833	0.00	0.04	0.036	I O				1.31
74.917	0.00	0.04	0.036	I O				1.30
75.000	0.00	0.04	0.036	I O				1.29
75.083	0.00	0.04	0.035	I O				1.28
75.167	0.00	0.04	0.035	I O				1.28
75.250	0.00	0.04	0.035	I O				1.27
75.333	0.00	0.04	0.034	I O				1.26
75.417	0.00	0.04	0.034	I O				1.25
75.500	0.00	0.04	0.034	I O				1.25
75.583	0.00	0.04	0.034	I O				1.24
75.667	0.00	0.04	0.033	I O				1.23
75.750	0.00	0.04	0.033	I O				1.22
75.833	0.00	0.04	0.033	I O				1.21
75.917	0.00	0.04	0.032	I O				1.21
76.000	0.00	0.04	0.032	I O				1.20
76.083	0.00	0.04	0.032	I O				1.19
76.167	0.00	0.04	0.031	I O				1.18
76.250	0.00	0.04	0.031	I O				1.18
76.333	0.00	0.04	0.031	I O				1.17
76.417	0.00	0.04	0.030	I O				1.16
76.500	0.00	0.04	0.030	I O				1.15
76.583	0.00	0.04	0.030	I O				1.15
76.667	0.00	0.04	0.029	I O				1.14
76.750	0.00	0.04	0.029	I O				1.13
76.833	0.00	0.04	0.029	I O				1.12
76.917	0.00	0.04	0.029	I O				1.11
77.000	0.00	0.04	0.028	I O				1.11
77.083	0.00	0.04	0.028	I O				1.10
77.167	0.00	0.04	0.028	I O				1.09
77.250	0.00	0.04	0.027	I O				1.08
77.333	0.00	0.04	0.027	I O				1.08

77.417	0.00	0.04	0.027	I O				1.07
77.500	0.00	0.04	0.026	I O				1.06
77.583	0.00	0.04	0.026	I O				1.05
77.667	0.00	0.04	0.026	I O				1.04
77.750	0.00	0.04	0.025	I O				1.04
77.833	0.00	0.04	0.025	I O				1.03
77.917	0.00	0.04	0.025	I O				1.02
78.000	0.00	0.04	0.025	I O				1.01
78.083	0.00	0.04	0.024	I O				1.01
78.167	0.00	0.04	0.024	I O				1.00
78.250	0.00	0.04	0.024	I O				0.98
78.333	0.00	0.04	0.023	I O				0.97
78.417	0.00	0.04	0.023	I O				0.96
78.500	0.00	0.04	0.023	I O				0.95
78.583	0.00	0.04	0.022	I O				0.93
78.667	0.00	0.04	0.022	I O				0.92
78.750	0.00	0.04	0.022	I O				0.91
78.833	0.00	0.04	0.022	I O				0.90
78.917	0.00	0.04	0.021	I O				0.89
79.000	0.00	0.04	0.021	I O				0.88
79.083	0.00	0.04	0.021	I O				0.86
79.167	0.00	0.04	0.020	I O				0.85
79.250	0.00	0.04	0.020	I O				0.84
79.333	0.00	0.04	0.020	I O				0.83
79.417	0.00	0.04	0.020	I O				0.82
79.500	0.00	0.04	0.019	I O				0.81
79.583	0.00	0.04	0.019	I O				0.80
79.667	0.00	0.04	0.019	I O				0.79
79.750	0.00	0.04	0.019	I O				0.78
79.833	0.00	0.03	0.018	I O				0.77
79.917	0.00	0.03	0.018	I O				0.76
80.000	0.00	0.03	0.018	I O				0.75
80.083	0.00	0.03	0.018	I O				0.74
80.167	0.00	0.03	0.018	I O				0.73
80.250	0.00	0.03	0.017	I O				0.72
80.333	0.00	0.03	0.017	I O				0.71
80.417	0.00	0.03	0.017	I O				0.70
80.500	0.00	0.03	0.017	I O				0.69
80.583	0.00	0.03	0.016	IO				0.69
80.667	0.00	0.03	0.016	IO				0.68
80.750	0.00	0.03	0.016	IO				0.67
80.833	0.00	0.03	0.016	IO				0.66
80.917	0.00	0.03	0.016	IO				0.65
81.000	0.00	0.03	0.015	IO				0.64
81.083	0.00	0.03	0.015	IO				0.63
81.167	0.00	0.03	0.015	IO				0.63
81.250	0.00	0.03	0.015	IO				0.62
81.333	0.00	0.03	0.015	IO				0.61
81.417	0.00	0.03	0.014	IO				0.60
81.500	0.00	0.03	0.014	IO				0.59

81.583	0.00	0.03	0.014	IO				0.59
81.667	0.00	0.03	0.014	IO				0.58
81.750	0.00	0.03	0.014	IO				0.57
81.833	0.00	0.03	0.014	IO				0.56
81.917	0.00	0.03	0.013	IO				0.56
82.000	0.00	0.02	0.013	IO				0.55
82.083	0.00	0.02	0.013	IO				0.54
82.167	0.00	0.02	0.013	IO				0.54
82.250	0.00	0.02	0.013	IO				0.53
82.333	0.00	0.02	0.013	IO				0.52
82.417	0.00	0.02	0.012	IO				0.52
82.500	0.00	0.02	0.012	IO				0.51
82.583	0.00	0.02	0.012	IO				0.50
82.667	0.00	0.02	0.012	IO				0.50
82.750	0.00	0.02	0.012	IO				0.49
82.833	0.00	0.02	0.012	IO				0.48
82.917	0.00	0.02	0.011	IO				0.48
83.000	0.00	0.02	0.011	IO				0.47
83.083	0.00	0.02	0.011	IO				0.47
83.167	0.00	0.02	0.011	IO				0.46
83.250	0.00	0.02	0.011	IO				0.45
83.333	0.00	0.02	0.011	IO				0.45
83.417	0.00	0.02	0.011	IO				0.44
83.500	0.00	0.02	0.010	IO				0.44
83.583	0.00	0.02	0.010	IO				0.43
83.667	0.00	0.02	0.010	IO				0.42
83.750	0.00	0.02	0.010	IO				0.42
83.833	0.00	0.02	0.010	IO				0.41
83.917	0.00	0.02	0.010	IO				0.41
84.000	0.00	0.02	0.010	IO				0.40
84.083	0.00	0.02	0.010	IO				0.40
84.167	0.00	0.02	0.009	IO				0.39
84.250	0.00	0.02	0.009	IO				0.39
84.333	0.00	0.02	0.009	IO				0.38
84.417	0.00	0.02	0.009	IO				0.38
84.500	0.00	0.02	0.009	IO				0.37
84.583	0.00	0.02	0.009	IO				0.37
84.667	0.00	0.02	0.009	IO				0.36
84.750	0.00	0.02	0.009	IO				0.36
84.833	0.00	0.02	0.009	IO				0.35
84.917	0.00	0.02	0.008	IO				0.35
85.000	0.00	0.02	0.008	IO				0.35
85.083	0.00	0.02	0.008	O				0.34
85.167	0.00	0.02	0.008	O				0.34
85.250	0.00	0.01	0.008	O				0.33
85.333	0.00	0.01	0.008	O				0.33
85.417	0.00	0.01	0.008	O				0.32
85.500	0.00	0.01	0.008	O				0.32
85.583	0.00	0.01	0.008	O				0.32
85.667	0.00	0.01	0.007	O				0.31

85.750	0.00	0.01	0.007	O				0.31
85.833	0.00	0.01	0.007	O				0.30
85.917	0.00	0.01	0.007	O				0.30
86.000	0.00	0.01	0.007	O				0.30
86.083	0.00	0.01	0.007	O				0.29
86.167	0.00	0.01	0.007	O				0.29
86.250	0.00	0.01	0.007	O				0.28
86.333	0.00	0.01	0.007	O				0.28
86.417	0.00	0.01	0.007	O				0.28
86.500	0.00	0.01	0.007	O				0.27
86.583	0.00	0.01	0.006	O				0.27
86.667	0.00	0.01	0.006	O				0.27
86.750	0.00	0.01	0.006	O				0.26
86.833	0.00	0.01	0.006	O				0.26
86.917	0.00	0.01	0.006	O				0.26
87.000	0.00	0.01	0.006	O				0.25
87.083	0.00	0.01	0.006	O				0.25
87.167	0.00	0.01	0.006	O				0.25
87.250	0.00	0.01	0.006	O				0.24
87.333	0.00	0.01	0.006	O				0.24
87.417	0.00	0.01	0.006	O				0.24
87.500	0.00	0.01	0.006	O				0.23
87.583	0.00	0.01	0.006	O				0.23
87.667	0.00	0.01	0.005	O				0.23
87.750	0.00	0.01	0.005	O				0.23
87.833	0.00	0.01	0.005	O				0.22
87.917	0.00	0.01	0.005	O				0.22
88.000	0.00	0.01	0.005	O				0.22
88.083	0.00	0.01	0.005	O				0.21
88.167	0.00	0.01	0.005	O				0.21
88.250	0.00	0.01	0.005	O				0.21
88.333	0.00	0.01	0.005	O				0.21
88.417	0.00	0.01	0.005	O				0.20
88.500	0.00	0.01	0.005	O				0.20
88.583	0.00	0.01	0.005	O				0.20
88.667	0.00	0.01	0.005	O				0.20
88.750	0.00	0.01	0.005	O				0.19
88.833	0.00	0.01	0.005	O				0.19
88.917	0.00	0.01	0.005	O				0.19
89.000	0.00	0.01	0.004	O				0.19
89.083	0.00	0.01	0.004	O				0.18
89.167	0.00	0.01	0.004	O				0.18
89.250	0.00	0.01	0.004	O				0.18
89.333	0.00	0.01	0.004	O				0.18
89.417	0.00	0.01	0.004	O				0.17
89.500	0.00	0.01	0.004	O				0.17
89.583	0.00	0.01	0.004	O				0.17
89.667	0.00	0.01	0.004	O				0.17
89.750	0.00	0.01	0.004	O				0.17
89.833	0.00	0.01	0.004	O				0.16

89.917	0.00	0.01	0.004	O				0.16
90.000	0.00	0.01	0.004	O				0.16
90.083	0.00	0.01	0.004	O				0.16
90.167	0.00	0.01	0.004	O				0.16
90.250	0.00	0.01	0.004	O				0.15
90.333	0.00	0.01	0.004	O				0.15
90.417	0.00	0.01	0.004	O				0.15
90.500	0.00	0.01	0.004	O				0.15
90.583	0.00	0.01	0.003	O				0.15
90.667	0.00	0.01	0.003	O				0.14
90.750	0.00	0.01	0.003	O				0.14
90.833	0.00	0.01	0.003	O				0.14
90.917	0.00	0.01	0.003	O				0.14
91.000	0.00	0.01	0.003	O				0.14
91.083	0.00	0.01	0.003	O				0.13
91.167	0.00	0.01	0.003	O				0.13
91.250	0.00	0.01	0.003	O				0.13
91.333	0.00	0.01	0.003	O				0.13
91.417	0.00	0.01	0.003	O				0.13
91.500	0.00	0.01	0.003	O				0.13
91.583	0.00	0.01	0.003	O				0.12
91.667	0.00	0.01	0.003	O				0.12
91.750	0.00	0.01	0.003	O				0.12
91.833	0.00	0.01	0.003	O				0.12
91.917	0.00	0.01	0.003	O				0.12
92.000	0.00	0.01	0.003	O				0.12
92.083	0.00	0.01	0.003	O				0.12
92.167	0.00	0.01	0.003	O				0.11
92.250	0.00	0.01	0.003	O				0.11
92.333	0.00	0.00	0.003	O				0.11
92.417	0.00	0.00	0.003	O				0.11
92.500	0.00	0.00	0.003	O				0.11
92.583	0.00	0.00	0.003	O				0.11
92.667	0.00	0.00	0.003	O				0.11
92.750	0.00	0.00	0.002	O				0.10
92.833	0.00	0.00	0.002	O				0.10
92.917	0.00	0.00	0.002	O				0.10
93.000	0.00	0.00	0.002	O				0.10
93.083	0.00	0.00	0.002	O				0.10
93.167	0.00	0.00	0.002	O				0.10
93.250	0.00	0.00	0.002	O				0.10
93.333	0.00	0.00	0.002	O				0.10
93.417	0.00	0.00	0.002	O				0.09
93.500	0.00	0.00	0.002	O				0.09
93.583	0.00	0.00	0.002	O				0.09
93.667	0.00	0.00	0.002	O				0.09
93.750	0.00	0.00	0.002	O				0.09
93.833	0.00	0.00	0.002	O				0.09
93.917	0.00	0.00	0.002	O				0.09
94.000	0.00	0.00	0.002	O				0.09

94.083	0.00	0.00	0.002	O	|	|	|	0.08
94.167	0.00	0.00	0.002	O	|	|	|	0.08
94.250	0.00	0.00	0.002	O	|	|	|	0.08
94.333	0.00	0.00	0.002	O	|	|	|	0.08
94.417	0.00	0.00	0.002	O	|	|	|	0.08
94.500	0.00	0.00	0.002	O	|	|	|	0.08
94.583	0.00	0.00	0.002	O	|	|	|	0.08
94.667	0.00	0.00	0.002	O	|	|	|	0.08
94.750	0.00	0.00	0.002	O	|	|	|	0.08
94.833	0.00	0.00	0.002	O	|	|	|	0.08
94.917	0.00	0.00	0.002	O	|	|	|	0.07
95.000	0.00	0.00	0.002	O	|	|	|	0.07
95.083	0.00	0.00	0.002	O	|	|	|	0.07
95.167	0.00	0.00	0.002	O	|	|	|	0.07
95.250	0.00	0.00	0.002	O	|	|	|	0.07
95.333	0.00	0.00	0.002	O	|	|	|	0.07
95.417	0.00	0.00	0.002	O	|	|	|	0.07
95.500	0.00	0.00	0.002	O	|	|	|	0.07
95.583	0.00	0.00	0.002	O	|	|	|	0.07
95.667	0.00	0.00	0.002	O	|	|	|	0.07
95.750	0.00	0.00	0.002	O	|	|	|	0.07
95.833	0.00	0.00	0.002	O	|	|	|	0.06
95.917	0.00	0.00	0.002	O	|	|	|	0.06
96.000	0.00	0.00	0.002	O	|	|	|	0.06
96.083	0.00	0.00	0.001	O	|	|	|	0.06
96.167	0.00	0.00	0.001	O	|	|	|	0.06
96.250	0.00	0.00	0.001	O	|	|	|	0.06
96.333	0.00	0.00	0.001	O	|	|	|	0.06
96.417	0.00	0.00	0.001	O	|	|	|	0.06
96.500	0.00	0.00	0.001	O	|	|	|	0.06
96.583	0.00	0.00	0.001	O	|	|	|	0.06
96.667	0.00	0.00	0.001	O	|	|	|	0.06
96.750	0.00	0.00	0.001	O	|	|	|	0.06
96.833	0.00	0.00	0.001	O	|	|	|	0.06
96.917	0.00	0.00	0.001	O	|	|	|	0.05
97.000	0.00	0.00	0.001	O	|	|	|	0.05
97.083	0.00	0.00	0.001	O	|	|	|	0.05
97.167	0.00	0.00	0.001	O	|	|	|	0.05
97.250	0.00	0.00	0.001	O	|	|	|	0.05
97.333	0.00	0.00	0.001	O	|	|	|	0.05
97.417	0.00	0.00	0.001	O	|	|	|	0.05
97.500	0.00	0.00	0.001	O	|	|	|	0.05
97.583	0.00	0.00	0.001	O	|	|	|	0.05
97.667	0.00	0.00	0.001	O	|	|	|	0.05
97.750	0.00	0.00	0.001	O	|	|	|	0.05
97.833	0.00	0.00	0.001	O	|	|	|	0.05
97.917	0.00	0.00	0.001	O	|	|	|	0.05
98.000	0.00	0.00	0.001	O	|	|	|	0.05
98.083	0.00	0.00	0.001	O	|	|	|	0.05
98.167	0.00	0.00	0.001	O	|	|	|	0.04

98.250	0.00	0.00	0.001	O				0.04
98.333	0.00	0.00	0.001	O				0.04
98.417	0.00	0.00	0.001	O				0.04
98.500	0.00	0.00	0.001	O				0.04
98.583	0.00	0.00	0.001	O				0.04
98.667	0.00	0.00	0.001	O				0.04
98.750	0.00	0.00	0.001	O				0.04
98.833	0.00	0.00	0.001	O				0.04
98.917	0.00	0.00	0.001	O				0.04
99.000	0.00	0.00	0.001	O				0.04
99.083	0.00	0.00	0.001	O				0.04
99.167	0.00	0.00	0.001	O				0.04
99.250	0.00	0.00	0.001	O				0.04
99.333	0.00	0.00	0.001	O				0.04
99.417	0.00	0.00	0.001	O				0.04
99.500	0.00	0.00	0.001	O				0.04
99.583	0.00	0.00	0.001	O				0.04
99.667	0.00	0.00	0.001	O				0.04
99.750	0.00	0.00	0.001	O				0.04
99.833	0.00	0.00	0.001	O				0.03
99.917	0.00	0.00	0.001	O				0.03
100.000	0.00	0.00	0.001	O				0.03
100.083	0.00	0.00	0.001	O				0.03
100.167	0.00	0.00	0.001	O				0.03
100.250	0.00	0.00	0.001	O				0.03
100.333	0.00	0.00	0.001	O				0.03
100.417	0.00	0.00	0.001	O				0.03
100.500	0.00	0.00	0.001	O				0.03
100.583	0.00	0.00	0.001	O				0.03
100.667	0.00	0.00	0.001	O				0.03
100.750	0.00	0.00	0.001	O				0.03
100.833	0.00	0.00	0.001	O				0.03
100.917	0.00	0.00	0.001	O				0.03
101.000	0.00	0.00	0.001	O				0.03
101.083	0.00	0.00	0.001	O				0.03
101.167	0.00	0.00	0.001	O				0.03
101.250	0.00	0.00	0.001	O				0.03
101.333	0.00	0.00	0.001	O				0.03
101.417	0.00	0.00	0.001	O				0.03
101.500	0.00	0.00	0.001	O				0.03
101.583	0.00	0.00	0.001	O				0.03
101.667	0.00	0.00	0.001	O				0.03
101.750	0.00	0.00	0.001	O				0.03
101.833	0.00	0.00	0.001	O				0.03
101.917	0.00	0.00	0.001	O				0.03
102.000	0.00	0.00	0.001	O				0.02
102.083	0.00	0.00	0.001	O				0.02
102.167	0.00	0.00	0.001	O				0.02
102.250	0.00	0.00	0.001	O				0.02
102.333	0.00	0.00	0.001	O				0.02

102.417	0.00	0.00	0.001	O	|	|	|	0.02
102.500	0.00	0.00	0.001	O	|	|	|	0.02
102.583	0.00	0.00	0.001	O	|	|	|	0.02
102.667	0.00	0.00	0.001	O	|	|	|	0.02
102.750	0.00	0.00	0.001	O	|	|	|	0.02

**********HYDROGRAPH DATA**********

Number of intervals = 1233
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.045 (CFS)
Total volume = 0.302 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
10 yr
1 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris110.rte
**********HYDROGRAPH DATA**********
Number of intervals = 20
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 2.774 (CFS)
Total volume = 0.097 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 20
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.7 1.39 2.08 2.77	Depth (Ft.)
0.083	0.10	0.00	0.000	OI	0.01
0.167	0.37	0.00	0.002	O I	0.08
0.250	0.48	0.01	0.005	O I	0.20
0.333	0.57	0.02	0.008	O I	0.35
0.417	0.63	0.02	0.012	O I	0.52
0.500	0.72	0.03	0.017	O I	0.70
0.583	0.82	0.04	0.022	O I	0.91
0.667	0.94	0.04	0.028	O I	1.09
0.750	1.17	0.04	0.035	O I	1.26
0.833	1.99	0.04	0.045	O I	1.53
0.917	2.77	0.04	0.061	O I	1.93
1.000	1.51	0.04	0.076	O I	2.29
1.083	0.93	0.04	0.084	O I	2.49
1.167	0.44	0.04	0.088	O I	2.61
1.250	0.26	0.04	0.090	O I	2.66
1.333	0.16	0.04	0.091	OI	2.69
1.417	0.10	0.04	0.092	OI	2.70
1.500	0.06	0.04	0.092	O	2.71
1.583	0.01	0.04	0.092	O	2.70
1.667	0.01	0.04	0.092	O	2.70
1.750	0.00	0.04	0.092	O	2.69
1.833	0.00	0.04	0.091	O	2.68
1.917	0.00	0.04	0.091	O	2.68
2.000	0.00	0.04	0.091	O	2.67
2.083	0.00	0.04	0.090	O	2.66
2.167	0.00	0.04	0.090	O	2.65
2.250	0.00	0.04	0.090	O	2.64
2.333	0.00	0.04	0.089	O	2.64

2.417	0.00	0.04	0.089	O				2.63
2.500	0.00	0.04	0.089	O				2.62
2.583	0.00	0.04	0.089	O				2.61
2.667	0.00	0.04	0.088	O				2.61
2.750	0.00	0.04	0.088	O				2.60
2.833	0.00	0.04	0.088	O				2.59
2.917	0.00	0.04	0.087	O				2.58
3.000	0.00	0.04	0.087	O				2.57
3.083	0.00	0.04	0.087	O				2.57
3.167	0.00	0.04	0.086	O				2.56
3.250	0.00	0.04	0.086	O				2.55
3.333	0.00	0.04	0.086	O				2.54
3.417	0.00	0.04	0.085	O				2.54
3.500	0.00	0.04	0.085	O				2.53
3.583	0.00	0.04	0.085	O				2.52
3.667	0.00	0.04	0.085	O				2.51
3.750	0.00	0.04	0.084	O				2.50
3.833	0.00	0.04	0.084	O				2.50
3.917	0.00	0.04	0.084	O				2.49
4.000	0.00	0.04	0.083	O				2.48
4.083	0.00	0.04	0.083	O				2.47
4.167	0.00	0.04	0.083	O				2.47
4.250	0.00	0.04	0.082	O				2.46
4.333	0.00	0.04	0.082	O				2.45
4.417	0.00	0.04	0.082	O				2.44
4.500	0.00	0.04	0.081	O				2.44
4.583	0.00	0.04	0.081	O				2.43
4.667	0.00	0.04	0.081	O				2.42
4.750	0.00	0.04	0.080	O				2.41
4.833	0.00	0.04	0.080	O				2.40
4.917	0.00	0.04	0.080	O				2.40
5.000	0.00	0.04	0.080	O				2.39
5.083	0.00	0.04	0.079	O				2.38
5.167	0.00	0.04	0.079	O				2.37
5.250	0.00	0.04	0.079	O				2.37
5.333	0.00	0.04	0.078	O				2.36
5.417	0.00	0.04	0.078	O				2.35
5.500	0.00	0.04	0.078	O				2.34
5.583	0.00	0.04	0.077	O				2.33
5.667	0.00	0.04	0.077	O				2.33
5.750	0.00	0.04	0.077	O				2.32
5.833	0.00	0.04	0.076	O				2.31
5.917	0.00	0.04	0.076	O				2.30
6.000	0.00	0.04	0.076	O				2.30
6.083	0.00	0.04	0.076	O				2.29
6.167	0.00	0.04	0.075	O				2.28
6.250	0.00	0.04	0.075	O				2.27
6.333	0.00	0.04	0.075	O				2.26
6.417	0.00	0.04	0.074	O				2.26
6.500	0.00	0.04	0.074	O				2.25

6.583	0.00	0.04	0.074	O				2.24
6.667	0.00	0.04	0.073	O				2.23
6.750	0.00	0.04	0.073	O				2.23
6.833	0.00	0.04	0.073	O				2.22
6.917	0.00	0.04	0.072	O				2.21
7.000	0.00	0.04	0.072	O				2.20
7.083	0.00	0.04	0.072	O				2.19
7.167	0.00	0.04	0.071	O				2.19
7.250	0.00	0.04	0.071	O				2.18
7.333	0.00	0.04	0.071	O				2.17
7.417	0.00	0.04	0.071	O				2.16
7.500	0.00	0.04	0.070	O				2.16
7.583	0.00	0.04	0.070	O				2.15
7.667	0.00	0.04	0.070	O				2.14
7.750	0.00	0.04	0.069	O				2.13
7.833	0.00	0.04	0.069	O				2.13
7.917	0.00	0.04	0.069	O				2.12
8.000	0.00	0.04	0.068	O				2.11
8.083	0.00	0.04	0.068	O				2.10
8.167	0.00	0.04	0.068	O				2.09
8.250	0.00	0.04	0.067	O				2.09
8.333	0.00	0.04	0.067	O				2.08
8.417	0.00	0.04	0.067	O				2.07
8.500	0.00	0.04	0.067	O				2.06
8.583	0.00	0.04	0.066	O				2.06
8.667	0.00	0.04	0.066	O				2.05
8.750	0.00	0.04	0.066	O				2.04
8.833	0.00	0.04	0.065	O				2.03
8.917	0.00	0.04	0.065	O				2.02
9.000	0.00	0.04	0.065	O				2.02
9.083	0.00	0.04	0.064	O				2.01
9.167	0.00	0.04	0.064	O				2.00
9.250	0.00	0.04	0.064	O				1.99
9.333	0.00	0.04	0.063	O				1.99
9.417	0.00	0.04	0.063	O				1.98
9.500	0.00	0.04	0.063	O				1.97
9.583	0.00	0.04	0.062	O				1.96
9.667	0.00	0.04	0.062	O				1.95
9.750	0.00	0.04	0.062	O				1.95
9.833	0.00	0.04	0.062	O				1.94
9.917	0.00	0.04	0.061	O				1.93
10.000	0.00	0.04	0.061	O				1.92
10.083	0.00	0.04	0.061	O				1.92
10.167	0.00	0.04	0.060	O				1.91
10.250	0.00	0.04	0.060	O				1.90
10.333	0.00	0.04	0.060	O				1.89
10.417	0.00	0.04	0.059	O				1.88
10.500	0.00	0.04	0.059	O				1.88
10.583	0.00	0.04	0.059	O				1.87
10.667	0.00	0.04	0.058	O				1.86

10.750	0.00	0.04	0.058	O				1.85
10.833	0.00	0.04	0.058	O				1.85
10.917	0.00	0.04	0.058	O				1.84
11.000	0.00	0.04	0.057	O				1.83
11.083	0.00	0.04	0.057	O				1.82
11.167	0.00	0.04	0.057	O				1.82
11.250	0.00	0.04	0.056	O				1.81
11.333	0.00	0.04	0.056	O				1.80
11.417	0.00	0.04	0.056	O				1.79
11.500	0.00	0.04	0.055	O				1.78
11.583	0.00	0.04	0.055	O				1.78
11.667	0.00	0.04	0.055	O				1.77
11.750	0.00	0.04	0.054	O				1.76
11.833	0.00	0.04	0.054	O				1.75
11.917	0.00	0.04	0.054	O				1.75
12.000	0.00	0.04	0.054	O				1.74
12.083	0.00	0.04	0.053	O				1.73
12.167	0.00	0.04	0.053	O				1.72
12.250	0.00	0.04	0.053	O				1.71
12.333	0.00	0.04	0.052	O				1.71
12.417	0.00	0.04	0.052	O				1.70
12.500	0.00	0.04	0.052	O				1.69
12.583	0.00	0.04	0.051	O				1.68
12.667	0.00	0.04	0.051	O				1.68
12.750	0.00	0.04	0.051	O				1.67
12.833	0.00	0.04	0.050	O				1.66
12.917	0.00	0.04	0.050	O				1.65
13.000	0.00	0.04	0.050	O				1.64
13.083	0.00	0.04	0.049	O				1.64
13.167	0.00	0.04	0.049	O				1.63
13.250	0.00	0.04	0.049	O				1.62
13.333	0.00	0.04	0.049	O				1.61
13.417	0.00	0.04	0.048	O				1.61
13.500	0.00	0.04	0.048	O				1.60
13.583	0.00	0.04	0.048	O				1.59
13.667	0.00	0.04	0.047	O				1.58
13.750	0.00	0.04	0.047	O				1.58
13.833	0.00	0.04	0.047	O				1.57
13.917	0.00	0.04	0.046	O				1.56
14.000	0.00	0.04	0.046	O				1.55
14.083	0.00	0.04	0.046	O				1.54
14.167	0.00	0.04	0.045	O				1.54
14.250	0.00	0.04	0.045	O				1.53
14.333	0.00	0.04	0.045	O				1.52
14.417	0.00	0.04	0.045	O				1.51
14.500	0.00	0.04	0.044	O				1.51
14.583	0.00	0.04	0.044	O				1.50
14.667	0.00	0.04	0.044	O				1.49
14.750	0.00	0.04	0.043	O				1.48
14.833	0.00	0.04	0.043	O				1.47

14.917	0.00	0.04	0.043	O	|	|	|	1.47
15.000	0.00	0.04	0.042	O	|	|	|	1.46
15.083	0.00	0.04	0.042	O	|	|	|	1.45
15.167	0.00	0.04	0.042	O	|	|	|	1.44
15.250	0.00	0.04	0.041	O	|	|	|	1.44
15.333	0.00	0.04	0.041	O	|	|	|	1.43
15.417	0.00	0.04	0.041	O	|	|	|	1.42
15.500	0.00	0.04	0.040	O	|	|	|	1.41
15.583	0.00	0.04	0.040	O	|	|	|	1.40
15.667	0.00	0.04	0.040	O	|	|	|	1.40
15.750	0.00	0.04	0.040	O	|	|	|	1.39
15.833	0.00	0.04	0.039	O	|	|	|	1.38
15.917	0.00	0.04	0.039	O	|	|	|	1.37
16.000	0.00	0.04	0.039	O	|	|	|	1.37
16.083	0.00	0.04	0.038	O	|	|	|	1.36
16.167	0.00	0.04	0.038	O	|	|	|	1.35
16.250	0.00	0.04	0.038	O	|	|	|	1.34
16.333	0.00	0.04	0.037	O	|	|	|	1.33
16.417	0.00	0.04	0.037	O	|	|	|	1.33
16.500	0.00	0.04	0.037	O	|	|	|	1.32
16.583	0.00	0.04	0.036	O	|	|	|	1.31
16.667	0.00	0.04	0.036	O	|	|	|	1.30
16.750	0.00	0.04	0.036	O	|	|	|	1.30
16.833	0.00	0.04	0.036	O	|	|	|	1.29
16.917	0.00	0.04	0.035	O	|	|	|	1.28
17.000	0.00	0.04	0.035	O	|	|	|	1.27
17.083	0.00	0.04	0.035	O	|	|	|	1.27
17.167	0.00	0.04	0.034	O	|	|	|	1.26
17.250	0.00	0.04	0.034	O	|	|	|	1.25
17.333	0.00	0.04	0.034	O	|	|	|	1.24
17.417	0.00	0.04	0.033	O	|	|	|	1.23
17.500	0.00	0.04	0.033	O	|	|	|	1.23
17.583	0.00	0.04	0.033	O	|	|	|	1.22
17.667	0.00	0.04	0.032	O	|	|	|	1.21
17.750	0.00	0.04	0.032	O	|	|	|	1.20
17.833	0.00	0.04	0.032	O	|	|	|	1.20
17.917	0.00	0.04	0.032	O	|	|	|	1.19
18.000	0.00	0.04	0.031	O	|	|	|	1.18
18.083	0.00	0.04	0.031	O	|	|	|	1.17
18.167	0.00	0.04	0.031	O	|	|	|	1.16
18.250	0.00	0.04	0.030	O	|	|	|	1.16
18.333	0.00	0.04	0.030	O	|	|	|	1.15
18.417	0.00	0.04	0.030	O	|	|	|	1.14
18.500	0.00	0.04	0.029	O	|	|	|	1.13
18.583	0.00	0.04	0.029	O	|	|	|	1.13
18.667	0.00	0.04	0.029	O	|	|	|	1.12
18.750	0.00	0.04	0.028	O	|	|	|	1.11
18.833	0.00	0.04	0.028	O	|	|	|	1.10
18.917	0.00	0.04	0.028	O	|	|	|	1.09
19.000	0.00	0.04	0.027	O	|	|	|	1.09

19.083	0.00	0.04	0.027	O				1.08
19.167	0.00	0.04	0.027	O				1.07
19.250	0.00	0.04	0.027	O				1.06
19.333	0.00	0.04	0.026	O				1.06
19.417	0.00	0.04	0.026	O				1.05
19.500	0.00	0.04	0.026	O				1.04
19.583	0.00	0.04	0.025	O				1.03
19.667	0.00	0.04	0.025	O				1.02
19.750	0.00	0.04	0.025	O				1.02
19.833	0.00	0.04	0.024	O				1.01
19.917	0.00	0.04	0.024	O				1.00
20.000	0.00	0.04	0.024	O				0.99
20.083	0.00	0.04	0.023	O				0.98
20.167	0.00	0.04	0.023	O				0.96
20.250	0.00	0.04	0.023	O				0.95
20.333	0.00	0.04	0.023	O				0.94
20.417	0.00	0.04	0.022	O				0.93
20.500	0.00	0.04	0.022	O				0.92
20.583	0.00	0.04	0.022	O				0.90
20.667	0.00	0.04	0.021	O				0.89
20.750	0.00	0.04	0.021	O				0.88
20.833	0.00	0.04	0.021	O				0.87
20.917	0.00	0.04	0.021	O				0.86
21.000	0.00	0.04	0.020	O				0.85
21.083	0.00	0.04	0.020	O				0.84
21.167	0.00	0.04	0.020	O				0.83
21.250	0.00	0.04	0.020	O				0.82
21.333	0.00	0.04	0.019	O				0.81
21.417	0.00	0.04	0.019	O				0.79
21.500	0.00	0.04	0.019	O				0.78
21.583	0.00	0.03	0.019	O				0.77
21.667	0.00	0.03	0.018	O				0.76
21.750	0.00	0.03	0.018	O				0.75
21.833	0.00	0.03	0.018	O				0.75
21.917	0.00	0.03	0.018	O				0.74
22.000	0.00	0.03	0.017	O				0.73
22.083	0.00	0.03	0.017	O				0.72
22.167	0.00	0.03	0.017	O				0.71
22.250	0.00	0.03	0.017	O				0.70
22.333	0.00	0.03	0.017	O				0.69
22.417	0.00	0.03	0.016	O				0.68
22.500	0.00	0.03	0.016	O				0.67
22.583	0.00	0.03	0.016	O				0.66
22.667	0.00	0.03	0.016	O				0.65
22.750	0.00	0.03	0.016	O				0.65
22.833	0.00	0.03	0.015	O				0.64
22.917	0.00	0.03	0.015	O				0.63
23.000	0.00	0.03	0.015	O				0.62
23.083	0.00	0.03	0.015	O				0.61
23.167	0.00	0.03	0.015	O				0.61

23.250	0.00	0.03	0.014	O				0.60
23.333	0.00	0.03	0.014	O				0.59
23.417	0.00	0.03	0.014	O				0.58
23.500	0.00	0.03	0.014	O				0.58
23.583	0.00	0.03	0.014	O				0.57
23.667	0.00	0.03	0.013	O				0.56
23.750	0.00	0.02	0.013	O				0.55
23.833	0.00	0.02	0.013	O				0.55
23.917	0.00	0.02	0.013	O				0.54
24.000	0.00	0.02	0.013	O				0.53
24.083	0.00	0.02	0.013	O				0.53
24.167	0.00	0.02	0.012	O				0.52
24.250	0.00	0.02	0.012	O				0.51
24.333	0.00	0.02	0.012	O				0.51
24.417	0.00	0.02	0.012	O				0.50
24.500	0.00	0.02	0.012	O				0.49
24.583	0.00	0.02	0.012	O				0.49
24.667	0.00	0.02	0.012	O				0.48
24.750	0.00	0.02	0.011	O				0.47
24.833	0.00	0.02	0.011	O				0.47
24.917	0.00	0.02	0.011	O				0.46
25.000	0.00	0.02	0.011	O				0.46
25.083	0.00	0.02	0.011	O				0.45
25.167	0.00	0.02	0.011	O				0.44
25.250	0.00	0.02	0.011	O				0.44
25.333	0.00	0.02	0.010	O				0.43
25.417	0.00	0.02	0.010	O				0.43
25.500	0.00	0.02	0.010	O				0.42
25.583	0.00	0.02	0.010	O				0.42
25.667	0.00	0.02	0.010	O				0.41
25.750	0.00	0.02	0.010	O				0.41
25.833	0.00	0.02	0.010	O				0.40
25.917	0.00	0.02	0.009	O				0.40
26.000	0.00	0.02	0.009	O				0.39
26.083	0.00	0.02	0.009	O				0.39
26.167	0.00	0.02	0.009	O				0.38
26.250	0.00	0.02	0.009	O				0.38
26.333	0.00	0.02	0.009	O				0.37
26.417	0.00	0.02	0.009	O				0.37
26.500	0.00	0.02	0.009	O				0.36
26.583	0.00	0.02	0.009	O				0.36
26.667	0.00	0.02	0.008	O				0.35
26.750	0.00	0.02	0.008	O				0.35
26.833	0.00	0.02	0.008	O				0.34
26.917	0.00	0.02	0.008	O				0.34
27.000	0.00	0.02	0.008	O				0.33
27.083	0.00	0.01	0.008	O				0.33
27.167	0.00	0.01	0.008	O				0.33
27.250	0.00	0.01	0.008	O				0.32
27.333	0.00	0.01	0.008	O				0.32

27.417	0.00	0.01	0.008	O	|	|	|	0.31
27.500	0.00	0.01	0.007	O	|	|	|	0.31
27.583	0.00	0.01	0.007	O	|	|	|	0.31
27.667	0.00	0.01	0.007	O	|	|	|	0.30
27.750	0.00	0.01	0.007	O	|	|	|	0.30
27.833	0.00	0.01	0.007	O	|	|	|	0.29
27.917	0.00	0.01	0.007	O	|	|	|	0.29
28.000	0.00	0.01	0.007	O	|	|	|	0.29
28.083	0.00	0.01	0.007	O	|	|	|	0.28
28.167	0.00	0.01	0.007	O	|	|	|	0.28
28.250	0.00	0.01	0.007	O	|	|	|	0.28
28.333	0.00	0.01	0.007	O	|	|	|	0.27
28.417	0.00	0.01	0.006	O	|	|	|	0.27
28.500	0.00	0.01	0.006	O	|	|	|	0.27
28.583	0.00	0.01	0.006	O	|	|	|	0.26
28.667	0.00	0.01	0.006	O	|	|	|	0.26
28.750	0.00	0.01	0.006	O	|	|	|	0.26
28.833	0.00	0.01	0.006	O	|	|	|	0.25
28.917	0.00	0.01	0.006	O	|	|	|	0.25
29.000	0.00	0.01	0.006	O	|	|	|	0.25
29.083	0.00	0.01	0.006	O	|	|	|	0.24
29.167	0.00	0.01	0.006	O	|	|	|	0.24
29.250	0.00	0.01	0.006	O	|	|	|	0.24
29.333	0.00	0.01	0.006	O	|	|	|	0.23
29.417	0.00	0.01	0.006	O	|	|	|	0.23
29.500	0.00	0.01	0.005	O	|	|	|	0.23
29.583	0.00	0.01	0.005	O	|	|	|	0.22
29.667	0.00	0.01	0.005	O	|	|	|	0.22
29.750	0.00	0.01	0.005	O	|	|	|	0.22
29.833	0.00	0.01	0.005	O	|	|	|	0.22
29.917	0.00	0.01	0.005	O	|	|	|	0.21
30.000	0.00	0.01	0.005	O	|	|	|	0.21
30.083	0.00	0.01	0.005	O	|	|	|	0.21
30.167	0.00	0.01	0.005	O	|	|	|	0.20
30.250	0.00	0.01	0.005	O	|	|	|	0.20
30.333	0.00	0.01	0.005	O	|	|	|	0.20
30.417	0.00	0.01	0.005	O	|	|	|	0.20
30.500	0.00	0.01	0.005	O	|	|	|	0.19
30.583	0.00	0.01	0.005	O	|	|	|	0.19
30.667	0.00	0.01	0.005	O	|	|	|	0.19
30.750	0.00	0.01	0.004	O	|	|	|	0.19
30.833	0.00	0.01	0.004	O	|	|	|	0.18
30.917	0.00	0.01	0.004	O	|	|	|	0.18
31.000	0.00	0.01	0.004	O	|	|	|	0.18
31.083	0.00	0.01	0.004	O	|	|	|	0.18
31.167	0.00	0.01	0.004	O	|	|	|	0.18
31.250	0.00	0.01	0.004	O	|	|	|	0.17
31.333	0.00	0.01	0.004	O	|	|	|	0.17
31.417	0.00	0.01	0.004	O	|	|	|	0.17
31.500	0.00	0.01	0.004	O	|	|	|	0.17

31.583	0.00	0.01	0.004	O	|	|	|	0.16
31.667	0.00	0.01	0.004	O	|	|	|	0.16
31.750	0.00	0.01	0.004	O	|	|	|	0.16
31.833	0.00	0.01	0.004	O	|	|	|	0.16
31.917	0.00	0.01	0.004	O	|	|	|	0.16
32.000	0.00	0.01	0.004	O	|	|	|	0.15
32.083	0.00	0.01	0.004	O	|	|	|	0.15
32.167	0.00	0.01	0.004	O	|	|	|	0.15
32.250	0.00	0.01	0.004	O	|	|	|	0.15
32.333	0.00	0.01	0.004	O	|	|	|	0.15
32.417	0.00	0.01	0.003	O	|	|	|	0.14
32.500	0.00	0.01	0.003	O	|	|	|	0.14
32.583	0.00	0.01	0.003	O	|	|	|	0.14
32.667	0.00	0.01	0.003	O	|	|	|	0.14
32.750	0.00	0.01	0.003	O	|	|	|	0.14
32.833	0.00	0.01	0.003	O	|	|	|	0.14
32.917	0.00	0.01	0.003	O	|	|	|	0.13
33.000	0.00	0.01	0.003	O	|	|	|	0.13
33.083	0.00	0.01	0.003	O	|	|	|	0.13
33.167	0.00	0.01	0.003	O	|	|	|	0.13
33.250	0.00	0.01	0.003	O	|	|	|	0.13
33.333	0.00	0.01	0.003	O	|	|	|	0.13
33.417	0.00	0.01	0.003	O	|	|	|	0.12
33.500	0.00	0.01	0.003	O	|	|	|	0.12
33.583	0.00	0.01	0.003	O	|	|	|	0.12
33.667	0.00	0.01	0.003	O	|	|	|	0.12
33.750	0.00	0.01	0.003	O	|	|	|	0.12
33.833	0.00	0.01	0.003	O	|	|	|	0.12
33.917	0.00	0.01	0.003	O	|	|	|	0.11
34.000	0.00	0.01	0.003	O	|	|	|	0.11
34.083	0.00	0.01	0.003	O	|	|	|	0.11
34.167	0.00	0.00	0.003	O	|	|	|	0.11
34.250	0.00	0.00	0.003	O	|	|	|	0.11
34.333	0.00	0.00	0.003	O	|	|	|	0.11
34.417	0.00	0.00	0.003	O	|	|	|	0.11
34.500	0.00	0.00	0.003	O	|	|	|	0.10
34.583	0.00	0.00	0.002	O	|	|	|	0.10
34.667	0.00	0.00	0.002	O	|	|	|	0.10
34.750	0.00	0.00	0.002	O	|	|	|	0.10
34.833	0.00	0.00	0.002	O	|	|	|	0.10
34.917	0.00	0.00	0.002	O	|	|	|	0.10
35.000	0.00	0.00	0.002	O	|	|	|	0.10
35.083	0.00	0.00	0.002	O	|	|	|	0.10
35.167	0.00	0.00	0.002	O	|	|	|	0.09
35.250	0.00	0.00	0.002	O	|	|	|	0.09
35.333	0.00	0.00	0.002	O	|	|	|	0.09
35.417	0.00	0.00	0.002	O	|	|	|	0.09
35.500	0.00	0.00	0.002	O	|	|	|	0.09
35.583	0.00	0.00	0.002	O	|	|	|	0.09
35.667	0.00	0.00	0.002	O	|	|	|	0.09

35.750	0.00	0.00	0.002	O	|	|	|	0.09
35.833	0.00	0.00	0.002	O	|	|	|	0.09
35.917	0.00	0.00	0.002	O	|	|	|	0.08
36.000	0.00	0.00	0.002	O	|	|	|	0.08
36.083	0.00	0.00	0.002	O	|	|	|	0.08
36.167	0.00	0.00	0.002	O	|	|	|	0.08
36.250	0.00	0.00	0.002	O	|	|	|	0.08
36.333	0.00	0.00	0.002	O	|	|	|	0.08
36.417	0.00	0.00	0.002	O	|	|	|	0.08
36.500	0.00	0.00	0.002	O	|	|	|	0.08
36.583	0.00	0.00	0.002	O	|	|	|	0.08
36.667	0.00	0.00	0.002	O	|	|	|	0.07
36.750	0.00	0.00	0.002	O	|	|	|	0.07
36.833	0.00	0.00	0.002	O	|	|	|	0.07
36.917	0.00	0.00	0.002	O	|	|	|	0.07
37.000	0.00	0.00	0.002	O	|	|	|	0.07
37.083	0.00	0.00	0.002	O	|	|	|	0.07
37.167	0.00	0.00	0.002	O	|	|	|	0.07
37.250	0.00	0.00	0.002	O	|	|	|	0.07
37.333	0.00	0.00	0.002	O	|	|	|	0.07
37.417	0.00	0.00	0.002	O	|	|	|	0.07
37.500	0.00	0.00	0.002	O	|	|	|	0.07
37.583	0.00	0.00	0.002	O	|	|	|	0.06
37.667	0.00	0.00	0.002	O	|	|	|	0.06
37.750	0.00	0.00	0.002	O	|	|	|	0.06
37.833	0.00	0.00	0.001	O	|	|	|	0.06
37.917	0.00	0.00	0.001	O	|	|	|	0.06
38.000	0.00	0.00	0.001	O	|	|	|	0.06
38.083	0.00	0.00	0.001	O	|	|	|	0.06
38.167	0.00	0.00	0.001	O	|	|	|	0.06
38.250	0.00	0.00	0.001	O	|	|	|	0.06
38.333	0.00	0.00	0.001	O	|	|	|	0.06
38.417	0.00	0.00	0.001	O	|	|	|	0.06
38.500	0.00	0.00	0.001	O	|	|	|	0.06
38.583	0.00	0.00	0.001	O	|	|	|	0.06
38.667	0.00	0.00	0.001	O	|	|	|	0.05
38.750	0.00	0.00	0.001	O	|	|	|	0.05
38.833	0.00	0.00	0.001	O	|	|	|	0.05
38.917	0.00	0.00	0.001	O	|	|	|	0.05
39.000	0.00	0.00	0.001	O	|	|	|	0.05
39.083	0.00	0.00	0.001	O	|	|	|	0.05
39.167	0.00	0.00	0.001	O	|	|	|	0.05
39.250	0.00	0.00	0.001	O	|	|	|	0.05
39.333	0.00	0.00	0.001	O	|	|	|	0.05
39.417	0.00	0.00	0.001	O	|	|	|	0.05
39.500	0.00	0.00	0.001	O	|	|	|	0.05
39.583	0.00	0.00	0.001	O	|	|	|	0.05
39.667	0.00	0.00	0.001	O	|	|	|	0.05
39.750	0.00	0.00	0.001	O	|	|	|	0.05
39.833	0.00	0.00	0.001	O	|	|	|	0.05

39.917	0.00	0.00	0.001	O				0.05
40.000	0.00	0.00	0.001	O				0.04
40.083	0.00	0.00	0.001	O				0.04
40.167	0.00	0.00	0.001	O				0.04
40.250	0.00	0.00	0.001	O				0.04
40.333	0.00	0.00	0.001	O				0.04
40.417	0.00	0.00	0.001	O				0.04
40.500	0.00	0.00	0.001	O				0.04
40.583	0.00	0.00	0.001	O				0.04
40.667	0.00	0.00	0.001	O				0.04
40.750	0.00	0.00	0.001	O				0.04
40.833	0.00	0.00	0.001	O				0.04
40.917	0.00	0.00	0.001	O				0.04
41.000	0.00	0.00	0.001	O				0.04
41.083	0.00	0.00	0.001	O				0.04
41.167	0.00	0.00	0.001	O				0.04
41.250	0.00	0.00	0.001	O				0.04
41.333	0.00	0.00	0.001	O				0.04
41.417	0.00	0.00	0.001	O				0.04
41.500	0.00	0.00	0.001	O				0.04
41.583	0.00	0.00	0.001	O				0.03
41.667	0.00	0.00	0.001	O				0.03
41.750	0.00	0.00	0.001	O				0.03
41.833	0.00	0.00	0.001	O				0.03
41.917	0.00	0.00	0.001	O				0.03
42.000	0.00	0.00	0.001	O				0.03
42.083	0.00	0.00	0.001	O				0.03
42.167	0.00	0.00	0.001	O				0.03
42.250	0.00	0.00	0.001	O				0.03
42.333	0.00	0.00	0.001	O				0.03
42.417	0.00	0.00	0.001	O				0.03
42.500	0.00	0.00	0.001	O				0.03
42.583	0.00	0.00	0.001	O				0.03
42.667	0.00	0.00	0.001	O				0.03
42.750	0.00	0.00	0.001	O				0.03
42.833	0.00	0.00	0.001	O				0.03
42.917	0.00	0.00	0.001	O				0.03
43.000	0.00	0.00	0.001	O				0.03
43.083	0.00	0.00	0.001	O				0.03
43.167	0.00	0.00	0.001	O				0.03
43.250	0.00	0.00	0.001	O				0.03
43.333	0.00	0.00	0.001	O				0.03
43.417	0.00	0.00	0.001	O				0.03
43.500	0.00	0.00	0.001	O				0.03
43.583	0.00	0.00	0.001	O				0.03
43.667	0.00	0.00	0.001	O				0.03
43.750	0.00	0.00	0.001	O				0.02
43.833	0.00	0.00	0.001	O				0.02
43.917	0.00	0.00	0.001	O				0.02
44.000	0.00	0.00	0.001	O				0.02

44.083	0.00	0.00	0.001	O	|	|	|	|	0.02
44.167	0.00	0.00	0.001	O	|	|	|	|	0.02
44.250	0.00	0.00	0.001	O	|	|	|	|	0.02
44.333	0.00	0.00	0.001	O	|	|	|	|	0.02
44.417	0.00	0.00	0.001	O	|	|	|	|	0.02
44.500	0.00	0.00	0.001	O	|	|	|	|	0.02
44.583	0.00	0.00	0.001	O	|	|	|	|	0.02

**********HYDROGRAPH DATA**********

Number of intervals = 535
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.045 (CFS)
Total volume = 0.096 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
10 yr
3 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris310.rte
**********HYDROGRAPH DATA**********
Number of intervals = 44
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.644 (CFS)
Total volume = 0.152 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 44
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.4 0.82 1.23 1.64	Depth (Ft.)
0.083	0.05	0.00	0.000	O | | | |	0.01
0.167	0.18	0.00	0.001	O I | | | |	0.04
0.250	0.22	0.00	0.002	O I | | | |	0.10
0.333	0.24	0.01	0.004	O I | | | |	0.16
0.417	0.28	0.01	0.006	O I | | | |	0.23
0.500	0.31	0.01	0.008	O I | | | |	0.32
0.583	0.34	0.02	0.010	O I | | | |	0.41
0.667	0.34	0.02	0.012	O I | | | |	0.50
0.750	0.37	0.03	0.014	O I| | | |	0.59
0.833	0.37	0.03	0.017	O I| | | |	0.69
0.917	0.34	0.04	0.019	O I | | | |	0.78
1.000	0.35	0.04	0.021	O I | | | |	0.87
1.083	0.39	0.04	0.023	O I| | | |	0.97
1.167	0.44	0.04	0.026	O I | | |	1.04
1.250	0.46	0.04	0.029	O I | | |	1.11
1.333	0.46	0.04	0.031	O I | | |	1.18
1.417	0.46	0.04	0.034	O I | | |	1.26
1.500	0.52	0.04	0.037	O | I | | |	1.33
1.583	0.54	0.04	0.041	O | I | | |	1.42
1.667	0.54	0.04	0.044	O | I | | |	1.50
1.750	0.59	0.04	0.048	O | I | | |	1.59
1.833	0.65	0.04	0.052	O | I | | |	1.69
1.917	0.65	0.04	0.056	O | I | | |	1.79
2.000	0.63	0.04	0.060	O | I | | |	1.90
2.083	0.65	0.04	0.064	O | I | | |	2.00
2.167	0.70	0.04	0.068	O | I | | |	2.11
2.250	0.85	0.04	0.073	O | I | |	2.23
2.333	0.92	0.04	0.079	O | |I | |	2.38

```
2.417    0.96    0.04      0.085  O       |        | I     |        |     2.53
2.500    1.34    0.04      0.093  O       |        |       | I      |     2.72
2.583    1.56    0.04      0.103  O       |        |       |     I  |     2.96
2.667    1.64    0.04      0.113  O       |        |       |       I|     3.23
2.750    1.27    0.04      0.123  O       |        |       I        |     3.47
2.833    0.78    0.04      0.130  O       |       I|       |        |     3.64
2.917    0.59    0.04      0.134  O       |  I     |       |        |     3.75
3.000    0.46    0.04      0.137  O       |I       |       |        |     3.84
3.083    0.27    0.04      0.140  O    I  |        |       |        |     3.89
3.167    0.13    0.04      0.141  O I     |        |       |        |     3.92
3.250    0.07    0.04      0.141  OI      |        |       |        |     3.93
3.333    0.04    0.04      0.141  O       |        |       |        |     3.93
3.417    0.02    0.04      0.141  O       |        |       |        |     3.93
3.500    0.01    0.04      0.141  O       |        |       |        |     3.92
3.583    0.00    0.04      0.141  O       |        |       |        |     3.92
3.667    0.00    0.04      0.140  O       |        |       |        |     3.91
3.750    0.00    0.04      0.140  O       |        |       |        |     3.90
3.833    0.00    0.04      0.140  O       |        |       |        |     3.89
3.917    0.00    0.04      0.139  O       |        |       |        |     3.89
4.000    0.00    0.04      0.139  O       |        |       |        |     3.88
4.083    0.00    0.04      0.139  O       |        |       |        |     3.87
4.167    0.00    0.04      0.139  O       |        |       |        |     3.86
4.250    0.00    0.04      0.138  O       |        |       |        |     3.86
4.333    0.00    0.04      0.138  O       |        |       |        |     3.85
4.417    0.00    0.04      0.138  O       |        |       |        |     3.84
4.500    0.00    0.04      0.137  O       |        |       |        |     3.83
4.583    0.00    0.04      0.137  O       |        |       |        |     3.82
4.667    0.00    0.04      0.137  O       |        |       |        |     3.82
4.750    0.00    0.04      0.136  O       |        |       |        |     3.81
4.833    0.00    0.04      0.136  O       |        |       |        |     3.80
4.917    0.00    0.04      0.136  O       |        |       |        |     3.79
5.000    0.00    0.04      0.135  O       |        |       |        |     3.79
5.083    0.00    0.04      0.135  O       |        |       |        |     3.78
5.167    0.00    0.04      0.135  O       |        |       |        |     3.77
5.250    0.00    0.04      0.134  O       |        |       |        |     3.76
5.333    0.00    0.04      0.134  O       |        |       |        |     3.75
5.417    0.00    0.04      0.134  O       |        |       |        |     3.75
5.500    0.00    0.04      0.134  O       |        |       |        |     3.74
5.583    0.00    0.04      0.133  O       |        |       |        |     3.73
5.667    0.00    0.04      0.133  O       |        |       |        |     3.72
5.750    0.00    0.04      0.133  O       |        |       |        |     3.72
5.833    0.00    0.04      0.132  O       |        |       |        |     3.71
5.917    0.00    0.04      0.132  O       |        |       |        |     3.70
6.000    0.00    0.04      0.132  O       |        |       |        |     3.69
6.083    0.00    0.04      0.131  O       |        |       |        |     3.68
6.167    0.00    0.04      0.131  O       |        |       |        |     3.68
6.250    0.00    0.04      0.131  O       |        |       |        |     3.67
6.333    0.00    0.04      0.130  O       |        |       |        |     3.66
6.417    0.00    0.04      0.130  O       |        |       |        |     3.65
6.500    0.00    0.04      0.130  O       |        |       |        |     3.65
```

6.583	0.00	0.04	0.130	O				3.64
6.667	0.00	0.04	0.129	O				3.63
6.750	0.00	0.04	0.129	O				3.62
6.833	0.00	0.04	0.129	O				3.62
6.917	0.00	0.04	0.128	O				3.61
7.000	0.00	0.04	0.128	O				3.60
7.083	0.00	0.04	0.128	O				3.59
7.167	0.00	0.04	0.127	O				3.58
7.250	0.00	0.04	0.127	O				3.58
7.333	0.00	0.04	0.127	O				3.57
7.417	0.00	0.04	0.126	O				3.56
7.500	0.00	0.04	0.126	O				3.55
7.583	0.00	0.04	0.126	O				3.55
7.667	0.00	0.04	0.126	O				3.54
7.750	0.00	0.04	0.125	O				3.53
7.833	0.00	0.04	0.125	O				3.52
7.917	0.00	0.04	0.125	O				3.51
8.000	0.00	0.04	0.124	O				3.51
8.083	0.00	0.04	0.124	O				3.50
8.167	0.00	0.04	0.124	O				3.49
8.250	0.00	0.04	0.123	O				3.48
8.333	0.00	0.04	0.123	O				3.48
8.417	0.00	0.04	0.123	O				3.47
8.500	0.00	0.04	0.122	O				3.46
8.583	0.00	0.04	0.122	O				3.45
8.667	0.00	0.04	0.122	O				3.44
8.750	0.00	0.04	0.121	O				3.44
8.833	0.00	0.04	0.121	O				3.43
8.917	0.00	0.04	0.121	O				3.42
9.000	0.00	0.04	0.121	O				3.41
9.083	0.00	0.04	0.120	O				3.41
9.167	0.00	0.04	0.120	O				3.40
9.250	0.00	0.04	0.120	O				3.39
9.333	0.00	0.04	0.119	O				3.38
9.417	0.00	0.04	0.119	O				3.37
9.500	0.00	0.04	0.119	O				3.37
9.583	0.00	0.04	0.118	O				3.36
9.667	0.00	0.04	0.118	O				3.35
9.750	0.00	0.04	0.118	O				3.34
9.833	0.00	0.04	0.117	O				3.34
9.917	0.00	0.04	0.117	O				3.33
10.000	0.00	0.04	0.117	O				3.32
10.083	0.00	0.04	0.117	O				3.31
10.167	0.00	0.04	0.116	O				3.31
10.250	0.00	0.04	0.116	O				3.30
10.333	0.00	0.04	0.116	O				3.29
10.417	0.00	0.04	0.115	O				3.28
10.500	0.00	0.04	0.115	O				3.27
10.583	0.00	0.04	0.115	O				3.27
10.667	0.00	0.04	0.114	O				3.26

10.750	0.00	0.04	0.114	O				3.25
10.833	0.00	0.04	0.114	O				3.24
10.917	0.00	0.04	0.113	O				3.24
11.000	0.00	0.04	0.113	O				3.23
11.083	0.00	0.04	0.113	O				3.22
11.167	0.00	0.04	0.112	O				3.21
11.250	0.00	0.04	0.112	O				3.20
11.333	0.00	0.04	0.112	O				3.20
11.417	0.00	0.04	0.112	O				3.19
11.500	0.00	0.04	0.111	O				3.18
11.583	0.00	0.04	0.111	O				3.17
11.667	0.00	0.04	0.111	O				3.17
11.750	0.00	0.04	0.110	O				3.16
11.833	0.00	0.04	0.110	O				3.15
11.917	0.00	0.04	0.110	O				3.14
12.000	0.00	0.04	0.109	O				3.13
12.083	0.00	0.04	0.109	O				3.13
12.167	0.00	0.04	0.109	O				3.12
12.250	0.00	0.04	0.108	O				3.11
12.333	0.00	0.04	0.108	O				3.10
12.417	0.00	0.04	0.108	O				3.10
12.500	0.00	0.04	0.108	O				3.09
12.583	0.00	0.04	0.107	O				3.08
12.667	0.00	0.04	0.107	O				3.07
12.750	0.00	0.04	0.107	O				3.06
12.833	0.00	0.04	0.106	O				3.06
12.917	0.00	0.04	0.106	O				3.05
13.000	0.00	0.04	0.106	O				3.04
13.083	0.00	0.04	0.105	O				3.03
13.167	0.00	0.04	0.105	O				3.03
13.250	0.00	0.04	0.105	O				3.02
13.333	0.00	0.04	0.104	O				3.01
13.417	0.00	0.04	0.104	O				3.00
13.500	0.00	0.04	0.104	O				3.00
13.583	0.00	0.04	0.103	O				2.99
13.667	0.00	0.04	0.103	O				2.98
13.750	0.00	0.04	0.103	O				2.97
13.833	0.00	0.04	0.103	O				2.96
13.917	0.00	0.04	0.102	O				2.96
14.000	0.00	0.04	0.102	O				2.95
14.083	0.00	0.04	0.102	O				2.94
14.167	0.00	0.04	0.101	O				2.93
14.250	0.00	0.04	0.101	O				2.93
14.333	0.00	0.04	0.101	O				2.92
14.417	0.00	0.04	0.100	O				2.91
14.500	0.00	0.04	0.100	O				2.90
14.583	0.00	0.04	0.100	O				2.89
14.667	0.00	0.04	0.099	O				2.89
14.750	0.00	0.04	0.099	O				2.88
14.833	0.00	0.04	0.099	O				2.87

14.917	0.00	0.04	0.099	O				2.86
15.000	0.00	0.04	0.098	O				2.86
15.083	0.00	0.04	0.098	O				2.85
15.167	0.00	0.04	0.098	O				2.84
15.250	0.00	0.04	0.097	O				2.83
15.333	0.00	0.04	0.097	O				2.82
15.417	0.00	0.04	0.097	O				2.82
15.500	0.00	0.04	0.096	O				2.81
15.583	0.00	0.04	0.096	O				2.80
15.667	0.00	0.04	0.096	O				2.79
15.750	0.00	0.04	0.095	O				2.79
15.833	0.00	0.04	0.095	O				2.78
15.917	0.00	0.04	0.095	O				2.77
16.000	0.00	0.04	0.095	O				2.76
16.083	0.00	0.04	0.094	O				2.76
16.167	0.00	0.04	0.094	O				2.75
16.250	0.00	0.04	0.094	O				2.74
16.333	0.00	0.04	0.093	O				2.73
16.417	0.00	0.04	0.093	O				2.72
16.500	0.00	0.04	0.093	O				2.72
16.583	0.00	0.04	0.092	O				2.71
16.667	0.00	0.04	0.092	O				2.70
16.750	0.00	0.04	0.092	O				2.69
16.833	0.00	0.04	0.091	O				2.69
16.917	0.00	0.04	0.091	O				2.68
17.000	0.00	0.04	0.091	O				2.67
17.083	0.00	0.04	0.090	O				2.66
17.167	0.00	0.04	0.090	O				2.65
17.250	0.00	0.04	0.090	O				2.65
17.333	0.00	0.04	0.090	O				2.64
17.417	0.00	0.04	0.089	O				2.63
17.500	0.00	0.04	0.089	O				2.62
17.583	0.00	0.04	0.089	O				2.62
17.667	0.00	0.04	0.088	O				2.61
17.750	0.00	0.04	0.088	O				2.60
17.833	0.00	0.04	0.088	O				2.59
17.917	0.00	0.04	0.087	O				2.58
18.000	0.00	0.04	0.087	O				2.58
18.083	0.00	0.04	0.087	O				2.57
18.167	0.00	0.04	0.086	O				2.56
18.250	0.00	0.04	0.086	O				2.55
18.333	0.00	0.04	0.086	O				2.55
18.417	0.00	0.04	0.086	O				2.54
18.500	0.00	0.04	0.085	O				2.53
18.583	0.00	0.04	0.085	O				2.52
18.667	0.00	0.04	0.085	O				2.51
18.750	0.00	0.04	0.084	O				2.51
18.833	0.00	0.04	0.084	O				2.50
18.917	0.00	0.04	0.084	O				2.49
19.000	0.00	0.04	0.083	O				2.48

19.083	0.00	0.04	0.083	O				2.48
19.167	0.00	0.04	0.083	O				2.47
19.250	0.00	0.04	0.082	O				2.46
19.333	0.00	0.04	0.082	O				2.45
19.417	0.00	0.04	0.082	O				2.45
19.500	0.00	0.04	0.081	O				2.44
19.583	0.00	0.04	0.081	O				2.43
19.667	0.00	0.04	0.081	O				2.42
19.750	0.00	0.04	0.081	O				2.41
19.833	0.00	0.04	0.080	O				2.41
19.917	0.00	0.04	0.080	O				2.40
20.000	0.00	0.04	0.080	O				2.39
20.083	0.00	0.04	0.079	O				2.38
20.167	0.00	0.04	0.079	O				2.38
20.250	0.00	0.04	0.079	O				2.37
20.333	0.00	0.04	0.078	O				2.36
20.417	0.00	0.04	0.078	O				2.35
20.500	0.00	0.04	0.078	O				2.34
20.583	0.00	0.04	0.077	O				2.34
20.667	0.00	0.04	0.077	O				2.33
20.750	0.00	0.04	0.077	O				2.32
20.833	0.00	0.04	0.077	O				2.31
20.917	0.00	0.04	0.076	O				2.31
21.000	0.00	0.04	0.076	O				2.30
21.083	0.00	0.04	0.076	O				2.29
21.167	0.00	0.04	0.075	O				2.28
21.250	0.00	0.04	0.075	O				2.27
21.333	0.00	0.04	0.075	O				2.27
21.417	0.00	0.04	0.074	O				2.26
21.500	0.00	0.04	0.074	O				2.25
21.583	0.00	0.04	0.074	O				2.24
21.667	0.00	0.04	0.073	O				2.24
21.750	0.00	0.04	0.073	O				2.23
21.833	0.00	0.04	0.073	O				2.22
21.917	0.00	0.04	0.073	O				2.21
22.000	0.00	0.04	0.072	O				2.20
22.083	0.00	0.04	0.072	O				2.20
22.167	0.00	0.04	0.072	O				2.19
22.250	0.00	0.04	0.071	O				2.18
22.333	0.00	0.04	0.071	O				2.17
22.417	0.00	0.04	0.071	O				2.17
22.500	0.00	0.04	0.070	O				2.16
22.583	0.00	0.04	0.070	O				2.15
22.667	0.00	0.04	0.070	O				2.14
22.750	0.00	0.04	0.069	O				2.14
22.833	0.00	0.04	0.069	O				2.13
22.917	0.00	0.04	0.069	O				2.12
23.000	0.00	0.04	0.068	O				2.11
23.083	0.00	0.04	0.068	O				2.10
23.167	0.00	0.04	0.068	O				2.10

23.250	0.00	0.04	0.068	O	|	|	|	2.09
23.333	0.00	0.04	0.067	O	|	|	|	2.08
23.417	0.00	0.04	0.067	O	|	|	|	2.07
23.500	0.00	0.04	0.067	O	|	|	|	2.07
23.583	0.00	0.04	0.066	O	|	|	|	2.06
23.667	0.00	0.04	0.066	O	|	|	|	2.05
23.750	0.00	0.04	0.066	O	|	|	|	2.04
23.833	0.00	0.04	0.065	O	|	|	|	2.03
23.917	0.00	0.04	0.065	O	|	|	|	2.03
24.000	0.00	0.04	0.065	O	|	|	|	2.02
24.083	0.00	0.04	0.064	O	|	|	|	2.01
24.167	0.00	0.04	0.064	O	|	|	|	2.00
24.250	0.00	0.04	0.064	O	|	|	|	2.00
24.333	0.00	0.04	0.064	O	|	|	|	1.99
24.417	0.00	0.04	0.063	O	|	|	|	1.98
24.500	0.00	0.04	0.063	O	|	|	|	1.97
24.583	0.00	0.04	0.063	O	|	|	|	1.96
24.667	0.00	0.04	0.062	O	|	|	|	1.96
24.750	0.00	0.04	0.062	O	|	|	|	1.95
24.833	0.00	0.04	0.062	O	|	|	|	1.94
24.917	0.00	0.04	0.061	O	|	|	|	1.93
25.000	0.00	0.04	0.061	O	|	|	|	1.93
25.083	0.00	0.04	0.061	O	|	|	|	1.92
25.167	0.00	0.04	0.060	O	|	|	|	1.91
25.250	0.00	0.04	0.060	O	|	|	|	1.90
25.333	0.00	0.04	0.060	O	|	|	|	1.90
25.417	0.00	0.04	0.059	O	|	|	|	1.89
25.500	0.00	0.04	0.059	O	|	|	|	1.88
25.583	0.00	0.04	0.059	O	|	|	|	1.87
25.667	0.00	0.04	0.059	O	|	|	|	1.86
25.750	0.00	0.04	0.058	O	|	|	|	1.86
25.833	0.00	0.04	0.058	O	|	|	|	1.85
25.917	0.00	0.04	0.058	O	|	|	|	1.84
26.000	0.00	0.04	0.057	O	|	|	|	1.83
26.083	0.00	0.04	0.057	O	|	|	|	1.83
26.167	0.00	0.04	0.057	O	|	|	|	1.82
26.250	0.00	0.04	0.056	O	|	|	|	1.81
26.333	0.00	0.04	0.056	O	|	|	|	1.80
26.417	0.00	0.04	0.056	O	|	|	|	1.79
26.500	0.00	0.04	0.055	O	|	|	|	1.79
26.583	0.00	0.04	0.055	O	|	|	|	1.78
26.667	0.00	0.04	0.055	O	|	|	|	1.77
26.750	0.00	0.04	0.055	O	|	|	|	1.76
26.833	0.00	0.04	0.054	O	|	|	|	1.76
26.917	0.00	0.04	0.054	O	|	|	|	1.75
27.000	0.00	0.04	0.054	O	|	|	|	1.74
27.083	0.00	0.04	0.053	O	|	|	|	1.73
27.167	0.00	0.04	0.053	O	|	|	|	1.72
27.250	0.00	0.04	0.053	O	|	|	|	1.72
27.333	0.00	0.04	0.052	O	|	|	|	1.71

27.417	0.00	0.04	0.052	O				1.70
27.500	0.00	0.04	0.052	O				1.69
27.583	0.00	0.04	0.051	O				1.69
27.667	0.00	0.04	0.051	O				1.68
27.750	0.00	0.04	0.051	O				1.67
27.833	0.00	0.04	0.051	O				1.66
27.917	0.00	0.04	0.050	O				1.65
28.000	0.00	0.04	0.050	O				1.65
28.083	0.00	0.04	0.050	O				1.64
28.167	0.00	0.04	0.049	O				1.63
28.250	0.00	0.04	0.049	O				1.62
28.333	0.00	0.04	0.049	O				1.62
28.417	0.00	0.04	0.048	O				1.61
28.500	0.00	0.04	0.048	O				1.60
28.583	0.00	0.04	0.048	O				1.59
28.667	0.00	0.04	0.047	O				1.59
28.750	0.00	0.04	0.047	O				1.58
28.833	0.00	0.04	0.047	O				1.57
28.917	0.00	0.04	0.046	O				1.56
29.000	0.00	0.04	0.046	O				1.55
29.083	0.00	0.04	0.046	O				1.55
29.167	0.00	0.04	0.046	O				1.54
29.250	0.00	0.04	0.045	O				1.53
29.333	0.00	0.04	0.045	O				1.52
29.417	0.00	0.04	0.045	O				1.52
29.500	0.00	0.04	0.044	O				1.51
29.583	0.00	0.04	0.044	O				1.50
29.667	0.00	0.04	0.044	O				1.49
29.750	0.00	0.04	0.043	O				1.48
29.833	0.00	0.04	0.043	O				1.48
29.917	0.00	0.04	0.043	O				1.47
30.000	0.00	0.04	0.042	O				1.46
30.083	0.00	0.04	0.042	O				1.45
30.167	0.00	0.04	0.042	O				1.45
30.250	0.00	0.04	0.042	O				1.44
30.333	0.00	0.04	0.041	O				1.43
30.417	0.00	0.04	0.041	O				1.42
30.500	0.00	0.04	0.041	O				1.41
30.583	0.00	0.04	0.040	O				1.41
30.667	0.00	0.04	0.040	O				1.40
30.750	0.00	0.04	0.040	O				1.39
30.833	0.00	0.04	0.039	O				1.38
30.917	0.00	0.04	0.039	O				1.38
31.000	0.00	0.04	0.039	O				1.37
31.083	0.00	0.04	0.038	O				1.36
31.167	0.00	0.04	0.038	O				1.35
31.250	0.00	0.04	0.038	O				1.34
31.333	0.00	0.04	0.037	O				1.34
31.417	0.00	0.04	0.037	O				1.33
31.500	0.00	0.04	0.037	O				1.32

31.583	0.00	0.04	0.037	O	|	|	|	1.31
31.667	0.00	0.04	0.036	O	|	|	|	1.31
31.750	0.00	0.04	0.036	O	|	|	|	1.30
31.833	0.00	0.04	0.036	O	|	|	|	1.29
31.917	0.00	0.04	0.035	O	|	|	|	1.28
32.000	0.00	0.04	0.035	O	|	|	|	1.28
32.083	0.00	0.04	0.035	O	|	|	|	1.27
32.167	0.00	0.04	0.034	O	|	|	|	1.26
32.250	0.00	0.04	0.034	O	|	|	|	1.25
32.333	0.00	0.04	0.034	O	|	|	|	1.24
32.417	0.00	0.04	0.033	O	|	|	|	1.24
32.500	0.00	0.04	0.033	O	|	|	|	1.23
32.583	0.00	0.04	0.033	O	|	|	|	1.22
32.667	0.00	0.04	0.033	O	|	|	|	1.21
32.750	0.00	0.04	0.032	O	|	|	|	1.21
32.833	0.00	0.04	0.032	O	|	|	|	1.20
32.917	0.00	0.04	0.032	O	|	|	|	1.19
33.000	0.00	0.04	0.031	O	|	|	|	1.18
33.083	0.00	0.04	0.031	O	|	|	|	1.17
33.167	0.00	0.04	0.031	O	|	|	|	1.17
33.250	0.00	0.04	0.030	O	|	|	|	1.16
33.333	0.00	0.04	0.030	O	|	|	|	1.15
33.417	0.00	0.04	0.030	O	|	|	|	1.14
33.500	0.00	0.04	0.029	O	|	|	|	1.14
33.583	0.00	0.04	0.029	O	|	|	|	1.13
33.667	0.00	0.04	0.029	O	|	|	|	1.12
33.750	0.00	0.04	0.028	O	|	|	|	1.11
33.833	0.00	0.04	0.028	O	|	|	|	1.10
33.917	0.00	0.04	0.028	O	|	|	|	1.10
34.000	0.00	0.04	0.028	O	|	|	|	1.09
34.083	0.00	0.04	0.027	O	|	|	|	1.08
34.167	0.00	0.04	0.027	O	|	|	|	1.07
34.250	0.00	0.04	0.027	O	|	|	|	1.07
34.333	0.00	0.04	0.026	O	|	|	|	1.06
34.417	0.00	0.04	0.026	O	|	|	|	1.05
34.500	0.00	0.04	0.026	O	|	|	|	1.04
34.583	0.00	0.04	0.025	O	|	|	|	1.03
34.667	0.00	0.04	0.025	O	|	|	|	1.03
34.750	0.00	0.04	0.025	O	|	|	|	1.02
34.833	0.00	0.04	0.024	O	|	|	|	1.01
34.917	0.00	0.04	0.024	O	|	|	|	1.00
35.000	0.00	0.04	0.024	O	|	|	|	0.99
35.083	0.00	0.04	0.024	O	|	|	|	0.98
35.167	0.00	0.04	0.023	O	|	|	|	0.97
35.250	0.00	0.04	0.023	O	|	|	|	0.96
35.333	0.00	0.04	0.023	O	|	|	|	0.94
35.417	0.00	0.04	0.022	O	|	|	|	0.93
35.500	0.00	0.04	0.022	O	|	|	|	0.92
35.583	0.00	0.04	0.022	O	|	|	|	0.91
35.667	0.00	0.04	0.022	O	|	|	|	0.90

35.750	0.00	0.04	0.021	O				0.88
35.833	0.00	0.04	0.021	O				0.87
35.917	0.00	0.04	0.021	O				0.86
36.000	0.00	0.04	0.020	O				0.85
36.083	0.00	0.04	0.020	O				0.84
36.167	0.00	0.04	0.020	O				0.83
36.250	0.00	0.04	0.020	O				0.82
36.333	0.00	0.04	0.019	O				0.81
36.417	0.00	0.04	0.019	O				0.80
36.500	0.00	0.04	0.019	O				0.79
36.583	0.00	0.03	0.019	O				0.78
36.667	0.00	0.03	0.018	O				0.77
36.750	0.00	0.03	0.018	O				0.76
36.833	0.00	0.03	0.018	O				0.75
36.917	0.00	0.03	0.018	O				0.74
37.000	0.00	0.03	0.017	O				0.73
37.083	0.00	0.03	0.017	O				0.72
37.167	0.00	0.03	0.017	O				0.71
37.250	0.00	0.03	0.017	O				0.70
37.333	0.00	0.03	0.017	O				0.69
37.417	0.00	0.03	0.016	O				0.68
37.500	0.00	0.03	0.016	O				0.67
37.583	0.00	0.03	0.016	O				0.67
37.667	0.00	0.03	0.016	O				0.66
37.750	0.00	0.03	0.016	O				0.65
37.833	0.00	0.03	0.015	O				0.64
37.917	0.00	0.03	0.015	O				0.63
38.000	0.00	0.03	0.015	O				0.62
38.083	0.00	0.03	0.015	O				0.62
38.167	0.00	0.03	0.015	O				0.61
38.250	0.00	0.03	0.014	O				0.60
38.333	0.00	0.03	0.014	O				0.59
38.417	0.00	0.03	0.014	O				0.59
38.500	0.00	0.03	0.014	O				0.58
38.583	0.00	0.03	0.014	O				0.57
38.667	0.00	0.03	0.014	O				0.56
38.750	0.00	0.03	0.013	O				0.56
38.833	0.00	0.02	0.013	O				0.55
38.917	0.00	0.02	0.013	O				0.54
39.000	0.00	0.02	0.013	O				0.53
39.083	0.00	0.02	0.013	O				0.53
39.167	0.00	0.02	0.013	O				0.52
39.250	0.00	0.02	0.012	O				0.51
39.333	0.00	0.02	0.012	O				0.51
39.417	0.00	0.02	0.012	O				0.50
39.500	0.00	0.02	0.012	O				0.49
39.583	0.00	0.02	0.012	O				0.49
39.667	0.00	0.02	0.012	O				0.48
39.750	0.00	0.02	0.011	O				0.48
39.833	0.00	0.02	0.011	O				0.47

39.917	0.00	0.02	0.011	O				0.46
40.000	0.00	0.02	0.011	O				0.46
40.083	0.00	0.02	0.011	O				0.45
40.167	0.00	0.02	0.011	O				0.45
40.250	0.00	0.02	0.011	O				0.44
40.333	0.00	0.02	0.010	O				0.43
40.417	0.00	0.02	0.010	O				0.43
40.500	0.00	0.02	0.010	O				0.42
40.583	0.00	0.02	0.010	O				0.42
40.667	0.00	0.02	0.010	O				0.41
40.750	0.00	0.02	0.010	O				0.41
40.833	0.00	0.02	0.010	O				0.40
40.917	0.00	0.02	0.010	O				0.40
41.000	0.00	0.02	0.009	O				0.39
41.083	0.00	0.02	0.009	O				0.39
41.167	0.00	0.02	0.009	O				0.38
41.250	0.00	0.02	0.009	O				0.38
41.333	0.00	0.02	0.009	O				0.37
41.417	0.00	0.02	0.009	O				0.37
41.500	0.00	0.02	0.009	O				0.36
41.583	0.00	0.02	0.009	O				0.36
41.667	0.00	0.02	0.008	O				0.35
41.750	0.00	0.02	0.008	O				0.35
41.833	0.00	0.02	0.008	O				0.34
41.917	0.00	0.02	0.008	O				0.34
42.000	0.00	0.02	0.008	O				0.34
42.083	0.00	0.01	0.008	O				0.33
42.167	0.00	0.01	0.008	O				0.33
42.250	0.00	0.01	0.008	O				0.32
42.333	0.00	0.01	0.008	O				0.32
42.417	0.00	0.01	0.008	O				0.31
42.500	0.00	0.01	0.007	O				0.31
42.583	0.00	0.01	0.007	O				0.31
42.667	0.00	0.01	0.007	O				0.30
42.750	0.00	0.01	0.007	O				0.30
42.833	0.00	0.01	0.007	O				0.30
42.917	0.00	0.01	0.007	O				0.29
43.000	0.00	0.01	0.007	O				0.29
43.083	0.00	0.01	0.007	O				0.28
43.167	0.00	0.01	0.007	O				0.28
43.250	0.00	0.01	0.007	O				0.28
43.333	0.00	0.01	0.007	O				0.27
43.417	0.00	0.01	0.006	O				0.27
43.500	0.00	0.01	0.006	O				0.27
43.583	0.00	0.01	0.006	O				0.26
43.667	0.00	0.01	0.006	O				0.26
43.750	0.00	0.01	0.006	O				0.26
43.833	0.00	0.01	0.006	O				0.25
43.917	0.00	0.01	0.006	O				0.25
44.000	0.00	0.01	0.006	O				0.25

44.083	0.00	0.01	0.006	O				0.24
44.167	0.00	0.01	0.006	O				0.24
44.250	0.00	0.01	0.006	O				0.24
44.333	0.00	0.01	0.006	O				0.23
44.417	0.00	0.01	0.006	O				0.23
44.500	0.00	0.01	0.005	O				0.23
44.583	0.00	0.01	0.005	O				0.23
44.667	0.00	0.01	0.005	O				0.22
44.750	0.00	0.01	0.005	O				0.22
44.833	0.00	0.01	0.005	O				0.22
44.917	0.00	0.01	0.005	O				0.21
45.000	0.00	0.01	0.005	O				0.21
45.083	0.00	0.01	0.005	O				0.21
45.167	0.00	0.01	0.005	O				0.21
45.250	0.00	0.01	0.005	O				0.20
45.333	0.00	0.01	0.005	O				0.20
45.417	0.00	0.01	0.005	O				0.20
45.500	0.00	0.01	0.005	O				0.20
45.583	0.00	0.01	0.005	O				0.19
45.667	0.00	0.01	0.005	O				0.19
45.750	0.00	0.01	0.005	O				0.19
45.833	0.00	0.01	0.004	O				0.19
45.917	0.00	0.01	0.004	O				0.18
46.000	0.00	0.01	0.004	O				0.18
46.083	0.00	0.01	0.004	O				0.18
46.167	0.00	0.01	0.004	O				0.18
46.250	0.00	0.01	0.004	O				0.17
46.333	0.00	0.01	0.004	O				0.17
46.417	0.00	0.01	0.004	O				0.17
46.500	0.00	0.01	0.004	O				0.17
46.583	0.00	0.01	0.004	O				0.17
46.667	0.00	0.01	0.004	O				0.16
46.750	0.00	0.01	0.004	O				0.16
46.833	0.00	0.01	0.004	O				0.16
46.917	0.00	0.01	0.004	O				0.16
47.000	0.00	0.01	0.004	O				0.15
47.083	0.00	0.01	0.004	O				0.15
47.167	0.00	0.01	0.004	O				0.15
47.250	0.00	0.01	0.004	O				0.15
47.333	0.00	0.01	0.004	O				0.15
47.417	0.00	0.01	0.003	O				0.15
47.500	0.00	0.01	0.003	O				0.14
47.583	0.00	0.01	0.003	O				0.14
47.667	0.00	0.01	0.003	O				0.14
47.750	0.00	0.01	0.003	O				0.14
47.833	0.00	0.01	0.003	O				0.14
47.917	0.00	0.01	0.003	O				0.13
48.000	0.00	0.01	0.003	O				0.13
48.083	0.00	0.01	0.003	O				0.13
48.167	0.00	0.01	0.003	O				0.13

48.250	0.00	0.01	0.003	O	|	|	|	0.13
48.333	0.00	0.01	0.003	O	|	|	|	0.13
48.417	0.00	0.01	0.003	O	|	|	|	0.12
48.500	0.00	0.01	0.003	O	|	|	|	0.12
48.583	0.00	0.01	0.003	O	|	|	|	0.12
48.667	0.00	0.01	0.003	O	|	|	|	0.12
48.750	0.00	0.01	0.003	O	|	|	|	0.12
48.833	0.00	0.01	0.003	O	|	|	|	0.12
48.917	0.00	0.01	0.003	O	|	|	|	0.12
49.000	0.00	0.01	0.003	O	|	|	|	0.11
49.083	0.00	0.01	0.003	O	|	|	|	0.11
49.167	0.00	0.00	0.003	O	|	|	|	0.11
49.250	0.00	0.00	0.003	O	|	|	|	0.11
49.333	0.00	0.00	0.003	O	|	|	|	0.11
49.417	0.00	0.00	0.003	O	|	|	|	0.11
49.500	0.00	0.00	0.003	O	|	|	|	0.11
49.583	0.00	0.00	0.002	O	|	|	|	0.10
49.667	0.00	0.00	0.002	O	|	|	|	0.10
49.750	0.00	0.00	0.002	O	|	|	|	0.10
49.833	0.00	0.00	0.002	O	|	|	|	0.10
49.917	0.00	0.00	0.002	O	|	|	|	0.10
50.000	0.00	0.00	0.002	O	|	|	|	0.10
50.083	0.00	0.00	0.002	O	|	|	|	0.10
50.167	0.00	0.00	0.002	O	|	|	|	0.09
50.250	0.00	0.00	0.002	O	|	|	|	0.09
50.333	0.00	0.00	0.002	O	|	|	|	0.09
50.417	0.00	0.00	0.002	O	|	|	|	0.09
50.500	0.00	0.00	0.002	O	|	|	|	0.09
50.583	0.00	0.00	0.002	O	|	|	|	0.09
50.667	0.00	0.00	0.002	O	|	|	|	0.09
50.750	0.00	0.00	0.002	O	|	|	|	0.09
50.833	0.00	0.00	0.002	O	|	|	|	0.09
50.917	0.00	0.00	0.002	O	|	|	|	0.08
51.000	0.00	0.00	0.002	O	|	|	|	0.08
51.083	0.00	0.00	0.002	O	|	|	|	0.08
51.167	0.00	0.00	0.002	O	|	|	|	0.08
51.250	0.00	0.00	0.002	O	|	|	|	0.08
51.333	0.00	0.00	0.002	O	|	|	|	0.08
51.417	0.00	0.00	0.002	O	|	|	|	0.08
51.500	0.00	0.00	0.002	O	|	|	|	0.08
51.583	0.00	0.00	0.002	O	|	|	|	0.08
51.667	0.00	0.00	0.002	O	|	|	|	0.08
51.750	0.00	0.00	0.002	O	|	|	|	0.07
51.833	0.00	0.00	0.002	O	|	|	|	0.07
51.917	0.00	0.00	0.002	O	|	|	|	0.07
52.000	0.00	0.00	0.002	O	|	|	|	0.07
52.083	0.00	0.00	0.002	O	|	|	|	0.07
52.167	0.00	0.00	0.002	O	|	|	|	0.07
52.250	0.00	0.00	0.002	O	|	|	|	0.07
52.333	0.00	0.00	0.002	O	|	|	|	0.07

52.417	0.00	0.00	0.002	O	|	|	|	0.07
52.500	0.00	0.00	0.002	O	|	|	|	0.07
52.583	0.00	0.00	0.002	O	|	|	|	0.07
52.667	0.00	0.00	0.002	O	|	|	|	0.06
52.750	0.00	0.00	0.002	O	|	|	|	0.06
52.833	0.00	0.00	0.002	O	|	|	|	0.06
52.917	0.00	0.00	0.001	O	|	|	|	0.06
53.000	0.00	0.00	0.001	O	|	|	|	0.06
53.083	0.00	0.00	0.001	O	|	|	|	0.06
53.167	0.00	0.00	0.001	O	|	|	|	0.06
53.250	0.00	0.00	0.001	O	|	|	|	0.06
53.333	0.00	0.00	0.001	O	|	|	|	0.06
53.417	0.00	0.00	0.001	O	|	|	|	0.06
53.500	0.00	0.00	0.001	O	|	|	|	0.06
53.583	0.00	0.00	0.001	O	|	|	|	0.06
53.667	0.00	0.00	0.001	O	|	|	|	0.06
53.750	0.00	0.00	0.001	O	|	|	|	0.05
53.833	0.00	0.00	0.001	O	|	|	|	0.05
53.917	0.00	0.00	0.001	O	|	|	|	0.05
54.000	0.00	0.00	0.001	O	|	|	|	0.05
54.083	0.00	0.00	0.001	O	|	|	|	0.05
54.167	0.00	0.00	0.001	O	|	|	|	0.05
54.250	0.00	0.00	0.001	O	|	|	|	0.05
54.333	0.00	0.00	0.001	O	|	|	|	0.05
54.417	0.00	0.00	0.001	O	|	|	|	0.05
54.500	0.00	0.00	0.001	O	|	|	|	0.05
54.583	0.00	0.00	0.001	O	|	|	|	0.05
54.667	0.00	0.00	0.001	O	|	|	|	0.05
54.750	0.00	0.00	0.001	O	|	|	|	0.05
54.833	0.00	0.00	0.001	O	|	|	|	0.05
54.917	0.00	0.00	0.001	O	|	|	|	0.05
55.000	0.00	0.00	0.001	O	|	|	|	0.04
55.083	0.00	0.00	0.001	O	|	|	|	0.04
55.167	0.00	0.00	0.001	O	|	|	|	0.04
55.250	0.00	0.00	0.001	O	|	|	|	0.04
55.333	0.00	0.00	0.001	O	|	|	|	0.04
55.417	0.00	0.00	0.001	O	|	|	|	0.04
55.500	0.00	0.00	0.001	O	|	|	|	0.04
55.583	0.00	0.00	0.001	O	|	|	|	0.04
55.667	0.00	0.00	0.001	O	|	|	|	0.04
55.750	0.00	0.00	0.001	O	|	|	|	0.04
55.833	0.00	0.00	0.001	O	|	|	|	0.04
55.917	0.00	0.00	0.001	O	|	|	|	0.04
56.000	0.00	0.00	0.001	O	|	|	|	0.04
56.083	0.00	0.00	0.001	O	|	|	|	0.04
56.167	0.00	0.00	0.001	O	|	|	|	0.04
56.250	0.00	0.00	0.001	O	|	|	|	0.04
56.333	0.00	0.00	0.001	O	|	|	|	0.04
56.417	0.00	0.00	0.001	O	|	|	|	0.04
56.500	0.00	0.00	0.001	O	|	|	|	0.04

56.583	0.00	0.00	0.001	O	|	|	|	|	0.04
56.667	0.00	0.00	0.001	O	|	|	|	|	0.03
56.750	0.00	0.00	0.001	O	|	|	|	|	0.03
56.833	0.00	0.00	0.001	O	|	|	|	|	0.03
56.917	0.00	0.00	0.001	O	|	|	|	|	0.03
57.000	0.00	0.00	0.001	O	|	|	|	|	0.03
57.083	0.00	0.00	0.001	O	|	|	|	|	0.03
57.167	0.00	0.00	0.001	O	|	|	|	|	0.03
57.250	0.00	0.00	0.001	O	|	|	|	|	0.03
57.333	0.00	0.00	0.001	O	|	|	|	|	0.03
57.417	0.00	0.00	0.001	O	|	|	|	|	0.03
57.500	0.00	0.00	0.001	O	|	|	|	|	0.03
57.583	0.00	0.00	0.001	O	|	|	|	|	0.03
57.667	0.00	0.00	0.001	O	|	|	|	|	0.03
57.750	0.00	0.00	0.001	O	|	|	|	|	0.03
57.833	0.00	0.00	0.001	O	|	|	|	|	0.03
57.917	0.00	0.00	0.001	O	|	|	|	|	0.03
58.000	0.00	0.00	0.001	O	|	|	|	|	0.03
58.083	0.00	0.00	0.001	O	|	|	|	|	0.03
58.167	0.00	0.00	0.001	O	|	|	|	|	0.03
58.250	0.00	0.00	0.001	O	|	|	|	|	0.03
58.333	0.00	0.00	0.001	O	|	|	|	|	0.03
58.417	0.00	0.00	0.001	O	|	|	|	|	0.03
58.500	0.00	0.00	0.001	O	|	|	|	|	0.03
58.583	0.00	0.00	0.001	O	|	|	|	|	0.03
58.667	0.00	0.00	0.001	O	|	|	|	|	0.03
58.750	0.00	0.00	0.001	O	|	|	|	|	0.03
58.833	0.00	0.00	0.001	O	|	|	|	|	0.02
58.917	0.00	0.00	0.001	O	|	|	|	|	0.02
59.000	0.00	0.00	0.001	O	|	|	|	|	0.02
59.083	0.00	0.00	0.001	O	|	|	|	|	0.02
59.167	0.00	0.00	0.001	O	|	|	|	|	0.02
59.250	0.00	0.00	0.001	O	|	|	|	|	0.02
59.333	0.00	0.00	0.001	O	|	|	|	|	0.02
59.417	0.00	0.00	0.001	O	|	|	|	|	0.02
59.500	0.00	0.00	0.001	O	|	|	|	|	0.02
59.583	0.00	0.00	0.001	O	|	|	|	|	0.02

**********HYDROGRAPH DATA**********

Number of intervals = 715
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.045 (CFS)
Total volume = 0.151 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
10 yr
6 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris610.rte
**********HYDROGRAPH DATA**********
Number of intervals = 80
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.431 (CFS)
Total volume = 0.207 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 80
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.4 0.72 1.07 1.43	Depth (Ft.)
0.083	0.03	0.00	0.000	O | | | |	0.00
0.167	0.10	0.00	0.001	O I | | | |	0.02
0.250	0.14	0.00	0.001	O I | | | |	0.06
0.333	0.16	0.00	0.002	O I | | | |	0.10
0.417	0.17	0.01	0.003	O I | | | |	0.14
0.500	0.18	0.01	0.005	O I | | | |	0.19
0.583	0.19	0.01	0.006	O I | | | |	0.24
0.667	0.20	0.01	0.007	O I | | | |	0.29
0.750	0.21	0.02	0.008	O I | | | |	0.35
0.833	0.21	0.02	0.010	O I | | | |	0.40
0.917	0.21	0.02	0.011	O I | | | |	0.46
1.000	0.21	0.02	0.012	O I | | | |	0.51
1.083	0.23	0.03	0.014	O I | | | |	0.57
1.167	0.23	0.03	0.015	O I | | | |	0.63
1.250	0.24	0.03	0.016	O I | | | |	0.68
1.333	0.24	0.03	0.018	O I | | | |	0.74
1.417	0.24	0.04	0.019	O I | | | |	0.80
1.500	0.24	0.04	0.021	O I | | | |	0.86
1.583	0.24	0.04	0.022	O I | | | |	0.91
1.667	0.24	0.04	0.023	O I | | | |	0.97
1.750	0.24	0.04	0.025	|O I | | | |	1.02
1.833	0.24	0.04	0.026	|O I | | | |	1.05
1.917	0.24	0.04	0.027	|O I | | | |	1.08
2.000	0.24	0.04	0.029	|O I | | | |	1.12
2.083	0.25	0.04	0.030	|O I | | | |	1.15
2.167	0.25	0.04	0.031	|O I | | | |	1.19
2.250	0.26	0.04	0.033	|O I | | | |	1.22
2.333	0.26	0.04	0.034	|O I | | | |	1.26

```
2.417    0.27    0.04      0.036  |O   I  |       |       |       |     1.30
2.500    0.27    0.04      0.037  |O   I  |       |       |       |     1.34
2.583    0.27    0.04      0.039  |O   I  |       |       |       |     1.37
2.667    0.27    0.04      0.040  |O   I  |       |       |       |     1.41
2.750    0.27    0.04      0.042  |O    I |       |       |       |     1.45
2.833    0.29    0.04      0.044  |O    I |       |       |       |     1.49
2.917    0.29    0.04      0.045  |O    I |       |       |       |     1.53
3.000    0.29    0.04      0.047  |O    I |       |       |       |     1.58
3.083    0.30    0.04      0.049  |O    I |       |       |       |     1.62
3.167    0.30    0.04      0.051  |O    I |       |       |       |     1.66
3.250    0.32    0.04      0.052  |O     I|       |       |       |     1.71
3.333    0.32    0.04      0.054  |O     I|       |       |       |     1.76
3.417    0.33    0.04      0.056  |O     I|       |       |       |     1.80
3.500    0.35    0.04      0.058  |O     I|       |       |       |     1.86
3.583    0.38    0.04      0.060  |O      I       |       |       |     1.91
3.667    0.40    0.04      0.063  |O      I       |       |       |     1.97
3.750    0.41    0.04      0.065  |O      |I      |       |       |     2.03
3.833    0.43    0.04      0.068  |O      |I      |       |       |     2.10
3.917    0.44    0.04      0.071  |O      |I      |       |       |     2.16
4.000    0.46    0.04      0.073  |O      | I     |       |       |     2.23
4.083    0.47    0.04      0.076  |O      | I     |       |       |     2.31
4.167    0.50    0.04      0.079  |O      |  I    |       |       |     2.38
4.250    0.52    0.04      0.082  |O      |  I    |       |       |     2.46
4.333    0.55    0.04      0.086  |O      |   I   |       |       |     2.55
4.417    0.58    0.04      0.089  |O      |   I   |       |       |     2.64
4.500    0.60    0.04      0.093  |O      |    I  |       |       |     2.73
4.583    0.62    0.04      0.097  |O      |    I  |       |       |     2.83
4.667    0.64    0.04      0.101  |O      |     I |       |       |     2.93
4.750    0.67    0.04      0.105  |O      |     I |       |       |     3.03
4.833    0.69    0.04      0.110  |O      |      I|       |       |     3.14
4.917    0.71    0.04      0.114  |O      |      I|       |       |     3.26
5.000    0.73    0.04      0.119  |O      |       I       |       |     3.37
5.083    0.78    0.04      0.124  |O      |       |I      |       |     3.50
5.167    0.89    0.04      0.129  |O      |       |  I    |       |     3.63
5.250    1.02    0.04      0.136  |O      |       |     I |       |     3.79
5.333    1.13    0.04      0.143  |O      |       |       |I      |     3.96
5.417    1.25    0.04      0.150  |O      |       |       |  I    |     4.16
5.500    1.43    0.04      0.159  |O      |       |       |      I|     4.38
5.583    1.41    0.04      0.169  |O      |       |       |     I|     4.62
5.667    0.84    0.04      0.176  |O      |       | I     |       |     4.80
5.750    0.52    0.04      0.181  |O      |  I    |       |       |     4.91
5.833    0.36    0.04      0.183  |O     I|       |       |       |     4.98
5.917    0.26    0.04      0.185  |O   I  |       |       |       |     5.02
6.000    0.18    0.04      0.186  |O I    |       |       |       |     5.05
6.083    0.11    0.04      0.187  |OI     |       |       |       |     5.07
6.167    0.05    0.04      0.187  |O      |       |       |       |     5.08
6.250    0.02    0.04      0.187  IO      |       |       |       |     5.07
6.333    0.01    0.04      0.187  IO      |       |       |       |     5.07
6.417    0.01    0.04      0.187  IO      |       |       |       |     5.06
6.500    0.00    0.04      0.187  IO      |       |       |       |     5.06
```

6.583	0.00	0.04	0.186	IO				5.05
6.667	0.00	0.04	0.186	IO				5.04
6.750	0.00	0.04	0.186	IO				5.03
6.833	0.00	0.04	0.185	IO				5.03
6.917	0.00	0.04	0.185	IO				5.02
7.000	0.00	0.04	0.185	IO				5.01
7.083	0.00	0.04	0.184	IO				5.00
7.167	0.00	0.04	0.184	IO				5.00
7.250	0.00	0.04	0.184	IO				4.99
7.333	0.00	0.04	0.183	IO				4.98
7.417	0.00	0.04	0.183	IO				4.97
7.500	0.00	0.04	0.183	IO				4.97
7.583	0.00	0.04	0.183	IO				4.96
7.667	0.00	0.04	0.182	IO				4.95
7.750	0.00	0.04	0.182	IO				4.94
7.833	0.00	0.04	0.182	IO				4.94
7.917	0.00	0.04	0.181	IO				4.93
8.000	0.00	0.04	0.181	IO				4.92
8.083	0.00	0.04	0.181	IO				4.91
8.167	0.00	0.04	0.180	IO				4.90
8.250	0.00	0.04	0.180	IO				4.90
8.333	0.00	0.04	0.180	IO				4.89
8.417	0.00	0.04	0.179	IO				4.88
8.500	0.00	0.04	0.179	IO				4.87
8.583	0.00	0.04	0.179	IO				4.87
8.667	0.00	0.04	0.179	IO				4.86
8.750	0.00	0.04	0.178	IO				4.85
8.833	0.00	0.04	0.178	IO				4.84
8.917	0.00	0.04	0.178	IO				4.84
9.000	0.00	0.04	0.177	IO				4.83
9.083	0.00	0.04	0.177	IO				4.82
9.167	0.00	0.04	0.177	IO				4.81
9.250	0.00	0.04	0.176	IO				4.81
9.333	0.00	0.04	0.176	IO				4.80
9.417	0.00	0.04	0.176	IO				4.79
9.500	0.00	0.04	0.175	IO				4.78
9.583	0.00	0.04	0.175	IO				4.77
9.667	0.00	0.04	0.175	IO				4.77
9.750	0.00	0.04	0.174	IO				4.76
9.833	0.00	0.04	0.174	IO				4.75
9.917	0.00	0.04	0.174	IO				4.74
10.000	0.00	0.04	0.174	IO				4.74
10.083	0.00	0.04	0.173	IO				4.73
10.167	0.00	0.04	0.173	IO				4.72
10.250	0.00	0.04	0.173	IO				4.71
10.333	0.00	0.04	0.172	IO				4.71
10.417	0.00	0.04	0.172	IO				4.70
10.500	0.00	0.04	0.172	IO				4.69
10.583	0.00	0.04	0.171	IO				4.68
10.667	0.00	0.04	0.171	IO				4.68

10.750	0.00	0.04	0.171	IO				4.67
10.833	0.00	0.04	0.170	IO				4.66
10.917	0.00	0.04	0.170	IO				4.65
11.000	0.00	0.04	0.170	IO				4.64
11.083	0.00	0.04	0.170	IO				4.64
11.167	0.00	0.04	0.169	IO				4.63
11.250	0.00	0.04	0.169	IO				4.62
11.333	0.00	0.04	0.169	IO				4.61
11.417	0.00	0.04	0.168	IO				4.61
11.500	0.00	0.04	0.168	IO				4.60
11.583	0.00	0.04	0.168	IO				4.59
11.667	0.00	0.04	0.167	IO				4.58
11.750	0.00	0.04	0.167	IO				4.58
11.833	0.00	0.04	0.167	IO				4.57
11.917	0.00	0.04	0.166	IO				4.56
12.000	0.00	0.04	0.166	IO				4.55
12.083	0.00	0.04	0.166	IO				4.54
12.167	0.00	0.04	0.166	IO				4.54
12.250	0.00	0.04	0.165	IO				4.53
12.333	0.00	0.04	0.165	IO				4.52
12.417	0.00	0.04	0.165	IO				4.51
12.500	0.00	0.04	0.164	IO				4.51
12.583	0.00	0.04	0.164	IO				4.50
12.667	0.00	0.04	0.164	IO				4.49
12.750	0.00	0.04	0.163	IO				4.48
12.833	0.00	0.04	0.163	IO				4.48
12.917	0.00	0.04	0.163	IO				4.47
13.000	0.00	0.04	0.162	IO				4.46
13.083	0.00	0.04	0.162	IO				4.45
13.167	0.00	0.04	0.162	IO				4.44
13.250	0.00	0.04	0.161	IO				4.44
13.333	0.00	0.04	0.161	IO				4.43
13.417	0.00	0.04	0.161	IO				4.42
13.500	0.00	0.04	0.161	IO				4.41
13.583	0.00	0.04	0.160	IO				4.41
13.667	0.00	0.04	0.160	IO				4.40
13.750	0.00	0.04	0.160	IO				4.39
13.833	0.00	0.04	0.159	IO				4.38
13.917	0.00	0.04	0.159	IO				4.38
14.000	0.00	0.04	0.159	IO				4.37
14.083	0.00	0.04	0.158	IO				4.36
14.167	0.00	0.04	0.158	IO				4.35
14.250	0.00	0.04	0.158	IO				4.34
14.333	0.00	0.04	0.157	IO				4.34
14.417	0.00	0.04	0.157	IO				4.33
14.500	0.00	0.04	0.157	IO				4.32
14.583	0.00	0.04	0.157	IO				4.31
14.667	0.00	0.04	0.156	IO				4.31
14.750	0.00	0.04	0.156	IO				4.30
14.833	0.00	0.04	0.156	IO				4.29

14.917	0.00	0.04	0.155	IO				4.28
15.000	0.00	0.04	0.155	IO				4.27
15.083	0.00	0.04	0.155	IO				4.27
15.167	0.00	0.04	0.154	IO				4.26
15.250	0.00	0.04	0.154	IO				4.25
15.333	0.00	0.04	0.154	IO				4.24
15.417	0.00	0.04	0.153	IO				4.24
15.500	0.00	0.04	0.153	IO				4.23
15.583	0.00	0.04	0.153	IO				4.22
15.667	0.00	0.04	0.152	IO				4.21
15.750	0.00	0.04	0.152	IO				4.20
15.833	0.00	0.04	0.152	IO				4.20
15.917	0.00	0.04	0.152	IO				4.19
16.000	0.00	0.04	0.151	IO				4.18
16.083	0.00	0.04	0.151	IO				4.17
16.167	0.00	0.04	0.151	IO				4.17
16.250	0.00	0.04	0.150	IO				4.16
16.333	0.00	0.04	0.150	IO				4.15
16.417	0.00	0.04	0.150	IO				4.14
16.500	0.00	0.04	0.149	IO				4.13
16.583	0.00	0.04	0.149	IO				4.13
16.667	0.00	0.04	0.149	IO				4.12
16.750	0.00	0.04	0.148	IO				4.11
16.833	0.00	0.04	0.148	IO				4.10
16.917	0.00	0.04	0.148	IO				4.10
17.000	0.00	0.04	0.148	IO				4.09
17.083	0.00	0.04	0.147	IO				4.08
17.167	0.00	0.04	0.147	IO				4.07
17.250	0.00	0.04	0.147	IO				4.07
17.333	0.00	0.04	0.146	IO				4.06
17.417	0.00	0.04	0.146	IO				4.05
17.500	0.00	0.04	0.146	IO				4.04
17.583	0.00	0.04	0.145	IO				4.03
17.667	0.00	0.04	0.145	IO				4.03
17.750	0.00	0.04	0.145	IO				4.02
17.833	0.00	0.04	0.144	IO				4.01
17.917	0.00	0.04	0.144	IO				4.00
18.000	0.00	0.04	0.144	IO				4.00
18.083	0.00	0.04	0.144	IO				3.99
18.167	0.00	0.04	0.143	IO				3.98
18.250	0.00	0.04	0.143	IO				3.97
18.333	0.00	0.04	0.143	IO				3.96
18.417	0.00	0.04	0.142	IO				3.96
18.500	0.00	0.04	0.142	IO				3.95
18.583	0.00	0.04	0.142	IO				3.94
18.667	0.00	0.04	0.141	IO				3.93
18.750	0.00	0.04	0.141	IO				3.93
18.833	0.00	0.04	0.141	IO				3.92
18.917	0.00	0.04	0.140	IO				3.91
19.000	0.00	0.04	0.140	IO				3.90

19.083	0.00	0.04	0.140	IO				3.89
19.167	0.00	0.04	0.139	IO				3.89
19.250	0.00	0.04	0.139	IO				3.88
19.333	0.00	0.04	0.139	IO				3.87
19.417	0.00	0.04	0.139	IO				3.86
19.500	0.00	0.04	0.138	IO				3.86
19.583	0.00	0.04	0.138	IO				3.85
19.667	0.00	0.04	0.138	IO				3.84
19.750	0.00	0.04	0.137	IO				3.83
19.833	0.00	0.04	0.137	IO				3.82
19.917	0.00	0.04	0.137	IO				3.82
20.000	0.00	0.04	0.136	IO				3.81
20.083	0.00	0.04	0.136	IO				3.80
20.167	0.00	0.04	0.136	IO				3.79
20.250	0.00	0.04	0.135	IO				3.79
20.333	0.00	0.04	0.135	IO				3.78
20.417	0.00	0.04	0.135	IO				3.77
20.500	0.00	0.04	0.135	IO				3.76
20.583	0.00	0.04	0.134	IO				3.76
20.667	0.00	0.04	0.134	IO				3.75
20.750	0.00	0.04	0.134	IO				3.74
20.833	0.00	0.04	0.133	IO				3.73
20.917	0.00	0.04	0.133	IO				3.72
21.000	0.00	0.04	0.133	IO				3.72
21.083	0.00	0.04	0.132	IO				3.71
21.167	0.00	0.04	0.132	IO				3.70
21.250	0.00	0.04	0.132	IO				3.69
21.333	0.00	0.04	0.131	IO				3.69
21.417	0.00	0.04	0.131	IO				3.68
21.500	0.00	0.04	0.131	IO				3.67
21.583	0.00	0.04	0.130	IO				3.66
21.667	0.00	0.04	0.130	IO				3.65
21.750	0.00	0.04	0.130	IO				3.65
21.833	0.00	0.04	0.130	IO				3.64
21.917	0.00	0.04	0.129	IO				3.63
22.000	0.00	0.04	0.129	IO				3.62
22.083	0.00	0.04	0.129	IO				3.62
22.167	0.00	0.04	0.128	IO				3.61
22.250	0.00	0.04	0.128	IO				3.60
22.333	0.00	0.04	0.128	IO				3.59
22.417	0.00	0.04	0.127	IO				3.58
22.500	0.00	0.04	0.127	IO				3.58
22.583	0.00	0.04	0.127	IO				3.57
22.667	0.00	0.04	0.126	IO				3.56
22.750	0.00	0.04	0.126	IO				3.55
22.833	0.00	0.04	0.126	IO				3.55
22.917	0.00	0.04	0.126	IO				3.54
23.000	0.00	0.04	0.125	IO				3.53
23.083	0.00	0.04	0.125	IO				3.52
23.167	0.00	0.04	0.125	IO				3.52

23.250	0.00	0.04	0.124	IO				3.51
23.333	0.00	0.04	0.124	IO				3.50
23.417	0.00	0.04	0.124	IO				3.49
23.500	0.00	0.04	0.123	IO				3.48
23.583	0.00	0.04	0.123	IO				3.48
23.667	0.00	0.04	0.123	IO				3.47
23.750	0.00	0.04	0.122	IO				3.46
23.833	0.00	0.04	0.122	IO				3.45
23.917	0.00	0.04	0.122	IO				3.45
24.000	0.00	0.04	0.122	IO				3.44
24.083	0.00	0.04	0.121	IO				3.43
24.167	0.00	0.04	0.121	IO				3.42
24.250	0.00	0.04	0.121	IO				3.41
24.333	0.00	0.04	0.120	IO				3.41
24.417	0.00	0.04	0.120	IO				3.40
24.500	0.00	0.04	0.120	IO				3.39
24.583	0.00	0.04	0.119	IO				3.38
24.667	0.00	0.04	0.119	IO				3.38
24.750	0.00	0.04	0.119	IO				3.37
24.833	0.00	0.04	0.118	IO				3.36
24.917	0.00	0.04	0.118	IO				3.35
25.000	0.00	0.04	0.118	IO				3.34
25.083	0.00	0.04	0.117	IO				3.34
25.167	0.00	0.04	0.117	IO				3.33
25.250	0.00	0.04	0.117	IO				3.32
25.333	0.00	0.04	0.117	IO				3.31
25.417	0.00	0.04	0.116	IO				3.31
25.500	0.00	0.04	0.116	IO				3.30
25.583	0.00	0.04	0.116	IO				3.29
25.667	0.00	0.04	0.115	IO				3.28
25.750	0.00	0.04	0.115	IO				3.27
25.833	0.00	0.04	0.115	IO				3.27
25.917	0.00	0.04	0.114	IO				3.26
26.000	0.00	0.04	0.114	IO				3.25
26.083	0.00	0.04	0.114	IO				3.24
26.167	0.00	0.04	0.113	IO				3.24
26.250	0.00	0.04	0.113	IO				3.23
26.333	0.00	0.04	0.113	IO				3.22
26.417	0.00	0.04	0.113	IO				3.21
26.500	0.00	0.04	0.112	IO				3.21
26.583	0.00	0.04	0.112	IO				3.20
26.667	0.00	0.04	0.112	IO				3.19
26.750	0.00	0.04	0.111	IO				3.18
26.833	0.00	0.04	0.111	IO				3.17
26.917	0.00	0.04	0.111	IO				3.17
27.000	0.00	0.04	0.110	IO				3.16
27.083	0.00	0.04	0.110	IO				3.15
27.167	0.00	0.04	0.110	IO				3.14
27.250	0.00	0.04	0.109	IO				3.14
27.333	0.00	0.04	0.109	IO				3.13

27.417	0.00	0.04	0.109	IO				3.12
27.500	0.00	0.04	0.108	IO				3.11
27.583	0.00	0.04	0.108	IO				3.10
27.667	0.00	0.04	0.108	IO				3.10
27.750	0.00	0.04	0.108	IO				3.09
27.833	0.00	0.04	0.107	IO				3.08
27.917	0.00	0.04	0.107	IO				3.07
28.000	0.00	0.04	0.107	IO				3.07
28.083	0.00	0.04	0.106	IO				3.06
28.167	0.00	0.04	0.106	IO				3.05
28.250	0.00	0.04	0.106	IO				3.04
28.333	0.00	0.04	0.105	IO				3.03
28.417	0.00	0.04	0.105	IO				3.03
28.500	0.00	0.04	0.105	IO				3.02
28.583	0.00	0.04	0.104	IO				3.01
28.667	0.00	0.04	0.104	IO				3.00
28.750	0.00	0.04	0.104	IO				3.00
28.833	0.00	0.04	0.104	IO				2.99
28.917	0.00	0.04	0.103	IO				2.98
29.000	0.00	0.04	0.103	IO				2.97
29.083	0.00	0.04	0.103	IO				2.96
29.167	0.00	0.04	0.102	IO				2.96
29.250	0.00	0.04	0.102	IO				2.95
29.333	0.00	0.04	0.102	IO				2.94
29.417	0.00	0.04	0.101	IO				2.93
29.500	0.00	0.04	0.101	IO				2.93
29.583	0.00	0.04	0.101	IO				2.92
29.667	0.00	0.04	0.100	IO				2.91
29.750	0.00	0.04	0.100	IO				2.90
29.833	0.00	0.04	0.100	IO				2.90
29.917	0.00	0.04	0.099	IO				2.89
30.000	0.00	0.04	0.099	IO				2.88
30.083	0.00	0.04	0.099	IO				2.87
30.167	0.00	0.04	0.099	IO				2.86
30.250	0.00	0.04	0.098	IO				2.86
30.333	0.00	0.04	0.098	IO				2.85
30.417	0.00	0.04	0.098	IO				2.84
30.500	0.00	0.04	0.097	IO				2.83
30.583	0.00	0.04	0.097	IO				2.83
30.667	0.00	0.04	0.097	IO				2.82
30.750	0.00	0.04	0.096	IO				2.81
30.833	0.00	0.04	0.096	IO				2.80
30.917	0.00	0.04	0.096	IO				2.79
31.000	0.00	0.04	0.095	IO				2.79
31.083	0.00	0.04	0.095	IO				2.78
31.167	0.00	0.04	0.095	IO				2.77
31.250	0.00	0.04	0.095	IO				2.76
31.333	0.00	0.04	0.094	IO				2.76
31.417	0.00	0.04	0.094	IO				2.75
31.500	0.00	0.04	0.094	IO				2.74

31.583	0.00	0.04	0.093	IO				2.73
31.667	0.00	0.04	0.093	IO				2.72
31.750	0.00	0.04	0.093	IO				2.72
31.833	0.00	0.04	0.092	IO				2.71
31.917	0.00	0.04	0.092	IO				2.70
32.000	0.00	0.04	0.092	IO				2.69
32.083	0.00	0.04	0.091	IO				2.69
32.167	0.00	0.04	0.091	IO				2.68
32.250	0.00	0.04	0.091	IO				2.67
32.333	0.00	0.04	0.091	IO				2.66
32.417	0.00	0.04	0.090	IO				2.66
32.500	0.00	0.04	0.090	IO				2.65
32.583	0.00	0.04	0.090	IO				2.64
32.667	0.00	0.04	0.089	IO				2.63
32.750	0.00	0.04	0.089	IO				2.62
32.833	0.00	0.04	0.089	IO				2.62
32.917	0.00	0.04	0.088	IO				2.61
33.000	0.00	0.04	0.088	IO				2.60
33.083	0.00	0.04	0.088	IO				2.59
33.167	0.00	0.04	0.087	IO				2.59
33.250	0.00	0.04	0.087	IO				2.58
33.333	0.00	0.04	0.087	IO				2.57
33.417	0.00	0.04	0.086	IO				2.56
33.500	0.00	0.04	0.086	IO				2.55
33.583	0.00	0.04	0.086	IO				2.55
33.667	0.00	0.04	0.086	IO				2.54
33.750	0.00	0.04	0.085	IO				2.53
33.833	0.00	0.04	0.085	IO				2.52
33.917	0.00	0.04	0.085	IO				2.52
34.000	0.00	0.04	0.084	IO				2.51
34.083	0.00	0.04	0.084	IO				2.50
34.167	0.00	0.04	0.084	IO				2.49
34.250	0.00	0.04	0.083	IO				2.48
34.333	0.00	0.04	0.083	IO				2.48
34.417	0.00	0.04	0.083	IO				2.47
34.500	0.00	0.04	0.082	IO				2.46
34.583	0.00	0.04	0.082	IO				2.45
34.667	0.00	0.04	0.082	IO				2.45
34.750	0.00	0.04	0.082	IO				2.44
34.833	0.00	0.04	0.081	IO				2.43
34.917	0.00	0.04	0.081	IO				2.42
35.000	0.00	0.04	0.081	IO				2.41
35.083	0.00	0.04	0.080	IO				2.41
35.167	0.00	0.04	0.080	IO				2.40
35.250	0.00	0.04	0.080	IO				2.39
35.333	0.00	0.04	0.079	IO				2.38
35.417	0.00	0.04	0.079	IO				2.38
35.500	0.00	0.04	0.079	IO				2.37
35.583	0.00	0.04	0.078	IO				2.36
35.667	0.00	0.04	0.078	IO				2.35

35.750	0.00	0.04	0.078	IO				2.35
35.833	0.00	0.04	0.077	IO				2.34
35.917	0.00	0.04	0.077	IO				2.33
36.000	0.00	0.04	0.077	IO				2.32
36.083	0.00	0.04	0.077	IO				2.31
36.167	0.00	0.04	0.076	IO				2.31
36.250	0.00	0.04	0.076	IO				2.30
36.333	0.00	0.04	0.076	IO				2.29
36.417	0.00	0.04	0.075	IO				2.28
36.500	0.00	0.04	0.075	IO				2.28
36.583	0.00	0.04	0.075	IO				2.27
36.667	0.00	0.04	0.074	IO				2.26
36.750	0.00	0.04	0.074	IO				2.25
36.833	0.00	0.04	0.074	IO				2.24
36.917	0.00	0.04	0.073	IO				2.24
37.000	0.00	0.04	0.073	IO				2.23
37.083	0.00	0.04	0.073	IO				2.22
37.167	0.00	0.04	0.073	IO				2.21
37.250	0.00	0.04	0.072	IO				2.21
37.333	0.00	0.04	0.072	IO				2.20
37.417	0.00	0.04	0.072	IO				2.19
37.500	0.00	0.04	0.071	IO				2.18
37.583	0.00	0.04	0.071	IO				2.17
37.667	0.00	0.04	0.071	IO				2.17
37.750	0.00	0.04	0.070	IO				2.16
37.833	0.00	0.04	0.070	IO				2.15
37.917	0.00	0.04	0.070	IO				2.14
38.000	0.00	0.04	0.069	IO				2.14
38.083	0.00	0.04	0.069	IO				2.13
38.167	0.00	0.04	0.069	IO				2.12
38.250	0.00	0.04	0.069	IO				2.11
38.333	0.00	0.04	0.068	IO				2.10
38.417	0.00	0.04	0.068	IO				2.10
38.500	0.00	0.04	0.068	IO				2.09
38.583	0.00	0.04	0.067	IO				2.08
38.667	0.00	0.04	0.067	IO				2.07
38.750	0.00	0.04	0.067	IO				2.07
38.833	0.00	0.04	0.066	IO				2.06
38.917	0.00	0.04	0.066	IO				2.05
39.000	0.00	0.04	0.066	IO				2.04
39.083	0.00	0.04	0.065	IO				2.04
39.167	0.00	0.04	0.065	IO				2.03
39.250	0.00	0.04	0.065	IO				2.02
39.333	0.00	0.04	0.064	IO				2.01
39.417	0.00	0.04	0.064	IO				2.00
39.500	0.00	0.04	0.064	IO				2.00
39.583	0.00	0.04	0.064	IO				1.99
39.667	0.00	0.04	0.063	IO				1.98
39.750	0.00	0.04	0.063	IO				1.97
39.833	0.00	0.04	0.063	IO				1.97

39.917	0.00	0.04	0.062	IO				1.96
40.000	0.00	0.04	0.062	IO				1.95
40.083	0.00	0.04	0.062	IO				1.94
40.167	0.00	0.04	0.061	IO				1.93
40.250	0.00	0.04	0.061	IO				1.93
40.333	0.00	0.04	0.061	IO				1.92
40.417	0.00	0.04	0.060	IO				1.91
40.500	0.00	0.04	0.060	IO				1.90
40.583	0.00	0.04	0.060	IO				1.90
40.667	0.00	0.04	0.060	IO				1.89
40.750	0.00	0.04	0.059	IO				1.88
40.833	0.00	0.04	0.059	IO				1.87
40.917	0.00	0.04	0.059	IO				1.86
41.000	0.00	0.04	0.058	IO				1.86
41.083	0.00	0.04	0.058	IO				1.85
41.167	0.00	0.04	0.058	IO				1.84
41.250	0.00	0.04	0.057	IO				1.83
41.333	0.00	0.04	0.057	IO				1.83
41.417	0.00	0.04	0.057	IO				1.82
41.500	0.00	0.04	0.056	IO				1.81
41.583	0.00	0.04	0.056	IO				1.80
41.667	0.00	0.04	0.056	IO				1.79
41.750	0.00	0.04	0.055	IO				1.79
41.833	0.00	0.04	0.055	IO				1.78
41.917	0.00	0.04	0.055	IO				1.77
42.000	0.00	0.04	0.055	IO				1.76
42.083	0.00	0.04	0.054	IO				1.76
42.167	0.00	0.04	0.054	IO				1.75
42.250	0.00	0.04	0.054	IO				1.74
42.333	0.00	0.04	0.053	IO				1.73
42.417	0.00	0.04	0.053	IO				1.73
42.500	0.00	0.04	0.053	IO				1.72
42.583	0.00	0.04	0.052	IO				1.71
42.667	0.00	0.04	0.052	IO				1.70
42.750	0.00	0.04	0.052	IO				1.69
42.833	0.00	0.04	0.051	IO				1.69
42.917	0.00	0.04	0.051	IO				1.68
43.000	0.00	0.04	0.051	IO				1.67
43.083	0.00	0.04	0.051	IO				1.66
43.167	0.00	0.04	0.050	IO				1.66
43.250	0.00	0.04	0.050	IO				1.65
43.333	0.00	0.04	0.050	IO				1.64
43.417	0.00	0.04	0.049	IO				1.63
43.500	0.00	0.04	0.049	IO				1.62
43.583	0.00	0.04	0.049	IO				1.62
43.667	0.00	0.04	0.048	IO				1.61
43.750	0.00	0.04	0.048	IO				1.60
43.833	0.00	0.04	0.048	IO				1.59
43.917	0.00	0.04	0.047	IO				1.59
44.000	0.00	0.04	0.047	IO				1.58

44.083	0.00	0.04	0.047	IO				1.57
44.167	0.00	0.04	0.047	IO				1.56
44.250	0.00	0.04	0.046	IO				1.55
44.333	0.00	0.04	0.046	IO				1.55
44.417	0.00	0.04	0.046	IO				1.54
44.500	0.00	0.04	0.045	IO				1.53
44.583	0.00	0.04	0.045	IO				1.52
44.667	0.00	0.04	0.045	IO				1.52
44.750	0.00	0.04	0.044	IO				1.51
44.833	0.00	0.04	0.044	IO				1.50
44.917	0.00	0.04	0.044	IO				1.49
45.000	0.00	0.04	0.043	IO				1.49
45.083	0.00	0.04	0.043	IO				1.48
45.167	0.00	0.04	0.043	IO				1.47
45.250	0.00	0.04	0.042	IO				1.46
45.333	0.00	0.04	0.042	IO				1.45
45.417	0.00	0.04	0.042	IO				1.45
45.500	0.00	0.04	0.042	IO				1.44
45.583	0.00	0.04	0.041	IO				1.43
45.667	0.00	0.04	0.041	IO				1.42
45.750	0.00	0.04	0.041	IO				1.42
45.833	0.00	0.04	0.040	IO				1.41
45.917	0.00	0.04	0.040	IO				1.40
46.000	0.00	0.04	0.040	IO				1.39
46.083	0.00	0.04	0.039	IO				1.38
46.167	0.00	0.04	0.039	IO				1.38
46.250	0.00	0.04	0.039	IO				1.37
46.333	0.00	0.04	0.038	IO				1.36
46.417	0.00	0.04	0.038	IO				1.35
46.500	0.00	0.04	0.038	IO				1.35
46.583	0.00	0.04	0.038	IO				1.34
46.667	0.00	0.04	0.037	IO				1.33
46.750	0.00	0.04	0.037	IO				1.32
46.833	0.00	0.04	0.037	IO				1.31
46.917	0.00	0.04	0.036	IO				1.31
47.000	0.00	0.04	0.036	IO				1.30
47.083	0.00	0.04	0.036	IO				1.29
47.167	0.00	0.04	0.035	IO				1.28
47.250	0.00	0.04	0.035	IO				1.28
47.333	0.00	0.04	0.035	IO				1.27
47.417	0.00	0.04	0.034	IO				1.26
47.500	0.00	0.04	0.034	IO				1.25
47.583	0.00	0.04	0.034	IO				1.24
47.667	0.00	0.04	0.033	IO				1.24
47.750	0.00	0.04	0.033	IO				1.23
47.833	0.00	0.04	0.033	IO				1.22
47.917	0.00	0.04	0.033	IO				1.21
48.000	0.00	0.04	0.032	IO				1.21
48.083	0.00	0.04	0.032	IO				1.20
48.167	0.00	0.04	0.032	IO				1.19

48.250	0.00	0.04	0.031	IO				1.18
48.333	0.00	0.04	0.031	IO				1.18
48.417	0.00	0.04	0.031	IO				1.17
48.500	0.00	0.04	0.030	IO				1.16
48.583	0.00	0.04	0.030	IO				1.15
48.667	0.00	0.04	0.030	IO				1.14
48.750	0.00	0.04	0.029	IO				1.14
48.833	0.00	0.04	0.029	IO				1.13
48.917	0.00	0.04	0.029	IO				1.12
49.000	0.00	0.04	0.029	IO				1.11
49.083	0.00	0.04	0.028	IO				1.11
49.167	0.00	0.04	0.028	IO				1.10
49.250	0.00	0.04	0.028	IO				1.09
49.333	0.00	0.04	0.027	IO				1.08
49.417	0.00	0.04	0.027	IO				1.07
49.500	0.00	0.04	0.027	IO				1.07
49.583	0.00	0.04	0.026	IO				1.06
49.667	0.00	0.04	0.026	IO				1.05
49.750	0.00	0.04	0.026	IO				1.04
49.833	0.00	0.04	0.025	IO				1.04
49.917	0.00	0.04	0.025	IO				1.03
50.000	0.00	0.04	0.025	IO				1.02
50.083	0.00	0.04	0.024	IO				1.01
50.167	0.00	0.04	0.024	IO				1.00
50.250	0.00	0.04	0.024	IO				0.99
50.333	0.00	0.04	0.024	O				0.98
50.417	0.00	0.04	0.023	O				0.97
50.500	0.00	0.04	0.023	O				0.96
50.583	0.00	0.04	0.023	O				0.94
50.667	0.00	0.04	0.022	O				0.93
50.750	0.00	0.04	0.022	O				0.92
50.833	0.00	0.04	0.022	O				0.91
50.917	0.00	0.04	0.022	O				0.90
51.000	0.00	0.04	0.021	O				0.89
51.083	0.00	0.04	0.021	O				0.87
51.167	0.00	0.04	0.021	O				0.86
51.250	0.00	0.04	0.020	O				0.85
51.333	0.00	0.04	0.020	O				0.84
51.417	0.00	0.04	0.020	O				0.83
51.500	0.00	0.04	0.020	O				0.82
51.583	0.00	0.04	0.019	O				0.81
51.667	0.00	0.04	0.019	O				0.80
51.750	0.00	0.04	0.019	O				0.79
51.833	0.00	0.04	0.019	O				0.78
51.917	0.00	0.03	0.018	O				0.77
52.000	0.00	0.03	0.018	O				0.76
52.083	0.00	0.03	0.018	O				0.75
52.167	0.00	0.03	0.018	O				0.74
52.250	0.00	0.03	0.018	O				0.73
52.333	0.00	0.03	0.017	O				0.72

52.417	0.00	0.03	0.017	O				0.71
52.500	0.00	0.03	0.017	O				0.70
52.583	0.00	0.03	0.017	O				0.69
52.667	0.00	0.03	0.016	O				0.68
52.750	0.00	0.03	0.016	O				0.68
52.833	0.00	0.03	0.016	O				0.67
52.917	0.00	0.03	0.016	O				0.66
53.000	0.00	0.03	0.016	O				0.65
53.083	0.00	0.03	0.015	O				0.64
53.167	0.00	0.03	0.015	O				0.63
53.250	0.00	0.03	0.015	O				0.63
53.333	0.00	0.03	0.015	O				0.62
53.417	0.00	0.03	0.015	O				0.61
53.500	0.00	0.03	0.014	O				0.60
53.583	0.00	0.03	0.014	O				0.59
53.667	0.00	0.03	0.014	O				0.59
53.750	0.00	0.03	0.014	O				0.58
53.833	0.00	0.03	0.014	O				0.57
53.917	0.00	0.03	0.014	O				0.56
54.000	0.00	0.03	0.013	O				0.56
54.083	0.00	0.02	0.013	O				0.55
54.167	0.00	0.02	0.013	O				0.54
54.250	0.00	0.02	0.013	O				0.54
54.333	0.00	0.02	0.013	O				0.53
54.417	0.00	0.02	0.013	O				0.52
54.500	0.00	0.02	0.012	O				0.51
54.583	0.00	0.02	0.012	O				0.51
54.667	0.00	0.02	0.012	O				0.50
54.750	0.00	0.02	0.012	O				0.50
54.833	0.00	0.02	0.012	O				0.49
54.917	0.00	0.02	0.012	O				0.48
55.000	0.00	0.02	0.011	O				0.48
55.083	0.00	0.02	0.011	O				0.47
55.167	0.00	0.02	0.011	O				0.46
55.250	0.00	0.02	0.011	O				0.46
55.333	0.00	0.02	0.011	O				0.45
55.417	0.00	0.02	0.011	O				0.45
55.500	0.00	0.02	0.011	O				0.44
55.583	0.00	0.02	0.010	O				0.44
55.667	0.00	0.02	0.010	O				0.43
55.750	0.00	0.02	0.010	O				0.42
55.833	0.00	0.02	0.010	O				0.42
55.917	0.00	0.02	0.010	O				0.41
56.000	0.00	0.02	0.010	O				0.41
56.083	0.00	0.02	0.010	O				0.40
56.167	0.00	0.02	0.010	O				0.40
56.250	0.00	0.02	0.009	O				0.39
56.333	0.00	0.02	0.009	O				0.39
56.417	0.00	0.02	0.009	O				0.38
56.500	0.00	0.02	0.009	O				0.38

56.583	0.00	0.02	0.009	O				0.37
56.667	0.00	0.02	0.009	O				0.37
56.750	0.00	0.02	0.009	O				0.36
56.833	0.00	0.02	0.009	O				0.36
56.917	0.00	0.02	0.008	O				0.35
57.000	0.00	0.02	0.008	O				0.35
57.083	0.00	0.02	0.008	O				0.35
57.167	0.00	0.02	0.008	O				0.34
57.250	0.00	0.02	0.008	O				0.34
57.333	0.00	0.01	0.008	O				0.33
57.417	0.00	0.01	0.008	O				0.33
57.500	0.00	0.01	0.008	O				0.32
57.583	0.00	0.01	0.008	O				0.32
57.667	0.00	0.01	0.008	O				0.32
57.750	0.00	0.01	0.007	O				0.31
57.833	0.00	0.01	0.007	O				0.31
57.917	0.00	0.01	0.007	O				0.30
58.000	0.00	0.01	0.007	O				0.30
58.083	0.00	0.01	0.007	O				0.30
58.167	0.00	0.01	0.007	O				0.29
58.250	0.00	0.01	0.007	O				0.29
58.333	0.00	0.01	0.007	O				0.28
58.417	0.00	0.01	0.007	O				0.28
58.500	0.00	0.01	0.007	O				0.28
58.583	0.00	0.01	0.007	O				0.27
58.667	0.00	0.01	0.006	O				0.27
58.750	0.00	0.01	0.006	O				0.27
58.833	0.00	0.01	0.006	O				0.26
58.917	0.00	0.01	0.006	O				0.26
59.000	0.00	0.01	0.006	O				0.26
59.083	0.00	0.01	0.006	O				0.25
59.167	0.00	0.01	0.006	O				0.25
59.250	0.00	0.01	0.006	O				0.25
59.333	0.00	0.01	0.006	O				0.24
59.417	0.00	0.01	0.006	O				0.24
59.500	0.00	0.01	0.006	O				0.24
59.583	0.00	0.01	0.006	O				0.23
59.667	0.00	0.01	0.006	O				0.23
59.750	0.00	0.01	0.005	O				0.23
59.833	0.00	0.01	0.005	O				0.23
59.917	0.00	0.01	0.005	O				0.22
60.000	0.00	0.01	0.005	O				0.22
60.083	0.00	0.01	0.005	O				0.22
60.167	0.00	0.01	0.005	O				0.21
60.250	0.00	0.01	0.005	O				0.21
60.333	0.00	0.01	0.005	O				0.21
60.417	0.00	0.01	0.005	O				0.21
60.500	0.00	0.01	0.005	O				0.20
60.583	0.00	0.01	0.005	O				0.20
60.667	0.00	0.01	0.005	O				0.20

60.750	0.00	0.01	0.005	O	|	|	|	0.20
60.833	0.00	0.01	0.005	O	|	|	|	0.19
60.917	0.00	0.01	0.005	O	|	|	|	0.19
61.000	0.00	0.01	0.005	O	|	|	|	0.19
61.083	0.00	0.01	0.004	O	|	|	|	0.19
61.167	0.00	0.01	0.004	O	|	|	|	0.18
61.250	0.00	0.01	0.004	O	|	|	|	0.18
61.333	0.00	0.01	0.004	O	|	|	|	0.18
61.417	0.00	0.01	0.004	O	|	|	|	0.18
61.500	0.00	0.01	0.004	O	|	|	|	0.17
61.583	0.00	0.01	0.004	O	|	|	|	0.17
61.667	0.00	0.01	0.004	O	|	|	|	0.17
61.750	0.00	0.01	0.004	O	|	|	|	0.17
61.833	0.00	0.01	0.004	O	|	|	|	0.17
61.917	0.00	0.01	0.004	O	|	|	|	0.16
62.000	0.00	0.01	0.004	O	|	|	|	0.16
62.083	0.00	0.01	0.004	O	|	|	|	0.16
62.167	0.00	0.01	0.004	O	|	|	|	0.16
62.250	0.00	0.01	0.004	O	|	|	|	0.15
62.333	0.00	0.01	0.004	O	|	|	|	0.15
62.417	0.00	0.01	0.004	O	|	|	|	0.15
62.500	0.00	0.01	0.004	O	|	|	|	0.15
62.583	0.00	0.01	0.004	O	|	|	|	0.15
62.667	0.00	0.01	0.003	O	|	|	|	0.15
62.750	0.00	0.01	0.003	O	|	|	|	0.14
62.833	0.00	0.01	0.003	O	|	|	|	0.14
62.917	0.00	0.01	0.003	O	|	|	|	0.14
63.000	0.00	0.01	0.003	O	|	|	|	0.14
63.083	0.00	0.01	0.003	O	|	|	|	0.14
63.167	0.00	0.01	0.003	O	|	|	|	0.13
63.250	0.00	0.01	0.003	O	|	|	|	0.13
63.333	0.00	0.01	0.003	O	|	|	|	0.13
63.417	0.00	0.01	0.003	O	|	|	|	0.13
63.500	0.00	0.01	0.003	O	|	|	|	0.13
63.583	0.00	0.01	0.003	O	|	|	|	0.13
63.667	0.00	0.01	0.003	O	|	|	|	0.12
63.750	0.00	0.01	0.003	O	|	|	|	0.12
63.833	0.00	0.01	0.003	O	|	|	|	0.12
63.917	0.00	0.01	0.003	O	|	|	|	0.12
64.000	0.00	0.01	0.003	O	|	|	|	0.12
64.083	0.00	0.01	0.003	O	|	|	|	0.12
64.167	0.00	0.01	0.003	O	|	|	|	0.12
64.250	0.00	0.01	0.003	O	|	|	|	0.11
64.333	0.00	0.01	0.003	O	|	|	|	0.11
64.417	0.00	0.00	0.003	O	|	|	|	0.11
64.500	0.00	0.00	0.003	O	|	|	|	0.11
64.583	0.00	0.00	0.003	O	|	|	|	0.11
64.667	0.00	0.00	0.003	O	|	|	|	0.11
64.750	0.00	0.00	0.003	O	|	|	|	0.11
64.833	0.00	0.00	0.002	O	|	|	|	0.10

64.917	0.00	0.00	0.002	O	|	|	|	0.10
65.000	0.00	0.00	0.002	O	|	|	|	0.10
65.083	0.00	0.00	0.002	O	|	|	|	0.10
65.167	0.00	0.00	0.002	O	|	|	|	0.10
65.250	0.00	0.00	0.002	O	|	|	|	0.10
65.333	0.00	0.00	0.002	O	|	|	|	0.10
65.417	0.00	0.00	0.002	O	|	|	|	0.09
65.500	0.00	0.00	0.002	O	|	|	|	0.09
65.583	0.00	0.00	0.002	O	|	|	|	0.09
65.667	0.00	0.00	0.002	O	|	|	|	0.09
65.750	0.00	0.00	0.002	O	|	|	|	0.09
65.833	0.00	0.00	0.002	O	|	|	|	0.09
65.917	0.00	0.00	0.002	O	|	|	|	0.09
66.000	0.00	0.00	0.002	O	|	|	|	0.09
66.083	0.00	0.00	0.002	O	|	|	|	0.09
66.167	0.00	0.00	0.002	O	|	|	|	0.08
66.250	0.00	0.00	0.002	O	|	|	|	0.08
66.333	0.00	0.00	0.002	O	|	|	|	0.08
66.417	0.00	0.00	0.002	O	|	|	|	0.08
66.500	0.00	0.00	0.002	O	|	|	|	0.08
66.583	0.00	0.00	0.002	O	|	|	|	0.08
66.667	0.00	0.00	0.002	O	|	|	|	0.08
66.750	0.00	0.00	0.002	O	|	|	|	0.08
66.833	0.00	0.00	0.002	O	|	|	|	0.08
66.917	0.00	0.00	0.002	O	|	|	|	0.08
67.000	0.00	0.00	0.002	O	|	|	|	0.07
67.083	0.00	0.00	0.002	O	|	|	|	0.07
67.167	0.00	0.00	0.002	O	|	|	|	0.07
67.250	0.00	0.00	0.002	O	|	|	|	0.07
67.333	0.00	0.00	0.002	O	|	|	|	0.07
67.417	0.00	0.00	0.002	O	|	|	|	0.07
67.500	0.00	0.00	0.002	O	|	|	|	0.07
67.583	0.00	0.00	0.002	O	|	|	|	0.07
67.667	0.00	0.00	0.002	O	|	|	|	0.07
67.750	0.00	0.00	0.002	O	|	|	|	0.07
67.833	0.00	0.00	0.002	O	|	|	|	0.07
67.917	0.00	0.00	0.002	O	|	|	|	0.06
68.000	0.00	0.00	0.002	O	|	|	|	0.06
68.083	0.00	0.00	0.002	O	|	|	|	0.06
68.167	0.00	0.00	0.001	O	|	|	|	0.06
68.250	0.00	0.00	0.001	O	|	|	|	0.06
68.333	0.00	0.00	0.001	O	|	|	|	0.06
68.417	0.00	0.00	0.001	O	|	|	|	0.06
68.500	0.00	0.00	0.001	O	|	|	|	0.06
68.583	0.00	0.00	0.001	O	|	|	|	0.06
68.667	0.00	0.00	0.001	O	|	|	|	0.06
68.750	0.00	0.00	0.001	O	|	|	|	0.06
68.833	0.00	0.00	0.001	O	|	|	|	0.06
68.917	0.00	0.00	0.001	O	|	|	|	0.06
69.000	0.00	0.00	0.001	O	|	|	|	0.05

69.083	0.00	0.00	0.001	O				0.05
69.167	0.00	0.00	0.001	O				0.05
69.250	0.00	0.00	0.001	O				0.05
69.333	0.00	0.00	0.001	O				0.05
69.417	0.00	0.00	0.001	O				0.05
69.500	0.00	0.00	0.001	O				0.05
69.583	0.00	0.00	0.001	O				0.05
69.667	0.00	0.00	0.001	O				0.05
69.750	0.00	0.00	0.001	O				0.05
69.833	0.00	0.00	0.001	O				0.05
69.917	0.00	0.00	0.001	O				0.05
70.000	0.00	0.00	0.001	O				0.05
70.083	0.00	0.00	0.001	O				0.05
70.167	0.00	0.00	0.001	O				0.05
70.250	0.00	0.00	0.001	O				0.04
70.333	0.00	0.00	0.001	O				0.04
70.417	0.00	0.00	0.001	O				0.04
70.500	0.00	0.00	0.001	O				0.04
70.583	0.00	0.00	0.001	O				0.04
70.667	0.00	0.00	0.001	O				0.04
70.750	0.00	0.00	0.001	O				0.04
70.833	0.00	0.00	0.001	O				0.04
70.917	0.00	0.00	0.001	O				0.04
71.000	0.00	0.00	0.001	O				0.04
71.083	0.00	0.00	0.001	O				0.04
71.167	0.00	0.00	0.001	O				0.04
71.250	0.00	0.00	0.001	O				0.04
71.333	0.00	0.00	0.001	O				0.04
71.417	0.00	0.00	0.001	O				0.04
71.500	0.00	0.00	0.001	O				0.04
71.583	0.00	0.00	0.001	O				0.04
71.667	0.00	0.00	0.001	O				0.04
71.750	0.00	0.00	0.001	O				0.04
71.833	0.00	0.00	0.001	O				0.04
71.917	0.00	0.00	0.001	O				0.03
72.000	0.00	0.00	0.001	O				0.03
72.083	0.00	0.00	0.001	O				0.03
72.167	0.00	0.00	0.001	O				0.03
72.250	0.00	0.00	0.001	O				0.03
72.333	0.00	0.00	0.001	O				0.03
72.417	0.00	0.00	0.001	O				0.03
72.500	0.00	0.00	0.001	O				0.03
72.583	0.00	0.00	0.001	O				0.03
72.667	0.00	0.00	0.001	O				0.03
72.750	0.00	0.00	0.001	O				0.03
72.833	0.00	0.00	0.001	O				0.03
72.917	0.00	0.00	0.001	O				0.03
73.000	0.00	0.00	0.001	O				0.03
73.083	0.00	0.00	0.001	O				0.03
73.167	0.00	0.00	0.001	O				0.03

73.250	0.00	0.00	0.001	O	|	|	|	|	0.03
73.333	0.00	0.00	0.001	O	|	|	|	|	0.03
73.417	0.00	0.00	0.001	O	|	|	|	|	0.03
73.500	0.00	0.00	0.001	O	|	|	|	|	0.03
73.583	0.00	0.00	0.001	O	|	|	|	|	0.03
73.667	0.00	0.00	0.001	O	|	|	|	|	0.03
73.750	0.00	0.00	0.001	O	|	|	|	|	0.03
73.833	0.00	0.00	0.001	O	|	|	|	|	0.03
73.917	0.00	0.00	0.001	O	|	|	|	|	0.03
74.000	0.00	0.00	0.001	O	|	|	|	|	0.03
74.083	0.00	0.00	0.001	O	|	|	|	|	0.02
74.167	0.00	0.00	0.001	O	|	|	|	|	0.02
74.250	0.00	0.00	0.001	O	|	|	|	|	0.02
74.333	0.00	0.00	0.001	O	|	|	|	|	0.02
74.417	0.00	0.00	0.001	O	|	|	|	|	0.02
74.500	0.00	0.00	0.001	O	|	|	|	|	0.02
74.583	0.00	0.00	0.001	O	|	|	|	|	0.02
74.667	0.00	0.00	0.001	O	|	|	|	|	0.02
74.750	0.00	0.00	0.001	O	|	|	|	|	0.02
74.833	0.00	0.00	0.001	O	|	|	|	|	0.02

**********HYDROGRAPH DATA**********

Number of intervals = 898
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.045 (CFS)
Total volume = 0.207 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
10 yr
24 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris2410.rte

**********HYDROGRAPH DATA**********

Number of intervals = 296
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.595 (CFS)
Total volume = 0.363 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++++++++++

Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 296
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.1 0.30 0.45 0.59	Depth (Ft.)
0.083	0.01	0.00	0.000	O	0.00
0.167	0.02	0.00	0.000	OI	0.01
0.250	0.03	0.00	0.000	OI	0.01
0.333	0.03	0.00	0.001	OI	0.02
0.417	0.04	0.00	0.001	O I	0.03
0.500	0.05	0.00	0.001	O I	0.05
0.583	0.05	0.00	0.001	O I	0.06
0.667	0.05	0.00	0.002	O I	0.07
0.750	0.05	0.00	0.002	O I	0.09
0.833	0.06	0.00	0.002	O I	0.10
0.917	0.06	0.01	0.003	O I	0.12
1.000	0.07	0.01	0.003	O I	0.13
1.083	0.07	0.01	0.004	O I	0.15
1.167	0.06	0.01	0.004	O I	0.17
1.250	0.06	0.01	0.004	O I	0.18
1.333	0.05	0.01	0.005	O I	0.19
1.417	0.05	0.01	0.005	O I	0.21
1.500	0.05	0.01	0.005	O I	0.22
1.583	0.05	0.01	0.006	O I	0.23
1.667	0.05	0.01	0.006	O I	0.24
1.750	0.05	0.01	0.006	O I	0.26
1.833	0.06	0.01	0.006	O I	0.27
1.917	0.06	0.01	0.007	O I	0.28
2.000	0.07	0.01	0.007	O I	0.30
2.083	0.07	0.01	0.007	O I	0.31
2.167	0.07	0.01	0.008	O I	0.33
2.250	0.07	0.02	0.008	O I	0.34
2.333	0.07	0.02	0.009	O I	0.36

2.417	0.07	0.02	0.009	O I |	|	|	|	0.37
2.500	0.07	0.02	0.009	O I |	|	|	|	0.39
2.583	0.07	0.02	0.010	O I |	|	|	|	0.41
2.667	0.08	0.02	0.010	|O I |	|	|	|	0.42
2.750	0.08	0.02	0.011	|O I |	|	|	|	0.44
2.833	0.09	0.02	0.011	|O I |	|	|	|	0.46
2.917	0.09	0.02	0.011	|O I |	|	|	|	0.48
3.000	0.09	0.02	0.012	|O I |	|	|	|	0.50
3.083	0.09	0.02	0.012	|O I |	|	|	|	0.52
3.167	0.09	0.02	0.013	|O I |	|	|	|	0.53
3.250	0.09	0.02	0.013	|O I |	|	|	|	0.55
3.333	0.09	0.03	0.014	|O I |	|	|	|	0.57
3.417	0.09	0.03	0.014	|O I |	|	|	|	0.59
3.500	0.09	0.03	0.015	|O I |	|	|	|	0.61
3.583	0.09	0.03	0.015	|O I |	|	|	|	0.62
3.667	0.09	0.03	0.015	|O I |	|	|	|	0.64
3.750	0.09	0.03	0.016	|O I |	|	|	|	0.66
3.833	0.09	0.03	0.016	|O I |	|	|	|	0.67
3.917	0.10	0.03	0.017	|O I |	|	|	|	0.69
4.000	0.10	0.03	0.017	|O I |	|	|	|	0.71
4.083	0.10	0.03	0.018	|O I |	|	|	|	0.73
4.167	0.10	0.03	0.018	|O I |	|	|	|	0.75
4.250	0.10	0.03	0.019	|O I |	|	|	|	0.77
4.333	0.11	0.04	0.019	|O I |	|	|	|	0.79
4.417	0.12	0.04	0.020	|O I |	|	|	|	0.82
4.500	0.12	0.04	0.020	| O I |	|	|	|	0.84
4.583	0.12	0.04	0.021	| O I |	|	|	|	0.86
4.667	0.12	0.04	0.021	| O I |	|	|	|	0.89
4.750	0.12	0.04	0.022	| O I |	|	|	|	0.91
4.833	0.13	0.04	0.022	| O I |	|	|	|	0.93
4.917	0.13	0.04	0.023	| O I|	|	|	|	0.96
5.000	0.14	0.04	0.024	| O I|	|	|	|	0.98
5.083	0.13	0.04	0.024	| O I|	|	|	|	1.01
5.167	0.12	0.04	0.025	| O I |	|	|	|	1.02
5.250	0.11	0.04	0.025	| O I |	|	|	|	1.03
5.333	0.11	0.04	0.026	| O I |	|	|	|	1.04
5.417	0.12	0.04	0.026	| O I |	|	|	|	1.06
5.500	0.12	0.04	0.027	| O I |	|	|	|	1.07
5.583	0.13	0.04	0.027	| O I |	|	|	|	1.08
5.667	0.13	0.04	0.028	| O I|	|	|	|	1.10
5.750	0.14	0.04	0.028	| O I|	|	|	|	1.11
5.833	0.14	0.04	0.029	| O I|	|	|	|	1.13
5.917	0.14	0.04	0.030	| O I|	|	|	|	1.14
6.000	0.14	0.04	0.030	| O I|	|	|	|	1.16
6.083	0.14	0.04	0.031	| O I|	|	|	|	1.18
6.167	0.15	0.04	0.032	| O I	|	|	|	1.19
6.250	0.16	0.04	0.033	| O I	|	|	|	1.21
6.333	0.16	0.04	0.033	| O I	|	|	|	1.23
6.417	0.16	0.04	0.034	| O I	|	|	|	1.25
6.500	0.16	0.04	0.035	| O I	|	|	|	1.27

6.583	0.16	0.04	0.036	O	I			1.29
6.667	0.17	0.04	0.036	O	I			1.31
6.750	0.17	0.04	0.037	O	I			1.33
6.833	0.17	0.04	0.038	O	I			1.36
6.917	0.17	0.04	0.039	O	I			1.38
7.000	0.18	0.04	0.040	O	I			1.40
7.083	0.18	0.04	0.041	O	I			1.42
7.167	0.18	0.04	0.042	O	I			1.45
7.250	0.18	0.04	0.043	O	I			1.47
7.333	0.18	0.04	0.044	O	I			1.49
7.417	0.19	0.04	0.045	O	I			1.51
7.500	0.19	0.04	0.046	O	I			1.54
7.583	0.19	0.04	0.047	O	I			1.56
7.667	0.20	0.04	0.048	O	I			1.59
7.750	0.21	0.04	0.049	O	I			1.62
7.833	0.21	0.04	0.050	O	I			1.65
7.917	0.22	0.04	0.051	O	I			1.68
8.000	0.22	0.04	0.052	O	I			1.71
8.083	0.23	0.04	0.054	O	I			1.74
8.167	0.25	0.04	0.055	O	I			1.77
8.250	0.26	0.04	0.056	O	I			1.81
8.333	0.26	0.04	0.058	O	I			1.85
8.417	0.26	0.04	0.059	O	I			1.88
8.500	0.26	0.04	0.061	O	I			1.92
8.583	0.27	0.04	0.062	O	I			1.96
8.667	0.28	0.04	0.064	O	I			2.00
8.750	0.28	0.04	0.065	O	I			2.04
8.833	0.28	0.04	0.067	O	I			2.08
8.917	0.29	0.04	0.069	O	I			2.12
9.000	0.30	0.04	0.070	O	I			2.16
9.083	0.30	0.04	0.072	O	I			2.21
9.167	0.32	0.04	0.074	O	I			2.25
9.250	0.33	0.04	0.076	O	I			2.30
9.333	0.33	0.04	0.078	O	I			2.35
9.417	0.34	0.04	0.080	O	I			2.40
9.500	0.35	0.04	0.082	O	I			2.45
9.583	0.35	0.04	0.084	O	I			2.50
9.667	0.36	0.04	0.086	O	I			2.56
9.750	0.37	0.04	0.088	O	I			2.61
9.833	0.37	0.04	0.091	O	I			2.67
9.917	0.38	0.04	0.093	O	I			2.72
10.000	0.38	0.04	0.095	O	I			2.78
10.083	0.36	0.04	0.098	O	I			2.84
10.167	0.30	0.04	0.100	O	I			2.89
10.250	0.29	0.04	0.101	O	I			2.93
10.333	0.28	0.04	0.103	O	I			2.97
10.417	0.27	0.04	0.104	O	I			3.01
10.500	0.27	0.04	0.106	O	I			3.05
10.583	0.28	0.04	0.108	O	I			3.09
10.667	0.32	0.04	0.109	O	I			3.13

10.750	0.34	0.04	0.111	O		I		3.18
10.833	0.34	0.04	0.113	O		I		3.23
10.917	0.35	0.04	0.115	O		I		3.29
11.000	0.35	0.04	0.118	O		I		3.34
11.083	0.35	0.04	0.120	O		I		3.39
11.167	0.34	0.04	0.122	O		I		3.44
11.250	0.34	0.04	0.124	O		I		3.49
11.333	0.34	0.04	0.126	O		I		3.54
11.417	0.34	0.04	0.128	O		I		3.59
11.500	0.33	0.04	0.130	O		I		3.64
11.583	0.33	0.04	0.132	O		I		3.69
11.667	0.31	0.04	0.134	O		I		3.74
11.750	0.31	0.04	0.135	O		I		3.78
11.833	0.31	0.04	0.137	O		I		3.83
11.917	0.31	0.04	0.139	O		I		3.87
12.000	0.31	0.04	0.141	O		I		3.92
12.083	0.34	0.04	0.143	O		I		3.97
12.167	0.40	0.04	0.145	O		I		4.02
12.250	0.42	0.04	0.147	O		I		4.09
12.333	0.43	0.04	0.150	O		I		4.15
12.417	0.44	0.04	0.153	O		I		4.22
12.500	0.45	0.04	0.156	O		I		4.29
12.583	0.46	0.04	0.158	O		I		4.36
12.667	0.48	0.04	0.161	O		I		4.43
12.750	0.49	0.04	0.164	O		I		4.51
12.833	0.49	0.04	0.167	O		I		4.58
12.917	0.50	0.04	0.170	O		I		4.66
13.000	0.51	0.04	0.174	O		I		4.74
13.083	0.52	0.04	0.177	O		I		4.82
13.167	0.57	0.04	0.180	O		I		4.90
13.250	0.58	0.04	0.184	O		I		4.99
13.333	0.59	0.04	0.188	O		I		5.08
13.417	0.59	0.04	0.191	O		I		5.18
13.500	0.59	0.04	0.195	O		I		5.27
13.583	0.56	0.04	0.199	O		I		5.36
13.667	0.47	0.04	0.202	O		I		5.44
13.750	0.44	0.04	0.205	O		I		5.51
13.833	0.42	0.04	0.208	O		I		5.58
13.917	0.42	0.04	0.210	O		I		5.64
14.000	0.41	0.04	0.213	O		I		5.70
14.083	0.42	0.04	0.215	O		I		5.77
14.167	0.45	0.04	0.218	O		I		5.83
14.250	0.46	0.04	0.221	O		I		5.90
14.333	0.46	0.04	0.224	O		I		5.97
14.417	0.46	0.04	0.227	O		I		6.05
14.500	0.46	0.04	0.229	O		I		6.12
14.583	0.46	0.04	0.232	O		I		6.19
14.667	0.46	0.04	0.235	O		I		6.26
14.750	0.46	0.04	0.238	O		I		6.33
14.833	0.45	0.04	0.241	O		I		6.40

14.917	0.45	0.04	0.244	O			I	6.47
15.000	0.44	0.04	0.246	O			I	6.53
15.083	0.44	0.04	0.249	O			I	6.60
15.167	0.43	0.04	0.252	O			I	6.67
15.250	0.43	0.04	0.254	O			I	6.73
15.333	0.42	0.04	0.257	O			I	6.80
15.417	0.41	0.04	0.260	O			I	6.86
15.500	0.41	0.04	0.262	O			I	6.92
15.583	0.39	0.04	0.265	O			I	6.98
15.667	0.36	0.04	0.267	O		I		7.04
15.750	0.35	0.04	0.269	O		I		7.09
15.833	0.34	0.04	0.271	O		I		7.14
15.917	0.34	0.04	0.273	O		I		7.19
16.000	0.34	0.04	0.275	O		I		7.24
16.083	0.29	0.04	0.277	O	I			7.29
16.167	0.16	0.04	0.278	O	I			7.32
16.250	0.12	0.04	0.279	O	I			7.33
16.333	0.10	0.04	0.279	O	I			7.34
16.417	0.09	0.04	0.280	O	I			7.35
16.500	0.08	0.04	0.280	O	I			7.36
16.583	0.07	0.04	0.280	O	I			7.36
16.667	0.06	0.04	0.280	O	I			7.37
16.750	0.06	0.04	0.280	O	I			7.37
16.833	0.05	0.04	0.280	O				7.37
16.917	0.05	0.04	0.280	O				7.37
17.000	0.05	0.04	0.280	O				7.38
17.083	0.06	0.04	0.281	O	I			7.38
17.167	0.08	0.04	0.281	O	I			7.38
17.250	0.08	0.04	0.281	O	I			7.39
17.333	0.08	0.04	0.281	O	I			7.39
17.417	0.09	0.04	0.281	O	I			7.40
17.500	0.09	0.04	0.282	O	I			7.41
17.583	0.09	0.04	0.282	O	I			7.41
17.667	0.09	0.04	0.282	O	I			7.42
17.750	0.09	0.04	0.283	O	I			7.43
17.833	0.08	0.04	0.283	O	I			7.44
17.917	0.08	0.04	0.283	O	I			7.44
18.000	0.07	0.04	0.283	O	I			7.45
18.083	0.07	0.04	0.284	O	I			7.45
18.167	0.07	0.04	0.284	O	I			7.46
18.250	0.07	0.04	0.284	O	I			7.46
18.333	0.07	0.04	0.284	O	I			7.46
18.417	0.07	0.04	0.284	O	I			7.47
18.500	0.07	0.04	0.284	O	I			7.47
18.583	0.07	0.04	0.285	O	I			7.48
18.667	0.06	0.04	0.285	O	I			7.48
18.750	0.06	0.04	0.285	O	I			7.48
18.833	0.05	0.04	0.285	O				7.48
18.917	0.04	0.04	0.285	O				7.48
19.000	0.04	0.04	0.285	O				7.48

19.083	0.04	0.04	0.285	O				7.48
19.167	0.05	0.04	0.285	O				7.48
19.250	0.05	0.04	0.285	O				7.48
19.333	0.05	0.04	0.285	O				7.48
19.417	0.06	0.04	0.285	OI				7.49
19.500	0.07	0.04	0.285	OI				7.49
19.583	0.07	0.04	0.285	OI				7.49
19.667	0.06	0.04	0.285	OI				7.50
19.750	0.06	0.04	0.285	O				7.50
19.833	0.05	0.04	0.286	O				7.50
19.917	0.04	0.04	0.286	O				7.50
20.000	0.04	0.04	0.285	O				7.50
20.083	0.04	0.04	0.285	O				7.50
20.167	0.05	0.04	0.285	O				7.50
20.250	0.05	0.04	0.285	O				7.50
20.333	0.05	0.04	0.286	O				7.50
20.417	0.05	0.04	0.286	O				7.50
20.500	0.05	0.04	0.286	O				7.50
20.583	0.05	0.04	0.286	O				7.50
20.667	0.05	0.04	0.286	O				7.51
20.750	0.05	0.04	0.286	O				7.51
20.833	0.05	0.04	0.286	O				7.51
20.917	0.04	0.04	0.286	O				7.51
21.000	0.04	0.04	0.286	O				7.51
21.083	0.04	0.04	0.286	O				7.51
21.167	0.05	0.04	0.286	O				7.51
21.250	0.05	0.04	0.286	O				7.51
21.333	0.05	0.04	0.286	O				7.51
21.417	0.04	0.04	0.286	O				7.51
21.500	0.04	0.04	0.286	O				7.51
21.583	0.04	0.04	0.286	O				7.50
21.667	0.05	0.04	0.286	O				7.50
21.750	0.05	0.04	0.286	O				7.51
21.833	0.05	0.04	0.286	O				7.51
21.917	0.04	0.04	0.286	O				7.51
22.000	0.04	0.04	0.286	O				7.50
22.083	0.04	0.04	0.286	O				7.50
22.167	0.05	0.04	0.286	O				7.50
22.250	0.05	0.04	0.286	O				7.50
22.333	0.05	0.04	0.286	O				7.50
22.417	0.04	0.04	0.286	O				7.50
22.500	0.04	0.04	0.286	O				7.50
22.583	0.04	0.04	0.286	IO				7.50
22.667	0.04	0.04	0.286	IO				7.50
22.750	0.04	0.04	0.285	IO				7.50
22.833	0.04	0.04	0.285	IO				7.50
22.917	0.04	0.04	0.285	IO				7.50
23.000	0.04	0.04	0.285	IO				7.49
23.083	0.04	0.04	0.285	IO				7.49
23.167	0.04	0.04	0.285	IO				7.49

23.250	0.04	0.04	0.285	|IO	|	|	|	7.49
23.333	0.04	0.04	0.285	|IO	|	|	|	7.49
23.417	0.04	0.04	0.285	|IO	|	|	|	7.49
23.500	0.04	0.04	0.285	|IO	|	|	|	7.48
23.583	0.04	0.04	0.285	|IO	|	|	|	7.48
23.667	0.04	0.04	0.285	|IO	|	|	|	7.48
23.750	0.04	0.04	0.285	|IO	|	|	|	7.48
23.833	0.04	0.04	0.285	|IO	|	|	|	7.48
23.917	0.04	0.04	0.285	|IO	|	|	|	7.48
24.000	0.04	0.04	0.284	|IO	|	|	|	7.47
24.083	0.03	0.04	0.284	|IO	|	|	|	7.47
24.167	0.01	0.04	0.284	I O	|	|	|	7.47
24.250	0.01	0.04	0.284	I O	|	|	|	7.46
24.333	0.00	0.04	0.284	I O	|	|	|	7.46
24.417	0.00	0.04	0.283	I O	|	|	|	7.45
24.500	0.00	0.04	0.283	I O	|	|	|	7.44
24.583	0.00	0.04	0.283	I O	|	|	|	7.43
24.667	0.00	0.04	0.282	I O	|	|	|	7.43
24.750	0.00	0.04	0.282	I O	|	|	|	7.42
24.833	0.00	0.04	0.282	I O	|	|	|	7.41
24.917	0.00	0.04	0.282	I O	|	|	|	7.40
25.000	0.00	0.04	0.281	I O	|	|	|	7.40
25.083	0.00	0.04	0.281	I O	|	|	|	7.39
25.167	0.00	0.04	0.281	I O	|	|	|	7.38
25.250	0.00	0.04	0.280	I O	|	|	|	7.37
25.333	0.00	0.04	0.280	I O	|	|	|	7.36
25.417	0.00	0.04	0.280	I O	|	|	|	7.36
25.500	0.00	0.04	0.279	I O	|	|	|	7.35
25.583	0.00	0.04	0.279	I O	|	|	|	7.34
25.667	0.00	0.04	0.279	I O	|	|	|	7.33
25.750	0.00	0.04	0.278	I O	|	|	|	7.33
25.833	0.00	0.04	0.278	I O	|	|	|	7.32
25.917	0.00	0.04	0.278	I O	|	|	|	7.31
26.000	0.00	0.04	0.278	I O	|	|	|	7.30
26.083	0.00	0.04	0.277	I O	|	|	|	7.30
26.167	0.00	0.04	0.277	I O	|	|	|	7.29
26.250	0.00	0.04	0.277	I O	|	|	|	7.28
26.333	0.00	0.04	0.276	I O	|	|	|	7.27
26.417	0.00	0.04	0.276	I O	|	|	|	7.27
26.500	0.00	0.04	0.276	I O	|	|	|	7.26
26.583	0.00	0.04	0.275	I O	|	|	|	7.25
26.667	0.00	0.04	0.275	I O	|	|	|	7.24
26.750	0.00	0.04	0.275	I O	|	|	|	7.23
26.833	0.00	0.04	0.274	I O	|	|	|	7.23
26.917	0.00	0.04	0.274	I O	|	|	|	7.22
27.000	0.00	0.04	0.274	I O	|	|	|	7.21
27.083	0.00	0.04	0.274	I O	|	|	|	7.20
27.167	0.00	0.04	0.273	I O	|	|	|	7.20
27.250	0.00	0.04	0.273	I O	|	|	|	7.19
27.333	0.00	0.04	0.273	I O	|	|	|	7.18

27.417	0.00	0.04	0.272	I	O	|	|	|	7.17
27.500	0.00	0.04	0.272	I	O	|	|	|	7.17
27.583	0.00	0.04	0.272	I	O	|	|	|	7.16
27.667	0.00	0.04	0.271	I	O	|	|	|	7.15
27.750	0.00	0.04	0.271	I	O	|	|	|	7.14
27.833	0.00	0.04	0.271	I	O	|	|	|	7.13
27.917	0.00	0.04	0.270	I	O	|	|	|	7.13
28.000	0.00	0.04	0.270	I	O	|	|	|	7.12
28.083	0.00	0.04	0.270	I	O	|	|	|	7.11
28.167	0.00	0.04	0.269	I	O	|	|	|	7.10
28.250	0.00	0.04	0.269	I	O	|	|	|	7.10
28.333	0.00	0.04	0.269	I	O	|	|	|	7.09
28.417	0.00	0.04	0.269	I	O	|	|	|	7.08
28.500	0.00	0.04	0.268	I	O	|	|	|	7.07
28.583	0.00	0.04	0.268	I	O	|	|	|	7.07
28.667	0.00	0.04	0.268	I	O	|	|	|	7.06
28.750	0.00	0.04	0.267	I	O	|	|	|	7.05
28.833	0.00	0.04	0.267	I	O	|	|	|	7.04
28.917	0.00	0.04	0.267	I	O	|	|	|	7.04
29.000	0.00	0.04	0.266	I	O	|	|	|	7.03
29.083	0.00	0.04	0.266	I	O	|	|	|	7.02
29.167	0.00	0.04	0.266	I	O	|	|	|	7.01
29.250	0.00	0.04	0.265	I	O	|	|	|	7.00
29.333	0.00	0.04	0.265	I	O	|	|	|	7.00
29.417	0.00	0.04	0.265	I	O	|	|	|	6.99
29.500	0.00	0.04	0.265	I	O	|	|	|	6.98
29.583	0.00	0.04	0.264	I	O	|	|	|	6.97
29.667	0.00	0.04	0.264	I	O	|	|	|	6.97
29.750	0.00	0.04	0.264	I	O	|	|	|	6.96
29.833	0.00	0.04	0.263	I	O	|	|	|	6.95
29.917	0.00	0.04	0.263	I	O	|	|	|	6.94
30.000	0.00	0.04	0.263	I	O	|	|	|	6.94
30.083	0.00	0.04	0.262	I	O	|	|	|	6.93
30.167	0.00	0.04	0.262	I	O	|	|	|	6.92
30.250	0.00	0.04	0.262	I	O	|	|	|	6.91
30.333	0.00	0.04	0.261	I	O	|	|	|	6.91
30.417	0.00	0.04	0.261	I	O	|	|	|	6.90
30.500	0.00	0.04	0.261	I	O	|	|	|	6.89
30.583	0.00	0.04	0.260	I	O	|	|	|	6.88
30.667	0.00	0.04	0.260	I	O	|	|	|	6.87
30.750	0.00	0.04	0.260	I	O	|	|	|	6.87
30.833	0.00	0.04	0.260	I	O	|	|	|	6.86
30.917	0.00	0.04	0.259	I	O	|	|	|	6.85
31.000	0.00	0.04	0.259	I	O	|	|	|	6.84
31.083	0.00	0.04	0.259	I	O	|	|	|	6.84
31.167	0.00	0.04	0.258	I	O	|	|	|	6.83
31.250	0.00	0.04	0.258	I	O	|	|	|	6.82
31.333	0.00	0.04	0.258	I	O	|	|	|	6.81
31.417	0.00	0.04	0.257	I	O	|	|	|	6.81
31.500	0.00	0.04	0.257	I	O	|	|	|	6.80

31.583	0.00	0.04	0.257	I	O	|	|	|	6.79
31.667	0.00	0.04	0.256	I	O	|	|	|	6.78
31.750	0.00	0.04	0.256	I	O	|	|	|	6.78
31.833	0.00	0.04	0.256	I	O	|	|	|	6.77
31.917	0.00	0.04	0.256	I	O	|	|	|	6.76
32.000	0.00	0.04	0.255	I	O	|	|	|	6.75
32.083	0.00	0.04	0.255	I	O	|	|	|	6.74
32.167	0.00	0.04	0.255	I	O	|	|	|	6.74
32.250	0.00	0.04	0.254	I	O	|	|	|	6.73
32.333	0.00	0.04	0.254	I	O	|	|	|	6.72
32.417	0.00	0.04	0.254	I	O	|	|	|	6.71
32.500	0.00	0.04	0.253	I	O	|	|	|	6.71
32.583	0.00	0.04	0.253	I	O	|	|	|	6.70
32.667	0.00	0.04	0.253	I	O	|	|	|	6.69
32.750	0.00	0.04	0.252	I	O	|	|	|	6.68
32.833	0.00	0.04	0.252	I	O	|	|	|	6.68
32.917	0.00	0.04	0.252	I	O	|	|	|	6.67
33.000	0.00	0.04	0.252	I	O	|	|	|	6.66
33.083	0.00	0.04	0.251	I	O	|	|	|	6.65
33.167	0.00	0.04	0.251	I	O	|	|	|	6.65
33.250	0.00	0.04	0.251	I	O	|	|	|	6.64
33.333	0.00	0.04	0.250	I	O	|	|	|	6.63
33.417	0.00	0.04	0.250	I	O	|	|	|	6.62
33.500	0.00	0.04	0.250	I	O	|	|	|	6.61
33.583	0.00	0.04	0.249	I	O	|	|	|	6.61
33.667	0.00	0.04	0.249	I	O	|	|	|	6.60
33.750	0.00	0.04	0.249	I	O	|	|	|	6.59
33.833	0.00	0.04	0.248	I	O	|	|	|	6.58
33.917	0.00	0.04	0.248	I	O	|	|	|	6.58
34.000	0.00	0.04	0.248	I	O	|	|	|	6.57
34.083	0.00	0.04	0.247	I	O	|	|	|	6.56
34.167	0.00	0.04	0.247	I	O	|	|	|	6.55
34.250	0.00	0.04	0.247	I	O	|	|	|	6.55
34.333	0.00	0.04	0.247	I	O	|	|	|	6.54
34.417	0.00	0.04	0.246	I	O	|	|	|	6.53
34.500	0.00	0.04	0.246	I	O	|	|	|	6.52
34.583	0.00	0.04	0.246	I	O	|	|	|	6.52
34.667	0.00	0.04	0.245	I	O	|	|	|	6.51
34.750	0.00	0.04	0.245	I	O	|	|	|	6.50
34.833	0.00	0.04	0.245	I	O	|	|	|	6.49
34.917	0.00	0.04	0.244	I	O	|	|	|	6.48
35.000	0.00	0.04	0.244	I	O	|	|	|	6.48
35.083	0.00	0.04	0.244	I	O	|	|	|	6.47
35.167	0.00	0.04	0.243	I	O	|	|	|	6.46
35.250	0.00	0.04	0.243	I	O	|	|	|	6.45
35.333	0.00	0.04	0.243	I	O	|	|	|	6.45
35.417	0.00	0.04	0.243	I	O	|	|	|	6.44
35.500	0.00	0.04	0.242	I	O	|	|	|	6.43
35.583	0.00	0.04	0.242	I	O	|	|	|	6.42
35.667	0.00	0.04	0.242	I	O	|	|	|	6.42

35.750	0.00	0.04	0.241	I	O	|	|	|	| 6.41
35.833	0.00	0.04	0.241	I	O	|	|	|	| 6.40
35.917	0.00	0.04	0.241	I	O	|	|	|	| 6.39
36.000	0.00	0.04	0.240	I	O	|	|	|	| 6.39
36.083	0.00	0.04	0.240	I	O	|	|	|	| 6.38
36.167	0.00	0.04	0.240	I	O	|	|	|	| 6.37
36.250	0.00	0.04	0.239	I	O	|	|	|	| 6.36
36.333	0.00	0.04	0.239	I	O	|	|	|	| 6.35
36.417	0.00	0.04	0.239	I	O	|	|	|	| 6.35
36.500	0.00	0.04	0.238	I	O	|	|	|	| 6.34
36.583	0.00	0.04	0.238	I	O	|	|	|	| 6.33
36.667	0.00	0.04	0.238	I	O	|	|	|	| 6.32
36.750	0.00	0.04	0.238	I	O	|	|	|	| 6.32
36.833	0.00	0.04	0.237	I	O	|	|	|	| 6.31
36.917	0.00	0.04	0.237	I	O	|	|	|	| 6.30
37.000	0.00	0.04	0.237	I	O	|	|	|	| 6.29
37.083	0.00	0.04	0.236	I	O	|	|	|	| 6.29
37.167	0.00	0.04	0.236	I	O	|	|	|	| 6.28
37.250	0.00	0.04	0.236	I	O	|	|	|	| 6.27
37.333	0.00	0.04	0.235	I	O	|	|	|	| 6.26
37.417	0.00	0.04	0.235	I	O	|	|	|	| 6.25
37.500	0.00	0.04	0.235	I	O	|	|	|	| 6.25
37.583	0.00	0.04	0.234	I	O	|	|	|	| 6.24
37.667	0.00	0.04	0.234	I	O	|	|	|	| 6.23
37.750	0.00	0.04	0.234	I	O	|	|	|	| 6.22
37.833	0.00	0.04	0.234	I	O	|	|	|	| 6.22
37.917	0.00	0.04	0.233	I	O	|	|	|	| 6.21
38.000	0.00	0.04	0.233	I	O	|	|	|	| 6.20
38.083	0.00	0.04	0.233	I	O	|	|	|	| 6.19
38.167	0.00	0.04	0.232	I	O	|	|	|	| 6.19
38.250	0.00	0.04	0.232	I	O	|	|	|	| 6.18
38.333	0.00	0.04	0.232	I	O	|	|	|	| 6.17
38.417	0.00	0.04	0.231	I	O	|	|	|	| 6.16
38.500	0.00	0.04	0.231	I	O	|	|	|	| 6.16
38.583	0.00	0.04	0.231	I	O	|	|	|	| 6.15
38.667	0.00	0.04	0.230	I	O	|	|	|	| 6.14
38.750	0.00	0.04	0.230	I	O	|	|	|	| 6.13
38.833	0.00	0.04	0.230	I	O	|	|	|	| 6.12
38.917	0.00	0.04	0.229	I	O	|	|	|	| 6.12
39.000	0.00	0.04	0.229	I	O	|	|	|	| 6.11
39.083	0.00	0.04	0.229	I	O	|	|	|	| 6.10
39.167	0.00	0.04	0.229	I	O	|	|	|	| 6.09
39.250	0.00	0.04	0.228	I	O	|	|	|	| 6.09
39.333	0.00	0.04	0.228	I	O	|	|	|	| 6.08
39.417	0.00	0.04	0.228	I	O	|	|	|	| 6.07
39.500	0.00	0.04	0.227	I	O	|	|	|	| 6.06
39.583	0.00	0.04	0.227	I	O	|	|	|	| 6.06
39.667	0.00	0.04	0.227	I	O	|	|	|	| 6.05
39.750	0.00	0.04	0.226	I	O	|	|	|	| 6.04
39.833	0.00	0.04	0.226	I	O	|	|	|	| 6.03

39.917	0.00	0.04	0.226	I	O	|	|	|	6.03
40.000	0.00	0.04	0.225	I	O	|	|	|	6.02
40.083	0.00	0.04	0.225	I	O	|	|	|	6.01
40.167	0.00	0.04	0.225	I	O	|	|	|	6.00
40.250	0.00	0.04	0.225	I	O	|	|	|	5.99
40.333	0.00	0.04	0.224	I	O	|	|	|	5.99
40.417	0.00	0.04	0.224	I	O	|	|	|	5.98
40.500	0.00	0.04	0.224	I	O	|	|	|	5.97
40.583	0.00	0.04	0.223	I	O	|	|	|	5.96
40.667	0.00	0.04	0.223	I	O	|	|	|	5.96
40.750	0.00	0.04	0.223	I	O	|	|	|	5.95
40.833	0.00	0.04	0.222	I	O	|	|	|	5.94
40.917	0.00	0.04	0.222	I	O	|	|	|	5.93
41.000	0.00	0.04	0.222	I	O	|	|	|	5.93
41.083	0.00	0.04	0.221	I	O	|	|	|	5.92
41.167	0.00	0.04	0.221	I	O	|	|	|	5.91
41.250	0.00	0.04	0.221	I	O	|	|	|	5.90
41.333	0.00	0.04	0.221	I	O	|	|	|	5.90
41.417	0.00	0.04	0.220	I	O	|	|	|	5.89
41.500	0.00	0.04	0.220	I	O	|	|	|	5.88
41.583	0.00	0.04	0.220	I	O	|	|	|	5.87
41.667	0.00	0.04	0.219	I	O	|	|	|	5.86
41.750	0.00	0.04	0.219	I	O	|	|	|	5.86
41.833	0.00	0.04	0.219	I	O	|	|	|	5.85
41.917	0.00	0.04	0.218	I	O	|	|	|	5.84
42.000	0.00	0.04	0.218	I	O	|	|	|	5.83
42.083	0.00	0.04	0.218	I	O	|	|	|	5.83
42.167	0.00	0.04	0.217	I	O	|	|	|	5.82
42.250	0.00	0.04	0.217	I	O	|	|	|	5.81
42.333	0.00	0.04	0.217	I	O	|	|	|	5.80
42.417	0.00	0.04	0.216	I	O	|	|	|	5.80
42.500	0.00	0.04	0.216	I	O	|	|	|	5.79
42.583	0.00	0.04	0.216	I	O	|	|	|	5.78
42.667	0.00	0.04	0.216	I	O	|	|	|	5.77
42.750	0.00	0.04	0.215	I	O	|	|	|	5.77
42.833	0.00	0.04	0.215	I	O	|	|	|	5.76
42.917	0.00	0.04	0.215	I	O	|	|	|	5.75
43.000	0.00	0.04	0.214	I	O	|	|	|	5.74
43.083	0.00	0.04	0.214	I	O	|	|	|	5.73
43.167	0.00	0.04	0.214	I	O	|	|	|	5.73
43.250	0.00	0.04	0.213	I	O	|	|	|	5.72
43.333	0.00	0.04	0.213	I	O	|	|	|	5.71
43.417	0.00	0.04	0.213	I	O	|	|	|	5.70
43.500	0.00	0.04	0.212	I	O	|	|	|	5.70
43.583	0.00	0.04	0.212	I	O	|	|	|	5.69
43.667	0.00	0.04	0.212	I	O	|	|	|	5.68
43.750	0.00	0.04	0.212	I	O	|	|	|	5.67
43.833	0.00	0.04	0.211	I	O	|	|	|	5.67
43.917	0.00	0.04	0.211	I	O	|	|	|	5.66
44.000	0.00	0.04	0.211	I	O	|	|	|	5.65

44.083	0.00	0.04	0.210	I O				5.64
44.167	0.00	0.04	0.210	I O				5.64
44.250	0.00	0.04	0.210	I O				5.63
44.333	0.00	0.04	0.209	I O				5.62
44.417	0.00	0.04	0.209	I O				5.61
44.500	0.00	0.04	0.209	I O				5.60
44.583	0.00	0.04	0.208	I O				5.60
44.667	0.00	0.04	0.208	I O				5.59
44.750	0.00	0.04	0.208	I O				5.58
44.833	0.00	0.04	0.207	I O				5.57
44.917	0.00	0.04	0.207	I O				5.57
45.000	0.00	0.04	0.207	I O				5.56
45.083	0.00	0.04	0.207	I O				5.55
45.167	0.00	0.04	0.206	I O				5.54
45.250	0.00	0.04	0.206	I O				5.54
45.333	0.00	0.04	0.206	I O				5.53
45.417	0.00	0.04	0.205	I O				5.52
45.500	0.00	0.04	0.205	I O				5.51
45.583	0.00	0.04	0.205	I O				5.51
45.667	0.00	0.04	0.204	I O				5.50
45.750	0.00	0.04	0.204	I O				5.49
45.833	0.00	0.04	0.204	I O				5.48
45.917	0.00	0.04	0.203	I O				5.47
46.000	0.00	0.04	0.203	I O				5.47
46.083	0.00	0.04	0.203	I O				5.46
46.167	0.00	0.04	0.203	I O				5.45
46.250	0.00	0.04	0.202	I O				5.44
46.333	0.00	0.04	0.202	I O				5.44
46.417	0.00	0.04	0.202	I O				5.43
46.500	0.00	0.04	0.201	I O				5.42
46.583	0.00	0.04	0.201	I O				5.41
46.667	0.00	0.04	0.201	I O				5.41
46.750	0.00	0.04	0.200	I O				5.40
46.833	0.00	0.04	0.200	I O				5.39
46.917	0.00	0.04	0.200	I O				5.38
47.000	0.00	0.04	0.199	I O				5.37
47.083	0.00	0.04	0.199	I O				5.37
47.167	0.00	0.04	0.199	I O				5.36
47.250	0.00	0.04	0.199	I O				5.35
47.333	0.00	0.04	0.198	I O				5.34
47.417	0.00	0.04	0.198	I O				5.34
47.500	0.00	0.04	0.198	I O				5.33
47.583	0.00	0.04	0.197	I O				5.32
47.667	0.00	0.04	0.197	I O				5.31
47.750	0.00	0.04	0.197	I O				5.31
47.833	0.00	0.04	0.196	I O				5.30
47.917	0.00	0.04	0.196	I O				5.29
48.000	0.00	0.04	0.196	I O				5.28
48.083	0.00	0.04	0.195	I O				5.28
48.167	0.00	0.04	0.195	I O				5.27

48.250	0.00	0.04	0.195	I	O	|	|	|	5.26
48.333	0.00	0.04	0.194	I	O	|	|	|	5.25
48.417	0.00	0.04	0.194	I	O	|	|	|	5.24
48.500	0.00	0.04	0.194	I	O	|	|	|	5.24
48.583	0.00	0.04	0.194	I	O	|	|	|	5.23
48.667	0.00	0.04	0.193	I	O	|	|	|	5.22
48.750	0.00	0.04	0.193	I	O	|	|	|	5.21
48.833	0.00	0.04	0.193	I	O	|	|	|	5.21
48.917	0.00	0.04	0.192	I	O	|	|	|	5.20
49.000	0.00	0.04	0.192	I	O	|	|	|	5.19
49.083	0.00	0.04	0.192	I	O	|	|	|	5.18
49.167	0.00	0.04	0.191	I	O	|	|	|	5.18
49.250	0.00	0.04	0.191	I	O	|	|	|	5.17
49.333	0.00	0.04	0.191	I	O	|	|	|	5.16
49.417	0.00	0.04	0.190	I	O	|	|	|	5.15
49.500	0.00	0.04	0.190	I	O	|	|	|	5.15
49.583	0.00	0.04	0.190	I	O	|	|	|	5.14
49.667	0.00	0.04	0.190	I	O	|	|	|	5.13
49.750	0.00	0.04	0.189	I	O	|	|	|	5.12
49.833	0.00	0.04	0.189	I	O	|	|	|	5.11
49.917	0.00	0.04	0.189	I	O	|	|	|	5.11
50.000	0.00	0.04	0.188	I	O	|	|	|	5.10
50.083	0.00	0.04	0.188	I	O	|	|	|	5.09
50.167	0.00	0.04	0.188	I	O	|	|	|	5.08
50.250	0.00	0.04	0.187	I	O	|	|	|	5.08
50.333	0.00	0.04	0.187	I	O	|	|	|	5.07
50.417	0.00	0.04	0.187	I	O	|	|	|	5.06
50.500	0.00	0.04	0.186	I	O	|	|	|	5.05
50.583	0.00	0.04	0.186	I	O	|	|	|	5.05
50.667	0.00	0.04	0.186	I	O	|	|	|	5.04
50.750	0.00	0.04	0.185	I	O	|	|	|	5.03
50.833	0.00	0.04	0.185	I	O	|	|	|	5.02
50.917	0.00	0.04	0.185	I	O	|	|	|	5.02
51.000	0.00	0.04	0.185	I	O	|	|	|	5.01
51.083	0.00	0.04	0.184	I	O	|	|	|	5.00
51.167	0.00	0.04	0.184	I	O	|	|	|	4.99
51.250	0.00	0.04	0.184	I	O	|	|	|	4.98
51.333	0.00	0.04	0.183	I	O	|	|	|	4.98
51.417	0.00	0.04	0.183	I	O	|	|	|	4.97
51.500	0.00	0.04	0.183	I	O	|	|	|	4.96
51.583	0.00	0.04	0.182	I	O	|	|	|	4.95
51.667	0.00	0.04	0.182	I	O	|	|	|	4.95
51.750	0.00	0.04	0.182	I	O	|	|	|	4.94
51.833	0.00	0.04	0.181	I	O	|	|	|	4.93
51.917	0.00	0.04	0.181	I	O	|	|	|	4.92
52.000	0.00	0.04	0.181	I	O	|	|	|	4.92
52.083	0.00	0.04	0.181	I	O	|	|	|	4.91
52.167	0.00	0.04	0.180	I	O	|	|	|	4.90
52.250	0.00	0.04	0.180	I	O	|	|	|	4.89
52.333	0.00	0.04	0.180	I	O	|	|	|	4.89

52.417	0.00	0.04	0.179	I O				4.88
52.500	0.00	0.04	0.179	I O				4.87
52.583	0.00	0.04	0.179	I O				4.86
52.667	0.00	0.04	0.178	I O				4.85
52.750	0.00	0.04	0.178	I O				4.85
52.833	0.00	0.04	0.178	I O				4.84
52.917	0.00	0.04	0.177	I O				4.83
53.000	0.00	0.04	0.177	I O				4.82
53.083	0.00	0.04	0.177	I O				4.82
53.167	0.00	0.04	0.177	I O				4.81
53.250	0.00	0.04	0.176	I O				4.80
53.333	0.00	0.04	0.176	I O				4.79
53.417	0.00	0.04	0.176	I O				4.79
53.500	0.00	0.04	0.175	I O				4.78
53.583	0.00	0.04	0.175	I O				4.77
53.667	0.00	0.04	0.175	I O				4.76
53.750	0.00	0.04	0.174	I O				4.76
53.833	0.00	0.04	0.174	I O				4.75
53.917	0.00	0.04	0.174	I O				4.74
54.000	0.00	0.04	0.173	I O				4.73
54.083	0.00	0.04	0.173	I O				4.72
54.167	0.00	0.04	0.173	I O				4.72
54.250	0.00	0.04	0.172	I O				4.71
54.333	0.00	0.04	0.172	I O				4.70
54.417	0.00	0.04	0.172	I O				4.69
54.500	0.00	0.04	0.172	I O				4.69
54.583	0.00	0.04	0.171	I O				4.68
54.667	0.00	0.04	0.171	I O				4.67
54.750	0.00	0.04	0.171	I O				4.66
54.833	0.00	0.04	0.170	I O				4.66
54.917	0.00	0.04	0.170	I O				4.65
55.000	0.00	0.04	0.170	I O				4.64
55.083	0.00	0.04	0.169	I O				4.63
55.167	0.00	0.04	0.169	I O				4.63
55.250	0.00	0.04	0.169	I O				4.62
55.333	0.00	0.04	0.168	I O				4.61
55.417	0.00	0.04	0.168	I O				4.60
55.500	0.00	0.04	0.168	I O				4.59
55.583	0.00	0.04	0.168	I O				4.59
55.667	0.00	0.04	0.167	I O				4.58
55.750	0.00	0.04	0.167	I O				4.57
55.833	0.00	0.04	0.167	I O				4.56
55.917	0.00	0.04	0.166	I O				4.56
56.000	0.00	0.04	0.166	I O				4.55
56.083	0.00	0.04	0.166	I O				4.54
56.167	0.00	0.04	0.165	I O				4.53
56.250	0.00	0.04	0.165	I O				4.53
56.333	0.00	0.04	0.165	I O				4.52
56.417	0.00	0.04	0.164	I O				4.51
56.500	0.00	0.04	0.164	I O				4.50

56.583	0.00	0.04	0.164	I	O	|	|	|	4.49
56.667	0.00	0.04	0.163	I	O	|	|	|	4.49
56.750	0.00	0.04	0.163	I	O	|	|	|	4.48
56.833	0.00	0.04	0.163	I	O	|	|	|	4.47
56.917	0.00	0.04	0.163	I	O	|	|	|	4.46
57.000	0.00	0.04	0.162	I	O	|	|	|	4.46
57.083	0.00	0.04	0.162	I	O	|	|	|	4.45
57.167	0.00	0.04	0.162	I	O	|	|	|	4.44
57.250	0.00	0.04	0.161	I	O	|	|	|	4.43
57.333	0.00	0.04	0.161	I	O	|	|	|	4.43
57.417	0.00	0.04	0.161	I	O	|	|	|	4.42
57.500	0.00	0.04	0.160	I	O	|	|	|	4.41
57.583	0.00	0.04	0.160	I	O	|	|	|	4.40
57.667	0.00	0.04	0.160	I	O	|	|	|	4.39
57.750	0.00	0.04	0.159	I	O	|	|	|	4.39
57.833	0.00	0.04	0.159	I	O	|	|	|	4.38
57.917	0.00	0.04	0.159	I	O	|	|	|	4.37
58.000	0.00	0.04	0.159	I	O	|	|	|	4.36
58.083	0.00	0.04	0.158	I	O	|	|	|	4.36
58.167	0.00	0.04	0.158	I	O	|	|	|	4.35
58.250	0.00	0.04	0.158	I	O	|	|	|	4.34
58.333	0.00	0.04	0.157	I	O	|	|	|	4.33
58.417	0.00	0.04	0.157	I	O	|	|	|	4.32
58.500	0.00	0.04	0.157	I	O	|	|	|	4.32
58.583	0.00	0.04	0.156	I	O	|	|	|	4.31
58.667	0.00	0.04	0.156	I	O	|	|	|	4.30
58.750	0.00	0.04	0.156	I	O	|	|	|	4.29
58.833	0.00	0.04	0.155	I	O	|	|	|	4.29
58.917	0.00	0.04	0.155	I	O	|	|	|	4.28
59.000	0.00	0.04	0.155	I	O	|	|	|	4.27
59.083	0.00	0.04	0.154	I	O	|	|	|	4.26
59.167	0.00	0.04	0.154	I	O	|	|	|	4.25
59.250	0.00	0.04	0.154	I	O	|	|	|	4.25
59.333	0.00	0.04	0.154	I	O	|	|	|	4.24
59.417	0.00	0.04	0.153	I	O	|	|	|	4.23
59.500	0.00	0.04	0.153	I	O	|	|	|	4.22
59.583	0.00	0.04	0.153	I	O	|	|	|	4.22
59.667	0.00	0.04	0.152	I	O	|	|	|	4.21
59.750	0.00	0.04	0.152	I	O	|	|	|	4.20
59.833	0.00	0.04	0.152	I	O	|	|	|	4.19
59.917	0.00	0.04	0.151	I	O	|	|	|	4.18
60.000	0.00	0.04	0.151	I	O	|	|	|	4.18
60.083	0.00	0.04	0.151	I	O	|	|	|	4.17
60.167	0.00	0.04	0.150	I	O	|	|	|	4.16
60.250	0.00	0.04	0.150	I	O	|	|	|	4.15
60.333	0.00	0.04	0.150	I	O	|	|	|	4.15
60.417	0.00	0.04	0.150	I	O	|	|	|	4.14
60.500	0.00	0.04	0.149	I	O	|	|	|	4.13
60.583	0.00	0.04	0.149	I	O	|	|	|	4.12
60.667	0.00	0.04	0.149	I	O	|	|	|	4.12

60.750	0.00	0.04	0.148	I O				4.11
60.833	0.00	0.04	0.148	I O				4.10
60.917	0.00	0.04	0.148	I O				4.09
61.000	0.00	0.04	0.147	I O				4.08
61.083	0.00	0.04	0.147	I O				4.08
61.167	0.00	0.04	0.147	I O				4.07
61.250	0.00	0.04	0.146	I O				4.06
61.333	0.00	0.04	0.146	I O				4.05
61.417	0.00	0.04	0.146	I O				4.05
61.500	0.00	0.04	0.146	I O				4.04
61.583	0.00	0.04	0.145	I O				4.03
61.667	0.00	0.04	0.145	I O				4.02
61.750	0.00	0.04	0.145	I O				4.01
61.833	0.00	0.04	0.144	I O				4.01
61.917	0.00	0.04	0.144	I O				4.00
62.000	0.00	0.04	0.144	I O				3.99
62.083	0.00	0.04	0.143	I O				3.98
62.167	0.00	0.04	0.143	I O				3.98
62.250	0.00	0.04	0.143	I O				3.97
62.333	0.00	0.04	0.142	I O				3.96
62.417	0.00	0.04	0.142	I O				3.95
62.500	0.00	0.04	0.142	I O				3.94
62.583	0.00	0.04	0.141	I O				3.94
62.667	0.00	0.04	0.141	I O				3.93
62.750	0.00	0.04	0.141	I O				3.92
62.833	0.00	0.04	0.141	I O				3.91
62.917	0.00	0.04	0.140	I O				3.91
63.000	0.00	0.04	0.140	I O				3.90
63.083	0.00	0.04	0.140	I O				3.89
63.167	0.00	0.04	0.139	I O				3.88
63.250	0.00	0.04	0.139	I O				3.88
63.333	0.00	0.04	0.139	I O				3.87
63.417	0.00	0.04	0.138	I O				3.86
63.500	0.00	0.04	0.138	I O				3.85
63.583	0.00	0.04	0.138	I O				3.84
63.667	0.00	0.04	0.137	I O				3.84
63.750	0.00	0.04	0.137	I O				3.83
63.833	0.00	0.04	0.137	I O				3.82
63.917	0.00	0.04	0.137	I O				3.81
64.000	0.00	0.04	0.136	I O				3.81
64.083	0.00	0.04	0.136	I O				3.80
64.167	0.00	0.04	0.136	I O				3.79
64.250	0.00	0.04	0.135	I O				3.78
64.333	0.00	0.04	0.135	I O				3.77
64.417	0.00	0.04	0.135	I O				3.77
64.500	0.00	0.04	0.134	I O				3.76
64.583	0.00	0.04	0.134	I O				3.75
64.667	0.00	0.04	0.134	I O				3.74
64.750	0.00	0.04	0.133	I O				3.74
64.833	0.00	0.04	0.133	I O				3.73

64.917	0.00	0.04	0.133	I	O	|	|	|	| 3.72
65.000	0.00	0.04	0.132	I	O	|	|	|	| 3.71
65.083	0.00	0.04	0.132	I	O	|	|	|	| 3.70
65.167	0.00	0.04	0.132	I	O	|	|	|	| 3.70
65.250	0.00	0.04	0.132	I	O	|	|	|	| 3.69
65.333	0.00	0.04	0.131	I	O	|	|	|	| 3.68
65.417	0.00	0.04	0.131	I	O	|	|	|	| 3.67
65.500	0.00	0.04	0.131	I	O	|	|	|	| 3.67
65.583	0.00	0.04	0.130	I	O	|	|	|	| 3.66
65.667	0.00	0.04	0.130	I	O	|	|	|	| 3.65
65.750	0.00	0.04	0.130	I	O	|	|	|	| 3.64
65.833	0.00	0.04	0.129	I	O	|	|	|	| 3.63
65.917	0.00	0.04	0.129	I	O	|	|	|	| 3.63
66.000	0.00	0.04	0.129	I	O	|	|	|	| 3.62
66.083	0.00	0.04	0.128	I	O	|	|	|	| 3.61
66.167	0.00	0.04	0.128	I	O	|	|	|	| 3.60
66.250	0.00	0.04	0.128	I	O	|	|	|	| 3.60
66.333	0.00	0.04	0.128	I	O	|	|	|	| 3.59
66.417	0.00	0.04	0.127	I	O	|	|	|	| 3.58
66.500	0.00	0.04	0.127	I	O	|	|	|	| 3.57
66.583	0.00	0.04	0.127	I	O	|	|	|	| 3.57
66.667	0.00	0.04	0.126	I	O	|	|	|	| 3.56
66.750	0.00	0.04	0.126	I	O	|	|	|	| 3.55
66.833	0.00	0.04	0.126	I	O	|	|	|	| 3.54
66.917	0.00	0.04	0.125	I	O	|	|	|	| 3.53
67.000	0.00	0.04	0.125	I	O	|	|	|	| 3.53
67.083	0.00	0.04	0.125	I	O	|	|	|	| 3.52
67.167	0.00	0.04	0.124	I	O	|	|	|	| 3.51
67.250	0.00	0.04	0.124	I	O	|	|	|	| 3.50
67.333	0.00	0.04	0.124	I	O	|	|	|	| 3.50
67.417	0.00	0.04	0.124	I	O	|	|	|	| 3.49
67.500	0.00	0.04	0.123	I	O	|	|	|	| 3.48
67.583	0.00	0.04	0.123	I	O	|	|	|	| 3.47
67.667	0.00	0.04	0.123	I	O	|	|	|	| 3.46
67.750	0.00	0.04	0.122	I	O	|	|	|	| 3.46
67.833	0.00	0.04	0.122	I	O	|	|	|	| 3.45
67.917	0.00	0.04	0.122	I	O	|	|	|	| 3.44
68.000	0.00	0.04	0.121	I	O	|	|	|	| 3.43
68.083	0.00	0.04	0.121	I	O	|	|	|	| 3.43
68.167	0.00	0.04	0.121	I	O	|	|	|	| 3.42
68.250	0.00	0.04	0.120	I	O	|	|	|	| 3.41
68.333	0.00	0.04	0.120	I	O	|	|	|	| 3.40
68.417	0.00	0.04	0.120	I	O	|	|	|	| 3.39
68.500	0.00	0.04	0.119	I	O	|	|	|	| 3.39
68.583	0.00	0.04	0.119	I	O	|	|	|	| 3.38
68.667	0.00	0.04	0.119	I	O	|	|	|	| 3.37
68.750	0.00	0.04	0.119	I	O	|	|	|	| 3.36
68.833	0.00	0.04	0.118	I	O	|	|	|	| 3.36
68.917	0.00	0.04	0.118	I	O	|	|	|	| 3.35
69.000	0.00	0.04	0.118	I	O	|	|	|	| 3.34

69.083	0.00	0.04	0.117	I	O	|	|	|	3.33
69.167	0.00	0.04	0.117	I	O	|	|	|	3.32
69.250	0.00	0.04	0.117	I	O	|	|	|	3.32
69.333	0.00	0.04	0.116	I	O	|	|	|	3.31
69.417	0.00	0.04	0.116	I	O	|	|	|	3.30
69.500	0.00	0.04	0.116	I	O	|	|	|	3.29
69.583	0.00	0.04	0.115	I	O	|	|	|	3.29
69.667	0.00	0.04	0.115	I	O	|	|	|	3.28
69.750	0.00	0.04	0.115	I	O	|	|	|	3.27
69.833	0.00	0.04	0.115	I	O	|	|	|	3.26
69.917	0.00	0.04	0.114	I	O	|	|	|	3.26
70.000	0.00	0.04	0.114	I	O	|	|	|	3.25
70.083	0.00	0.04	0.114	I	O	|	|	|	3.24
70.167	0.00	0.04	0.113	I	O	|	|	|	3.23
70.250	0.00	0.04	0.113	I	O	|	|	|	3.22
70.333	0.00	0.04	0.113	I	O	|	|	|	3.22
70.417	0.00	0.04	0.112	I	O	|	|	|	3.21
70.500	0.00	0.04	0.112	I	O	|	|	|	3.20
70.583	0.00	0.04	0.112	I	O	|	|	|	3.19
70.667	0.00	0.04	0.111	I	O	|	|	|	3.19
70.750	0.00	0.04	0.111	I	O	|	|	|	3.18
70.833	0.00	0.04	0.111	I	O	|	|	|	3.17
70.917	0.00	0.04	0.110	I	O	|	|	|	3.16
71.000	0.00	0.04	0.110	I	O	|	|	|	3.15
71.083	0.00	0.04	0.110	I	O	|	|	|	3.15
71.167	0.00	0.04	0.110	I	O	|	|	|	3.14
71.250	0.00	0.04	0.109	I	O	|	|	|	3.13
71.333	0.00	0.04	0.109	I	O	|	|	|	3.12
71.417	0.00	0.04	0.109	I	O	|	|	|	3.12
71.500	0.00	0.04	0.108	I	O	|	|	|	3.11
71.583	0.00	0.04	0.108	I	O	|	|	|	3.10
71.667	0.00	0.04	0.108	I	O	|	|	|	3.09
71.750	0.00	0.04	0.107	I	O	|	|	|	3.08
71.833	0.00	0.04	0.107	I	O	|	|	|	3.08
71.917	0.00	0.04	0.107	I	O	|	|	|	3.07
72.000	0.00	0.04	0.106	I	O	|	|	|	3.06
72.083	0.00	0.04	0.106	I	O	|	|	|	3.05
72.167	0.00	0.04	0.106	I	O	|	|	|	3.05
72.250	0.00	0.04	0.106	I	O	|	|	|	3.04
72.333	0.00	0.04	0.105	I	O	|	|	|	3.03
72.417	0.00	0.04	0.105	I	O	|	|	|	3.02
72.500	0.00	0.04	0.105	I	O	|	|	|	3.02
72.583	0.00	0.04	0.104	I	O	|	|	|	3.01
72.667	0.00	0.04	0.104	I	O	|	|	|	3.00
72.750	0.00	0.04	0.104	I	O	|	|	|	2.99
72.833	0.00	0.04	0.103	I	O	|	|	|	2.98
72.917	0.00	0.04	0.103	I	O	|	|	|	2.98
73.000	0.00	0.04	0.103	I	O	|	|	|	2.97
73.083	0.00	0.04	0.102	I	O	|	|	|	2.96
73.167	0.00	0.04	0.102	I	O	|	|	|	2.95

73.250	0.00	0.04	0.102	I O				2.95
73.333	0.00	0.04	0.102	I O				2.94
73.417	0.00	0.04	0.101	I O				2.93
73.500	0.00	0.04	0.101	I O				2.92
73.583	0.00	0.04	0.101	I O				2.91
73.667	0.00	0.04	0.100	I O				2.91
73.750	0.00	0.04	0.100	I O				2.90
73.833	0.00	0.04	0.100	I O				2.89
73.917	0.00	0.04	0.099	I O				2.88
74.000	0.00	0.04	0.099	I O				2.88
74.083	0.00	0.04	0.099	I O				2.87
74.167	0.00	0.04	0.098	I O				2.86
74.250	0.00	0.04	0.098	I O				2.85
74.333	0.00	0.04	0.098	I O				2.84
74.417	0.00	0.04	0.097	I O				2.84
74.500	0.00	0.04	0.097	I O				2.83
74.583	0.00	0.04	0.097	I O				2.82
74.667	0.00	0.04	0.097	I O				2.81
74.750	0.00	0.04	0.096	I O				2.81
74.833	0.00	0.04	0.096	I O				2.80
74.917	0.00	0.04	0.096	I O				2.79
75.000	0.00	0.04	0.095	I O				2.78
75.083	0.00	0.04	0.095	I O				2.77
75.167	0.00	0.04	0.095	I O				2.77
75.250	0.00	0.04	0.094	I O				2.76
75.333	0.00	0.04	0.094	I O				2.75
75.417	0.00	0.04	0.094	I O				2.74
75.500	0.00	0.04	0.093	I O				2.74
75.583	0.00	0.04	0.093	I O				2.73
75.667	0.00	0.04	0.093	I O				2.72
75.750	0.00	0.04	0.093	I O				2.71
75.833	0.00	0.04	0.092	I O				2.71
75.917	0.00	0.04	0.092	I O				2.70
76.000	0.00	0.04	0.092	I O				2.69
76.083	0.00	0.04	0.091	I O				2.68
76.167	0.00	0.04	0.091	I O				2.67
76.250	0.00	0.04	0.091	I O				2.67
76.333	0.00	0.04	0.090	I O				2.66
76.417	0.00	0.04	0.090	I O				2.65
76.500	0.00	0.04	0.090	I O				2.64
76.583	0.00	0.04	0.089	I O				2.64
76.667	0.00	0.04	0.089	I O				2.63
76.750	0.00	0.04	0.089	I O				2.62
76.833	0.00	0.04	0.088	I O				2.61
76.917	0.00	0.04	0.088	I O				2.60
77.000	0.00	0.04	0.088	I O				2.60
77.083	0.00	0.04	0.088	I O				2.59
77.167	0.00	0.04	0.087	I O				2.58
77.250	0.00	0.04	0.087	I O				2.57
77.333	0.00	0.04	0.087	I O				2.57

77.417	0.00	0.04	0.086	I	O	|	|	|	2.56
77.500	0.00	0.04	0.086	I	O	|	|	|	2.55
77.583	0.00	0.04	0.086	I	O	|	|	|	2.54
77.667	0.00	0.04	0.085	I	O	|	|	|	2.53
77.750	0.00	0.04	0.085	I	O	|	|	|	2.53
77.833	0.00	0.04	0.085	I	O	|	|	|	2.52
77.917	0.00	0.04	0.084	I	O	|	|	|	2.51
78.000	0.00	0.04	0.084	I	O	|	|	|	2.50
78.083	0.00	0.04	0.084	I	O	|	|	|	2.50
78.167	0.00	0.04	0.084	I	O	|	|	|	2.49
78.250	0.00	0.04	0.083	I	O	|	|	|	2.48
78.333	0.00	0.04	0.083	I	O	|	|	|	2.47
78.417	0.00	0.04	0.083	I	O	|	|	|	2.46
78.500	0.00	0.04	0.082	I	O	|	|	|	2.46
78.583	0.00	0.04	0.082	I	O	|	|	|	2.45
78.667	0.00	0.04	0.082	I	O	|	|	|	2.44
78.750	0.00	0.04	0.081	I	O	|	|	|	2.43
78.833	0.00	0.04	0.081	I	O	|	|	|	2.43
78.917	0.00	0.04	0.081	I	O	|	|	|	2.42
79.000	0.00	0.04	0.080	I	O	|	|	|	2.41
79.083	0.00	0.04	0.080	I	O	|	|	|	2.40
79.167	0.00	0.04	0.080	I	O	|	|	|	2.40
79.250	0.00	0.04	0.079	I	O	|	|	|	2.39
79.333	0.00	0.04	0.079	I	O	|	|	|	2.38
79.417	0.00	0.04	0.079	I	O	|	|	|	2.37
79.500	0.00	0.04	0.079	I	O	|	|	|	2.36
79.583	0.00	0.04	0.078	I	O	|	|	|	2.36
79.667	0.00	0.04	0.078	I	O	|	|	|	2.35
79.750	0.00	0.04	0.078	I	O	|	|	|	2.34
79.833	0.00	0.04	0.077	I	O	|	|	|	2.33
79.917	0.00	0.04	0.077	I	O	|	|	|	2.33
80.000	0.00	0.04	0.077	I	O	|	|	|	2.32
80.083	0.00	0.04	0.076	I	O	|	|	|	2.31
80.167	0.00	0.04	0.076	I	O	|	|	|	2.30
80.250	0.00	0.04	0.076	I	O	|	|	|	2.29
80.333	0.00	0.04	0.075	I	O	|	|	|	2.29
80.417	0.00	0.04	0.075	I	O	|	|	|	2.28
80.500	0.00	0.04	0.075	I	O	|	|	|	2.27
80.583	0.00	0.04	0.075	I	O	|	|	|	2.26
80.667	0.00	0.04	0.074	I	O	|	|	|	2.26
80.750	0.00	0.04	0.074	I	O	|	|	|	2.25
80.833	0.00	0.04	0.074	I	O	|	|	|	2.24
80.917	0.00	0.04	0.073	I	O	|	|	|	2.23
81.000	0.00	0.04	0.073	I	O	|	|	|	2.22
81.083	0.00	0.04	0.073	I	O	|	|	|	2.22
81.167	0.00	0.04	0.072	I	O	|	|	|	2.21
81.250	0.00	0.04	0.072	I	O	|	|	|	2.20
81.333	0.00	0.04	0.072	I	O	|	|	|	2.19
81.417	0.00	0.04	0.071	I	O	|	|	|	2.19
81.500	0.00	0.04	0.071	I	O	|	|	|	2.18

81.583	0.00	0.04	0.071	I	O	|	|	|	|	2.17
81.667	0.00	0.04	0.071	I	O	|	|	|	|	2.16
81.750	0.00	0.04	0.070	I	O	|	|	|	|	2.15
81.833	0.00	0.04	0.070	I	O	|	|	|	|	2.15
81.917	0.00	0.04	0.070	I	O	|	|	|	|	2.14
82.000	0.00	0.04	0.069	I	O	|	|	|	|	2.13
82.083	0.00	0.04	0.069	I	O	|	|	|	|	2.12
82.167	0.00	0.04	0.069	I	O	|	|	|	|	2.12
82.250	0.00	0.04	0.068	I	O	|	|	|	|	2.11
82.333	0.00	0.04	0.068	I	O	|	|	|	|	2.10
82.417	0.00	0.04	0.068	I	O	|	|	|	|	2.09
82.500	0.00	0.04	0.067	I	O	|	|	|	|	2.09
82.583	0.00	0.04	0.067	I	O	|	|	|	|	2.08
82.667	0.00	0.04	0.067	I	O	|	|	|	|	2.07
82.750	0.00	0.04	0.066	I	O	|	|	|	|	2.06
82.833	0.00	0.04	0.066	I	O	|	|	|	|	2.05
82.917	0.00	0.04	0.066	I	O	|	|	|	|	2.05
83.000	0.00	0.04	0.066	I	O	|	|	|	|	2.04
83.083	0.00	0.04	0.065	I	O	|	|	|	|	2.03
83.167	0.00	0.04	0.065	I	O	|	|	|	|	2.02
83.250	0.00	0.04	0.065	I	O	|	|	|	|	2.02
83.333	0.00	0.04	0.064	I	O	|	|	|	|	2.01
83.417	0.00	0.04	0.064	I	O	|	|	|	|	2.00
83.500	0.00	0.04	0.064	I	O	|	|	|	|	1.99
83.583	0.00	0.04	0.063	I	O	|	|	|	|	1.98
83.667	0.00	0.04	0.063	I	O	|	|	|	|	1.98
83.750	0.00	0.04	0.063	I	O	|	|	|	|	1.97
83.833	0.00	0.04	0.062	I	O	|	|	|	|	1.96
83.917	0.00	0.04	0.062	I	O	|	|	|	|	1.95
84.000	0.00	0.04	0.062	I	O	|	|	|	|	1.95
84.083	0.00	0.04	0.062	I	O	|	|	|	|	1.94
84.167	0.00	0.04	0.061	I	O	|	|	|	|	1.93
84.250	0.00	0.04	0.061	I	O	|	|	|	|	1.92
84.333	0.00	0.04	0.061	I	O	|	|	|	|	1.91
84.417	0.00	0.04	0.060	I	O	|	|	|	|	1.91
84.500	0.00	0.04	0.060	I	O	|	|	|	|	1.90
84.583	0.00	0.04	0.060	I	O	|	|	|	|	1.89
84.667	0.00	0.04	0.059	I	O	|	|	|	|	1.88
84.750	0.00	0.04	0.059	I	O	|	|	|	|	1.88
84.833	0.00	0.04	0.059	I	O	|	|	|	|	1.87
84.917	0.00	0.04	0.058	I	O	|	|	|	|	1.86
85.000	0.00	0.04	0.058	I	O	|	|	|	|	1.85
85.083	0.00	0.04	0.058	I	O	|	|	|	|	1.85
85.167	0.00	0.04	0.057	I	O	|	|	|	|	1.84
85.250	0.00	0.04	0.057	I	O	|	|	|	|	1.83
85.333	0.00	0.04	0.057	I	O	|	|	|	|	1.82
85.417	0.00	0.04	0.057	I	O	|	|	|	|	1.81
85.500	0.00	0.04	0.056	I	O	|	|	|	|	1.81
85.583	0.00	0.04	0.056	I	O	|	|	|	|	1.80
85.667	0.00	0.04	0.056	I	O	|	|	|	|	1.79

85.750	0.00	0.04	0.055	I	O	|	|	|	1.78
85.833	0.00	0.04	0.055	I	O	|	|	|	1.78
85.917	0.00	0.04	0.055	I	O	|	|	|	1.77
86.000	0.00	0.04	0.054	I	O	|	|	|	1.76
86.083	0.00	0.04	0.054	I	O	|	|	|	1.75
86.167	0.00	0.04	0.054	I	O	|	|	|	1.74
86.250	0.00	0.04	0.053	I	O	|	|	|	1.74
86.333	0.00	0.04	0.053	I	O	|	|	|	1.73
86.417	0.00	0.04	0.053	I	O	|	|	|	1.72
86.500	0.00	0.04	0.053	I	O	|	|	|	1.71
86.583	0.00	0.04	0.052	I	O	|	|	|	1.71
86.667	0.00	0.04	0.052	I	O	|	|	|	1.70
86.750	0.00	0.04	0.052	I	O	|	|	|	1.69
86.833	0.00	0.04	0.051	I	O	|	|	|	1.68
86.917	0.00	0.04	0.051	I	O	|	|	|	1.67
87.000	0.00	0.04	0.051	I	O	|	|	|	1.67
87.083	0.00	0.04	0.050	I	O	|	|	|	1.66
87.167	0.00	0.04	0.050	I	O	|	|	|	1.65
87.250	0.00	0.04	0.050	I	O	|	|	|	1.64
87.333	0.00	0.04	0.049	I	O	|	|	|	1.64
87.417	0.00	0.04	0.049	I	O	|	|	|	1.63
87.500	0.00	0.04	0.049	I	O	|	|	|	1.62
87.583	0.00	0.04	0.049	I	O	|	|	|	1.61
87.667	0.00	0.04	0.048	I	O	|	|	|	1.60
87.750	0.00	0.04	0.048	I	O	|	|	|	1.60
87.833	0.00	0.04	0.048	I	O	|	|	|	1.59
87.917	0.00	0.04	0.047	I	O	|	|	|	1.58
88.000	0.00	0.04	0.047	I	O	|	|	|	1.57
88.083	0.00	0.04	0.047	I	O	|	|	|	1.57
88.167	0.00	0.04	0.046	I	O	|	|	|	1.56
88.250	0.00	0.04	0.046	I	O	|	|	|	1.55
88.333	0.00	0.04	0.046	I	O	|	|	|	1.54
88.417	0.00	0.04	0.045	I	O	|	|	|	1.54
88.500	0.00	0.04	0.045	I	O	|	|	|	1.53
88.583	0.00	0.04	0.045	I	O	|	|	|	1.52
88.667	0.00	0.04	0.044	I	O	|	|	|	1.51
88.750	0.00	0.04	0.044	I	O	|	|	|	1.50
88.833	0.00	0.04	0.044	I	O	|	|	|	1.50
88.917	0.00	0.04	0.044	I	O	|	|	|	1.49
89.000	0.00	0.04	0.043	I	O	|	|	|	1.48
89.083	0.00	0.04	0.043	I	O	|	|	|	1.47
89.167	0.00	0.04	0.043	I	O	|	|	|	1.47
89.250	0.00	0.04	0.042	I	O	|	|	|	1.46
89.333	0.00	0.04	0.042	I	O	|	|	|	1.45
89.417	0.00	0.04	0.042	I	O	|	|	|	1.44
89.500	0.00	0.04	0.041	I	O	|	|	|	1.43
89.583	0.00	0.04	0.041	I	O	|	|	|	1.43
89.667	0.00	0.04	0.041	I	O	|	|	|	1.42
89.750	0.00	0.04	0.040	I	O	|	|	|	1.41
89.833	0.00	0.04	0.040	I	O	|	|	|	1.40

89.917	0.00	0.04	0.040	I O				1.40
90.000	0.00	0.04	0.040	I O				1.39
90.083	0.00	0.04	0.039	I O				1.38
90.167	0.00	0.04	0.039	I O				1.37
90.250	0.00	0.04	0.039	I O				1.36
90.333	0.00	0.04	0.038	I O				1.36
90.417	0.00	0.04	0.038	I O				1.35
90.500	0.00	0.04	0.038	I O				1.34
90.583	0.00	0.04	0.037	I O				1.33
90.667	0.00	0.04	0.037	I O				1.33
90.750	0.00	0.04	0.037	I O				1.32
90.833	0.00	0.04	0.036	I O				1.31
90.917	0.00	0.04	0.036	I O				1.30
91.000	0.00	0.04	0.036	I O				1.29
91.083	0.00	0.04	0.035	I O				1.29
91.167	0.00	0.04	0.035	I O				1.28
91.250	0.00	0.04	0.035	I O				1.27
91.333	0.00	0.04	0.035	I O				1.26
91.417	0.00	0.04	0.034	I O				1.26
91.500	0.00	0.04	0.034	I O				1.25
91.583	0.00	0.04	0.034	I O				1.24
91.667	0.00	0.04	0.033	I O				1.23
91.750	0.00	0.04	0.033	I O				1.23
91.833	0.00	0.04	0.033	I O				1.22
91.917	0.00	0.04	0.032	I O				1.21
92.000	0.00	0.04	0.032	I O				1.20
92.083	0.00	0.04	0.032	I O				1.19
92.167	0.00	0.04	0.031	I O				1.19
92.250	0.00	0.04	0.031	I O				1.18
92.333	0.00	0.04	0.031	I O				1.17
92.417	0.00	0.04	0.031	I O				1.16
92.500	0.00	0.04	0.030	I O				1.16
92.583	0.00	0.04	0.030	I O				1.15
92.667	0.00	0.04	0.030	I O				1.14
92.750	0.00	0.04	0.029	I O				1.13
92.833	0.00	0.04	0.029	I O				1.12
92.917	0.00	0.04	0.029	I O				1.12
93.000	0.00	0.04	0.028	I O				1.11
93.083	0.00	0.04	0.028	I O				1.10
93.167	0.00	0.04	0.028	I O				1.09
93.250	0.00	0.04	0.027	I O				1.09
93.333	0.00	0.04	0.027	I O				1.08
93.417	0.00	0.04	0.027	I O				1.07
93.500	0.00	0.04	0.027	I O				1.06
93.583	0.00	0.04	0.026	I O				1.05
93.667	0.00	0.04	0.026	I O				1.05
93.750	0.00	0.04	0.026	I O				1.04
93.833	0.00	0.04	0.025	I O				1.03
93.917	0.00	0.04	0.025	I O				1.02
94.000	0.00	0.04	0.025	I O				1.02

94.083	0.00	0.04	0.024	I O				1.01
94.167	0.00	0.04	0.024	I O				1.00
94.250	0.00	0.04	0.024	I O				0.99
94.333	0.00	0.04	0.023	I O				0.98
94.417	0.00	0.04	0.023	I O				0.96
94.500	0.00	0.04	0.023	I O				0.95
94.583	0.00	0.04	0.023	I O				0.94
94.667	0.00	0.04	0.022	I O				0.93
94.750	0.00	0.04	0.022	I O				0.91
94.833	0.00	0.04	0.022	I O				0.90
94.917	0.00	0.04	0.021	I O				0.89
95.000	0.00	0.04	0.021	I O				0.88
95.083	0.00	0.04	0.021	I O				0.87
95.167	0.00	0.04	0.021	I O				0.86
95.250	0.00	0.04	0.020	I O				0.85
95.333	0.00	0.04	0.020	I O				0.84
95.417	0.00	0.04	0.020	IO				0.82
95.500	0.00	0.04	0.020	IO				0.81
95.583	0.00	0.04	0.019	IO				0.80
95.667	0.00	0.04	0.019	IO				0.79
95.750	0.00	0.04	0.019	IO				0.78
95.833	0.00	0.03	0.019	IO				0.77
95.917	0.00	0.03	0.018	IO				0.76
96.000	0.00	0.03	0.018	IO				0.75
96.083	0.00	0.03	0.018	IO				0.74
96.167	0.00	0.03	0.018	IO				0.73
96.250	0.00	0.03	0.017	IO				0.72
96.333	0.00	0.03	0.017	IO				0.72
96.417	0.00	0.03	0.017	IO				0.71
96.500	0.00	0.03	0.017	IO				0.70
96.583	0.00	0.03	0.017	IO				0.69
96.667	0.00	0.03	0.016	IO				0.68
96.750	0.00	0.03	0.016	IO				0.67
96.833	0.00	0.03	0.016	IO				0.66
96.917	0.00	0.03	0.016	IO				0.65
97.000	0.00	0.03	0.015	IO				0.65
97.083	0.00	0.03	0.015	IO				0.64
97.167	0.00	0.03	0.015	IO				0.63
97.250	0.00	0.03	0.015	IO				0.62
97.333	0.00	0.03	0.015	IO				0.61
97.417	0.00	0.03	0.015	IO				0.60
97.500	0.00	0.03	0.014	IO				0.60
97.583	0.00	0.03	0.014	IO				0.59
97.667	0.00	0.03	0.014	IO				0.58
97.750	0.00	0.03	0.014	IO				0.57
97.833	0.00	0.03	0.014	IO				0.57
97.917	0.00	0.03	0.013	IO				0.56
98.000	0.00	0.02	0.013	IO				0.55
98.083	0.00	0.02	0.013	IO				0.55
98.167	0.00	0.02	0.013	IO				0.54

98.250	0.00	0.02	0.013	IO				0.53
98.333	0.00	0.02	0.013	IO				0.52
98.417	0.00	0.02	0.012	IO				0.52
98.500	0.00	0.02	0.012	IO				0.51
98.583	0.00	0.02	0.012	IO				0.50
98.667	0.00	0.02	0.012	IO				0.50
98.750	0.00	0.02	0.012	IO				0.49
98.833	0.00	0.02	0.012	IO				0.49
98.917	0.00	0.02	0.012	IO				0.48
99.000	0.00	0.02	0.011	IO				0.47
99.083	0.00	0.02	0.011	IO				0.47
99.167	0.00	0.02	0.011	IO				0.46
99.250	0.00	0.02	0.011	IO				0.46
99.333	0.00	0.02	0.011	IO				0.45
99.417	0.00	0.02	0.011	IO				0.44
99.500	0.00	0.02	0.011	IO				0.44
99.583	0.00	0.02	0.010	IO				0.43
99.667	0.00	0.02	0.010	IO				0.43
99.750	0.00	0.02	0.010	IO				0.42
99.833	0.00	0.02	0.010	IO				0.42
99.917	0.00	0.02	0.010	O				0.41
100.000	0.00	0.02	0.010	O				0.41
100.083	0.00	0.02	0.010	O				0.40
100.167	0.00	0.02	0.009	O				0.40
100.250	0.00	0.02	0.009	O				0.39
100.333	0.00	0.02	0.009	O				0.38
100.417	0.00	0.02	0.009	O				0.38
100.500	0.00	0.02	0.009	O				0.38
100.583	0.00	0.02	0.009	O				0.37
100.667	0.00	0.02	0.009	O				0.37
100.750	0.00	0.02	0.009	O				0.36
100.833	0.00	0.02	0.009	O				0.36
100.917	0.00	0.02	0.008	O				0.35
101.000	0.00	0.02	0.008	O				0.35
101.083	0.00	0.02	0.008	O				0.34
101.167	0.00	0.02	0.008	O				0.34
101.250	0.00	0.02	0.008	O				0.33
101.333	0.00	0.01	0.008	O				0.33
101.417	0.00	0.01	0.008	O				0.33
101.500	0.00	0.01	0.008	O				0.32
101.583	0.00	0.01	0.008	O				0.32
101.667	0.00	0.01	0.008	O				0.31
101.750	0.00	0.01	0.007	O				0.31
101.833	0.00	0.01	0.007	O				0.31
101.917	0.00	0.01	0.007	O				0.30
102.000	0.00	0.01	0.007	O				0.30
102.083	0.00	0.01	0.007	O				0.29
102.167	0.00	0.01	0.007	O				0.29
102.250	0.00	0.01	0.007	O				0.29
102.333	0.00	0.01	0.007	O				0.28

102.417	0.00	0.01	0.007	O	|	|	|	0.28
102.500	0.00	0.01	0.007	O	|	|	|	0.28
102.583	0.00	0.01	0.007	O	|	|	|	0.27
102.667	0.00	0.01	0.006	O	|	|	|	0.27
102.750	0.00	0.01	0.006	O	|	|	|	0.26
102.833	0.00	0.01	0.006	O	|	|	|	0.26
102.917	0.00	0.01	0.006	O	|	|	|	0.26
103.000	0.00	0.01	0.006	O	|	|	|	0.25
103.083	0.00	0.01	0.006	O	|	|	|	0.25
103.167	0.00	0.01	0.006	O	|	|	|	0.25
103.250	0.00	0.01	0.006	O	|	|	|	0.24
103.333	0.00	0.01	0.006	O	|	|	|	0.24
103.417	0.00	0.01	0.006	O	|	|	|	0.24
103.500	0.00	0.01	0.006	O	|	|	|	0.24
103.583	0.00	0.01	0.006	O	|	|	|	0.23
103.667	0.00	0.01	0.006	O	|	|	|	0.23
103.750	0.00	0.01	0.005	O	|	|	|	0.23
103.833	0.00	0.01	0.005	O	|	|	|	0.22
103.917	0.00	0.01	0.005	O	|	|	|	0.22
104.000	0.00	0.01	0.005	O	|	|	|	0.22
104.083	0.00	0.01	0.005	O	|	|	|	0.22
104.167	0.00	0.01	0.005	O	|	|	|	0.21
104.250	0.00	0.01	0.005	O	|	|	|	0.21
104.333	0.00	0.01	0.005	O	|	|	|	0.21
104.417	0.00	0.01	0.005	O	|	|	|	0.20
104.500	0.00	0.01	0.005	O	|	|	|	0.20
104.583	0.00	0.01	0.005	O	|	|	|	0.20
104.667	0.00	0.01	0.005	O	|	|	|	0.20
104.750	0.00	0.01	0.005	O	|	|	|	0.19
104.833	0.00	0.01	0.005	O	|	|	|	0.19
104.917	0.00	0.01	0.005	O	|	|	|	0.19
105.000	0.00	0.01	0.004	O	|	|	|	0.19
105.083	0.00	0.01	0.004	O	|	|	|	0.18
105.167	0.00	0.01	0.004	O	|	|	|	0.18
105.250	0.00	0.01	0.004	O	|	|	|	0.18
105.333	0.00	0.01	0.004	O	|	|	|	0.18
105.417	0.00	0.01	0.004	O	|	|	|	0.18
105.500	0.00	0.01	0.004	O	|	|	|	0.17
105.583	0.00	0.01	0.004	O	|	|	|	0.17
105.667	0.00	0.01	0.004	O	|	|	|	0.17
105.750	0.00	0.01	0.004	O	|	|	|	0.17
105.833	0.00	0.01	0.004	O	|	|	|	0.16
105.917	0.00	0.01	0.004	O	|	|	|	0.16
106.000	0.00	0.01	0.004	O	|	|	|	0.16
106.083	0.00	0.01	0.004	O	|	|	|	0.16
106.167	0.00	0.01	0.004	O	|	|	|	0.16
106.250	0.00	0.01	0.004	O	|	|	|	0.15
106.333	0.00	0.01	0.004	O	|	|	|	0.15
106.417	0.00	0.01	0.004	O	|	|	|	0.15
106.500	0.00	0.01	0.004	O	|	|	|	0.15

106.583	0.00	0.01	0.004	O	|	|	|	0.15
106.667	0.00	0.01	0.003	O	|	|	|	0.14
106.750	0.00	0.01	0.003	O	|	|	|	0.14
106.833	0.00	0.01	0.003	O	|	|	|	0.14
106.917	0.00	0.01	0.003	O	|	|	|	0.14
107.000	0.00	0.01	0.003	O	|	|	|	0.14
107.083	0.00	0.01	0.003	O	|	|	|	0.14
107.167	0.00	0.01	0.003	O	|	|	|	0.13
107.250	0.00	0.01	0.003	O	|	|	|	0.13
107.333	0.00	0.01	0.003	O	|	|	|	0.13
107.417	0.00	0.01	0.003	O	|	|	|	0.13
107.500	0.00	0.01	0.003	O	|	|	|	0.13
107.583	0.00	0.01	0.003	O	|	|	|	0.13
107.667	0.00	0.01	0.003	O	|	|	|	0.12
107.750	0.00	0.01	0.003	O	|	|	|	0.12
107.833	0.00	0.01	0.003	O	|	|	|	0.12
107.917	0.00	0.01	0.003	O	|	|	|	0.12
108.000	0.00	0.01	0.003	O	|	|	|	0.12
108.083	0.00	0.01	0.003	O	|	|	|	0.12
108.167	0.00	0.01	0.003	O	|	|	|	0.11
108.250	0.00	0.01	0.003	O	|	|	|	0.11
108.333	0.00	0.01	0.003	O	|	|	|	0.11
108.417	0.00	0.00	0.003	O	|	|	|	0.11
108.500	0.00	0.00	0.003	O	|	|	|	0.11
108.583	0.00	0.00	0.003	O	|	|	|	0.11
108.667	0.00	0.00	0.003	O	|	|	|	0.11
108.750	0.00	0.00	0.003	O	|	|	|	0.10
108.833	0.00	0.00	0.002	O	|	|	|	0.10
108.917	0.00	0.00	0.002	O	|	|	|	0.10
109.000	0.00	0.00	0.002	O	|	|	|	0.10
109.083	0.00	0.00	0.002	O	|	|	|	0.10
109.167	0.00	0.00	0.002	O	|	|	|	0.10
109.250	0.00	0.00	0.002	O	|	|	|	0.10
109.333	0.00	0.00	0.002	O	|	|	|	0.10
109.417	0.00	0.00	0.002	O	|	|	|	0.09
109.500	0.00	0.00	0.002	O	|	|	|	0.09
109.583	0.00	0.00	0.002	O	|	|	|	0.09
109.667	0.00	0.00	0.002	O	|	|	|	0.09
109.750	0.00	0.00	0.002	O	|	|	|	0.09
109.833	0.00	0.00	0.002	O	|	|	|	0.09
109.917	0.00	0.00	0.002	O	|	|	|	0.09
110.000	0.00	0.00	0.002	O	|	|	|	0.09
110.083	0.00	0.00	0.002	O	|	|	|	0.08
110.167	0.00	0.00	0.002	O	|	|	|	0.08
110.250	0.00	0.00	0.002	O	|	|	|	0.08
110.333	0.00	0.00	0.002	O	|	|	|	0.08
110.417	0.00	0.00	0.002	O	|	|	|	0.08
110.500	0.00	0.00	0.002	O	|	|	|	0.08
110.583	0.00	0.00	0.002	O	|	|	|	0.08
110.667	0.00	0.00	0.002	O	|	|	|	0.08

110.750	0.00	0.00	0.002	O	|	|	|	0.08
110.833	0.00	0.00	0.002	O	|	|	|	0.08
110.917	0.00	0.00	0.002	O	|	|	|	0.07
111.000	0.00	0.00	0.002	O	|	|	|	0.07
111.083	0.00	0.00	0.002	O	|	|	|	0.07
111.167	0.00	0.00	0.002	O	|	|	|	0.07
111.250	0.00	0.00	0.002	O	|	|	|	0.07
111.333	0.00	0.00	0.002	O	|	|	|	0.07
111.417	0.00	0.00	0.002	O	|	|	|	0.07
111.500	0.00	0.00	0.002	O	|	|	|	0.07
111.583	0.00	0.00	0.002	O	|	|	|	0.07
111.667	0.00	0.00	0.002	O	|	|	|	0.07
111.750	0.00	0.00	0.002	O	|	|	|	0.07
111.833	0.00	0.00	0.002	O	|	|	|	0.06
111.917	0.00	0.00	0.002	O	|	|	|	0.06
112.000	0.00	0.00	0.002	O	|	|	|	0.06
112.083	0.00	0.00	0.001	O	|	|	|	0.06
112.167	0.00	0.00	0.001	O	|	|	|	0.06
112.250	0.00	0.00	0.001	O	|	|	|	0.06
112.333	0.00	0.00	0.001	O	|	|	|	0.06
112.417	0.00	0.00	0.001	O	|	|	|	0.06
112.500	0.00	0.00	0.001	O	|	|	|	0.06
112.583	0.00	0.00	0.001	O	|	|	|	0.06
112.667	0.00	0.00	0.001	O	|	|	|	0.06
112.750	0.00	0.00	0.001	O	|	|	|	0.06
112.833	0.00	0.00	0.001	O	|	|	|	0.06
112.917	0.00	0.00	0.001	O	|	|	|	0.05
113.000	0.00	0.00	0.001	O	|	|	|	0.05
113.083	0.00	0.00	0.001	O	|	|	|	0.05
113.167	0.00	0.00	0.001	O	|	|	|	0.05
113.250	0.00	0.00	0.001	O	|	|	|	0.05
113.333	0.00	0.00	0.001	O	|	|	|	0.05
113.417	0.00	0.00	0.001	O	|	|	|	0.05
113.500	0.00	0.00	0.001	O	|	|	|	0.05
113.583	0.00	0.00	0.001	O	|	|	|	0.05
113.667	0.00	0.00	0.001	O	|	|	|	0.05
113.750	0.00	0.00	0.001	O	|	|	|	0.05
113.833	0.00	0.00	0.001	O	|	|	|	0.05
113.917	0.00	0.00	0.001	O	|	|	|	0.05
114.000	0.00	0.00	0.001	O	|	|	|	0.05
114.083	0.00	0.00	0.001	O	|	|	|	0.05
114.167	0.00	0.00	0.001	O	|	|	|	0.05
114.250	0.00	0.00	0.001	O	|	|	|	0.04
114.333	0.00	0.00	0.001	O	|	|	|	0.04
114.417	0.00	0.00	0.001	O	|	|	|	0.04
114.500	0.00	0.00	0.001	O	|	|	|	0.04
114.583	0.00	0.00	0.001	O	|	|	|	0.04
114.667	0.00	0.00	0.001	O	|	|	|	0.04
114.750	0.00	0.00	0.001	O	|	|	|	0.04
114.833	0.00	0.00	0.001	O	|	|	|	0.04

114.917	0.00	0.00	0.001	O	|	|	|	0.04
115.000	0.00	0.00	0.001	O	|	|	|	0.04
115.083	0.00	0.00	0.001	O	|	|	|	0.04
115.167	0.00	0.00	0.001	O	|	|	|	0.04
115.250	0.00	0.00	0.001	O	|	|	|	0.04
115.333	0.00	0.00	0.001	O	|	|	|	0.04
115.417	0.00	0.00	0.001	O	|	|	|	0.04
115.500	0.00	0.00	0.001	O	|	|	|	0.04
115.583	0.00	0.00	0.001	O	|	|	|	0.04
115.667	0.00	0.00	0.001	O	|	|	|	0.04
115.750	0.00	0.00	0.001	O	|	|	|	0.04
115.833	0.00	0.00	0.001	O	|	|	|	0.03
115.917	0.00	0.00	0.001	O	|	|	|	0.03
116.000	0.00	0.00	0.001	O	|	|	|	0.03
116.083	0.00	0.00	0.001	O	|	|	|	0.03
116.167	0.00	0.00	0.001	O	|	|	|	0.03
116.250	0.00	0.00	0.001	O	|	|	|	0.03
116.333	0.00	0.00	0.001	O	|	|	|	0.03
116.417	0.00	0.00	0.001	O	|	|	|	0.03
116.500	0.00	0.00	0.001	O	|	|	|	0.03
116.583	0.00	0.00	0.001	O	|	|	|	0.03
116.667	0.00	0.00	0.001	O	|	|	|	0.03
116.750	0.00	0.00	0.001	O	|	|	|	0.03
116.833	0.00	0.00	0.001	O	|	|	|	0.03
116.917	0.00	0.00	0.001	O	|	|	|	0.03
117.000	0.00	0.00	0.001	O	|	|	|	0.03
117.083	0.00	0.00	0.001	O	|	|	|	0.03
117.167	0.00	0.00	0.001	O	|	|	|	0.03
117.250	0.00	0.00	0.001	O	|	|	|	0.03
117.333	0.00	0.00	0.001	O	|	|	|	0.03
117.417	0.00	0.00	0.001	O	|	|	|	0.03
117.500	0.00	0.00	0.001	O	|	|	|	0.03
117.583	0.00	0.00	0.001	O	|	|	|	0.03
117.667	0.00	0.00	0.001	O	|	|	|	0.03
117.750	0.00	0.00	0.001	O	|	|	|	0.03
117.833	0.00	0.00	0.001	O	|	|	|	0.03
117.917	0.00	0.00	0.001	O	|	|	|	0.03
118.000	0.00	0.00	0.001	O	|	|	|	0.02
118.083	0.00	0.00	0.001	O	|	|	|	0.02
118.167	0.00	0.00	0.001	O	|	|	|	0.02
118.250	0.00	0.00	0.001	O	|	|	|	0.02
118.333	0.00	0.00	0.001	O	|	|	|	0.02
118.417	0.00	0.00	0.001	O	|	|	|	0.02
118.500	0.00	0.00	0.001	O	|	|	|	0.02
118.583	0.00	0.00	0.001	O	|	|	|	0.02
118.667	0.00	0.00	0.001	O	|	|	|	0.02
118.750	0.00	0.00	0.001	O	|	|	|	0.02

**********HYDROGRAPH DATA**********

Number of intervals = 1425

```
                Time interval =    5.0 (Min.)
                Maximum/Peak flow rate =        0.045 (CFS)
                Total volume =       0.363 (Ac.Ft)
        Status of hydrographs being held in storage
                    Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
        Peak (CFS)      0.000     0.000     0.000     0.000     0.000
        Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
****************************************************************************

----------------------------------------------------------------------
```

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
100 yr
1 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris1100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 20
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 4.607 (CFS)
Total volume = 0.164 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 20
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.2 2.30 3.46 4.61	Depth (Ft.)
0.083	0.16	0.00	0.001	OI	0.02
0.167	0.61	0.01	0.003	O I	0.13
0.250	0.80	0.01	0.008	O I	0.33
0.333	0.96	0.03	0.014	O I	0.58
0.417	1.07	0.04	0.021	O I	0.86
0.500	1.24	0.04	0.028	O I	1.11
0.583	1.42	0.04	0.037	O I	1.33
0.667	1.65	0.04	0.047	O I	1.59
0.750	2.04	0.04	0.060	O I	1.90
0.833	3.36	0.04	0.078	O I	2.35
0.917	4.61	0.04	0.105	O I	3.03
1.000	2.56	0.04	0.130	O I	3.64
1.083	1.57	0.04	0.144	O I	3.99
1.167	0.75	0.04	0.151	O I	4.18
1.250	0.43	0.04	0.155	O I	4.28
1.333	0.27	0.04	0.157	OI	4.33
1.417	0.16	0.04	0.158	OI	4.36
1.500	0.10	0.04	0.159	O	4.37
1.583	0.03	0.04	0.159	O	4.38
1.667	0.01	0.04	0.159	O	4.37
1.750	0.00	0.04	0.159	O	4.36
1.833	0.00	0.04	0.158	O	4.36
1.917	0.00	0.04	0.158	O	4.35
2.000	0.00	0.04	0.158	O	4.34
2.083	0.00	0.04	0.157	O	4.33
2.167	0.00	0.04	0.157	O	4.32
2.250	0.00	0.04	0.157	O	4.32
2.333	0.00	0.04	0.156	O	4.31

2.417	0.00	0.04	0.156	O				4.30
2.500	0.00	0.04	0.156	O				4.29
2.583	0.00	0.04	0.155	O				4.29
2.667	0.00	0.04	0.155	O				4.28
2.750	0.00	0.04	0.155	O				4.27
2.833	0.00	0.04	0.155	O				4.26
2.917	0.00	0.04	0.154	O				4.26
3.000	0.00	0.04	0.154	O				4.25
3.083	0.00	0.04	0.154	O				4.24
3.167	0.00	0.04	0.153	O				4.23
3.250	0.00	0.04	0.153	O				4.22
3.333	0.00	0.04	0.153	O				4.22
3.417	0.00	0.04	0.152	O				4.21
3.500	0.00	0.04	0.152	O				4.20
3.583	0.00	0.04	0.152	O				4.19
3.667	0.00	0.04	0.151	O				4.19
3.750	0.00	0.04	0.151	O				4.18
3.833	0.00	0.04	0.151	O				4.17
3.917	0.00	0.04	0.150	O				4.16
4.000	0.00	0.04	0.150	O				4.15
4.083	0.00	0.04	0.150	O				4.15
4.167	0.00	0.04	0.150	O				4.14
4.250	0.00	0.04	0.149	O				4.13
4.333	0.00	0.04	0.149	O				4.12
4.417	0.00	0.04	0.149	O				4.12
4.500	0.00	0.04	0.148	O				4.11
4.583	0.00	0.04	0.148	O				4.10
4.667	0.00	0.04	0.148	O				4.09
4.750	0.00	0.04	0.147	O				4.08
4.833	0.00	0.04	0.147	O				4.08
4.917	0.00	0.04	0.147	O				4.07
5.000	0.00	0.04	0.146	O				4.06
5.083	0.00	0.04	0.146	O				4.05
5.167	0.00	0.04	0.146	O				4.05
5.250	0.00	0.04	0.146	O				4.04
5.333	0.00	0.04	0.145	O				4.03
5.417	0.00	0.04	0.145	O				4.02
5.500	0.00	0.04	0.145	O				4.01
5.583	0.00	0.04	0.144	O				4.01
5.667	0.00	0.04	0.144	O				4.00
5.750	0.00	0.04	0.144	O				3.99
5.833	0.00	0.04	0.143	O				3.98
5.917	0.00	0.04	0.143	O				3.98
6.000	0.00	0.04	0.143	O				3.97
6.083	0.00	0.04	0.142	O				3.96
6.167	0.00	0.04	0.142	O				3.95
6.250	0.00	0.04	0.142	O				3.95
6.333	0.00	0.04	0.141	O				3.94
6.417	0.00	0.04	0.141	O				3.93
6.500	0.00	0.04	0.141	O				3.92

6.583	0.00	0.04	0.141	O				3.91
6.667	0.00	0.04	0.140	O				3.91
6.750	0.00	0.04	0.140	O				3.90
6.833	0.00	0.04	0.140	O				3.89
6.917	0.00	0.04	0.139	O				3.88
7.000	0.00	0.04	0.139	O				3.88
7.083	0.00	0.04	0.139	O				3.87
7.167	0.00	0.04	0.138	O				3.86
7.250	0.00	0.04	0.138	O				3.85
7.333	0.00	0.04	0.138	O				3.84
7.417	0.00	0.04	0.137	O				3.84
7.500	0.00	0.04	0.137	O				3.83
7.583	0.00	0.04	0.137	O				3.82
7.667	0.00	0.04	0.137	O				3.81
7.750	0.00	0.04	0.136	O				3.81
7.833	0.00	0.04	0.136	O				3.80
7.917	0.00	0.04	0.136	O				3.79
8.000	0.00	0.04	0.135	O				3.78
8.083	0.00	0.04	0.135	O				3.77
8.167	0.00	0.04	0.135	O				3.77
8.250	0.00	0.04	0.134	O				3.76
8.333	0.00	0.04	0.134	O				3.75
8.417	0.00	0.04	0.134	O				3.74
8.500	0.00	0.04	0.133	O				3.74
8.583	0.00	0.04	0.133	O				3.73
8.667	0.00	0.04	0.133	O				3.72
8.750	0.00	0.04	0.133	O				3.71
8.833	0.00	0.04	0.132	O				3.71
8.917	0.00	0.04	0.132	O				3.70
9.000	0.00	0.04	0.132	O				3.69
9.083	0.00	0.04	0.131	O				3.68
9.167	0.00	0.04	0.131	O				3.67
9.250	0.00	0.04	0.131	O				3.67
9.333	0.00	0.04	0.130	O				3.66
9.417	0.00	0.04	0.130	O				3.65
9.500	0.00	0.04	0.130	O				3.64
9.583	0.00	0.04	0.129	O				3.64
9.667	0.00	0.04	0.129	O				3.63
9.750	0.00	0.04	0.129	O				3.62
9.833	0.00	0.04	0.128	O				3.61
9.917	0.00	0.04	0.128	O				3.60
10.000	0.00	0.04	0.128	O				3.60
10.083	0.00	0.04	0.128	O				3.59
10.167	0.00	0.04	0.127	O				3.58
10.250	0.00	0.04	0.127	O				3.57
10.333	0.00	0.04	0.127	O				3.57
10.417	0.00	0.04	0.126	O				3.56
10.500	0.00	0.04	0.126	O				3.55
10.583	0.00	0.04	0.126	O				3.54
10.667	0.00	0.04	0.125	O				3.53

10.750	0.00	0.04	0.125	O				3.53
10.833	0.00	0.04	0.125	O				3.52
10.917	0.00	0.04	0.124	O				3.51
11.000	0.00	0.04	0.124	O				3.50
11.083	0.00	0.04	0.124	O				3.50
11.167	0.00	0.04	0.124	O				3.49
11.250	0.00	0.04	0.123	O				3.48
11.333	0.00	0.04	0.123	O				3.47
11.417	0.00	0.04	0.123	O				3.46
11.500	0.00	0.04	0.122	O				3.46
11.583	0.00	0.04	0.122	O				3.45
11.667	0.00	0.04	0.122	O				3.44
11.750	0.00	0.04	0.121	O				3.43
11.833	0.00	0.04	0.121	O				3.43
11.917	0.00	0.04	0.121	O				3.42
12.000	0.00	0.04	0.120	O				3.41
12.083	0.00	0.04	0.120	O				3.40
12.167	0.00	0.04	0.120	O				3.40
12.250	0.00	0.04	0.119	O				3.39
12.333	0.00	0.04	0.119	O				3.38
12.417	0.00	0.04	0.119	O				3.37
12.500	0.00	0.04	0.119	O				3.36
12.583	0.00	0.04	0.118	O				3.36
12.667	0.00	0.04	0.118	O				3.35
12.750	0.00	0.04	0.118	O				3.34
12.833	0.00	0.04	0.117	O				3.33
12.917	0.00	0.04	0.117	O				3.33
13.000	0.00	0.04	0.117	O				3.32
13.083	0.00	0.04	0.116	O				3.31
13.167	0.00	0.04	0.116	O				3.30
13.250	0.00	0.04	0.116	O				3.29
13.333	0.00	0.04	0.115	O				3.29
13.417	0.00	0.04	0.115	O				3.28
13.500	0.00	0.04	0.115	O				3.27
13.583	0.00	0.04	0.115	O				3.26
13.667	0.00	0.04	0.114	O				3.26
13.750	0.00	0.04	0.114	O				3.25
13.833	0.00	0.04	0.114	O				3.24
13.917	0.00	0.04	0.113	O				3.23
14.000	0.00	0.04	0.113	O				3.22
14.083	0.00	0.04	0.113	O				3.22
14.167	0.00	0.04	0.112	O				3.21
14.250	0.00	0.04	0.112	O				3.20
14.333	0.00	0.04	0.112	O				3.19
14.417	0.00	0.04	0.111	O				3.19
14.500	0.00	0.04	0.111	O				3.18
14.583	0.00	0.04	0.111	O				3.17
14.667	0.00	0.04	0.111	O				3.16
14.750	0.00	0.04	0.110	O				3.15
14.833	0.00	0.04	0.110	O				3.15

14.917	0.00	0.04	0.110	O				3.14
15.000	0.00	0.04	0.109	O				3.13
15.083	0.00	0.04	0.109	O				3.12
15.167	0.00	0.04	0.109	O				3.12
15.250	0.00	0.04	0.108	O				3.11
15.333	0.00	0.04	0.108	O				3.10
15.417	0.00	0.04	0.108	O				3.09
15.500	0.00	0.04	0.107	O				3.09
15.583	0.00	0.04	0.107	O				3.08
15.667	0.00	0.04	0.107	O				3.07
15.750	0.00	0.04	0.106	O				3.06
15.833	0.00	0.04	0.106	O				3.05
15.917	0.00	0.04	0.106	O				3.05
16.000	0.00	0.04	0.106	O				3.04
16.083	0.00	0.04	0.105	O				3.03
16.167	0.00	0.04	0.105	O				3.02
16.250	0.00	0.04	0.105	O				3.02
16.333	0.00	0.04	0.104	O				3.01
16.417	0.00	0.04	0.104	O				3.00
16.500	0.00	0.04	0.104	O				2.99
16.583	0.00	0.04	0.103	O				2.98
16.667	0.00	0.04	0.103	O				2.98
16.750	0.00	0.04	0.103	O				2.97
16.833	0.00	0.04	0.102	O				2.96
16.917	0.00	0.04	0.102	O				2.95
17.000	0.00	0.04	0.102	O				2.95
17.083	0.00	0.04	0.102	O				2.94
17.167	0.00	0.04	0.101	O				2.93
17.250	0.00	0.04	0.101	O				2.92
17.333	0.00	0.04	0.101	O				2.91
17.417	0.00	0.04	0.100	O				2.91
17.500	0.00	0.04	0.100	O				2.90
17.583	0.00	0.04	0.100	O				2.89
17.667	0.00	0.04	0.099	O				2.88
17.750	0.00	0.04	0.099	O				2.88
17.833	0.00	0.04	0.099	O				2.87
17.917	0.00	0.04	0.098	O				2.86
18.000	0.00	0.04	0.098	O				2.85
18.083	0.00	0.04	0.098	O				2.85
18.167	0.00	0.04	0.097	O				2.84
18.250	0.00	0.04	0.097	O				2.83
18.333	0.00	0.04	0.097	O				2.82
18.417	0.00	0.04	0.097	O				2.81
18.500	0.00	0.04	0.096	O				2.81
18.583	0.00	0.04	0.096	O				2.80
18.667	0.00	0.04	0.096	O				2.79
18.750	0.00	0.04	0.095	O				2.78
18.833	0.00	0.04	0.095	O				2.78
18.917	0.00	0.04	0.095	O				2.77
19.000	0.00	0.04	0.094	O				2.76

19.083	0.00	0.04	0.094	O				2.75
19.167	0.00	0.04	0.094	O				2.74
19.250	0.00	0.04	0.093	O				2.74
19.333	0.00	0.04	0.093	O				2.73
19.417	0.00	0.04	0.093	O				2.72
19.500	0.00	0.04	0.093	O				2.71
19.583	0.00	0.04	0.092	O				2.71
19.667	0.00	0.04	0.092	O				2.70
19.750	0.00	0.04	0.092	O				2.69
19.833	0.00	0.04	0.091	O				2.68
19.917	0.00	0.04	0.091	O				2.67
20.000	0.00	0.04	0.091	O				2.67
20.083	0.00	0.04	0.090	O				2.66
20.167	0.00	0.04	0.090	O				2.65
20.250	0.00	0.04	0.090	O				2.64
20.333	0.00	0.04	0.089	O				2.64
20.417	0.00	0.04	0.089	O				2.63
20.500	0.00	0.04	0.089	O				2.62
20.583	0.00	0.04	0.089	O				2.61
20.667	0.00	0.04	0.088	O				2.60
20.750	0.00	0.04	0.088	O				2.60
20.833	0.00	0.04	0.088	O				2.59
20.917	0.00	0.04	0.087	O				2.58
21.000	0.00	0.04	0.087	O				2.57
21.083	0.00	0.04	0.087	O				2.57
21.167	0.00	0.04	0.086	O				2.56
21.250	0.00	0.04	0.086	O				2.55
21.333	0.00	0.04	0.086	O				2.54
21.417	0.00	0.04	0.085	O				2.54
21.500	0.00	0.04	0.085	O				2.53
21.583	0.00	0.04	0.085	O				2.52
21.667	0.00	0.04	0.084	O				2.51
21.750	0.00	0.04	0.084	O				2.50
21.833	0.00	0.04	0.084	O				2.50
21.917	0.00	0.04	0.084	O				2.49
22.000	0.00	0.04	0.083	O				2.48
22.083	0.00	0.04	0.083	O				2.47
22.167	0.00	0.04	0.083	O				2.47
22.250	0.00	0.04	0.082	O				2.46
22.333	0.00	0.04	0.082	O				2.45
22.417	0.00	0.04	0.082	O				2.44
22.500	0.00	0.04	0.081	O				2.43
22.583	0.00	0.04	0.081	O				2.43
22.667	0.00	0.04	0.081	O				2.42
22.750	0.00	0.04	0.080	O				2.41
22.833	0.00	0.04	0.080	O				2.40
22.917	0.00	0.04	0.080	O				2.40
23.000	0.00	0.04	0.080	O				2.39
23.083	0.00	0.04	0.079	O				2.38
23.167	0.00	0.04	0.079	O				2.37

23.250	0.00	0.04	0.079	O				2.36
23.333	0.00	0.04	0.078	O				2.36
23.417	0.00	0.04	0.078	O				2.35
23.500	0.00	0.04	0.078	O				2.34
23.583	0.00	0.04	0.077	O				2.33
23.667	0.00	0.04	0.077	O				2.33
23.750	0.00	0.04	0.077	O				2.32
23.833	0.00	0.04	0.076	O				2.31
23.917	0.00	0.04	0.076	O				2.30
24.000	0.00	0.04	0.076	O				2.29
24.083	0.00	0.04	0.075	O				2.29
24.167	0.00	0.04	0.075	O				2.28
24.250	0.00	0.04	0.075	O				2.27
24.333	0.00	0.04	0.075	O				2.26
24.417	0.00	0.04	0.074	O				2.26
24.500	0.00	0.04	0.074	O				2.25
24.583	0.00	0.04	0.074	O				2.24
24.667	0.00	0.04	0.073	O				2.23
24.750	0.00	0.04	0.073	O				2.23
24.833	0.00	0.04	0.073	O				2.22
24.917	0.00	0.04	0.072	O				2.21
25.000	0.00	0.04	0.072	O				2.20
25.083	0.00	0.04	0.072	O				2.19
25.167	0.00	0.04	0.071	O				2.19
25.250	0.00	0.04	0.071	O				2.18
25.333	0.00	0.04	0.071	O				2.17
25.417	0.00	0.04	0.071	O				2.16
25.500	0.00	0.04	0.070	O				2.16
25.583	0.00	0.04	0.070	O				2.15
25.667	0.00	0.04	0.070	O				2.14
25.750	0.00	0.04	0.069	O				2.13
25.833	0.00	0.04	0.069	O				2.12
25.917	0.00	0.04	0.069	O				2.12
26.000	0.00	0.04	0.068	O				2.11
26.083	0.00	0.04	0.068	O				2.10
26.167	0.00	0.04	0.068	O				2.09
26.250	0.00	0.04	0.067	O				2.09
26.333	0.00	0.04	0.067	O				2.08
26.417	0.00	0.04	0.067	O				2.07
26.500	0.00	0.04	0.066	O				2.06
26.583	0.00	0.04	0.066	O				2.05
26.667	0.00	0.04	0.066	O				2.05
26.750	0.00	0.04	0.066	O				2.04
26.833	0.00	0.04	0.065	O				2.03
26.917	0.00	0.04	0.065	O				2.02
27.000	0.00	0.04	0.065	O				2.02
27.083	0.00	0.04	0.064	O				2.01
27.167	0.00	0.04	0.064	O				2.00
27.250	0.00	0.04	0.064	O				1.99
27.333	0.00	0.04	0.063	O				1.99

27.417	0.00	0.04	0.063	O				1.98
27.500	0.00	0.04	0.063	O				1.97
27.583	0.00	0.04	0.062	O				1.96
27.667	0.00	0.04	0.062	O				1.95
27.750	0.00	0.04	0.062	O				1.95
27.833	0.00	0.04	0.062	O				1.94
27.917	0.00	0.04	0.061	O				1.93
28.000	0.00	0.04	0.061	O				1.92
28.083	0.00	0.04	0.061	O				1.92
28.167	0.00	0.04	0.060	O				1.91
28.250	0.00	0.04	0.060	O				1.90
28.333	0.00	0.04	0.060	O				1.89
28.417	0.00	0.04	0.059	O				1.88
28.500	0.00	0.04	0.059	O				1.88
28.583	0.00	0.04	0.059	O				1.87
28.667	0.00	0.04	0.058	O				1.86
28.750	0.00	0.04	0.058	O				1.85
28.833	0.00	0.04	0.058	O				1.85
28.917	0.00	0.04	0.058	O				1.84
29.000	0.00	0.04	0.057	O				1.83
29.083	0.00	0.04	0.057	O				1.82
29.167	0.00	0.04	0.057	O				1.81
29.250	0.00	0.04	0.056	O				1.81
29.333	0.00	0.04	0.056	O				1.80
29.417	0.00	0.04	0.056	O				1.79
29.500	0.00	0.04	0.055	O				1.78
29.583	0.00	0.04	0.055	O				1.78
29.667	0.00	0.04	0.055	O				1.77
29.750	0.00	0.04	0.054	O				1.76
29.833	0.00	0.04	0.054	O				1.75
29.917	0.00	0.04	0.054	O				1.74
30.000	0.00	0.04	0.053	O				1.74
30.083	0.00	0.04	0.053	O				1.73
30.167	0.00	0.04	0.053	O				1.72
30.250	0.00	0.04	0.053	O				1.71
30.333	0.00	0.04	0.052	O				1.71
30.417	0.00	0.04	0.052	O				1.70
30.500	0.00	0.04	0.052	O				1.69
30.583	0.00	0.04	0.051	O				1.68
30.667	0.00	0.04	0.051	O				1.68
30.750	0.00	0.04	0.051	O				1.67
30.833	0.00	0.04	0.050	O				1.66
30.917	0.00	0.04	0.050	O				1.65
31.000	0.00	0.04	0.050	O				1.64
31.083	0.00	0.04	0.049	O				1.64
31.167	0.00	0.04	0.049	O				1.63
31.250	0.00	0.04	0.049	O				1.62
31.333	0.00	0.04	0.049	O				1.61
31.417	0.00	0.04	0.048	O				1.61
31.500	0.00	0.04	0.048	O				1.60

31.583	0.00	0.04	0.048	O				1.59
31.667	0.00	0.04	0.047	O				1.58
31.750	0.00	0.04	0.047	O				1.57
31.833	0.00	0.04	0.047	O				1.57
31.917	0.00	0.04	0.046	O				1.56
32.000	0.00	0.04	0.046	O				1.55
32.083	0.00	0.04	0.046	O				1.54
32.167	0.00	0.04	0.045	O				1.54
32.250	0.00	0.04	0.045	O				1.53
32.333	0.00	0.04	0.045	O				1.52
32.417	0.00	0.04	0.044	O				1.51
32.500	0.00	0.04	0.044	O				1.50
32.583	0.00	0.04	0.044	O				1.50
32.667	0.00	0.04	0.044	O				1.49
32.750	0.00	0.04	0.043	O				1.48
32.833	0.00	0.04	0.043	O				1.47
32.917	0.00	0.04	0.043	O				1.47
33.000	0.00	0.04	0.042	O				1.46
33.083	0.00	0.04	0.042	O				1.45
33.167	0.00	0.04	0.042	O				1.44
33.250	0.00	0.04	0.041	O				1.43
33.333	0.00	0.04	0.041	O				1.43
33.417	0.00	0.04	0.041	O				1.42
33.500	0.00	0.04	0.040	O				1.41
33.583	0.00	0.04	0.040	O				1.40
33.667	0.00	0.04	0.040	O				1.40
33.750	0.00	0.04	0.040	O				1.39
33.833	0.00	0.04	0.039	O				1.38
33.917	0.00	0.04	0.039	O				1.37
34.000	0.00	0.04	0.039	O				1.37
34.083	0.00	0.04	0.038	O				1.36
34.167	0.00	0.04	0.038	O				1.35
34.250	0.00	0.04	0.038	O				1.34
34.333	0.00	0.04	0.037	O				1.33
34.417	0.00	0.04	0.037	O				1.33
34.500	0.00	0.04	0.037	O				1.32
34.583	0.00	0.04	0.036	O				1.31
34.667	0.00	0.04	0.036	O				1.30
34.750	0.00	0.04	0.036	O				1.30
34.833	0.00	0.04	0.036	O				1.29
34.917	0.00	0.04	0.035	O				1.28
35.000	0.00	0.04	0.035	O				1.27
35.083	0.00	0.04	0.035	O				1.26
35.167	0.00	0.04	0.034	O				1.26
35.250	0.00	0.04	0.034	O				1.25
35.333	0.00	0.04	0.034	O				1.24
35.417	0.00	0.04	0.033	O				1.23
35.500	0.00	0.04	0.033	O				1.23
35.583	0.00	0.04	0.033	O				1.22
35.667	0.00	0.04	0.032	O				1.21

35.750	0.00	0.04	0.032	O				1.20
35.833	0.00	0.04	0.032	O				1.19
35.917	0.00	0.04	0.031	O				1.19
36.000	0.00	0.04	0.031	O				1.18
36.083	0.00	0.04	0.031	O				1.17
36.167	0.00	0.04	0.031	O				1.16
36.250	0.00	0.04	0.030	O				1.16
36.333	0.00	0.04	0.030	O				1.15
36.417	0.00	0.04	0.030	O				1.14
36.500	0.00	0.04	0.029	O				1.13
36.583	0.00	0.04	0.029	O				1.12
36.667	0.00	0.04	0.029	O				1.12
36.750	0.00	0.04	0.028	O				1.11
36.833	0.00	0.04	0.028	O				1.10
36.917	0.00	0.04	0.028	O				1.09
37.000	0.00	0.04	0.027	O				1.09
37.083	0.00	0.04	0.027	O				1.08
37.167	0.00	0.04	0.027	O				1.07
37.250	0.00	0.04	0.027	O				1.06
37.333	0.00	0.04	0.026	O				1.06
37.417	0.00	0.04	0.026	O				1.05
37.500	0.00	0.04	0.026	O				1.04
37.583	0.00	0.04	0.025	O				1.03
37.667	0.00	0.04	0.025	O				1.02
37.750	0.00	0.04	0.025	O				1.02
37.833	0.00	0.04	0.024	O				1.01
37.917	0.00	0.04	0.024	O				1.00
38.000	0.00	0.04	0.024	O				0.99
38.083	0.00	0.04	0.023	O				0.98
38.167	0.00	0.04	0.023	O				0.96
38.250	0.00	0.04	0.023	O				0.95
38.333	0.00	0.04	0.023	O				0.94
38.417	0.00	0.04	0.022	O				0.93
38.500	0.00	0.04	0.022	O				0.92
38.583	0.00	0.04	0.022	O				0.90
38.667	0.00	0.04	0.021	O				0.89
38.750	0.00	0.04	0.021	O				0.88
38.833	0.00	0.04	0.021	O				0.87
38.917	0.00	0.04	0.021	O				0.86
39.000	0.00	0.04	0.020	O				0.85
39.083	0.00	0.04	0.020	O				0.84
39.167	0.00	0.04	0.020	O				0.83
39.250	0.00	0.04	0.020	O				0.81
39.333	0.00	0.04	0.019	O				0.80
39.417	0.00	0.04	0.019	O				0.79
39.500	0.00	0.04	0.019	O				0.78
39.583	0.00	0.03	0.019	O				0.77
39.667	0.00	0.03	0.018	O				0.76
39.750	0.00	0.03	0.018	O				0.75
39.833	0.00	0.03	0.018	O				0.74

39.917	0.00	0.03	0.018	O				0.73
40.000	0.00	0.03	0.017	O				0.73
40.083	0.00	0.03	0.017	O				0.72
40.167	0.00	0.03	0.017	O				0.71
40.250	0.00	0.03	0.017	O				0.70
40.333	0.00	0.03	0.017	O				0.69
40.417	0.00	0.03	0.016	O				0.68
40.500	0.00	0.03	0.016	O				0.67
40.583	0.00	0.03	0.016	O				0.66
40.667	0.00	0.03	0.016	O				0.65
40.750	0.00	0.03	0.015	O				0.65
40.833	0.00	0.03	0.015	O				0.64
40.917	0.00	0.03	0.015	O				0.63
41.000	0.00	0.03	0.015	O				0.62
41.083	0.00	0.03	0.015	O				0.61
41.167	0.00	0.03	0.015	O				0.61
41.250	0.00	0.03	0.014	O				0.60
41.333	0.00	0.03	0.014	O				0.59
41.417	0.00	0.03	0.014	O				0.58
41.500	0.00	0.03	0.014	O				0.57
41.583	0.00	0.03	0.014	O				0.57
41.667	0.00	0.03	0.013	O				0.56
41.750	0.00	0.02	0.013	O				0.55
41.833	0.00	0.02	0.013	O				0.55
41.917	0.00	0.02	0.013	O				0.54
42.000	0.00	0.02	0.013	O				0.53
42.083	0.00	0.02	0.013	O				0.53
42.167	0.00	0.02	0.012	O				0.52
42.250	0.00	0.02	0.012	O				0.51
42.333	0.00	0.02	0.012	O				0.51
42.417	0.00	0.02	0.012	O				0.50
42.500	0.00	0.02	0.012	O				0.49
42.583	0.00	0.02	0.012	O				0.49
42.667	0.00	0.02	0.012	O				0.48
42.750	0.00	0.02	0.011	O				0.47
42.833	0.00	0.02	0.011	O				0.47
42.917	0.00	0.02	0.011	O				0.46
43.000	0.00	0.02	0.011	O				0.46
43.083	0.00	0.02	0.011	O				0.45
43.167	0.00	0.02	0.011	O				0.44
43.250	0.00	0.02	0.011	O				0.44
43.333	0.00	0.02	0.010	O				0.43
43.417	0.00	0.02	0.010	O				0.43
43.500	0.00	0.02	0.010	O				0.42
43.583	0.00	0.02	0.010	O				0.42
43.667	0.00	0.02	0.010	O				0.41
43.750	0.00	0.02	0.010	O				0.41
43.833	0.00	0.02	0.010	O				0.40
43.917	0.00	0.02	0.009	O				0.40
44.000	0.00	0.02	0.009	O				0.39

44.083	0.00	0.02	0.009	O				0.39
44.167	0.00	0.02	0.009	O				0.38
44.250	0.00	0.02	0.009	O				0.38
44.333	0.00	0.02	0.009	O				0.37
44.417	0.00	0.02	0.009	O				0.37
44.500	0.00	0.02	0.009	O				0.36
44.583	0.00	0.02	0.009	O				0.36
44.667	0.00	0.02	0.008	O				0.35
44.750	0.00	0.02	0.008	O				0.35
44.833	0.00	0.02	0.008	O				0.34
44.917	0.00	0.02	0.008	O				0.34
45.000	0.00	0.02	0.008	O				0.33
45.083	0.00	0.01	0.008	O				0.33
45.167	0.00	0.01	0.008	O				0.33
45.250	0.00	0.01	0.008	O				0.32
45.333	0.00	0.01	0.008	O				0.32
45.417	0.00	0.01	0.008	O				0.31
45.500	0.00	0.01	0.007	O				0.31
45.583	0.00	0.01	0.007	O				0.31
45.667	0.00	0.01	0.007	O				0.30
45.750	0.00	0.01	0.007	O				0.30
45.833	0.00	0.01	0.007	O				0.29
45.917	0.00	0.01	0.007	O				0.29
46.000	0.00	0.01	0.007	O				0.29
46.083	0.00	0.01	0.007	O				0.28
46.167	0.00	0.01	0.007	O				0.28
46.250	0.00	0.01	0.007	O				0.28
46.333	0.00	0.01	0.007	O				0.27
46.417	0.00	0.01	0.006	O				0.27
46.500	0.00	0.01	0.006	O				0.26
46.583	0.00	0.01	0.006	O				0.26
46.667	0.00	0.01	0.006	O				0.26
46.750	0.00	0.01	0.006	O				0.25
46.833	0.00	0.01	0.006	O				0.25
46.917	0.00	0.01	0.006	O				0.25
47.000	0.00	0.01	0.006	O				0.25
47.083	0.00	0.01	0.006	O				0.24
47.167	0.00	0.01	0.006	O				0.24
47.250	0.00	0.01	0.006	O				0.24
47.333	0.00	0.01	0.006	O				0.23
47.417	0.00	0.01	0.006	O				0.23
47.500	0.00	0.01	0.005	O				0.23
47.583	0.00	0.01	0.005	O				0.22
47.667	0.00	0.01	0.005	O				0.22
47.750	0.00	0.01	0.005	O				0.22
47.833	0.00	0.01	0.005	O				0.22
47.917	0.00	0.01	0.005	O				0.21
48.000	0.00	0.01	0.005	O				0.21
48.083	0.00	0.01	0.005	O				0.21
48.167	0.00	0.01	0.005	O				0.20

48.250	0.00	0.01	0.005	O	|	|	|	0.20
48.333	0.00	0.01	0.005	O	|	|	|	0.20
48.417	0.00	0.01	0.005	O	|	|	|	0.20
48.500	0.00	0.01	0.005	O	|	|	|	0.19
48.583	0.00	0.01	0.005	O	|	|	|	0.19
48.667	0.00	0.01	0.005	O	|	|	|	0.19
48.750	0.00	0.01	0.004	O	|	|	|	0.19
48.833	0.00	0.01	0.004	O	|	|	|	0.18
48.917	0.00	0.01	0.004	O	|	|	|	0.18
49.000	0.00	0.01	0.004	O	|	|	|	0.18
49.083	0.00	0.01	0.004	O	|	|	|	0.18
49.167	0.00	0.01	0.004	O	|	|	|	0.18
49.250	0.00	0.01	0.004	O	|	|	|	0.17
49.333	0.00	0.01	0.004	O	|	|	|	0.17
49.417	0.00	0.01	0.004	O	|	|	|	0.17
49.500	0.00	0.01	0.004	O	|	|	|	0.17
49.583	0.00	0.01	0.004	O	|	|	|	0.16
49.667	0.00	0.01	0.004	O	|	|	|	0.16
49.750	0.00	0.01	0.004	O	|	|	|	0.16
49.833	0.00	0.01	0.004	O	|	|	|	0.16
49.917	0.00	0.01	0.004	O	|	|	|	0.16
50.000	0.00	0.01	0.004	O	|	|	|	0.15
50.083	0.00	0.01	0.004	O	|	|	|	0.15
50.167	0.00	0.01	0.004	O	|	|	|	0.15
50.250	0.00	0.01	0.004	O	|	|	|	0.15
50.333	0.00	0.01	0.004	O	|	|	|	0.15
50.417	0.00	0.01	0.003	O	|	|	|	0.14
50.500	0.00	0.01	0.003	O	|	|	|	0.14
50.583	0.00	0.01	0.003	O	|	|	|	0.14
50.667	0.00	0.01	0.003	O	|	|	|	0.14
50.750	0.00	0.01	0.003	O	|	|	|	0.14
50.833	0.00	0.01	0.003	O	|	|	|	0.14
50.917	0.00	0.01	0.003	O	|	|	|	0.13
51.000	0.00	0.01	0.003	O	|	|	|	0.13
51.083	0.00	0.01	0.003	O	|	|	|	0.13
51.167	0.00	0.01	0.003	O	|	|	|	0.13
51.250	0.00	0.01	0.003	O	|	|	|	0.13
51.333	0.00	0.01	0.003	O	|	|	|	0.13
51.417	0.00	0.01	0.003	O	|	|	|	0.12
51.500	0.00	0.01	0.003	O	|	|	|	0.12
51.583	0.00	0.01	0.003	O	|	|	|	0.12
51.667	0.00	0.01	0.003	O	|	|	|	0.12
51.750	0.00	0.01	0.003	O	|	|	|	0.12
51.833	0.00	0.01	0.003	O	|	|	|	0.12
51.917	0.00	0.01	0.003	O	|	|	|	0.11
52.000	0.00	0.01	0.003	O	|	|	|	0.11
52.083	0.00	0.01	0.003	O	|	|	|	0.11
52.167	0.00	0.00	0.003	O	|	|	|	0.11
52.250	0.00	0.00	0.003	O	|	|	|	0.11
52.333	0.00	0.00	0.003	O	|	|	|	0.11

52.417	0.00	0.00	0.003	O	|	|	|	|	0.11
52.500	0.00	0.00	0.003	O	|	|	|	|	0.10
52.583	0.00	0.00	0.002	O	|	|	|	|	0.10
52.667	0.00	0.00	0.002	O	|	|	|	|	0.10
52.750	0.00	0.00	0.002	O	|	|	|	|	0.10
52.833	0.00	0.00	0.002	O	|	|	|	|	0.10
52.917	0.00	0.00	0.002	O	|	|	|	|	0.10
53.000	0.00	0.00	0.002	O	|	|	|	|	0.10
53.083	0.00	0.00	0.002	O	|	|	|	|	0.10
53.167	0.00	0.00	0.002	O	|	|	|	|	0.09
53.250	0.00	0.00	0.002	O	|	|	|	|	0.09
53.333	0.00	0.00	0.002	O	|	|	|	|	0.09
53.417	0.00	0.00	0.002	O	|	|	|	|	0.09
53.500	0.00	0.00	0.002	O	|	|	|	|	0.09
53.583	0.00	0.00	0.002	O	|	|	|	|	0.09
53.667	0.00	0.00	0.002	O	|	|	|	|	0.09
53.750	0.00	0.00	0.002	O	|	|	|	|	0.09
53.833	0.00	0.00	0.002	O	|	|	|	|	0.09
53.917	0.00	0.00	0.002	O	|	|	|	|	0.08
54.000	0.00	0.00	0.002	O	|	|	|	|	0.08
54.083	0.00	0.00	0.002	O	|	|	|	|	0.08
54.167	0.00	0.00	0.002	O	|	|	|	|	0.08
54.250	0.00	0.00	0.002	O	|	|	|	|	0.08
54.333	0.00	0.00	0.002	O	|	|	|	|	0.08
54.417	0.00	0.00	0.002	O	|	|	|	|	0.08
54.500	0.00	0.00	0.002	O	|	|	|	|	0.08
54.583	0.00	0.00	0.002	O	|	|	|	|	0.08
54.667	0.00	0.00	0.002	O	|	|	|	|	0.07
54.750	0.00	0.00	0.002	O	|	|	|	|	0.07
54.833	0.00	0.00	0.002	O	|	|	|	|	0.07
54.917	0.00	0.00	0.002	O	|	|	|	|	0.07
55.000	0.00	0.00	0.002	O	|	|	|	|	0.07
55.083	0.00	0.00	0.002	O	|	|	|	|	0.07
55.167	0.00	0.00	0.002	O	|	|	|	|	0.07
55.250	0.00	0.00	0.002	O	|	|	|	|	0.07
55.333	0.00	0.00	0.002	O	|	|	|	|	0.07
55.417	0.00	0.00	0.002	O	|	|	|	|	0.07
55.500	0.00	0.00	0.002	O	|	|	|	|	0.07
55.583	0.00	0.00	0.002	O	|	|	|	|	0.06
55.667	0.00	0.00	0.002	O	|	|	|	|	0.06
55.750	0.00	0.00	0.002	O	|	|	|	|	0.06
55.833	0.00	0.00	0.001	O	|	|	|	|	0.06
55.917	0.00	0.00	0.001	O	|	|	|	|	0.06
56.000	0.00	0.00	0.001	O	|	|	|	|	0.06
56.083	0.00	0.00	0.001	O	|	|	|	|	0.06
56.167	0.00	0.00	0.001	O	|	|	|	|	0.06
56.250	0.00	0.00	0.001	O	|	|	|	|	0.06
56.333	0.00	0.00	0.001	O	|	|	|	|	0.06
56.417	0.00	0.00	0.001	O	|	|	|	|	0.06
56.500	0.00	0.00	0.001	O	|	|	|	|	0.06

56.583	0.00	0.00	0.001	O	|	|	|	0.06
56.667	0.00	0.00	0.001	O	|	|	|	0.05
56.750	0.00	0.00	0.001	O	|	|	|	0.05
56.833	0.00	0.00	0.001	O	|	|	|	0.05
56.917	0.00	0.00	0.001	O	|	|	|	0.05
57.000	0.00	0.00	0.001	O	|	|	|	0.05
57.083	0.00	0.00	0.001	O	|	|	|	0.05
57.167	0.00	0.00	0.001	O	|	|	|	0.05
57.250	0.00	0.00	0.001	O	|	|	|	0.05
57.333	0.00	0.00	0.001	O	|	|	|	0.05
57.417	0.00	0.00	0.001	O	|	|	|	0.05
57.500	0.00	0.00	0.001	O	|	|	|	0.05
57.583	0.00	0.00	0.001	O	|	|	|	0.05
57.667	0.00	0.00	0.001	O	|	|	|	0.05
57.750	0.00	0.00	0.001	O	|	|	|	0.05
57.833	0.00	0.00	0.001	O	|	|	|	0.05
57.917	0.00	0.00	0.001	O	|	|	|	0.05
58.000	0.00	0.00	0.001	O	|	|	|	0.04
58.083	0.00	0.00	0.001	O	|	|	|	0.04
58.167	0.00	0.00	0.001	O	|	|	|	0.04
58.250	0.00	0.00	0.001	O	|	|	|	0.04
58.333	0.00	0.00	0.001	O	|	|	|	0.04
58.417	0.00	0.00	0.001	O	|	|	|	0.04
58.500	0.00	0.00	0.001	O	|	|	|	0.04
58.583	0.00	0.00	0.001	O	|	|	|	0.04
58.667	0.00	0.00	0.001	O	|	|	|	0.04
58.750	0.00	0.00	0.001	O	|	|	|	0.04
58.833	0.00	0.00	0.001	O	|	|	|	0.04
58.917	0.00	0.00	0.001	O	|	|	|	0.04
59.000	0.00	0.00	0.001	O	|	|	|	0.04
59.083	0.00	0.00	0.001	O	|	|	|	0.04
59.167	0.00	0.00	0.001	O	|	|	|	0.04
59.250	0.00	0.00	0.001	O	|	|	|	0.04
59.333	0.00	0.00	0.001	O	|	|	|	0.04
59.417	0.00	0.00	0.001	O	|	|	|	0.04
59.500	0.00	0.00	0.001	O	|	|	|	0.04
59.583	0.00	0.00	0.001	O	|	|	|	0.03
59.667	0.00	0.00	0.001	O	|	|	|	0.03
59.750	0.00	0.00	0.001	O	|	|	|	0.03
59.833	0.00	0.00	0.001	O	|	|	|	0.03
59.917	0.00	0.00	0.001	O	|	|	|	0.03
60.000	0.00	0.00	0.001	O	|	|	|	0.03
60.083	0.00	0.00	0.001	O	|	|	|	0.03
60.167	0.00	0.00	0.001	O	|	|	|	0.03
60.250	0.00	0.00	0.001	O	|	|	|	0.03
60.333	0.00	0.00	0.001	O	|	|	|	0.03
60.417	0.00	0.00	0.001	O	|	|	|	0.03
60.500	0.00	0.00	0.001	O	|	|	|	0.03
60.583	0.00	0.00	0.001	O	|	|	|	0.03
60.667	0.00	0.00	0.001	O	|	|	|	0.03

60.750	0.00	0.00	0.001	O	|	|	|	0.03
60.833	0.00	0.00	0.001	O	|	|	|	0.03
60.917	0.00	0.00	0.001	O	|	|	|	0.03
61.000	0.00	0.00	0.001	O	|	|	|	0.03
61.083	0.00	0.00	0.001	O	|	|	|	0.03
61.167	0.00	0.00	0.001	O	|	|	|	0.03
61.250	0.00	0.00	0.001	O	|	|	|	0.03
61.333	0.00	0.00	0.001	O	|	|	|	0.03
61.417	0.00	0.00	0.001	O	|	|	|	0.03
61.500	0.00	0.00	0.001	O	|	|	|	0.03
61.583	0.00	0.00	0.001	O	|	|	|	0.03
61.667	0.00	0.00	0.001	O	|	|	|	0.03
61.750	0.00	0.00	0.001	O	|	|	|	0.02
61.833	0.00	0.00	0.001	O	|	|	|	0.02
61.917	0.00	0.00	0.001	O	|	|	|	0.02
62.000	0.00	0.00	0.001	O	|	|	|	0.02
62.083	0.00	0.00	0.001	O	|	|	|	0.02
62.167	0.00	0.00	0.001	O	|	|	|	0.02
62.250	0.00	0.00	0.001	O	|	|	|	0.02
62.333	0.00	0.00	0.001	O	|	|	|	0.02
62.417	0.00	0.00	0.001	O	|	|	|	0.02
62.500	0.00	0.00	0.001	O	|	|	|	0.02

**********HYDROGRAPH DATA**********

Number of intervals = 750
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.045 (CFS)
Total volume = 0.163 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
100 yr
3 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris3100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 44
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 2.680 (CFS)
Total volume = 0.242 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 44
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.7 1.34 2.01 2.68	Depth (Ft.)
0.083	0.08	0.00	0.000	O | | | |	0.01
0.167	0.28	0.00	0.001	O I | | | |	0.06
0.250	0.34	0.01	0.004	O I | | | |	0.15
0.333	0.36	0.01	0.006	O I | | | |	0.25
0.417	0.43	0.02	0.009	O I | | | |	0.36
0.500	0.48	0.02	0.012	O I | | | |	0.48
0.583	0.52	0.03	0.015	O I | | | |	0.62
0.667	0.52	0.03	0.018	O I | | | |	0.76
0.750	0.56	0.04	0.022	O I | | | |	0.91
0.833	0.56	0.04	0.025	O I | | | |	1.03
0.917	0.52	0.04	0.029	O I | | | |	1.12
1.000	0.54	0.04	0.032	O I | | | |	1.20
1.083	0.60	0.04	0.036	O I| | | |	1.29
1.167	0.67	0.04	0.040	O I| | | |	1.39
1.250	0.69	0.04	0.044	O I | | |	1.50
1.333	0.70	0.04	0.049	O I | | |	1.62
1.417	0.71	0.04	0.053	O I | | |	1.73
1.500	0.82	0.04	0.058	O |I | | |	1.85
1.583	0.85	0.04	0.063	O | I | | |	1.99
1.667	0.83	0.04	0.069	O |I | | |	2.12
1.750	0.92	0.04	0.075	O | I | | |	2.27
1.833	1.04	0.04	0.081	O | I | | |	2.43
1.917	1.04	0.04	0.088	O | I | | |	2.60
2.000	1.02	0.04	0.095	O | I | | |	2.77
2.083	1.04	0.04	0.102	O | I | | |	2.94
2.167	1.14	0.04	0.109	O | I | | |	3.12
2.250	1.42	0.04	0.117	O | I | |	3.33
2.333	1.54	0.04	0.127	O | | I | |	3.58

```
2.417    1.58    0.04      0.138  O       |        | I     |        |     3.84
2.500    2.19    0.04      0.150  O       |        |       | I      |     4.15
2.583    2.55    0.04      0.166  O       |        |       |     I  |     4.55
2.667    2.68    0.04      0.184  O       |        |       |       I|     4.99
2.750    2.08    0.04      0.200  O       |        |       I        |     5.39
2.833    1.25    0.04      0.211  O       |     I  |       |        |     5.66
2.917    0.94    0.04      0.218  O       |  I     |       |        |     5.84
3.000    0.73    0.04      0.224  O       I        |       |        |     5.98
3.083    0.43    0.04      0.227  O    I  |        |       |        |     6.07
3.167    0.21    0.04      0.229  O I     |        |       |        |     6.11
3.250    0.12    0.04      0.230  OI      |        |       |        |     6.13
3.333    0.06    0.04      0.230  O       |        |       |        |     6.14
3.417    0.03    0.04      0.230  O       |        |       |        |     6.14
3.500    0.01    0.04      0.230  O       |        |       |        |     6.14
3.583    0.01    0.04      0.230  O       |        |       |        |     6.13
3.667    0.00    0.04      0.230  O       |        |       |        |     6.12
3.750    0.00    0.04      0.229  O       |        |       |        |     6.11
3.833    0.00    0.04      0.229  O       |        |       |        |     6.11
3.917    0.00    0.04      0.229  O       |        |       |        |     6.10
4.000    0.00    0.04      0.228  O       |        |       |        |     6.09
4.083    0.00    0.04      0.228  O       |        |       |        |     6.08
4.167    0.00    0.04      0.228  O       |        |       |        |     6.08
4.250    0.00    0.04      0.228  O       |        |       |        |     6.07
4.333    0.00    0.04      0.227  O       |        |       |        |     6.06
4.417    0.00    0.04      0.227  O       |        |       |        |     6.05
4.500    0.00    0.04      0.227  O       |        |       |        |     6.05
4.583    0.00    0.04      0.226  O       |        |       |        |     6.04
4.667    0.00    0.04      0.226  O       |        |       |        |     6.03
4.750    0.00    0.04      0.226  O       |        |       |        |     6.02
4.833    0.00    0.04      0.225  O       |        |       |        |     6.02
4.917    0.00    0.04      0.225  O       |        |       |        |     6.01
5.000    0.00    0.04      0.225  O       |        |       |        |     6.00
5.083    0.00    0.04      0.224  O       |        |       |        |     5.99
5.167    0.00    0.04      0.224  O       |        |       |        |     5.98
5.250    0.00    0.04      0.224  O       |        |       |        |     5.98
5.333    0.00    0.04      0.224  O       |        |       |        |     5.97
5.417    0.00    0.04      0.223  O       |        |       |        |     5.96
5.500    0.00    0.04      0.223  O       |        |       |        |     5.95
5.583    0.00    0.04      0.223  O       |        |       |        |     5.95
5.667    0.00    0.04      0.222  O       |        |       |        |     5.94
5.750    0.00    0.04      0.222  O       |        |       |        |     5.93
5.833    0.00    0.04      0.222  O       |        |       |        |     5.92
5.917    0.00    0.04      0.221  O       |        |       |        |     5.92
6.000    0.00    0.04      0.221  O       |        |       |        |     5.91
6.083    0.00    0.04      0.221  O       |        |       |        |     5.90
6.167    0.00    0.04      0.220  O       |        |       |        |     5.89
6.250    0.00    0.04      0.220  O       |        |       |        |     5.89
6.333    0.00    0.04      0.220  O       |        |       |        |     5.88
6.417    0.00    0.04      0.219  O       |        |       |        |     5.87
6.500    0.00    0.04      0.219  O       |        |       |        |     5.86
```

6.583	0.00	0.04	0.219	O				5.85
6.667	0.00	0.04	0.219	O				5.85
6.750	0.00	0.04	0.218	O				5.84
6.833	0.00	0.04	0.218	O				5.83
6.917	0.00	0.04	0.218	O				5.82
7.000	0.00	0.04	0.217	O				5.82
7.083	0.00	0.04	0.217	O				5.81
7.167	0.00	0.04	0.217	O				5.80
7.250	0.00	0.04	0.216	O				5.79
7.333	0.00	0.04	0.216	O				5.79
7.417	0.00	0.04	0.216	O				5.78
7.500	0.00	0.04	0.215	O				5.77
7.583	0.00	0.04	0.215	O				5.76
7.667	0.00	0.04	0.215	O				5.76
7.750	0.00	0.04	0.215	O				5.75
7.833	0.00	0.04	0.214	O				5.74
7.917	0.00	0.04	0.214	O				5.73
8.000	0.00	0.04	0.214	O				5.72
8.083	0.00	0.04	0.213	O				5.72
8.167	0.00	0.04	0.213	O				5.71
8.250	0.00	0.04	0.213	O				5.70
8.333	0.00	0.04	0.212	O				5.69
8.417	0.00	0.04	0.212	O				5.69
8.500	0.00	0.04	0.212	O				5.68
8.583	0.00	0.04	0.211	O				5.67
8.667	0.00	0.04	0.211	O				5.66
8.750	0.00	0.04	0.211	O				5.66
8.833	0.00	0.04	0.211	O				5.65
8.917	0.00	0.04	0.210	O				5.64
9.000	0.00	0.04	0.210	O				5.63
9.083	0.00	0.04	0.210	O				5.63
9.167	0.00	0.04	0.209	O				5.62
9.250	0.00	0.04	0.209	O				5.61
9.333	0.00	0.04	0.209	O				5.60
9.417	0.00	0.04	0.208	O				5.59
9.500	0.00	0.04	0.208	O				5.59
9.583	0.00	0.04	0.208	O				5.58
9.667	0.00	0.04	0.207	O				5.57
9.750	0.00	0.04	0.207	O				5.56
9.833	0.00	0.04	0.207	O				5.56
9.917	0.00	0.04	0.206	O				5.55
10.000	0.00	0.04	0.206	O				5.54
10.083	0.00	0.04	0.206	O				5.53
10.167	0.00	0.04	0.206	O				5.53
10.250	0.00	0.04	0.205	O				5.52
10.333	0.00	0.04	0.205	O				5.51
10.417	0.00	0.04	0.205	O				5.50
10.500	0.00	0.04	0.204	O				5.50
10.583	0.00	0.04	0.204	O				5.49
10.667	0.00	0.04	0.204	O				5.48

10.750	0.00	0.04	0.203	O				5.47
10.833	0.00	0.04	0.203	O				5.46
10.917	0.00	0.04	0.203	O				5.46
11.000	0.00	0.04	0.202	O				5.45
11.083	0.00	0.04	0.202	O				5.44
11.167	0.00	0.04	0.202	O				5.43
11.250	0.00	0.04	0.202	O				5.43
11.333	0.00	0.04	0.201	O				5.42
11.417	0.00	0.04	0.201	O				5.41
11.500	0.00	0.04	0.201	O				5.40
11.583	0.00	0.04	0.200	O				5.40
11.667	0.00	0.04	0.200	O				5.39
11.750	0.00	0.04	0.200	O				5.38
11.833	0.00	0.04	0.199	O				5.37
11.917	0.00	0.04	0.199	O				5.37
12.000	0.00	0.04	0.199	O				5.36
12.083	0.00	0.04	0.198	O				5.35
12.167	0.00	0.04	0.198	O				5.34
12.250	0.00	0.04	0.198	O				5.33
12.333	0.00	0.04	0.197	O				5.33
12.417	0.00	0.04	0.197	O				5.32
12.500	0.00	0.04	0.197	O				5.31
12.583	0.00	0.04	0.197	O				5.30
12.667	0.00	0.04	0.196	O				5.30
12.750	0.00	0.04	0.196	O				5.29
12.833	0.00	0.04	0.196	O				5.28
12.917	0.00	0.04	0.195	O				5.27
13.000	0.00	0.04	0.195	O				5.27
13.083	0.00	0.04	0.195	O				5.26
13.167	0.00	0.04	0.194	O				5.25
13.250	0.00	0.04	0.194	O				5.24
13.333	0.00	0.04	0.194	O				5.23
13.417	0.00	0.04	0.193	O				5.23
13.500	0.00	0.04	0.193	O				5.22
13.583	0.00	0.04	0.193	O				5.21
13.667	0.00	0.04	0.193	O				5.20
13.750	0.00	0.04	0.192	O				5.20
13.833	0.00	0.04	0.192	O				5.19
13.917	0.00	0.04	0.192	O				5.18
14.000	0.00	0.04	0.191	O				5.17
14.083	0.00	0.04	0.191	O				5.17
14.167	0.00	0.04	0.191	O				5.16
14.250	0.00	0.04	0.190	O				5.15
14.333	0.00	0.04	0.190	O				5.14
14.417	0.00	0.04	0.190	O				5.14
14.500	0.00	0.04	0.189	O				5.13
14.583	0.00	0.04	0.189	O				5.12
14.667	0.00	0.04	0.189	O				5.11
14.750	0.00	0.04	0.188	O				5.10
14.833	0.00	0.04	0.188	O				5.10

14.917	0.00	0.04	0.188	O				5.09
15.000	0.00	0.04	0.188	O				5.08
15.083	0.00	0.04	0.187	O				5.07
15.167	0.00	0.04	0.187	O				5.07
15.250	0.00	0.04	0.187	O				5.06
15.333	0.00	0.04	0.186	O				5.05
15.417	0.00	0.04	0.186	O				5.04
15.500	0.00	0.04	0.186	O				5.04
15.583	0.00	0.04	0.185	O				5.03
15.667	0.00	0.04	0.185	O				5.02
15.750	0.00	0.04	0.185	O				5.01
15.833	0.00	0.04	0.184	O				5.01
15.917	0.00	0.04	0.184	O				5.00
16.000	0.00	0.04	0.184	O				4.99
16.083	0.00	0.04	0.184	O				4.98
16.167	0.00	0.04	0.183	O				4.97
16.250	0.00	0.04	0.183	O				4.97
16.333	0.00	0.04	0.183	O				4.96
16.417	0.00	0.04	0.182	O				4.95
16.500	0.00	0.04	0.182	O				4.94
16.583	0.00	0.04	0.182	O				4.94
16.667	0.00	0.04	0.181	O				4.93
16.750	0.00	0.04	0.181	O				4.92
16.833	0.00	0.04	0.181	O				4.91
16.917	0.00	0.04	0.180	O				4.91
17.000	0.00	0.04	0.180	O				4.90
17.083	0.00	0.04	0.180	O				4.89
17.167	0.00	0.04	0.180	O				4.88
17.250	0.00	0.04	0.179	O				4.88
17.333	0.00	0.04	0.179	O				4.87
17.417	0.00	0.04	0.179	O				4.86
17.500	0.00	0.04	0.178	O				4.85
17.583	0.00	0.04	0.178	O				4.84
17.667	0.00	0.04	0.178	O				4.84
17.750	0.00	0.04	0.177	O				4.83
17.833	0.00	0.04	0.177	O				4.82
17.917	0.00	0.04	0.177	O				4.81
18.000	0.00	0.04	0.176	O				4.81
18.083	0.00	0.04	0.176	O				4.80
18.167	0.00	0.04	0.176	O				4.79
18.250	0.00	0.04	0.175	O				4.78
18.333	0.00	0.04	0.175	O				4.78
18.417	0.00	0.04	0.175	O				4.77
18.500	0.00	0.04	0.175	O				4.76
18.583	0.00	0.04	0.174	O				4.75
18.667	0.00	0.04	0.174	O				4.75
18.750	0.00	0.04	0.174	O				4.74
18.833	0.00	0.04	0.173	O				4.73
18.917	0.00	0.04	0.173	O				4.72
19.000	0.00	0.04	0.173	O				4.71

19.083	0.00	0.04	0.172	O				4.71
19.167	0.00	0.04	0.172	O				4.70
19.250	0.00	0.04	0.172	O				4.69
19.333	0.00	0.04	0.171	O				4.68
19.417	0.00	0.04	0.171	O				4.68
19.500	0.00	0.04	0.171	O				4.67
19.583	0.00	0.04	0.171	O				4.66
19.667	0.00	0.04	0.170	O				4.65
19.750	0.00	0.04	0.170	O				4.65
19.833	0.00	0.04	0.170	O				4.64
19.917	0.00	0.04	0.169	O				4.63
20.000	0.00	0.04	0.169	O				4.62
20.083	0.00	0.04	0.169	O				4.62
20.167	0.00	0.04	0.168	O				4.61
20.250	0.00	0.04	0.168	O				4.60
20.333	0.00	0.04	0.168	O				4.59
20.417	0.00	0.04	0.167	O				4.58
20.500	0.00	0.04	0.167	O				4.58
20.583	0.00	0.04	0.167	O				4.57
20.667	0.00	0.04	0.166	O				4.56
20.750	0.00	0.04	0.166	O				4.55
20.833	0.00	0.04	0.166	O				4.55
20.917	0.00	0.04	0.166	O				4.54
21.000	0.00	0.04	0.165	O				4.53
21.083	0.00	0.04	0.165	O				4.52
21.167	0.00	0.04	0.165	O				4.52
21.250	0.00	0.04	0.164	O				4.51
21.333	0.00	0.04	0.164	O				4.50
21.417	0.00	0.04	0.164	O				4.49
21.500	0.00	0.04	0.163	O				4.48
21.583	0.00	0.04	0.163	O				4.48
21.667	0.00	0.04	0.163	O				4.47
21.750	0.00	0.04	0.162	O				4.46
21.833	0.00	0.04	0.162	O				4.45
21.917	0.00	0.04	0.162	O				4.45
22.000	0.00	0.04	0.162	O				4.44
22.083	0.00	0.04	0.161	O				4.43
22.167	0.00	0.04	0.161	O				4.42
22.250	0.00	0.04	0.161	O				4.42
22.333	0.00	0.04	0.160	O				4.41
22.417	0.00	0.04	0.160	O				4.40
22.500	0.00	0.04	0.160	O				4.39
22.583	0.00	0.04	0.159	O				4.38
22.667	0.00	0.04	0.159	O				4.38
22.750	0.00	0.04	0.159	O				4.37
22.833	0.00	0.04	0.158	O				4.36
22.917	0.00	0.04	0.158	O				4.35
23.000	0.00	0.04	0.158	O				4.35
23.083	0.00	0.04	0.158	O				4.34
23.167	0.00	0.04	0.157	O				4.33

23.250	0.00	0.04	0.157	O				4.32
23.333	0.00	0.04	0.157	O				4.31
23.417	0.00	0.04	0.156	O				4.31
23.500	0.00	0.04	0.156	O				4.30
23.583	0.00	0.04	0.156	O				4.29
23.667	0.00	0.04	0.155	O				4.28
23.750	0.00	0.04	0.155	O				4.28
23.833	0.00	0.04	0.155	O				4.27
23.917	0.00	0.04	0.154	O				4.26
24.000	0.00	0.04	0.154	O				4.25
24.083	0.00	0.04	0.154	O				4.24
24.167	0.00	0.04	0.153	O				4.24
24.250	0.00	0.04	0.153	O				4.23
24.333	0.00	0.04	0.153	O				4.22
24.417	0.00	0.04	0.153	O				4.21
24.500	0.00	0.04	0.152	O				4.21
24.583	0.00	0.04	0.152	O				4.20
24.667	0.00	0.04	0.152	O				4.19
24.750	0.00	0.04	0.151	O				4.18
24.833	0.00	0.04	0.151	O				4.17
24.917	0.00	0.04	0.151	O				4.17
25.000	0.00	0.04	0.150	O				4.16
25.083	0.00	0.04	0.150	O				4.15
25.167	0.00	0.04	0.150	O				4.14
25.250	0.00	0.04	0.149	O				4.14
25.333	0.00	0.04	0.149	O				4.13
25.417	0.00	0.04	0.149	O				4.12
25.500	0.00	0.04	0.149	O				4.11
25.583	0.00	0.04	0.148	O				4.11
25.667	0.00	0.04	0.148	O				4.10
25.750	0.00	0.04	0.148	O				4.09
25.833	0.00	0.04	0.147	O				4.08
25.917	0.00	0.04	0.147	O				4.07
26.000	0.00	0.04	0.147	O				4.07
26.083	0.00	0.04	0.146	O				4.06
26.167	0.00	0.04	0.146	O				4.05
26.250	0.00	0.04	0.146	O				4.04
26.333	0.00	0.04	0.145	O				4.04
26.417	0.00	0.04	0.145	O				4.03
26.500	0.00	0.04	0.145	O				4.02
26.583	0.00	0.04	0.144	O				4.01
26.667	0.00	0.04	0.144	O				4.00
26.750	0.00	0.04	0.144	O				4.00
26.833	0.00	0.04	0.144	O				3.99
26.917	0.00	0.04	0.143	O				3.98
27.000	0.00	0.04	0.143	O				3.97
27.083	0.00	0.04	0.143	O				3.97
27.167	0.00	0.04	0.142	O				3.96
27.250	0.00	0.04	0.142	O				3.95
27.333	0.00	0.04	0.142	O				3.94

27.417	0.00	0.04	0.141	O	|	|	|	3.93
27.500	0.00	0.04	0.141	O	|	|	|	3.93
27.583	0.00	0.04	0.141	O	|	|	|	3.92
27.667	0.00	0.04	0.140	O	|	|	|	3.91
27.750	0.00	0.04	0.140	O	|	|	|	3.90
27.833	0.00	0.04	0.140	O	|	|	|	3.90
27.917	0.00	0.04	0.140	O	|	|	|	3.89
28.000	0.00	0.04	0.139	O	|	|	|	3.88
28.083	0.00	0.04	0.139	O	|	|	|	3.87
28.167	0.00	0.04	0.139	O	|	|	|	3.87
28.250	0.00	0.04	0.138	O	|	|	|	3.86
28.333	0.00	0.04	0.138	O	|	|	|	3.85
28.417	0.00	0.04	0.138	O	|	|	|	3.84
28.500	0.00	0.04	0.137	O	|	|	|	3.83
28.583	0.00	0.04	0.137	O	|	|	|	3.83
28.667	0.00	0.04	0.137	O	|	|	|	3.82
28.750	0.00	0.04	0.136	O	|	|	|	3.81
28.833	0.00	0.04	0.136	O	|	|	|	3.80
28.917	0.00	0.04	0.136	O	|	|	|	3.80
29.000	0.00	0.04	0.136	O	|	|	|	3.79
29.083	0.00	0.04	0.135	O	|	|	|	3.78
29.167	0.00	0.04	0.135	O	|	|	|	3.77
29.250	0.00	0.04	0.135	O	|	|	|	3.76
29.333	0.00	0.04	0.134	O	|	|	|	3.76
29.417	0.00	0.04	0.134	O	|	|	|	3.75
29.500	0.00	0.04	0.134	O	|	|	|	3.74
29.583	0.00	0.04	0.133	O	|	|	|	3.73
29.667	0.00	0.04	0.133	O	|	|	|	3.73
29.750	0.00	0.04	0.133	O	|	|	|	3.72
29.833	0.00	0.04	0.132	O	|	|	|	3.71
29.917	0.00	0.04	0.132	O	|	|	|	3.70
30.000	0.00	0.04	0.132	O	|	|	|	3.69
30.083	0.00	0.04	0.131	O	|	|	|	3.69
30.167	0.00	0.04	0.131	O	|	|	|	3.68
30.250	0.00	0.04	0.131	O	|	|	|	3.67
30.333	0.00	0.04	0.131	O	|	|	|	3.66
30.417	0.00	0.04	0.130	O	|	|	|	3.66
30.500	0.00	0.04	0.130	O	|	|	|	3.65
30.583	0.00	0.04	0.130	O	|	|	|	3.64
30.667	0.00	0.04	0.129	O	|	|	|	3.63
30.750	0.00	0.04	0.129	O	|	|	|	3.62
30.833	0.00	0.04	0.129	O	|	|	|	3.62
30.917	0.00	0.04	0.128	O	|	|	|	3.61
31.000	0.00	0.04	0.128	O	|	|	|	3.60
31.083	0.00	0.04	0.128	O	|	|	|	3.59
31.167	0.00	0.04	0.127	O	|	|	|	3.59
31.250	0.00	0.04	0.127	O	|	|	|	3.58
31.333	0.00	0.04	0.127	O	|	|	|	3.57
31.417	0.00	0.04	0.127	O	|	|	|	3.56
31.500	0.00	0.04	0.126	O	|	|	|	3.56

31.583	0.00	0.04	0.126	O				3.55
31.667	0.00	0.04	0.126	O				3.54
31.750	0.00	0.04	0.125	O				3.53
31.833	0.00	0.04	0.125	O				3.52
31.917	0.00	0.04	0.125	O				3.52
32.000	0.00	0.04	0.124	O				3.51
32.083	0.00	0.04	0.124	O				3.50
32.167	0.00	0.04	0.124	O				3.49
32.250	0.00	0.04	0.123	O				3.49
32.333	0.00	0.04	0.123	O				3.48
32.417	0.00	0.04	0.123	O				3.47
32.500	0.00	0.04	0.122	O				3.46
32.583	0.00	0.04	0.122	O				3.45
32.667	0.00	0.04	0.122	O				3.45
32.750	0.00	0.04	0.122	O				3.44
32.833	0.00	0.04	0.121	O				3.43
32.917	0.00	0.04	0.121	O				3.42
33.000	0.00	0.04	0.121	O				3.42
33.083	0.00	0.04	0.120	O				3.41
33.167	0.00	0.04	0.120	O				3.40
33.250	0.00	0.04	0.120	O				3.39
33.333	0.00	0.04	0.119	O				3.38
33.417	0.00	0.04	0.119	O				3.38
33.500	0.00	0.04	0.119	O				3.37
33.583	0.00	0.04	0.118	O				3.36
33.667	0.00	0.04	0.118	O				3.35
33.750	0.00	0.04	0.118	O				3.35
33.833	0.00	0.04	0.118	O				3.34
33.917	0.00	0.04	0.117	O				3.33
34.000	0.00	0.04	0.117	O				3.32
34.083	0.00	0.04	0.117	O				3.31
34.167	0.00	0.04	0.116	O				3.31
34.250	0.00	0.04	0.116	O				3.30
34.333	0.00	0.04	0.116	O				3.29
34.417	0.00	0.04	0.115	O				3.28
34.500	0.00	0.04	0.115	O				3.28
34.583	0.00	0.04	0.115	O				3.27
34.667	0.00	0.04	0.114	O				3.26
34.750	0.00	0.04	0.114	O				3.25
34.833	0.00	0.04	0.114	O				3.25
34.917	0.00	0.04	0.113	O				3.24
35.000	0.00	0.04	0.113	O				3.23
35.083	0.00	0.04	0.113	O				3.22
35.167	0.00	0.04	0.113	O				3.21
35.250	0.00	0.04	0.112	O				3.21
35.333	0.00	0.04	0.112	O				3.20
35.417	0.00	0.04	0.112	O				3.19
35.500	0.00	0.04	0.111	O				3.18
35.583	0.00	0.04	0.111	O				3.18
35.667	0.00	0.04	0.111	O				3.17

35.750	0.00	0.04	0.110	O	|	|	|	3.16
35.833	0.00	0.04	0.110	O	|	|	|	3.15
35.917	0.00	0.04	0.110	O	|	|	|	3.14
36.000	0.00	0.04	0.109	O	|	|	|	3.14
36.083	0.00	0.04	0.109	O	|	|	|	3.13
36.167	0.00	0.04	0.109	O	|	|	|	3.12
36.250	0.00	0.04	0.109	O	|	|	|	3.11
36.333	0.00	0.04	0.108	O	|	|	|	3.11
36.417	0.00	0.04	0.108	O	|	|	|	3.10
36.500	0.00	0.04	0.108	O	|	|	|	3.09
36.583	0.00	0.04	0.107	O	|	|	|	3.08
36.667	0.00	0.04	0.107	O	|	|	|	3.07
36.750	0.00	0.04	0.107	O	|	|	|	3.07
36.833	0.00	0.04	0.106	O	|	|	|	3.06
36.917	0.00	0.04	0.106	O	|	|	|	3.05
37.000	0.00	0.04	0.106	O	|	|	|	3.04
37.083	0.00	0.04	0.105	O	|	|	|	3.04
37.167	0.00	0.04	0.105	O	|	|	|	3.03
37.250	0.00	0.04	0.105	O	|	|	|	3.02
37.333	0.00	0.04	0.105	O	|	|	|	3.01
37.417	0.00	0.04	0.104	O	|	|	|	3.01
37.500	0.00	0.04	0.104	O	|	|	|	3.00
37.583	0.00	0.04	0.104	O	|	|	|	2.99
37.667	0.00	0.04	0.103	O	|	|	|	2.98
37.750	0.00	0.04	0.103	O	|	|	|	2.97
37.833	0.00	0.04	0.103	O	|	|	|	2.97
37.917	0.00	0.04	0.102	O	|	|	|	2.96
38.000	0.00	0.04	0.102	O	|	|	|	2.95
38.083	0.00	0.04	0.102	O	|	|	|	2.94
38.167	0.00	0.04	0.101	O	|	|	|	2.94
38.250	0.00	0.04	0.101	O	|	|	|	2.93
38.333	0.00	0.04	0.101	O	|	|	|	2.92
38.417	0.00	0.04	0.100	O	|	|	|	2.91
38.500	0.00	0.04	0.100	O	|	|	|	2.90
38.583	0.00	0.04	0.100	O	|	|	|	2.90
38.667	0.00	0.04	0.100	O	|	|	|	2.89
38.750	0.00	0.04	0.099	O	|	|	|	2.88
38.833	0.00	0.04	0.099	O	|	|	|	2.87
38.917	0.00	0.04	0.099	O	|	|	|	2.87
39.000	0.00	0.04	0.098	O	|	|	|	2.86
39.083	0.00	0.04	0.098	O	|	|	|	2.85
39.167	0.00	0.04	0.098	O	|	|	|	2.84
39.250	0.00	0.04	0.097	O	|	|	|	2.83
39.333	0.00	0.04	0.097	O	|	|	|	2.83
39.417	0.00	0.04	0.097	O	|	|	|	2.82
39.500	0.00	0.04	0.096	O	|	|	|	2.81
39.583	0.00	0.04	0.096	O	|	|	|	2.80
39.667	0.00	0.04	0.096	O	|	|	|	2.80
39.750	0.00	0.04	0.096	O	|	|	|	2.79
39.833	0.00	0.04	0.095	O	|	|	|	2.78

39.917	0.00	0.04	0.095	O				2.77
40.000	0.00	0.04	0.095	O				2.76
40.083	0.00	0.04	0.094	O				2.76
40.167	0.00	0.04	0.094	O				2.75
40.250	0.00	0.04	0.094	O				2.74
40.333	0.00	0.04	0.093	O				2.73
40.417	0.00	0.04	0.093	O				2.73
40.500	0.00	0.04	0.093	O				2.72
40.583	0.00	0.04	0.092	O				2.71
40.667	0.00	0.04	0.092	O				2.70
40.750	0.00	0.04	0.092	O				2.70
40.833	0.00	0.04	0.091	O				2.69
40.917	0.00	0.04	0.091	O				2.68
41.000	0.00	0.04	0.091	O				2.67
41.083	0.00	0.04	0.091	O				2.66
41.167	0.00	0.04	0.090	O				2.66
41.250	0.00	0.04	0.090	O				2.65
41.333	0.00	0.04	0.090	O				2.64
41.417	0.00	0.04	0.089	O				2.63
41.500	0.00	0.04	0.089	O				2.63
41.583	0.00	0.04	0.089	O				2.62
41.667	0.00	0.04	0.088	O				2.61
41.750	0.00	0.04	0.088	O				2.60
41.833	0.00	0.04	0.088	O				2.59
41.917	0.00	0.04	0.087	O				2.59
42.000	0.00	0.04	0.087	O				2.58
42.083	0.00	0.04	0.087	O				2.57
42.167	0.00	0.04	0.087	O				2.56
42.250	0.00	0.04	0.086	O				2.56
42.333	0.00	0.04	0.086	O				2.55
42.417	0.00	0.04	0.086	O				2.54
42.500	0.00	0.04	0.085	O				2.53
42.583	0.00	0.04	0.085	O				2.52
42.667	0.00	0.04	0.085	O				2.52
42.750	0.00	0.04	0.084	O				2.51
42.833	0.00	0.04	0.084	O				2.50
42.917	0.00	0.04	0.084	O				2.49
43.000	0.00	0.04	0.083	O				2.49
43.083	0.00	0.04	0.083	O				2.48
43.167	0.00	0.04	0.083	O				2.47
43.250	0.00	0.04	0.083	O				2.46
43.333	0.00	0.04	0.082	O				2.45
43.417	0.00	0.04	0.082	O				2.45
43.500	0.00	0.04	0.082	O				2.44
43.583	0.00	0.04	0.081	O				2.43
43.667	0.00	0.04	0.081	O				2.42
43.750	0.00	0.04	0.081	O				2.42
43.833	0.00	0.04	0.080	O				2.41
43.917	0.00	0.04	0.080	O				2.40
44.000	0.00	0.04	0.080	O				2.39

44.083	0.00	0.04	0.079	O				2.39
44.167	0.00	0.04	0.079	O				2.38
44.250	0.00	0.04	0.079	O				2.37
44.333	0.00	0.04	0.078	O				2.36
44.417	0.00	0.04	0.078	O				2.35
44.500	0.00	0.04	0.078	O				2.35
44.583	0.00	0.04	0.078	O				2.34
44.667	0.00	0.04	0.077	O				2.33
44.750	0.00	0.04	0.077	O				2.32
44.833	0.00	0.04	0.077	O				2.32
44.917	0.00	0.04	0.076	O				2.31
45.000	0.00	0.04	0.076	O				2.30
45.083	0.00	0.04	0.076	O				2.29
45.167	0.00	0.04	0.075	O				2.28
45.250	0.00	0.04	0.075	O				2.28
45.333	0.00	0.04	0.075	O				2.27
45.417	0.00	0.04	0.074	O				2.26
45.500	0.00	0.04	0.074	O				2.25
45.583	0.00	0.04	0.074	O				2.25
45.667	0.00	0.04	0.074	O				2.24
45.750	0.00	0.04	0.073	O				2.23
45.833	0.00	0.04	0.073	O				2.22
45.917	0.00	0.04	0.073	O				2.21
46.000	0.00	0.04	0.072	O				2.21
46.083	0.00	0.04	0.072	O				2.20
46.167	0.00	0.04	0.072	O				2.19
46.250	0.00	0.04	0.071	O				2.18
46.333	0.00	0.04	0.071	O				2.18
46.417	0.00	0.04	0.071	O				2.17
46.500	0.00	0.04	0.070	O				2.16
46.583	0.00	0.04	0.070	O				2.15
46.667	0.00	0.04	0.070	O				2.14
46.750	0.00	0.04	0.069	O				2.14
46.833	0.00	0.04	0.069	O				2.13
46.917	0.00	0.04	0.069	O				2.12
47.000	0.00	0.04	0.069	O				2.11
47.083	0.00	0.04	0.068	O				2.11
47.167	0.00	0.04	0.068	O				2.10
47.250	0.00	0.04	0.068	O				2.09
47.333	0.00	0.04	0.067	O				2.08
47.417	0.00	0.04	0.067	O				2.08
47.500	0.00	0.04	0.067	O				2.07
47.583	0.00	0.04	0.066	O				2.06
47.667	0.00	0.04	0.066	O				2.05
47.750	0.00	0.04	0.066	O				2.04
47.833	0.00	0.04	0.065	O				2.04
47.917	0.00	0.04	0.065	O				2.03
48.000	0.00	0.04	0.065	O				2.02
48.083	0.00	0.04	0.065	O				2.01
48.167	0.00	0.04	0.064	O				2.01

48.250	0.00	0.04	0.064	O				2.00
48.333	0.00	0.04	0.064	O				1.99
48.417	0.00	0.04	0.063	O				1.98
48.500	0.00	0.04	0.063	O				1.97
48.583	0.00	0.04	0.063	O				1.97
48.667	0.00	0.04	0.062	O				1.96
48.750	0.00	0.04	0.062	O				1.95
48.833	0.00	0.04	0.062	O				1.94
48.917	0.00	0.04	0.061	O				1.94
49.000	0.00	0.04	0.061	O				1.93
49.083	0.00	0.04	0.061	O				1.92
49.167	0.00	0.04	0.061	O				1.91
49.250	0.00	0.04	0.060	O				1.90
49.333	0.00	0.04	0.060	O				1.90
49.417	0.00	0.04	0.060	O				1.89
49.500	0.00	0.04	0.059	O				1.88
49.583	0.00	0.04	0.059	O				1.87
49.667	0.00	0.04	0.059	O				1.87
49.750	0.00	0.04	0.058	O				1.86
49.833	0.00	0.04	0.058	O				1.85
49.917	0.00	0.04	0.058	O				1.84
50.000	0.00	0.04	0.057	O				1.84
50.083	0.00	0.04	0.057	O				1.83
50.167	0.00	0.04	0.057	O				1.82
50.250	0.00	0.04	0.056	O				1.81
50.333	0.00	0.04	0.056	O				1.80
50.417	0.00	0.04	0.056	O				1.80
50.500	0.00	0.04	0.056	O				1.79
50.583	0.00	0.04	0.055	O				1.78
50.667	0.00	0.04	0.055	O				1.77
50.750	0.00	0.04	0.055	O				1.77
50.833	0.00	0.04	0.054	O				1.76
50.917	0.00	0.04	0.054	O				1.75
51.000	0.00	0.04	0.054	O				1.74
51.083	0.00	0.04	0.053	O				1.73
51.167	0.00	0.04	0.053	O				1.73
51.250	0.00	0.04	0.053	O				1.72
51.333	0.00	0.04	0.052	O				1.71
51.417	0.00	0.04	0.052	O				1.70
51.500	0.00	0.04	0.052	O				1.70
51.583	0.00	0.04	0.052	O				1.69
51.667	0.00	0.04	0.051	O				1.68
51.750	0.00	0.04	0.051	O				1.67
51.833	0.00	0.04	0.051	O				1.66
51.917	0.00	0.04	0.050	O				1.66
52.000	0.00	0.04	0.050	O				1.65
52.083	0.00	0.04	0.050	O				1.64
52.167	0.00	0.04	0.049	O				1.63
52.250	0.00	0.04	0.049	O				1.63
52.333	0.00	0.04	0.049	O				1.62

52.417	0.00	0.04	0.048	O				1.61
52.500	0.00	0.04	0.048	O				1.60
52.583	0.00	0.04	0.048	O				1.59
52.667	0.00	0.04	0.047	O				1.59
52.750	0.00	0.04	0.047	O				1.58
52.833	0.00	0.04	0.047	O				1.57
52.917	0.00	0.04	0.047	O				1.56
53.000	0.00	0.04	0.046	O				1.56
53.083	0.00	0.04	0.046	O				1.55
53.167	0.00	0.04	0.046	O				1.54
53.250	0.00	0.04	0.045	O				1.53
53.333	0.00	0.04	0.045	O				1.53
53.417	0.00	0.04	0.045	O				1.52
53.500	0.00	0.04	0.044	O				1.51
53.583	0.00	0.04	0.044	O				1.50
53.667	0.00	0.04	0.044	O				1.49
53.750	0.00	0.04	0.043	O				1.49
53.833	0.00	0.04	0.043	O				1.48
53.917	0.00	0.04	0.043	O				1.47
54.000	0.00	0.04	0.043	O				1.46
54.083	0.00	0.04	0.042	O				1.46
54.167	0.00	0.04	0.042	O				1.45
54.250	0.00	0.04	0.042	O				1.44
54.333	0.00	0.04	0.041	O				1.43
54.417	0.00	0.04	0.041	O				1.42
54.500	0.00	0.04	0.041	O				1.42
54.583	0.00	0.04	0.040	O				1.41
54.667	0.00	0.04	0.040	O				1.40
54.750	0.00	0.04	0.040	O				1.39
54.833	0.00	0.04	0.039	O				1.39
54.917	0.00	0.04	0.039	O				1.38
55.000	0.00	0.04	0.039	O				1.37
55.083	0.00	0.04	0.038	O				1.36
55.167	0.00	0.04	0.038	O				1.35
55.250	0.00	0.04	0.038	O				1.35
55.333	0.00	0.04	0.038	O				1.34
55.417	0.00	0.04	0.037	O				1.33
55.500	0.00	0.04	0.037	O				1.32
55.583	0.00	0.04	0.037	O				1.32
55.667	0.00	0.04	0.036	O				1.31
55.750	0.00	0.04	0.036	O				1.30
55.833	0.00	0.04	0.036	O				1.29
55.917	0.00	0.04	0.035	O				1.28
56.000	0.00	0.04	0.035	O				1.28
56.083	0.00	0.04	0.035	O				1.27
56.167	0.00	0.04	0.034	O				1.26
56.250	0.00	0.04	0.034	O				1.25
56.333	0.00	0.04	0.034	O				1.25
56.417	0.00	0.04	0.034	O				1.24
56.500	0.00	0.04	0.033	O				1.23

56.583	0.00	0.04	0.033	O				1.22
56.667	0.00	0.04	0.033	O				1.22
56.750	0.00	0.04	0.032	O				1.21
56.833	0.00	0.04	0.032	O				1.20
56.917	0.00	0.04	0.032	O				1.19
57.000	0.00	0.04	0.031	O				1.18
57.083	0.00	0.04	0.031	O				1.18
57.167	0.00	0.04	0.031	O				1.17
57.250	0.00	0.04	0.030	O				1.16
57.333	0.00	0.04	0.030	O				1.15
57.417	0.00	0.04	0.030	O				1.15
57.500	0.00	0.04	0.030	O				1.14
57.583	0.00	0.04	0.029	O				1.13
57.667	0.00	0.04	0.029	O				1.12
57.750	0.00	0.04	0.029	O				1.11
57.833	0.00	0.04	0.028	O				1.11
57.917	0.00	0.04	0.028	O				1.10
58.000	0.00	0.04	0.028	O				1.09
58.083	0.00	0.04	0.027	O				1.08
58.167	0.00	0.04	0.027	O				1.08
58.250	0.00	0.04	0.027	O				1.07
58.333	0.00	0.04	0.026	O				1.06
58.417	0.00	0.04	0.026	O				1.05
58.500	0.00	0.04	0.026	O				1.04
58.583	0.00	0.04	0.025	O				1.04
58.667	0.00	0.04	0.025	O				1.03
58.750	0.00	0.04	0.025	O				1.02
58.833	0.00	0.04	0.025	O				1.01
58.917	0.00	0.04	0.024	O				1.01
59.000	0.00	0.04	0.024	O				1.00
59.083	0.00	0.04	0.024	O				0.98
59.167	0.00	0.04	0.023	O				0.97
59.250	0.00	0.04	0.023	O				0.96
59.333	0.00	0.04	0.023	O				0.95
59.417	0.00	0.04	0.022	O				0.93
59.500	0.00	0.04	0.022	O				0.92
59.583	0.00	0.04	0.022	O				0.91
59.667	0.00	0.04	0.022	O				0.90
59.750	0.00	0.04	0.021	O				0.89
59.833	0.00	0.04	0.021	O				0.88
59.917	0.00	0.04	0.021	O				0.87
60.000	0.00	0.04	0.020	O				0.85
60.083	0.00	0.04	0.020	O				0.84
60.167	0.00	0.04	0.020	O				0.83
60.250	0.00	0.04	0.020	O				0.82
60.333	0.00	0.04	0.019	O				0.81
60.417	0.00	0.04	0.019	O				0.80
60.500	0.00	0.04	0.019	O				0.79
60.583	0.00	0.04	0.019	O				0.78
60.667	0.00	0.03	0.018	O				0.77

60.750	0.00	0.03	0.018	O				0.76
60.833	0.00	0.03	0.018	O				0.75
60.917	0.00	0.03	0.018	O				0.74
61.000	0.00	0.03	0.018	O				0.73
61.083	0.00	0.03	0.017	O				0.72
61.167	0.00	0.03	0.017	O				0.71
61.250	0.00	0.03	0.017	O				0.70
61.333	0.00	0.03	0.017	O				0.69
61.417	0.00	0.03	0.016	O				0.69
61.500	0.00	0.03	0.016	O				0.68
61.583	0.00	0.03	0.016	O				0.67
61.667	0.00	0.03	0.016	O				0.66
61.750	0.00	0.03	0.016	O				0.65
61.833	0.00	0.03	0.015	O				0.64
61.917	0.00	0.03	0.015	O				0.63
62.000	0.00	0.03	0.015	O				0.63
62.083	0.00	0.03	0.015	O				0.62
62.167	0.00	0.03	0.015	O				0.61
62.250	0.00	0.03	0.014	O				0.60
62.333	0.00	0.03	0.014	O				0.59
62.417	0.00	0.03	0.014	O				0.59
62.500	0.00	0.03	0.014	O				0.58
62.583	0.00	0.03	0.014	O				0.57
62.667	0.00	0.03	0.014	O				0.56
62.750	0.00	0.03	0.013	O				0.56
62.833	0.00	0.02	0.013	O				0.55
62.917	0.00	0.02	0.013	O				0.54
63.000	0.00	0.02	0.013	O				0.54
63.083	0.00	0.02	0.013	O				0.53
63.167	0.00	0.02	0.013	O				0.52
63.250	0.00	0.02	0.012	O				0.52
63.333	0.00	0.02	0.012	O				0.51
63.417	0.00	0.02	0.012	O				0.50
63.500	0.00	0.02	0.012	O				0.50
63.583	0.00	0.02	0.012	O				0.49
63.667	0.00	0.02	0.012	O				0.48
63.750	0.00	0.02	0.011	O				0.48
63.833	0.00	0.02	0.011	O				0.47
63.917	0.00	0.02	0.011	O				0.47
64.000	0.00	0.02	0.011	O				0.46
64.083	0.00	0.02	0.011	O				0.45
64.167	0.00	0.02	0.011	O				0.45
64.250	0.00	0.02	0.011	O				0.44
64.333	0.00	0.02	0.010	O				0.44
64.417	0.00	0.02	0.010	O				0.43
64.500	0.00	0.02	0.010	O				0.43
64.583	0.00	0.02	0.010	O				0.42
64.667	0.00	0.02	0.010	O				0.41
64.750	0.00	0.02	0.010	O				0.41
64.833	0.00	0.02	0.010	O				0.40

64.917	0.00	0.02	0.010	O	|	|	|	0.40
65.000	0.00	0.02	0.009	O	|	|	|	0.39
65.083	0.00	0.02	0.009	O	|	|	|	0.39
65.167	0.00	0.02	0.009	O	|	|	|	0.38
65.250	0.00	0.02	0.009	O	|	|	|	0.38
65.333	0.00	0.02	0.009	O	|	|	|	0.37
65.417	0.00	0.02	0.009	O	|	|	|	0.37
65.500	0.00	0.02	0.009	O	|	|	|	0.36
65.583	0.00	0.02	0.009	O	|	|	|	0.36
65.667	0.00	0.02	0.009	O	|	|	|	0.35
65.750	0.00	0.02	0.008	O	|	|	|	0.35
65.833	0.00	0.02	0.008	O	|	|	|	0.35
65.917	0.00	0.02	0.008	O	|	|	|	0.34
66.000	0.00	0.02	0.008	O	|	|	|	0.34
66.083	0.00	0.01	0.008	O	|	|	|	0.33
66.167	0.00	0.01	0.008	O	|	|	|	0.33
66.250	0.00	0.01	0.008	O	|	|	|	0.32
66.333	0.00	0.01	0.008	O	|	|	|	0.32
66.417	0.00	0.01	0.008	O	|	|	|	0.32
66.500	0.00	0.01	0.007	O	|	|	|	0.31
66.583	0.00	0.01	0.007	O	|	|	|	0.31
66.667	0.00	0.01	0.007	O	|	|	|	0.30
66.750	0.00	0.01	0.007	O	|	|	|	0.30
66.833	0.00	0.01	0.007	O	|	|	|	0.30
66.917	0.00	0.01	0.007	O	|	|	|	0.29
67.000	0.00	0.01	0.007	O	|	|	|	0.29
67.083	0.00	0.01	0.007	O	|	|	|	0.28
67.167	0.00	0.01	0.007	O	|	|	|	0.28
67.250	0.00	0.01	0.007	O	|	|	|	0.28
67.333	0.00	0.01	0.007	O	|	|	|	0.27
67.417	0.00	0.01	0.006	O	|	|	|	0.27
67.500	0.00	0.01	0.006	O	|	|	|	0.27
67.583	0.00	0.01	0.006	O	|	|	|	0.26
67.667	0.00	0.01	0.006	O	|	|	|	0.26
67.750	0.00	0.01	0.006	O	|	|	|	0.26
67.833	0.00	0.01	0.006	O	|	|	|	0.25
67.917	0.00	0.01	0.006	O	|	|	|	0.25
68.000	0.00	0.01	0.006	O	|	|	|	0.25
68.083	0.00	0.01	0.006	O	|	|	|	0.24
68.167	0.00	0.01	0.006	O	|	|	|	0.24
68.250	0.00	0.01	0.006	O	|	|	|	0.24
68.333	0.00	0.01	0.006	O	|	|	|	0.23
68.417	0.00	0.01	0.006	O	|	|	|	0.23
68.500	0.00	0.01	0.005	O	|	|	|	0.23
68.583	0.00	0.01	0.005	O	|	|	|	0.23
68.667	0.00	0.01	0.005	O	|	|	|	0.22
68.750	0.00	0.01	0.005	O	|	|	|	0.22
68.833	0.00	0.01	0.005	O	|	|	|	0.22
68.917	0.00	0.01	0.005	O	|	|	|	0.21
69.000	0.00	0.01	0.005	O	|	|	|	0.21

69.083	0.00	0.01	0.005	O	|	|	|	0.21
69.167	0.00	0.01	0.005	O	|	|	|	0.21
69.250	0.00	0.01	0.005	O	|	|	|	0.20
69.333	0.00	0.01	0.005	O	|	|	|	0.20
69.417	0.00	0.01	0.005	O	|	|	|	0.20
69.500	0.00	0.01	0.005	O	|	|	|	0.20
69.583	0.00	0.01	0.005	O	|	|	|	0.19
69.667	0.00	0.01	0.005	O	|	|	|	0.19
69.750	0.00	0.01	0.005	O	|	|	|	0.19
69.833	0.00	0.01	0.004	O	|	|	|	0.19
69.917	0.00	0.01	0.004	O	|	|	|	0.18
70.000	0.00	0.01	0.004	O	|	|	|	0.18
70.083	0.00	0.01	0.004	O	|	|	|	0.18
70.167	0.00	0.01	0.004	O	|	|	|	0.18
70.250	0.00	0.01	0.004	O	|	|	|	0.17
70.333	0.00	0.01	0.004	O	|	|	|	0.17
70.417	0.00	0.01	0.004	O	|	|	|	0.17
70.500	0.00	0.01	0.004	O	|	|	|	0.17
70.583	0.00	0.01	0.004	O	|	|	|	0.17
70.667	0.00	0.01	0.004	O	|	|	|	0.16
70.750	0.00	0.01	0.004	O	|	|	|	0.16
70.833	0.00	0.01	0.004	O	|	|	|	0.16
70.917	0.00	0.01	0.004	O	|	|	|	0.16
71.000	0.00	0.01	0.004	O	|	|	|	0.16
71.083	0.00	0.01	0.004	O	|	|	|	0.15
71.167	0.00	0.01	0.004	O	|	|	|	0.15
71.250	0.00	0.01	0.004	O	|	|	|	0.15
71.333	0.00	0.01	0.004	O	|	|	|	0.15
71.417	0.00	0.01	0.003	O	|	|	|	0.15
71.500	0.00	0.01	0.003	O	|	|	|	0.14
71.583	0.00	0.01	0.003	O	|	|	|	0.14
71.667	0.00	0.01	0.003	O	|	|	|	0.14
71.750	0.00	0.01	0.003	O	|	|	|	0.14
71.833	0.00	0.01	0.003	O	|	|	|	0.14
71.917	0.00	0.01	0.003	O	|	|	|	0.13
72.000	0.00	0.01	0.003	O	|	|	|	0.13
72.083	0.00	0.01	0.003	O	|	|	|	0.13
72.167	0.00	0.01	0.003	O	|	|	|	0.13
72.250	0.00	0.01	0.003	O	|	|	|	0.13
72.333	0.00	0.01	0.003	O	|	|	|	0.13
72.417	0.00	0.01	0.003	O	|	|	|	0.12
72.500	0.00	0.01	0.003	O	|	|	|	0.12
72.583	0.00	0.01	0.003	O	|	|	|	0.12
72.667	0.00	0.01	0.003	O	|	|	|	0.12
72.750	0.00	0.01	0.003	O	|	|	|	0.12
72.833	0.00	0.01	0.003	O	|	|	|	0.12
72.917	0.00	0.01	0.003	O	|	|	|	0.12
73.000	0.00	0.01	0.003	O	|	|	|	0.11
73.083	0.00	0.01	0.003	O	|	|	|	0.11
73.167	0.00	0.00	0.003	O	|	|	|	0.11

73.250	0.00	0.00	0.003	O	|	|	|	0.11
73.333	0.00	0.00	0.003	O	|	|	|	0.11
73.417	0.00	0.00	0.003	O	|	|	|	0.11
73.500	0.00	0.00	0.003	O	|	|	|	0.11
73.583	0.00	0.00	0.002	O	|	|	|	0.10
73.667	0.00	0.00	0.002	O	|	|	|	0.10
73.750	0.00	0.00	0.002	O	|	|	|	0.10
73.833	0.00	0.00	0.002	O	|	|	|	0.10
73.917	0.00	0.00	0.002	O	|	|	|	0.10
74.000	0.00	0.00	0.002	O	|	|	|	0.10
74.083	0.00	0.00	0.002	O	|	|	|	0.10
74.167	0.00	0.00	0.002	O	|	|	|	0.10
74.250	0.00	0.00	0.002	O	|	|	|	0.09
74.333	0.00	0.00	0.002	O	|	|	|	0.09
74.417	0.00	0.00	0.002	O	|	|	|	0.09
74.500	0.00	0.00	0.002	O	|	|	|	0.09
74.583	0.00	0.00	0.002	O	|	|	|	0.09
74.667	0.00	0.00	0.002	O	|	|	|	0.09
74.750	0.00	0.00	0.002	O	|	|	|	0.09
74.833	0.00	0.00	0.002	O	|	|	|	0.09
74.917	0.00	0.00	0.002	O	|	|	|	0.08
75.000	0.00	0.00	0.002	O	|	|	|	0.08
75.083	0.00	0.00	0.002	O	|	|	|	0.08
75.167	0.00	0.00	0.002	O	|	|	|	0.08
75.250	0.00	0.00	0.002	O	|	|	|	0.08
75.333	0.00	0.00	0.002	O	|	|	|	0.08
75.417	0.00	0.00	0.002	O	|	|	|	0.08
75.500	0.00	0.00	0.002	O	|	|	|	0.08
75.583	0.00	0.00	0.002	O	|	|	|	0.08
75.667	0.00	0.00	0.002	O	|	|	|	0.08
75.750	0.00	0.00	0.002	O	|	|	|	0.07
75.833	0.00	0.00	0.002	O	|	|	|	0.07
75.917	0.00	0.00	0.002	O	|	|	|	0.07
76.000	0.00	0.00	0.002	O	|	|	|	0.07
76.083	0.00	0.00	0.002	O	|	|	|	0.07
76.167	0.00	0.00	0.002	O	|	|	|	0.07
76.250	0.00	0.00	0.002	O	|	|	|	0.07
76.333	0.00	0.00	0.002	O	|	|	|	0.07
76.417	0.00	0.00	0.002	O	|	|	|	0.07
76.500	0.00	0.00	0.002	O	|	|	|	0.07
76.583	0.00	0.00	0.002	O	|	|	|	0.07
76.667	0.00	0.00	0.002	O	|	|	|	0.06
76.750	0.00	0.00	0.002	O	|	|	|	0.06
76.833	0.00	0.00	0.002	O	|	|	|	0.06
76.917	0.00	0.00	0.001	O	|	|	|	0.06
77.000	0.00	0.00	0.001	O	|	|	|	0.06
77.083	0.00	0.00	0.001	O	|	|	|	0.06
77.167	0.00	0.00	0.001	O	|	|	|	0.06
77.250	0.00	0.00	0.001	O	|	|	|	0.06
77.333	0.00	0.00	0.001	O	|	|	|	0.06

77.417	0.00	0.00	0.001	O	|	|	|	0.06
77.500	0.00	0.00	0.001	O	|	|	|	0.06
77.583	0.00	0.00	0.001	O	|	|	|	0.06
77.667	0.00	0.00	0.001	O	|	|	|	0.06
77.750	0.00	0.00	0.001	O	|	|	|	0.05
77.833	0.00	0.00	0.001	O	|	|	|	0.05
77.917	0.00	0.00	0.001	O	|	|	|	0.05
78.000	0.00	0.00	0.001	O	|	|	|	0.05
78.083	0.00	0.00	0.001	O	|	|	|	0.05
78.167	0.00	0.00	0.001	O	|	|	|	0.05
78.250	0.00	0.00	0.001	O	|	|	|	0.05
78.333	0.00	0.00	0.001	O	|	|	|	0.05
78.417	0.00	0.00	0.001	O	|	|	|	0.05
78.500	0.00	0.00	0.001	O	|	|	|	0.05
78.583	0.00	0.00	0.001	O	|	|	|	0.05
78.667	0.00	0.00	0.001	O	|	|	|	0.05
78.750	0.00	0.00	0.001	O	|	|	|	0.05
78.833	0.00	0.00	0.001	O	|	|	|	0.05
78.917	0.00	0.00	0.001	O	|	|	|	0.05
79.000	0.00	0.00	0.001	O	|	|	|	0.04
79.083	0.00	0.00	0.001	O	|	|	|	0.04
79.167	0.00	0.00	0.001	O	|	|	|	0.04
79.250	0.00	0.00	0.001	O	|	|	|	0.04
79.333	0.00	0.00	0.001	O	|	|	|	0.04
79.417	0.00	0.00	0.001	O	|	|	|	0.04
79.500	0.00	0.00	0.001	O	|	|	|	0.04
79.583	0.00	0.00	0.001	O	|	|	|	0.04
79.667	0.00	0.00	0.001	O	|	|	|	0.04
79.750	0.00	0.00	0.001	O	|	|	|	0.04
79.833	0.00	0.00	0.001	O	|	|	|	0.04
79.917	0.00	0.00	0.001	O	|	|	|	0.04
80.000	0.00	0.00	0.001	O	|	|	|	0.04
80.083	0.00	0.00	0.001	O	|	|	|	0.04
80.167	0.00	0.00	0.001	O	|	|	|	0.04
80.250	0.00	0.00	0.001	O	|	|	|	0.04
80.333	0.00	0.00	0.001	O	|	|	|	0.04
80.417	0.00	0.00	0.001	O	|	|	|	0.04
80.500	0.00	0.00	0.001	O	|	|	|	0.04
80.583	0.00	0.00	0.001	O	|	|	|	0.04
80.667	0.00	0.00	0.001	O	|	|	|	0.03
80.750	0.00	0.00	0.001	O	|	|	|	0.03
80.833	0.00	0.00	0.001	O	|	|	|	0.03
80.917	0.00	0.00	0.001	O	|	|	|	0.03
81.000	0.00	0.00	0.001	O	|	|	|	0.03
81.083	0.00	0.00	0.001	O	|	|	|	0.03
81.167	0.00	0.00	0.001	O	|	|	|	0.03
81.250	0.00	0.00	0.001	O	|	|	|	0.03
81.333	0.00	0.00	0.001	O	|	|	|	0.03
81.417	0.00	0.00	0.001	O	|	|	|	0.03
81.500	0.00	0.00	0.001	O	|	|	|	0.03

81.583	0.00	0.00	0.001	O	|	|	|	|	0.03
81.667	0.00	0.00	0.001	O	|	|	|	|	0.03
81.750	0.00	0.00	0.001	O	|	|	|	|	0.03
81.833	0.00	0.00	0.001	O	|	|	|	|	0.03
81.917	0.00	0.00	0.001	O	|	|	|	|	0.03
82.000	0.00	0.00	0.001	O	|	|	|	|	0.03
82.083	0.00	0.00	0.001	O	|	|	|	|	0.03
82.167	0.00	0.00	0.001	O	|	|	|	|	0.03
82.250	0.00	0.00	0.001	O	|	|	|	|	0.03
82.333	0.00	0.00	0.001	O	|	|	|	|	0.03
82.417	0.00	0.00	0.001	O	|	|	|	|	0.03
82.500	0.00	0.00	0.001	O	|	|	|	|	0.03
82.583	0.00	0.00	0.001	O	|	|	|	|	0.03
82.667	0.00	0.00	0.001	O	|	|	|	|	0.03
82.750	0.00	0.00	0.001	O	|	|	|	|	0.03
82.833	0.00	0.00	0.001	O	|	|	|	|	0.02
82.917	0.00	0.00	0.001	O	|	|	|	|	0.02
83.000	0.00	0.00	0.001	O	|	|	|	|	0.02
83.083	0.00	0.00	0.001	O	|	|	|	|	0.02
83.167	0.00	0.00	0.001	O	|	|	|	|	0.02
83.250	0.00	0.00	0.001	O	|	|	|	|	0.02
83.333	0.00	0.00	0.001	O	|	|	|	|	0.02
83.417	0.00	0.00	0.001	O	|	|	|	|	0.02
83.500	0.00	0.00	0.001	O	|	|	|	|	0.02
83.583	0.00	0.00	0.001	O	|	|	|	|	0.02

**********HYDROGRAPH DATA**********

Number of intervals = 1003
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.045 (CFS)
Total volume = 0.241 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
100 yr
6 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris6100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 80
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 2.332 (CFS)
Total volume = 0.324 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 80
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.6	1.17	1.75	2.33	Depth (Ft.)
0.083	0.04	0.00	0.000	O	|	|	|	|	0.01
0.167	0.16	0.00	0.001	O I	|	|	|	|	0.03
0.250	0.21	0.00	0.002	O I	|	|	|	|	0.09
0.333	0.24	0.01	0.004	O I	|	|	|	|	0.15
0.417	0.25	0.01	0.005	O I	|	|	|	|	0.22
0.500	0.27	0.01	0.007	O I	|	|	|	|	0.29
0.583	0.29	0.02	0.009	O I	|	|	|	|	0.36
0.667	0.30	0.02	0.011	O I	|	|	|	|	0.45
0.750	0.31	0.02	0.013	O I	|	|	|	|	0.53
0.833	0.31	0.03	0.015	O I	|	|	|	|	0.61
0.917	0.31	0.03	0.017	O I	|	|	|	|	0.69
1.000	0.32	0.03	0.019	O I	|	|	|	|	0.77
1.083	0.34	0.04	0.021	O I	|	|	|	|	0.86
1.167	0.35	0.04	0.023	O I	|	|	|	|	0.95
1.250	0.36	0.04	0.025	O I	|	|	|	|	1.02
1.333	0.36	0.04	0.027	O I	|	|	|	|	1.07
1.417	0.36	0.04	0.029	O I	|	|	|	|	1.13
1.500	0.36	0.04	0.031	O I	|	|	|	|	1.18
1.583	0.36	0.04	0.033	O I	|	|	|	|	1.24
1.667	0.36	0.04	0.036	O I	|	|	|	|	1.29
1.750	0.36	0.04	0.038	O I	|	|	|	|	1.34
1.833	0.36	0.04	0.040	O I	|	|	|	|	1.40
1.917	0.36	0.04	0.042	O I	|	|	|	|	1.45
2.000	0.37	0.04	0.044	O I	|	|	|	|	1.51
2.083	0.38	0.04	0.047	O I	|	|	|	|	1.56
2.167	0.38	0.04	0.049	O I	|	|	|	|	1.62
2.250	0.39	0.04	0.051	O I	|	|	|	|	1.68
2.333	0.40	0.04	0.054	O I	|	|	|	|	1.74

```
2.417    0.40    0.04      0.056  O    I  |        |        |        |     1.80
2.500    0.40    0.04      0.059  O    I  |        |        |        |     1.86
2.583    0.40    0.04      0.061  O    I  |        |        |        |     1.93
2.667    0.40    0.04      0.063  O    I  |        |        |        |     1.99
2.750    0.41    0.04      0.066  O    I  |        |        |        |     2.05
2.833    0.43    0.04      0.069  O    I  |        |        |        |     2.11
2.917    0.44    0.04      0.071  O     I |        |        |        |     2.18
3.000    0.45    0.04      0.074  O     I |        |        |        |     2.25
3.083    0.45    0.04      0.077  O     I |        |        |        |     2.32
3.167    0.46    0.04      0.080  O     I |        |        |        |     2.39
3.250    0.48    0.04      0.083  O     I |        |        |        |     2.46
3.333    0.49    0.04      0.086  O     I |        |        |        |     2.54
3.417    0.50    0.04      0.089  O     I |        |        |        |     2.62
3.500    0.53    0.04      0.092  O      I|        |        |        |     2.70
3.583    0.57    0.04      0.095  O      I|        |        |        |     2.78
3.667    0.60    0.04      0.099  O       I        |        |        |     2.88
3.750    0.62    0.04      0.103  O       I        |        |        |     2.97
3.833    0.65    0.04      0.107  O       I        |        |        |     3.08
3.917    0.67    0.04      0.111  O       |I       |        |        |     3.18
4.000    0.70    0.04      0.116  O       |I       |        |        |     3.29
4.083    0.72    0.04      0.120  O       |I       |        |        |     3.40
4.167    0.75    0.04      0.125  O       | I      |        |        |     3.52
4.250    0.80    0.04      0.130  O       | I      |        |        |     3.65
4.333    0.85    0.04      0.135  O       |  I     |        |        |     3.78
4.417    0.90    0.04      0.141  O       |   I    |        |        |     3.93
4.500    0.95    0.04      0.147  O       |   I    |        |        |     4.08
4.583    0.97    0.04      0.153  O       |    I   |        |        |     4.24
4.667    1.02    0.04      0.160  O       |    I   |        |        |     4.40
4.750    1.07    0.04      0.167  O       |     I  |        |        |     4.57
4.833    1.11    0.04      0.174  O       |      I |        |        |     4.75
4.917    1.14    0.04      0.182  O       |      I |        |        |     4.93
5.000    1.18    0.04      0.189  O       |       I        |        |     5.12
5.083    1.27    0.04      0.197  O       |       |I       |        |     5.32
5.167    1.47    0.04      0.207  O       |       |   I    |        |     5.55
5.250    1.69    0.04      0.217  O       |       |      I |        |     5.81
5.333    1.86    0.04      0.229  O       |       |       |I       |     6.10
5.417    2.05    0.04      0.242  O       |       |       |   I    |     6.43
5.500    2.33    0.04      0.257  O       |       |       |      I |     6.79
5.583    2.28    0.04      0.273  O       |       |       |      I |     7.18
5.667    1.34    0.04      0.285  O       |       | I     |        |     7.48
5.750    0.82    0.04      0.292  O       |  I    |       |        |     7.66
5.833    0.56    0.04      0.296  O      I|       |       |        |     7.77
5.917    0.40    0.04      0.299  O    I  |       |       |        |     7.84
6.000    0.27    0.04      0.301  O  I    |       |       |        |     7.89
6.083    0.17    0.04      0.302  O I     |       |       |        |     7.92
6.167    0.08    0.04      0.303  OI      |       |       |        |     7.93
6.250    0.03    0.04      0.303  O       |       |       |        |     7.93
6.333    0.02    0.04      0.303  O       |       |       |        |     7.93
6.417    0.01    0.04      0.303  O       |       |       |        |     7.93
6.500    0.00    0.04      0.302  O       |       |       |        |     7.92
```

6.583	0.00	0.04	0.302	O				7.91
6.667	0.00	0.04	0.302	O				7.91
6.750	0.00	0.04	0.302	O				7.90
6.833	0.00	0.04	0.301	O				7.89
6.917	0.00	0.04	0.301	O				7.88
7.000	0.00	0.04	0.301	O				7.87
7.083	0.00	0.04	0.300	O				7.87
7.167	0.00	0.04	0.300	O				7.86
7.250	0.00	0.04	0.300	O				7.85
7.333	0.00	0.04	0.299	O				7.84
7.417	0.00	0.04	0.299	O				7.84
7.500	0.00	0.04	0.299	O				7.83
7.583	0.00	0.04	0.298	O				7.82
7.667	0.00	0.04	0.298	O				7.81
7.750	0.00	0.04	0.298	O				7.81
7.833	0.00	0.04	0.298	O				7.80
7.917	0.00	0.04	0.297	O				7.79
8.000	0.00	0.04	0.297	O				7.78
8.083	0.00	0.04	0.297	O				7.78
8.167	0.00	0.04	0.296	O				7.77
8.250	0.00	0.04	0.296	O				7.76
8.333	0.00	0.04	0.296	O				7.75
8.417	0.00	0.04	0.295	O				7.74
8.500	0.00	0.04	0.295	O				7.74
8.583	0.00	0.04	0.295	O				7.73
8.667	0.00	0.04	0.294	O				7.72
8.750	0.00	0.04	0.294	O				7.71
8.833	0.00	0.04	0.294	O				7.71
8.917	0.00	0.04	0.294	O				7.70
9.000	0.00	0.04	0.293	O				7.69
9.083	0.00	0.04	0.293	O				7.68
9.167	0.00	0.04	0.293	O				7.68
9.250	0.00	0.04	0.292	O				7.67
9.333	0.00	0.04	0.292	O				7.66
9.417	0.00	0.04	0.292	O				7.65
9.500	0.00	0.04	0.291	O				7.64
9.583	0.00	0.04	0.291	O				7.64
9.667	0.00	0.04	0.291	O				7.63
9.750	0.00	0.04	0.290	O				7.62
9.833	0.00	0.04	0.290	O				7.61
9.917	0.00	0.04	0.290	O				7.61
10.000	0.00	0.04	0.290	O				7.60
10.083	0.00	0.04	0.289	O				7.59
10.167	0.00	0.04	0.289	O				7.58
10.250	0.00	0.04	0.289	O				7.58
10.333	0.00	0.04	0.288	O				7.57
10.417	0.00	0.04	0.288	O				7.56
10.500	0.00	0.04	0.288	O				7.55
10.583	0.00	0.04	0.287	O				7.55
10.667	0.00	0.04	0.287	O				7.54

10.750	0.00	0.04	0.287	O	|	|	|	7.53
10.833	0.00	0.04	0.286	O	|	|	|	7.52
10.917	0.00	0.04	0.286	O	|	|	|	7.51
11.000	0.00	0.04	0.286	O	|	|	|	7.51
11.083	0.00	0.04	0.285	O	|	|	|	7.50
11.167	0.00	0.04	0.285	O	|	|	|	7.49
11.250	0.00	0.04	0.285	O	|	|	|	7.48
11.333	0.00	0.04	0.285	O	|	|	|	7.48
11.417	0.00	0.04	0.284	O	|	|	|	7.47
11.500	0.00	0.04	0.284	O	|	|	|	7.46
11.583	0.00	0.04	0.284	O	|	|	|	7.45
11.667	0.00	0.04	0.283	O	|	|	|	7.45
11.750	0.00	0.04	0.283	O	|	|	|	7.44
11.833	0.00	0.04	0.283	O	|	|	|	7.43
11.917	0.00	0.04	0.282	O	|	|	|	7.42
12.000	0.00	0.04	0.282	O	|	|	|	7.42
12.083	0.00	0.04	0.282	O	|	|	|	7.41
12.167	0.00	0.04	0.281	O	|	|	|	7.40
12.250	0.00	0.04	0.281	O	|	|	|	7.39
12.333	0.00	0.04	0.281	O	|	|	|	7.38
12.417	0.00	0.04	0.281	O	|	|	|	7.38
12.500	0.00	0.04	0.280	O	|	|	|	7.37
12.583	0.00	0.04	0.280	O	|	|	|	7.36
12.667	0.00	0.04	0.280	O	|	|	|	7.35
12.750	0.00	0.04	0.279	O	|	|	|	7.35
12.833	0.00	0.04	0.279	O	|	|	|	7.34
12.917	0.00	0.04	0.279	O	|	|	|	7.33
13.000	0.00	0.04	0.278	O	|	|	|	7.32
13.083	0.00	0.04	0.278	O	|	|	|	7.32
13.167	0.00	0.04	0.278	O	|	|	|	7.31
13.250	0.00	0.04	0.277	O	|	|	|	7.30
13.333	0.00	0.04	0.277	O	|	|	|	7.29
13.417	0.00	0.04	0.277	O	|	|	|	7.29
13.500	0.00	0.04	0.276	O	|	|	|	7.28
13.583	0.00	0.04	0.276	O	|	|	|	7.27
13.667	0.00	0.04	0.276	O	|	|	|	7.26
13.750	0.00	0.04	0.276	O	|	|	|	7.25
13.833	0.00	0.04	0.275	O	|	|	|	7.25
13.917	0.00	0.04	0.275	O	|	|	|	7.24
14.000	0.00	0.04	0.275	O	|	|	|	7.23
14.083	0.00	0.04	0.274	O	|	|	|	7.22
14.167	0.00	0.04	0.274	O	|	|	|	7.22
14.250	0.00	0.04	0.274	O	|	|	|	7.21
14.333	0.00	0.04	0.273	O	|	|	|	7.20
14.417	0.00	0.04	0.273	O	|	|	|	7.19
14.500	0.00	0.04	0.273	O	|	|	|	7.19
14.583	0.00	0.04	0.272	O	|	|	|	7.18
14.667	0.00	0.04	0.272	O	|	|	|	7.17
14.750	0.00	0.04	0.272	O	|	|	|	7.16
14.833	0.00	0.04	0.272	O	|	|	|	7.16

14.917	0.00	0.04	0.271	O	|	|	|	7.15
15.000	0.00	0.04	0.271	O	|	|	|	7.14
15.083	0.00	0.04	0.271	O	|	|	|	7.13
15.167	0.00	0.04	0.270	O	|	|	|	7.12
15.250	0.00	0.04	0.270	O	|	|	|	7.12
15.333	0.00	0.04	0.270	O	|	|	|	7.11
15.417	0.00	0.04	0.269	O	|	|	|	7.10
15.500	0.00	0.04	0.269	O	|	|	|	7.09
15.583	0.00	0.04	0.269	O	|	|	|	7.09
15.667	0.00	0.04	0.268	O	|	|	|	7.08
15.750	0.00	0.04	0.268	O	|	|	|	7.07
15.833	0.00	0.04	0.268	O	|	|	|	7.06
15.917	0.00	0.04	0.268	O	|	|	|	7.06
16.000	0.00	0.04	0.267	O	|	|	|	7.05
16.083	0.00	0.04	0.267	O	|	|	|	7.04
16.167	0.00	0.04	0.267	O	|	|	|	7.03
16.250	0.00	0.04	0.266	O	|	|	|	7.03
16.333	0.00	0.04	0.266	O	|	|	|	7.02
16.417	0.00	0.04	0.266	O	|	|	|	7.01
16.500	0.00	0.04	0.265	O	|	|	|	7.00
16.583	0.00	0.04	0.265	O	|	|	|	6.99
16.667	0.00	0.04	0.265	O	|	|	|	6.99
16.750	0.00	0.04	0.264	O	|	|	|	6.98
16.833	0.00	0.04	0.264	O	|	|	|	6.97
16.917	0.00	0.04	0.264	O	|	|	|	6.96
17.000	0.00	0.04	0.263	O	|	|	|	6.96
17.083	0.00	0.04	0.263	O	|	|	|	6.95
17.167	0.00	0.04	0.263	O	|	|	|	6.94
17.250	0.00	0.04	0.263	O	|	|	|	6.93
17.333	0.00	0.04	0.262	O	|	|	|	6.93
17.417	0.00	0.04	0.262	O	|	|	|	6.92
17.500	0.00	0.04	0.262	O	|	|	|	6.91
17.583	0.00	0.04	0.261	O	|	|	|	6.90
17.667	0.00	0.04	0.261	O	|	|	|	6.89
17.750	0.00	0.04	0.261	O	|	|	|	6.89
17.833	0.00	0.04	0.260	O	|	|	|	6.88
17.917	0.00	0.04	0.260	O	|	|	|	6.87
18.000	0.00	0.04	0.260	O	|	|	|	6.86
18.083	0.00	0.04	0.259	O	|	|	|	6.86
18.167	0.00	0.04	0.259	O	|	|	|	6.85
18.250	0.00	0.04	0.259	O	|	|	|	6.84
18.333	0.00	0.04	0.259	O	|	|	|	6.83
18.417	0.00	0.04	0.258	O	|	|	|	6.83
18.500	0.00	0.04	0.258	O	|	|	|	6.82
18.583	0.00	0.04	0.258	O	|	|	|	6.81
18.667	0.00	0.04	0.257	O	|	|	|	6.80
18.750	0.00	0.04	0.257	O	|	|	|	6.80
18.833	0.00	0.04	0.257	O	|	|	|	6.79
18.917	0.00	0.04	0.256	O	|	|	|	6.78
19.000	0.00	0.04	0.256	O	|	|	|	6.77

19.083	0.00	0.04	0.256	O	|	|	|	6.76
19.167	0.00	0.04	0.255	O	|	|	|	6.76
19.250	0.00	0.04	0.255	O	|	|	|	6.75
19.333	0.00	0.04	0.255	O	|	|	|	6.74
19.417	0.00	0.04	0.254	O	|	|	|	6.73
19.500	0.00	0.04	0.254	O	|	|	|	6.73
19.583	0.00	0.04	0.254	O	|	|	|	6.72
19.667	0.00	0.04	0.254	O	|	|	|	6.71
19.750	0.00	0.04	0.253	O	|	|	|	6.70
19.833	0.00	0.04	0.253	O	|	|	|	6.70
19.917	0.00	0.04	0.253	O	|	|	|	6.69
20.000	0.00	0.04	0.252	O	|	|	|	6.68
20.083	0.00	0.04	0.252	O	|	|	|	6.67
20.167	0.00	0.04	0.252	O	|	|	|	6.67
20.250	0.00	0.04	0.251	O	|	|	|	6.66
20.333	0.00	0.04	0.251	O	|	|	|	6.65
20.417	0.00	0.04	0.251	O	|	|	|	6.64
20.500	0.00	0.04	0.250	O	|	|	|	6.63
20.583	0.00	0.04	0.250	O	|	|	|	6.63
20.667	0.00	0.04	0.250	O	|	|	|	6.62
20.750	0.00	0.04	0.250	O	|	|	|	6.61
20.833	0.00	0.04	0.249	O	|	|	|	6.60
20.917	0.00	0.04	0.249	O	|	|	|	6.60
21.000	0.00	0.04	0.249	O	|	|	|	6.59
21.083	0.00	0.04	0.248	O	|	|	|	6.58
21.167	0.00	0.04	0.248	O	|	|	|	6.57
21.250	0.00	0.04	0.248	O	|	|	|	6.57
21.333	0.00	0.04	0.247	O	|	|	|	6.56
21.417	0.00	0.04	0.247	O	|	|	|	6.55
21.500	0.00	0.04	0.247	O	|	|	|	6.54
21.583	0.00	0.04	0.246	O	|	|	|	6.54
21.667	0.00	0.04	0.246	O	|	|	|	6.53
21.750	0.00	0.04	0.246	O	|	|	|	6.52
21.833	0.00	0.04	0.246	O	|	|	|	6.51
21.917	0.00	0.04	0.245	O	|	|	|	6.50
22.000	0.00	0.04	0.245	O	|	|	|	6.50
22.083	0.00	0.04	0.245	O	|	|	|	6.49
22.167	0.00	0.04	0.244	O	|	|	|	6.48
22.250	0.00	0.04	0.244	O	|	|	|	6.47
22.333	0.00	0.04	0.244	O	|	|	|	6.47
22.417	0.00	0.04	0.243	O	|	|	|	6.46
22.500	0.00	0.04	0.243	O	|	|	|	6.45
22.583	0.00	0.04	0.243	O	|	|	|	6.44
22.667	0.00	0.04	0.242	O	|	|	|	6.44
22.750	0.00	0.04	0.242	O	|	|	|	6.43
22.833	0.00	0.04	0.242	O	|	|	|	6.42
22.917	0.00	0.04	0.241	O	|	|	|	6.41
23.000	0.00	0.04	0.241	O	|	|	|	6.41
23.083	0.00	0.04	0.241	O	|	|	|	6.40
23.167	0.00	0.04	0.241	O	|	|	|	6.39

23.250	0.00	0.04	0.240	O	|	|	|	6.38
23.333	0.00	0.04	0.240	O	|	|	|	6.37
23.417	0.00	0.04	0.240	O	|	|	|	6.37
23.500	0.00	0.04	0.239	O	|	|	|	6.36
23.583	0.00	0.04	0.239	O	|	|	|	6.35
23.667	0.00	0.04	0.239	O	|	|	|	6.34
23.750	0.00	0.04	0.238	O	|	|	|	6.34
23.833	0.00	0.04	0.238	O	|	|	|	6.33
23.917	0.00	0.04	0.238	O	|	|	|	6.32
24.000	0.00	0.04	0.237	O	|	|	|	6.31
24.083	0.00	0.04	0.237	O	|	|	|	6.31
24.167	0.00	0.04	0.237	O	|	|	|	6.30
24.250	0.00	0.04	0.237	O	|	|	|	6.29
24.333	0.00	0.04	0.236	O	|	|	|	6.28
24.417	0.00	0.04	0.236	O	|	|	|	6.28
24.500	0.00	0.04	0.236	O	|	|	|	6.27
24.583	0.00	0.04	0.235	O	|	|	|	6.26
24.667	0.00	0.04	0.235	O	|	|	|	6.25
24.750	0.00	0.04	0.235	O	|	|	|	6.24
24.833	0.00	0.04	0.234	O	|	|	|	6.24
24.917	0.00	0.04	0.234	O	|	|	|	6.23
25.000	0.00	0.04	0.234	O	|	|	|	6.22
25.083	0.00	0.04	0.233	O	|	|	|	6.21
25.167	0.00	0.04	0.233	O	|	|	|	6.21
25.250	0.00	0.04	0.233	O	|	|	|	6.20
25.333	0.00	0.04	0.232	O	|	|	|	6.19
25.417	0.00	0.04	0.232	O	|	|	|	6.18
25.500	0.00	0.04	0.232	O	|	|	|	6.18
25.583	0.00	0.04	0.232	O	|	|	|	6.17
25.667	0.00	0.04	0.231	O	|	|	|	6.16
25.750	0.00	0.04	0.231	O	|	|	|	6.15
25.833	0.00	0.04	0.231	O	|	|	|	6.15
25.917	0.00	0.04	0.230	O	|	|	|	6.14
26.000	0.00	0.04	0.230	O	|	|	|	6.13
26.083	0.00	0.04	0.230	O	|	|	|	6.12
26.167	0.00	0.04	0.229	O	|	|	|	6.11
26.250	0.00	0.04	0.229	O	|	|	|	6.11
26.333	0.00	0.04	0.229	O	|	|	|	6.10
26.417	0.00	0.04	0.228	O	|	|	|	6.09
26.500	0.00	0.04	0.228	O	|	|	|	6.08
26.583	0.00	0.04	0.228	O	|	|	|	6.08
26.667	0.00	0.04	0.228	O	|	|	|	6.07
26.750	0.00	0.04	0.227	O	|	|	|	6.06
26.833	0.00	0.04	0.227	O	|	|	|	6.05
26.917	0.00	0.04	0.227	O	|	|	|	6.05
27.000	0.00	0.04	0.226	O	|	|	|	6.04
27.083	0.00	0.04	0.226	O	|	|	|	6.03
27.167	0.00	0.04	0.226	O	|	|	|	6.02
27.250	0.00	0.04	0.225	O	|	|	|	6.01
27.333	0.00	0.04	0.225	O	|	|	|	6.01

27.417	0.00	0.04	0.225	O				6.00
27.500	0.00	0.04	0.224	O				5.99
27.583	0.00	0.04	0.224	O				5.98
27.667	0.00	0.04	0.224	O				5.98
27.750	0.00	0.04	0.223	O				5.97
27.833	0.00	0.04	0.223	O				5.96
27.917	0.00	0.04	0.223	O				5.95
28.000	0.00	0.04	0.223	O				5.95
28.083	0.00	0.04	0.222	O				5.94
28.167	0.00	0.04	0.222	O				5.93
28.250	0.00	0.04	0.222	O				5.92
28.333	0.00	0.04	0.221	O				5.92
28.417	0.00	0.04	0.221	O				5.91
28.500	0.00	0.04	0.221	O				5.90
28.583	0.00	0.04	0.220	O				5.89
28.667	0.00	0.04	0.220	O				5.88
28.750	0.00	0.04	0.220	O				5.88
28.833	0.00	0.04	0.219	O				5.87
28.917	0.00	0.04	0.219	O				5.86
29.000	0.00	0.04	0.219	O				5.85
29.083	0.00	0.04	0.219	O				5.85
29.167	0.00	0.04	0.218	O				5.84
29.250	0.00	0.04	0.218	O				5.83
29.333	0.00	0.04	0.218	O				5.82
29.417	0.00	0.04	0.217	O				5.82
29.500	0.00	0.04	0.217	O				5.81
29.583	0.00	0.04	0.217	O				5.80
29.667	0.00	0.04	0.216	O				5.79
29.750	0.00	0.04	0.216	O				5.79
29.833	0.00	0.04	0.216	O				5.78
29.917	0.00	0.04	0.215	O				5.77
30.000	0.00	0.04	0.215	O				5.76
30.083	0.00	0.04	0.215	O				5.75
30.167	0.00	0.04	0.215	O				5.75
30.250	0.00	0.04	0.214	O				5.74
30.333	0.00	0.04	0.214	O				5.73
30.417	0.00	0.04	0.214	O				5.72
30.500	0.00	0.04	0.213	O				5.72
30.583	0.00	0.04	0.213	O				5.71
30.667	0.00	0.04	0.213	O				5.70
30.750	0.00	0.04	0.212	O				5.69
30.833	0.00	0.04	0.212	O				5.69
30.917	0.00	0.04	0.212	O				5.68
31.000	0.00	0.04	0.211	O				5.67
31.083	0.00	0.04	0.211	O				5.66
31.167	0.00	0.04	0.211	O				5.66
31.250	0.00	0.04	0.210	O				5.65
31.333	0.00	0.04	0.210	O				5.64
31.417	0.00	0.04	0.210	O				5.63
31.500	0.00	0.04	0.210	O				5.62

31.583	0.00	0.04	0.209	O				5.62
31.667	0.00	0.04	0.209	O				5.61
31.750	0.00	0.04	0.209	O				5.60
31.833	0.00	0.04	0.208	O				5.59
31.917	0.00	0.04	0.208	O				5.59
32.000	0.00	0.04	0.208	O				5.58
32.083	0.00	0.04	0.207	O				5.57
32.167	0.00	0.04	0.207	O				5.56
32.250	0.00	0.04	0.207	O				5.56
32.333	0.00	0.04	0.206	O				5.55
32.417	0.00	0.04	0.206	O				5.54
32.500	0.00	0.04	0.206	O				5.53
32.583	0.00	0.04	0.206	O				5.53
32.667	0.00	0.04	0.205	O				5.52
32.750	0.00	0.04	0.205	O				5.51
32.833	0.00	0.04	0.205	O				5.50
32.917	0.00	0.04	0.204	O				5.49
33.000	0.00	0.04	0.204	O				5.49
33.083	0.00	0.04	0.204	O				5.48
33.167	0.00	0.04	0.203	O				5.47
33.250	0.00	0.04	0.203	O				5.46
33.333	0.00	0.04	0.203	O				5.46
33.417	0.00	0.04	0.202	O				5.45
33.500	0.00	0.04	0.202	O				5.44
33.583	0.00	0.04	0.202	O				5.43
33.667	0.00	0.04	0.201	O				5.43
33.750	0.00	0.04	0.201	O				5.42
33.833	0.00	0.04	0.201	O				5.41
33.917	0.00	0.04	0.201	O				5.40
34.000	0.00	0.04	0.200	O				5.40
34.083	0.00	0.04	0.200	O				5.39
34.167	0.00	0.04	0.200	O				5.38
34.250	0.00	0.04	0.199	O				5.37
34.333	0.00	0.04	0.199	O				5.36
34.417	0.00	0.04	0.199	O				5.36
34.500	0.00	0.04	0.198	O				5.35
34.583	0.00	0.04	0.198	O				5.34
34.667	0.00	0.04	0.198	O				5.33
34.750	0.00	0.04	0.197	O				5.33
34.833	0.00	0.04	0.197	O				5.32
34.917	0.00	0.04	0.197	O				5.31
35.000	0.00	0.04	0.197	O				5.30
35.083	0.00	0.04	0.196	O				5.30
35.167	0.00	0.04	0.196	O				5.29
35.250	0.00	0.04	0.196	O				5.28
35.333	0.00	0.04	0.195	O				5.27
35.417	0.00	0.04	0.195	O				5.27
35.500	0.00	0.04	0.195	O				5.26
35.583	0.00	0.04	0.194	O				5.25
35.667	0.00	0.04	0.194	O				5.24

35.750	0.00	0.04	0.194	O				5.23
35.833	0.00	0.04	0.193	O				5.23
35.917	0.00	0.04	0.193	O				5.22
36.000	0.00	0.04	0.193	O				5.21
36.083	0.00	0.04	0.193	O				5.20
36.167	0.00	0.04	0.192	O				5.20
36.250	0.00	0.04	0.192	O				5.19
36.333	0.00	0.04	0.192	O				5.18
36.417	0.00	0.04	0.191	O				5.17
36.500	0.00	0.04	0.191	O				5.17
36.583	0.00	0.04	0.191	O				5.16
36.667	0.00	0.04	0.190	O				5.15
36.750	0.00	0.04	0.190	O				5.14
36.833	0.00	0.04	0.190	O				5.13
36.917	0.00	0.04	0.189	O				5.13
37.000	0.00	0.04	0.189	O				5.12
37.083	0.00	0.04	0.189	O				5.11
37.167	0.00	0.04	0.188	O				5.10
37.250	0.00	0.04	0.188	O				5.10
37.333	0.00	0.04	0.188	O				5.09
37.417	0.00	0.04	0.188	O				5.08
37.500	0.00	0.04	0.187	O				5.07
37.583	0.00	0.04	0.187	O				5.07
37.667	0.00	0.04	0.187	O				5.06
37.750	0.00	0.04	0.186	O				5.05
37.833	0.00	0.04	0.186	O				5.04
37.917	0.00	0.04	0.186	O				5.04
38.000	0.00	0.04	0.185	O				5.03
38.083	0.00	0.04	0.185	O				5.02
38.167	0.00	0.04	0.185	O				5.01
38.250	0.00	0.04	0.184	O				5.00
38.333	0.00	0.04	0.184	O				5.00
38.417	0.00	0.04	0.184	O				4.99
38.500	0.00	0.04	0.184	O				4.98
38.583	0.00	0.04	0.183	O				4.97
38.667	0.00	0.04	0.183	O				4.97
38.750	0.00	0.04	0.183	O				4.96
38.833	0.00	0.04	0.182	O				4.95
38.917	0.00	0.04	0.182	O				4.94
39.000	0.00	0.04	0.182	O				4.94
39.083	0.00	0.04	0.181	O				4.93
39.167	0.00	0.04	0.181	O				4.92
39.250	0.00	0.04	0.181	O				4.91
39.333	0.00	0.04	0.180	O				4.91
39.417	0.00	0.04	0.180	O				4.90
39.500	0.00	0.04	0.180	O				4.89
39.583	0.00	0.04	0.179	O				4.88
39.667	0.00	0.04	0.179	O				4.87
39.750	0.00	0.04	0.179	O				4.87
39.833	0.00	0.04	0.179	O				4.86

39.917	0.00	0.04	0.178	O				4.85
40.000	0.00	0.04	0.178	O				4.84
40.083	0.00	0.04	0.178	O				4.84
40.167	0.00	0.04	0.177	O				4.83
40.250	0.00	0.04	0.177	O				4.82
40.333	0.00	0.04	0.177	O				4.81
40.417	0.00	0.04	0.176	O				4.81
40.500	0.00	0.04	0.176	O				4.80
40.583	0.00	0.04	0.176	O				4.79
40.667	0.00	0.04	0.175	O				4.78
40.750	0.00	0.04	0.175	O				4.78
40.833	0.00	0.04	0.175	O				4.77
40.917	0.00	0.04	0.175	O				4.76
41.000	0.00	0.04	0.174	O				4.75
41.083	0.00	0.04	0.174	O				4.74
41.167	0.00	0.04	0.174	O				4.74
41.250	0.00	0.04	0.173	O				4.73
41.333	0.00	0.04	0.173	O				4.72
41.417	0.00	0.04	0.173	O				4.71
41.500	0.00	0.04	0.172	O				4.71
41.583	0.00	0.04	0.172	O				4.70
41.667	0.00	0.04	0.172	O				4.69
41.750	0.00	0.04	0.171	O				4.68
41.833	0.00	0.04	0.171	O				4.68
41.917	0.00	0.04	0.171	O				4.67
42.000	0.00	0.04	0.171	O				4.66
42.083	0.00	0.04	0.170	O				4.65
42.167	0.00	0.04	0.170	O				4.65
42.250	0.00	0.04	0.170	O				4.64
42.333	0.00	0.04	0.169	O				4.63
42.417	0.00	0.04	0.169	O				4.62
42.500	0.00	0.04	0.169	O				4.61
42.583	0.00	0.04	0.168	O				4.61
42.667	0.00	0.04	0.168	O				4.60
42.750	0.00	0.04	0.168	O				4.59
42.833	0.00	0.04	0.167	O				4.58
42.917	0.00	0.04	0.167	O				4.58
43.000	0.00	0.04	0.167	O				4.57
43.083	0.00	0.04	0.166	O				4.56
43.167	0.00	0.04	0.166	O				4.55
43.250	0.00	0.04	0.166	O				4.55
43.333	0.00	0.04	0.166	O				4.54
43.417	0.00	0.04	0.165	O				4.53
43.500	0.00	0.04	0.165	O				4.52
43.583	0.00	0.04	0.165	O				4.52
43.667	0.00	0.04	0.164	O				4.51
43.750	0.00	0.04	0.164	O				4.50
43.833	0.00	0.04	0.164	O				4.49
43.917	0.00	0.04	0.163	O				4.48
44.000	0.00	0.04	0.163	O				4.48

44.083	0.00	0.04	0.163	O				4.47
44.167	0.00	0.04	0.162	O				4.46
44.250	0.00	0.04	0.162	O				4.45
44.333	0.00	0.04	0.162	O				4.45
44.417	0.00	0.04	0.162	O				4.44
44.500	0.00	0.04	0.161	O				4.43
44.583	0.00	0.04	0.161	O				4.42
44.667	0.00	0.04	0.161	O				4.41
44.750	0.00	0.04	0.160	O				4.41
44.833	0.00	0.04	0.160	O				4.40
44.917	0.00	0.04	0.160	O				4.39
45.000	0.00	0.04	0.159	O				4.38
45.083	0.00	0.04	0.159	O				4.38
45.167	0.00	0.04	0.159	O				4.37
45.250	0.00	0.04	0.158	O				4.36
45.333	0.00	0.04	0.158	O				4.35
45.417	0.00	0.04	0.158	O				4.34
45.500	0.00	0.04	0.157	O				4.34
45.583	0.00	0.04	0.157	O				4.33
45.667	0.00	0.04	0.157	O				4.32
45.750	0.00	0.04	0.157	O				4.31
45.833	0.00	0.04	0.156	O				4.31
45.917	0.00	0.04	0.156	O				4.30
46.000	0.00	0.04	0.156	O				4.29
46.083	0.00	0.04	0.155	O				4.28
46.167	0.00	0.04	0.155	O				4.28
46.250	0.00	0.04	0.155	O				4.27
46.333	0.00	0.04	0.154	O				4.26
46.417	0.00	0.04	0.154	O				4.25
46.500	0.00	0.04	0.154	O				4.24
46.583	0.00	0.04	0.153	O				4.24
46.667	0.00	0.04	0.153	O				4.23
46.750	0.00	0.04	0.153	O				4.22
46.833	0.00	0.04	0.153	O				4.21
46.917	0.00	0.04	0.152	O				4.21
47.000	0.00	0.04	0.152	O				4.20
47.083	0.00	0.04	0.152	O				4.19
47.167	0.00	0.04	0.151	O				4.18
47.250	0.00	0.04	0.151	O				4.17
47.333	0.00	0.04	0.151	O				4.17
47.417	0.00	0.04	0.150	O				4.16
47.500	0.00	0.04	0.150	O				4.15
47.583	0.00	0.04	0.150	O				4.14
47.667	0.00	0.04	0.149	O				4.14
47.750	0.00	0.04	0.149	O				4.13
47.833	0.00	0.04	0.149	O				4.12
47.917	0.00	0.04	0.148	O				4.11
48.000	0.00	0.04	0.148	O				4.10
48.083	0.00	0.04	0.148	O				4.10
48.167	0.00	0.04	0.148	O				4.09

48.250	0.00	0.04	0.147	O				4.08
48.333	0.00	0.04	0.147	O				4.07
48.417	0.00	0.04	0.147	O				4.07
48.500	0.00	0.04	0.146	O				4.06
48.583	0.00	0.04	0.146	O				4.05
48.667	0.00	0.04	0.146	O				4.04
48.750	0.00	0.04	0.145	O				4.03
48.833	0.00	0.04	0.145	O				4.03
48.917	0.00	0.04	0.145	O				4.02
49.000	0.00	0.04	0.144	O				4.01
49.083	0.00	0.04	0.144	O				4.00
49.167	0.00	0.04	0.144	O				4.00
49.250	0.00	0.04	0.144	O				3.99
49.333	0.00	0.04	0.143	O				3.98
49.417	0.00	0.04	0.143	O				3.97
49.500	0.00	0.04	0.143	O				3.97
49.583	0.00	0.04	0.142	O				3.96
49.667	0.00	0.04	0.142	O				3.95
49.750	0.00	0.04	0.142	O				3.94
49.833	0.00	0.04	0.141	O				3.93
49.917	0.00	0.04	0.141	O				3.93
50.000	0.00	0.04	0.141	O				3.92
50.083	0.00	0.04	0.140	O				3.91
50.167	0.00	0.04	0.140	O				3.90
50.250	0.00	0.04	0.140	O				3.90
50.333	0.00	0.04	0.140	O				3.89
50.417	0.00	0.04	0.139	O				3.88
50.500	0.00	0.04	0.139	O				3.87
50.583	0.00	0.04	0.139	O				3.86
50.667	0.00	0.04	0.138	O				3.86
50.750	0.00	0.04	0.138	O				3.85
50.833	0.00	0.04	0.138	O				3.84
50.917	0.00	0.04	0.137	O				3.83
51.000	0.00	0.04	0.137	O				3.83
51.083	0.00	0.04	0.137	O				3.82
51.167	0.00	0.04	0.136	O				3.81
51.250	0.00	0.04	0.136	O				3.80
51.333	0.00	0.04	0.136	O				3.79
51.417	0.00	0.04	0.135	O				3.79
51.500	0.00	0.04	0.135	O				3.78
51.583	0.00	0.04	0.135	O				3.77
51.667	0.00	0.04	0.135	O				3.76
51.750	0.00	0.04	0.134	O				3.76
51.833	0.00	0.04	0.134	O				3.75
51.917	0.00	0.04	0.134	O				3.74
52.000	0.00	0.04	0.133	O				3.73
52.083	0.00	0.04	0.133	O				3.73
52.167	0.00	0.04	0.133	O				3.72
52.250	0.00	0.04	0.132	O				3.71
52.333	0.00	0.04	0.132	O				3.70

52.417	0.00	0.04	0.132	O				3.69
52.500	0.00	0.04	0.131	O				3.69
52.583	0.00	0.04	0.131	O				3.68
52.667	0.00	0.04	0.131	O				3.67
52.750	0.00	0.04	0.131	O				3.66
52.833	0.00	0.04	0.130	O				3.66
52.917	0.00	0.04	0.130	O				3.65
53.000	0.00	0.04	0.130	O				3.64
53.083	0.00	0.04	0.129	O				3.63
53.167	0.00	0.04	0.129	O				3.62
53.250	0.00	0.04	0.129	O				3.62
53.333	0.00	0.04	0.128	O				3.61
53.417	0.00	0.04	0.128	O				3.60
53.500	0.00	0.04	0.128	O				3.59
53.583	0.00	0.04	0.127	O				3.59
53.667	0.00	0.04	0.127	O				3.58
53.750	0.00	0.04	0.127	O				3.57
53.833	0.00	0.04	0.126	O				3.56
53.917	0.00	0.04	0.126	O				3.55
54.000	0.00	0.04	0.126	O				3.55
54.083	0.00	0.04	0.126	O				3.54
54.167	0.00	0.04	0.125	O				3.53
54.250	0.00	0.04	0.125	O				3.52
54.333	0.00	0.04	0.125	O				3.52
54.417	0.00	0.04	0.124	O				3.51
54.500	0.00	0.04	0.124	O				3.50
54.583	0.00	0.04	0.124	O				3.49
54.667	0.00	0.04	0.123	O				3.48
54.750	0.00	0.04	0.123	O				3.48
54.833	0.00	0.04	0.123	O				3.47
54.917	0.00	0.04	0.122	O				3.46
55.000	0.00	0.04	0.122	O				3.45
55.083	0.00	0.04	0.122	O				3.45
55.167	0.00	0.04	0.122	O				3.44
55.250	0.00	0.04	0.121	O				3.43
55.333	0.00	0.04	0.121	O				3.42
55.417	0.00	0.04	0.121	O				3.42
55.500	0.00	0.04	0.120	O				3.41
55.583	0.00	0.04	0.120	O				3.40
55.667	0.00	0.04	0.120	O				3.39
55.750	0.00	0.04	0.119	O				3.38
55.833	0.00	0.04	0.119	O				3.38
55.917	0.00	0.04	0.119	O				3.37
56.000	0.00	0.04	0.118	O				3.36
56.083	0.00	0.04	0.118	O				3.35
56.167	0.00	0.04	0.118	O				3.35
56.250	0.00	0.04	0.118	O				3.34
56.333	0.00	0.04	0.117	O				3.33
56.417	0.00	0.04	0.117	O				3.32
56.500	0.00	0.04	0.117	O				3.31

56.583	0.00	0.04	0.116	O				3.31
56.667	0.00	0.04	0.116	O				3.30
56.750	0.00	0.04	0.116	O				3.29
56.833	0.00	0.04	0.115	O				3.28
56.917	0.00	0.04	0.115	O				3.28
57.000	0.00	0.04	0.115	O				3.27
57.083	0.00	0.04	0.114	O				3.26
57.167	0.00	0.04	0.114	O				3.25
57.250	0.00	0.04	0.114	O				3.24
57.333	0.00	0.04	0.113	O				3.24
57.417	0.00	0.04	0.113	O				3.23
57.500	0.00	0.04	0.113	O				3.22
57.583	0.00	0.04	0.113	O				3.21
57.667	0.00	0.04	0.112	O				3.21
57.750	0.00	0.04	0.112	O				3.20
57.833	0.00	0.04	0.112	O				3.19
57.917	0.00	0.04	0.111	O				3.18
58.000	0.00	0.04	0.111	O				3.17
58.083	0.00	0.04	0.111	O				3.17
58.167	0.00	0.04	0.110	O				3.16
58.250	0.00	0.04	0.110	O				3.15
58.333	0.00	0.04	0.110	O				3.14
58.417	0.00	0.04	0.109	O				3.14
58.500	0.00	0.04	0.109	O				3.13
58.583	0.00	0.04	0.109	O				3.12
58.667	0.00	0.04	0.109	O				3.11
58.750	0.00	0.04	0.108	O				3.11
58.833	0.00	0.04	0.108	O				3.10
58.917	0.00	0.04	0.108	O				3.09
59.000	0.00	0.04	0.107	O				3.08
59.083	0.00	0.04	0.107	O				3.07
59.167	0.00	0.04	0.107	O				3.07
59.250	0.00	0.04	0.106	O				3.06
59.333	0.00	0.04	0.106	O				3.05
59.417	0.00	0.04	0.106	O				3.04
59.500	0.00	0.04	0.105	O				3.04
59.583	0.00	0.04	0.105	O				3.03
59.667	0.00	0.04	0.105	O				3.02
59.750	0.00	0.04	0.104	O				3.01
59.833	0.00	0.04	0.104	O				3.00
59.917	0.00	0.04	0.104	O				3.00
60.000	0.00	0.04	0.104	O				2.99
60.083	0.00	0.04	0.103	O				2.98
60.167	0.00	0.04	0.103	O				2.97
60.250	0.00	0.04	0.103	O				2.97
60.333	0.00	0.04	0.102	O				2.96
60.417	0.00	0.04	0.102	O				2.95
60.500	0.00	0.04	0.102	O				2.94
60.583	0.00	0.04	0.101	O				2.93
60.667	0.00	0.04	0.101	O				2.93

60.750	0.00	0.04	0.101	O	|	|	|	2.92
60.833	0.00	0.04	0.100	O	|	|	|	2.91
60.917	0.00	0.04	0.100	O	|	|	|	2.90
61.000	0.00	0.04	0.100	O	|	|	|	2.90
61.083	0.00	0.04	0.100	O	|	|	|	2.89
61.167	0.00	0.04	0.099	O	|	|	|	2.88
61.250	0.00	0.04	0.099	O	|	|	|	2.87
61.333	0.00	0.04	0.099	O	|	|	|	2.87
61.417	0.00	0.04	0.098	O	|	|	|	2.86
61.500	0.00	0.04	0.098	O	|	|	|	2.85
61.583	0.00	0.04	0.098	O	|	|	|	2.84
61.667	0.00	0.04	0.097	O	|	|	|	2.83
61.750	0.00	0.04	0.097	O	|	|	|	2.83
61.833	0.00	0.04	0.097	O	|	|	|	2.82
61.917	0.00	0.04	0.096	O	|	|	|	2.81
62.000	0.00	0.04	0.096	O	|	|	|	2.80
62.083	0.00	0.04	0.096	O	|	|	|	2.80
62.167	0.00	0.04	0.096	O	|	|	|	2.79
62.250	0.00	0.04	0.095	O	|	|	|	2.78
62.333	0.00	0.04	0.095	O	|	|	|	2.77
62.417	0.00	0.04	0.095	O	|	|	|	2.76
62.500	0.00	0.04	0.094	O	|	|	|	2.76
62.583	0.00	0.04	0.094	O	|	|	|	2.75
62.667	0.00	0.04	0.094	O	|	|	|	2.74
62.750	0.00	0.04	0.093	O	|	|	|	2.73
62.833	0.00	0.04	0.093	O	|	|	|	2.73
62.917	0.00	0.04	0.093	O	|	|	|	2.72
63.000	0.00	0.04	0.092	O	|	|	|	2.71
63.083	0.00	0.04	0.092	O	|	|	|	2.70
63.167	0.00	0.04	0.092	O	|	|	|	2.69
63.250	0.00	0.04	0.091	O	|	|	|	2.69
63.333	0.00	0.04	0.091	O	|	|	|	2.68
63.417	0.00	0.04	0.091	O	|	|	|	2.67
63.500	0.00	0.04	0.091	O	|	|	|	2.66
63.583	0.00	0.04	0.090	O	|	|	|	2.66
63.667	0.00	0.04	0.090	O	|	|	|	2.65
63.750	0.00	0.04	0.090	O	|	|	|	2.64
63.833	0.00	0.04	0.089	O	|	|	|	2.63
63.917	0.00	0.04	0.089	O	|	|	|	2.62
64.000	0.00	0.04	0.089	O	|	|	|	2.62
64.083	0.00	0.04	0.088	O	|	|	|	2.61
64.167	0.00	0.04	0.088	O	|	|	|	2.60
64.250	0.00	0.04	0.088	O	|	|	|	2.59
64.333	0.00	0.04	0.087	O	|	|	|	2.59
64.417	0.00	0.04	0.087	O	|	|	|	2.58
64.500	0.00	0.04	0.087	O	|	|	|	2.57
64.583	0.00	0.04	0.087	O	|	|	|	2.56
64.667	0.00	0.04	0.086	O	|	|	|	2.56
64.750	0.00	0.04	0.086	O	|	|	|	2.55
64.833	0.00	0.04	0.086	O	|	|	|	2.54

64.917	0.00	0.04	0.085	O				2.53
65.000	0.00	0.04	0.085	O				2.52
65.083	0.00	0.04	0.085	O				2.52
65.167	0.00	0.04	0.084	O				2.51
65.250	0.00	0.04	0.084	O				2.50
65.333	0.00	0.04	0.084	O				2.49
65.417	0.00	0.04	0.083	O				2.49
65.500	0.00	0.04	0.083	O				2.48
65.583	0.00	0.04	0.083	O				2.47
65.667	0.00	0.04	0.082	O				2.46
65.750	0.00	0.04	0.082	O				2.45
65.833	0.00	0.04	0.082	O				2.45
65.917	0.00	0.04	0.082	O				2.44
66.000	0.00	0.04	0.081	O				2.43
66.083	0.00	0.04	0.081	O				2.42
66.167	0.00	0.04	0.081	O				2.42
66.250	0.00	0.04	0.080	O				2.41
66.333	0.00	0.04	0.080	O				2.40
66.417	0.00	0.04	0.080	O				2.39
66.500	0.00	0.04	0.079	O				2.38
66.583	0.00	0.04	0.079	O				2.38
66.667	0.00	0.04	0.079	O				2.37
66.750	0.00	0.04	0.078	O				2.36
66.833	0.00	0.04	0.078	O				2.35
66.917	0.00	0.04	0.078	O				2.35
67.000	0.00	0.04	0.078	O				2.34
67.083	0.00	0.04	0.077	O				2.33
67.167	0.00	0.04	0.077	O				2.32
67.250	0.00	0.04	0.077	O				2.31
67.333	0.00	0.04	0.076	O				2.31
67.417	0.00	0.04	0.076	O				2.30
67.500	0.00	0.04	0.076	O				2.29
67.583	0.00	0.04	0.075	O				2.28
67.667	0.00	0.04	0.075	O				2.28
67.750	0.00	0.04	0.075	O				2.27
67.833	0.00	0.04	0.074	O				2.26
67.917	0.00	0.04	0.074	O				2.25
68.000	0.00	0.04	0.074	O				2.25
68.083	0.00	0.04	0.073	O				2.24
68.167	0.00	0.04	0.073	O				2.23
68.250	0.00	0.04	0.073	O				2.22
68.333	0.00	0.04	0.073	O				2.21
68.417	0.00	0.04	0.072	O				2.21
68.500	0.00	0.04	0.072	O				2.20
68.583	0.00	0.04	0.072	O				2.19
68.667	0.00	0.04	0.071	O				2.18
68.750	0.00	0.04	0.071	O				2.18
68.833	0.00	0.04	0.071	O				2.17
68.917	0.00	0.04	0.070	O				2.16
69.000	0.00	0.04	0.070	O				2.15

69.083	0.00	0.04	0.070	O				2.14
69.167	0.00	0.04	0.069	O				2.14
69.250	0.00	0.04	0.069	O				2.13
69.333	0.00	0.04	0.069	O				2.12
69.417	0.00	0.04	0.069	O				2.11
69.500	0.00	0.04	0.068	O				2.11
69.583	0.00	0.04	0.068	O				2.10
69.667	0.00	0.04	0.068	O				2.09
69.750	0.00	0.04	0.067	O				2.08
69.833	0.00	0.04	0.067	O				2.07
69.917	0.00	0.04	0.067	O				2.07
70.000	0.00	0.04	0.066	O				2.06
70.083	0.00	0.04	0.066	O				2.05
70.167	0.00	0.04	0.066	O				2.04
70.250	0.00	0.04	0.065	O				2.04
70.333	0.00	0.04	0.065	O				2.03
70.417	0.00	0.04	0.065	O				2.02
70.500	0.00	0.04	0.065	O				2.01
70.583	0.00	0.04	0.064	O				2.00
70.667	0.00	0.04	0.064	O				2.00
70.750	0.00	0.04	0.064	O				1.99
70.833	0.00	0.04	0.063	O				1.98
70.917	0.00	0.04	0.063	O				1.97
71.000	0.00	0.04	0.063	O				1.97
71.083	0.00	0.04	0.062	O				1.96
71.167	0.00	0.04	0.062	O				1.95
71.250	0.00	0.04	0.062	O				1.94
71.333	0.00	0.04	0.061	O				1.94
71.417	0.00	0.04	0.061	O				1.93
71.500	0.00	0.04	0.061	O				1.92
71.583	0.00	0.04	0.060	O				1.91
71.667	0.00	0.04	0.060	O				1.90
71.750	0.00	0.04	0.060	O				1.90
71.833	0.00	0.04	0.060	O				1.89
71.917	0.00	0.04	0.059	O				1.88
72.000	0.00	0.04	0.059	O				1.87
72.083	0.00	0.04	0.059	O				1.87
72.167	0.00	0.04	0.058	O				1.86
72.250	0.00	0.04	0.058	O				1.85
72.333	0.00	0.04	0.058	O				1.84
72.417	0.00	0.04	0.057	O				1.83
72.500	0.00	0.04	0.057	O				1.83
72.583	0.00	0.04	0.057	O				1.82
72.667	0.00	0.04	0.056	O				1.81
72.750	0.00	0.04	0.056	O				1.80
72.833	0.00	0.04	0.056	O				1.80
72.917	0.00	0.04	0.056	O				1.79
73.000	0.00	0.04	0.055	O				1.78
73.083	0.00	0.04	0.055	O				1.77
73.167	0.00	0.04	0.055	O				1.76

73.250	0.00	0.04	0.054	O				1.76
73.333	0.00	0.04	0.054	O				1.75
73.417	0.00	0.04	0.054	O				1.74
73.500	0.00	0.04	0.053	O				1.73
73.583	0.00	0.04	0.053	O				1.73
73.667	0.00	0.04	0.053	O				1.72
73.750	0.00	0.04	0.052	O				1.71
73.833	0.00	0.04	0.052	O				1.70
73.917	0.00	0.04	0.052	O				1.70
74.000	0.00	0.04	0.051	O				1.69
74.083	0.00	0.04	0.051	O				1.68
74.167	0.00	0.04	0.051	O				1.67
74.250	0.00	0.04	0.051	O				1.66
74.333	0.00	0.04	0.050	O				1.66
74.417	0.00	0.04	0.050	O				1.65
74.500	0.00	0.04	0.050	O				1.64
74.583	0.00	0.04	0.049	O				1.63
74.667	0.00	0.04	0.049	O				1.63
74.750	0.00	0.04	0.049	O				1.62
74.833	0.00	0.04	0.048	O				1.61
74.917	0.00	0.04	0.048	O				1.60
75.000	0.00	0.04	0.048	O				1.59
75.083	0.00	0.04	0.047	O				1.59
75.167	0.00	0.04	0.047	O				1.58
75.250	0.00	0.04	0.047	O				1.57
75.333	0.00	0.04	0.047	O				1.56
75.417	0.00	0.04	0.046	O				1.56
75.500	0.00	0.04	0.046	O				1.55
75.583	0.00	0.04	0.046	O				1.54
75.667	0.00	0.04	0.045	O				1.53
75.750	0.00	0.04	0.045	O				1.52
75.833	0.00	0.04	0.045	O				1.52
75.917	0.00	0.04	0.044	O				1.51
76.000	0.00	0.04	0.044	O				1.50
76.083	0.00	0.04	0.044	O				1.49
76.167	0.00	0.04	0.043	O				1.49
76.250	0.00	0.04	0.043	O				1.48
76.333	0.00	0.04	0.043	O				1.47
76.417	0.00	0.04	0.043	O				1.46
76.500	0.00	0.04	0.042	O				1.45
76.583	0.00	0.04	0.042	O				1.45
76.667	0.00	0.04	0.042	O				1.44
76.750	0.00	0.04	0.041	O				1.43
76.833	0.00	0.04	0.041	O				1.42
76.917	0.00	0.04	0.041	O				1.42
77.000	0.00	0.04	0.040	O				1.41
77.083	0.00	0.04	0.040	O				1.40
77.167	0.00	0.04	0.040	O				1.39
77.250	0.00	0.04	0.039	O				1.39
77.333	0.00	0.04	0.039	O				1.38

77.417	0.00	0.04	0.039	O				1.37
77.500	0.00	0.04	0.038	O				1.36
77.583	0.00	0.04	0.038	O				1.35
77.667	0.00	0.04	0.038	O				1.35
77.750	0.00	0.04	0.038	O				1.34
77.833	0.00	0.04	0.037	O				1.33
77.917	0.00	0.04	0.037	O				1.32
78.000	0.00	0.04	0.037	O				1.32
78.083	0.00	0.04	0.036	O				1.31
78.167	0.00	0.04	0.036	O				1.30
78.250	0.00	0.04	0.036	O				1.29
78.333	0.00	0.04	0.035	O				1.28
78.417	0.00	0.04	0.035	O				1.28
78.500	0.00	0.04	0.035	O				1.27
78.583	0.00	0.04	0.034	O				1.26
78.667	0.00	0.04	0.034	O				1.25
78.750	0.00	0.04	0.034	O				1.25
78.833	0.00	0.04	0.034	O				1.24
78.917	0.00	0.04	0.033	O				1.23
79.000	0.00	0.04	0.033	O				1.22
79.083	0.00	0.04	0.033	O				1.21
79.167	0.00	0.04	0.032	O				1.21
79.250	0.00	0.04	0.032	O				1.20
79.333	0.00	0.04	0.032	O				1.19
79.417	0.00	0.04	0.031	O				1.18
79.500	0.00	0.04	0.031	O				1.18
79.583	0.00	0.04	0.031	O				1.17
79.667	0.00	0.04	0.030	O				1.16
79.750	0.00	0.04	0.030	O				1.15
79.833	0.00	0.04	0.030	O				1.14
79.917	0.00	0.04	0.029	O				1.14
80.000	0.00	0.04	0.029	O				1.13
80.083	0.00	0.04	0.029	O				1.12
80.167	0.00	0.04	0.029	O				1.11
80.250	0.00	0.04	0.028	O				1.11
80.333	0.00	0.04	0.028	O				1.10
80.417	0.00	0.04	0.028	O				1.09
80.500	0.00	0.04	0.027	O				1.08
80.583	0.00	0.04	0.027	O				1.08
80.667	0.00	0.04	0.027	O				1.07
80.750	0.00	0.04	0.026	O				1.06
80.833	0.00	0.04	0.026	O				1.05
80.917	0.00	0.04	0.026	O				1.04
81.000	0.00	0.04	0.025	O				1.04
81.083	0.00	0.04	0.025	O				1.03
81.167	0.00	0.04	0.025	O				1.02
81.250	0.00	0.04	0.025	O				1.01
81.333	0.00	0.04	0.024	O				1.01
81.417	0.00	0.04	0.024	O				1.00
81.500	0.00	0.04	0.024	O				0.98

81.583	0.00	0.04	0.023	O	|	|	|	0.97
81.667	0.00	0.04	0.023	O	|	|	|	0.96
81.750	0.00	0.04	0.023	O	|	|	|	0.95
81.833	0.00	0.04	0.022	O	|	|	|	0.93
81.917	0.00	0.04	0.022	O	|	|	|	0.92
82.000	0.00	0.04	0.022	O	|	|	|	0.91
82.083	0.00	0.04	0.022	O	|	|	|	0.90
82.167	0.00	0.04	0.021	O	|	|	|	0.89
82.250	0.00	0.04	0.021	O	|	|	|	0.88
82.333	0.00	0.04	0.021	O	|	|	|	0.86
82.417	0.00	0.04	0.020	O	|	|	|	0.85
82.500	0.00	0.04	0.020	O	|	|	|	0.84
82.583	0.00	0.04	0.020	O	|	|	|	0.83
82.667	0.00	0.04	0.020	O	|	|	|	0.82
82.750	0.00	0.04	0.019	O	|	|	|	0.81
82.833	0.00	0.04	0.019	O	|	|	|	0.80
82.917	0.00	0.04	0.019	O	|	|	|	0.79
83.000	0.00	0.04	0.019	O	|	|	|	0.78
83.083	0.00	0.03	0.018	O	|	|	|	0.77
83.167	0.00	0.03	0.018	O	|	|	|	0.76
83.250	0.00	0.03	0.018	O	|	|	|	0.75
83.333	0.00	0.03	0.018	O	|	|	|	0.74
83.417	0.00	0.03	0.018	O	|	|	|	0.73
83.500	0.00	0.03	0.017	O	|	|	|	0.72
83.583	0.00	0.03	0.017	O	|	|	|	0.71
83.667	0.00	0.03	0.017	O	|	|	|	0.70
83.750	0.00	0.03	0.017	O	|	|	|	0.69
83.833	0.00	0.03	0.016	O	|	|	|	0.69
83.917	0.00	0.03	0.016	O	|	|	|	0.68
84.000	0.00	0.03	0.016	O	|	|	|	0.67
84.083	0.00	0.03	0.016	O	|	|	|	0.66
84.167	0.00	0.03	0.016	O	|	|	|	0.65
84.250	0.00	0.03	0.015	O	|	|	|	0.64
84.333	0.00	0.03	0.015	O	|	|	|	0.63
84.417	0.00	0.03	0.015	O	|	|	|	0.63
84.500	0.00	0.03	0.015	O	|	|	|	0.62
84.583	0.00	0.03	0.015	O	|	|	|	0.61
84.667	0.00	0.03	0.014	O	|	|	|	0.60
84.750	0.00	0.03	0.014	O	|	|	|	0.59
84.833	0.00	0.03	0.014	O	|	|	|	0.59
84.917	0.00	0.03	0.014	O	|	|	|	0.58
85.000	0.00	0.03	0.014	O	|	|	|	0.57
85.083	0.00	0.03	0.014	O	|	|	|	0.56
85.167	0.00	0.03	0.013	O	|	|	|	0.56
85.250	0.00	0.02	0.013	O	|	|	|	0.55
85.333	0.00	0.02	0.013	O	|	|	|	0.54
85.417	0.00	0.02	0.013	O	|	|	|	0.54
85.500	0.00	0.02	0.013	O	|	|	|	0.53
85.583	0.00	0.02	0.013	O	|	|	|	0.52
85.667	0.00	0.02	0.012	O	|	|	|	0.52

85.750	0.00	0.02	0.012	O				0.51
85.833	0.00	0.02	0.012	O				0.50
85.917	0.00	0.02	0.012	O				0.50
86.000	0.00	0.02	0.012	O				0.49
86.083	0.00	0.02	0.012	O				0.48
86.167	0.00	0.02	0.011	O				0.48
86.250	0.00	0.02	0.011	O				0.47
86.333	0.00	0.02	0.011	O				0.47
86.417	0.00	0.02	0.011	O				0.46
86.500	0.00	0.02	0.011	O				0.45
86.583	0.00	0.02	0.011	O				0.45
86.667	0.00	0.02	0.011	O				0.44
86.750	0.00	0.02	0.010	O				0.44
86.833	0.00	0.02	0.010	O				0.43
86.917	0.00	0.02	0.010	O				0.42
87.000	0.00	0.02	0.010	O				0.42
87.083	0.00	0.02	0.010	O				0.41
87.167	0.00	0.02	0.010	O				0.41
87.250	0.00	0.02	0.010	O				0.40
87.333	0.00	0.02	0.010	O				0.40
87.417	0.00	0.02	0.009	O				0.39
87.500	0.00	0.02	0.009	O				0.39
87.583	0.00	0.02	0.009	O				0.38
87.667	0.00	0.02	0.009	O				0.38
87.750	0.00	0.02	0.009	O				0.37
87.833	0.00	0.02	0.009	O				0.37
87.917	0.00	0.02	0.009	O				0.36
88.000	0.00	0.02	0.009	O				0.36
88.083	0.00	0.02	0.009	O				0.35
88.167	0.00	0.02	0.008	O				0.35
88.250	0.00	0.02	0.008	O				0.35
88.333	0.00	0.02	0.008	O				0.34
88.417	0.00	0.02	0.008	O				0.34
88.500	0.00	0.01	0.008	O				0.33
88.583	0.00	0.01	0.008	O				0.33
88.667	0.00	0.01	0.008	O				0.32
88.750	0.00	0.01	0.008	O				0.32
88.833	0.00	0.01	0.008	O				0.32
88.917	0.00	0.01	0.007	O				0.31
89.000	0.00	0.01	0.007	O				0.31
89.083	0.00	0.01	0.007	O				0.30
89.167	0.00	0.01	0.007	O				0.30
89.250	0.00	0.01	0.007	O				0.30
89.333	0.00	0.01	0.007	O				0.29
89.417	0.00	0.01	0.007	O				0.29
89.500	0.00	0.01	0.007	O				0.28
89.583	0.00	0.01	0.007	O				0.28
89.667	0.00	0.01	0.007	O				0.28
89.750	0.00	0.01	0.007	O				0.27
89.833	0.00	0.01	0.006	O				0.27

89.917	0.00	0.01	0.006	O				0.27
90.000	0.00	0.01	0.006	O				0.26
90.083	0.00	0.01	0.006	O				0.26
90.167	0.00	0.01	0.006	O				0.26
90.250	0.00	0.01	0.006	O				0.25
90.333	0.00	0.01	0.006	O				0.25
90.417	0.00	0.01	0.006	O				0.25
90.500	0.00	0.01	0.006	O				0.24
90.583	0.00	0.01	0.006	O				0.24
90.667	0.00	0.01	0.006	O				0.24
90.750	0.00	0.01	0.006	O				0.23
90.833	0.00	0.01	0.006	O				0.23
90.917	0.00	0.01	0.005	O				0.23
91.000	0.00	0.01	0.005	O				0.23
91.083	0.00	0.01	0.005	O				0.22
91.167	0.00	0.01	0.005	O				0.22
91.250	0.00	0.01	0.005	O				0.22
91.333	0.00	0.01	0.005	O				0.21
91.417	0.00	0.01	0.005	O				0.21
91.500	0.00	0.01	0.005	O				0.21
91.583	0.00	0.01	0.005	O				0.21
91.667	0.00	0.01	0.005	O				0.20
91.750	0.00	0.01	0.005	O				0.20
91.833	0.00	0.01	0.005	O				0.20
91.917	0.00	0.01	0.005	O				0.20
92.000	0.00	0.01	0.005	O				0.19
92.083	0.00	0.01	0.005	O				0.19
92.167	0.00	0.01	0.005	O				0.19
92.250	0.00	0.01	0.004	O				0.19
92.333	0.00	0.01	0.004	O				0.18
92.417	0.00	0.01	0.004	O				0.18
92.500	0.00	0.01	0.004	O				0.18
92.583	0.00	0.01	0.004	O				0.18
92.667	0.00	0.01	0.004	O				0.17
92.750	0.00	0.01	0.004	O				0.17
92.833	0.00	0.01	0.004	O				0.17
92.917	0.00	0.01	0.004	O				0.17
93.000	0.00	0.01	0.004	O				0.17
93.083	0.00	0.01	0.004	O				0.16
93.167	0.00	0.01	0.004	O				0.16
93.250	0.00	0.01	0.004	O				0.16
93.333	0.00	0.01	0.004	O				0.16
93.417	0.00	0.01	0.004	O				0.16
93.500	0.00	0.01	0.004	O				0.15
93.583	0.00	0.01	0.004	O				0.15
93.667	0.00	0.01	0.004	O				0.15
93.750	0.00	0.01	0.004	O				0.15
93.833	0.00	0.01	0.003	O				0.15
93.917	0.00	0.01	0.003	O				0.14
94.000	0.00	0.01	0.003	O				0.14

94.083	0.00	0.01	0.003	O				0.14
94.167	0.00	0.01	0.003	O				0.14
94.250	0.00	0.01	0.003	O				0.14
94.333	0.00	0.01	0.003	O				0.13
94.417	0.00	0.01	0.003	O				0.13
94.500	0.00	0.01	0.003	O				0.13
94.583	0.00	0.01	0.003	O				0.13
94.667	0.00	0.01	0.003	O				0.13
94.750	0.00	0.01	0.003	O				0.13
94.833	0.00	0.01	0.003	O				0.12
94.917	0.00	0.01	0.003	O				0.12
95.000	0.00	0.01	0.003	O				0.12
95.083	0.00	0.01	0.003	O				0.12
95.167	0.00	0.01	0.003	O				0.12
95.250	0.00	0.01	0.003	O				0.12
95.333	0.00	0.01	0.003	O				0.12
95.417	0.00	0.01	0.003	O				0.11
95.500	0.00	0.01	0.003	O				0.11
95.583	0.00	0.00	0.003	O				0.11
95.667	0.00	0.00	0.003	O				0.11
95.750	0.00	0.00	0.003	O				0.11
95.833	0.00	0.00	0.003	O				0.11
95.917	0.00	0.00	0.003	O				0.11
96.000	0.00	0.00	0.002	O				0.10
96.083	0.00	0.00	0.002	O				0.10
96.167	0.00	0.00	0.002	O				0.10
96.250	0.00	0.00	0.002	O				0.10
96.333	0.00	0.00	0.002	O				0.10
96.417	0.00	0.00	0.002	O				0.10
96.500	0.00	0.00	0.002	O				0.10
96.583	0.00	0.00	0.002	O				0.09
96.667	0.00	0.00	0.002	O				0.09
96.750	0.00	0.00	0.002	O				0.09
96.833	0.00	0.00	0.002	O				0.09
96.917	0.00	0.00	0.002	O				0.09
97.000	0.00	0.00	0.002	O				0.09
97.083	0.00	0.00	0.002	O				0.09
97.167	0.00	0.00	0.002	O				0.09
97.250	0.00	0.00	0.002	O				0.09
97.333	0.00	0.00	0.002	O				0.08
97.417	0.00	0.00	0.002	O				0.08
97.500	0.00	0.00	0.002	O				0.08
97.583	0.00	0.00	0.002	O				0.08
97.667	0.00	0.00	0.002	O				0.08
97.750	0.00	0.00	0.002	O				0.08
97.833	0.00	0.00	0.002	O				0.08
97.917	0.00	0.00	0.002	O				0.08
98.000	0.00	0.00	0.002	O				0.08
98.083	0.00	0.00	0.002	O				0.08
98.167	0.00	0.00	0.002	O				0.07

98.250	0.00	0.00	0.002	O				0.07
98.333	0.00	0.00	0.002	O				0.07
98.417	0.00	0.00	0.002	O				0.07
98.500	0.00	0.00	0.002	O				0.07
98.583	0.00	0.00	0.002	O				0.07
98.667	0.00	0.00	0.002	O				0.07
98.750	0.00	0.00	0.002	O				0.07
98.833	0.00	0.00	0.002	O				0.07
98.917	0.00	0.00	0.002	O				0.07
99.000	0.00	0.00	0.002	O				0.07
99.083	0.00	0.00	0.002	O				0.06
99.167	0.00	0.00	0.002	O				0.06
99.250	0.00	0.00	0.002	O				0.06
99.333	0.00	0.00	0.001	O				0.06
99.417	0.00	0.00	0.001	O				0.06
99.500	0.00	0.00	0.001	O				0.06
99.583	0.00	0.00	0.001	O				0.06
99.667	0.00	0.00	0.001	O				0.06
99.750	0.00	0.00	0.001	O				0.06
99.833	0.00	0.00	0.001	O				0.06
99.917	0.00	0.00	0.001	O				0.06
100.000	0.00	0.00	0.001	O				0.06
100.083	0.00	0.00	0.001	O				0.06
100.167	0.00	0.00	0.001	O				0.05
100.250	0.00	0.00	0.001	O				0.05
100.333	0.00	0.00	0.001	O				0.05
100.417	0.00	0.00	0.001	O				0.05
100.500	0.00	0.00	0.001	O				0.05
100.583	0.00	0.00	0.001	O				0.05
100.667	0.00	0.00	0.001	O				0.05
100.750	0.00	0.00	0.001	O				0.05
100.833	0.00	0.00	0.001	O				0.05
100.917	0.00	0.00	0.001	O				0.05
101.000	0.00	0.00	0.001	O				0.05
101.083	0.00	0.00	0.001	O				0.05
101.167	0.00	0.00	0.001	O				0.05
101.250	0.00	0.00	0.001	O				0.05
101.333	0.00	0.00	0.001	O				0.05
101.417	0.00	0.00	0.001	O				0.04
101.500	0.00	0.00	0.001	O				0.04
101.583	0.00	0.00	0.001	O				0.04
101.667	0.00	0.00	0.001	O				0.04
101.750	0.00	0.00	0.001	O				0.04
101.833	0.00	0.00	0.001	O				0.04
101.917	0.00	0.00	0.001	O				0.04
102.000	0.00	0.00	0.001	O				0.04
102.083	0.00	0.00	0.001	O				0.04
102.167	0.00	0.00	0.001	O				0.04
102.250	0.00	0.00	0.001	O				0.04
102.333	0.00	0.00	0.001	O				0.04

102.417	0.00	0.00	0.001	O	|	|	|	|	0.04
102.500	0.00	0.00	0.001	O	|	|	|	|	0.04
102.583	0.00	0.00	0.001	O	|	|	|	|	0.04
102.667	0.00	0.00	0.001	O	|	|	|	|	0.04
102.750	0.00	0.00	0.001	O	|	|	|	|	0.04
102.833	0.00	0.00	0.001	O	|	|	|	|	0.04
102.917	0.00	0.00	0.001	O	|	|	|	|	0.04
103.000	0.00	0.00	0.001	O	|	|	|	|	0.04
103.083	0.00	0.00	0.001	O	|	|	|	|	0.03
103.167	0.00	0.00	0.001	O	|	|	|	|	0.03
103.250	0.00	0.00	0.001	O	|	|	|	|	0.03
103.333	0.00	0.00	0.001	O	|	|	|	|	0.03
103.417	0.00	0.00	0.001	O	|	|	|	|	0.03
103.500	0.00	0.00	0.001	O	|	|	|	|	0.03
103.583	0.00	0.00	0.001	O	|	|	|	|	0.03
103.667	0.00	0.00	0.001	O	|	|	|	|	0.03
103.750	0.00	0.00	0.001	O	|	|	|	|	0.03
103.833	0.00	0.00	0.001	O	|	|	|	|	0.03
103.917	0.00	0.00	0.001	O	|	|	|	|	0.03
104.000	0.00	0.00	0.001	O	|	|	|	|	0.03
104.083	0.00	0.00	0.001	O	|	|	|	|	0.03
104.167	0.00	0.00	0.001	O	|	|	|	|	0.03
104.250	0.00	0.00	0.001	O	|	|	|	|	0.03
104.333	0.00	0.00	0.001	O	|	|	|	|	0.03
104.417	0.00	0.00	0.001	O	|	|	|	|	0.03
104.500	0.00	0.00	0.001	O	|	|	|	|	0.03
104.583	0.00	0.00	0.001	O	|	|	|	|	0.03
104.667	0.00	0.00	0.001	O	|	|	|	|	0.03
104.750	0.00	0.00	0.001	O	|	|	|	|	0.03
104.833	0.00	0.00	0.001	O	|	|	|	|	0.03
104.917	0.00	0.00	0.001	O	|	|	|	|	0.03
105.000	0.00	0.00	0.001	O	|	|	|	|	0.03
105.083	0.00	0.00	0.001	O	|	|	|	|	0.03
105.167	0.00	0.00	0.001	O	|	|	|	|	0.03
105.250	0.00	0.00	0.001	O	|	|	|	|	0.02
105.333	0.00	0.00	0.001	O	|	|	|	|	0.02
105.417	0.00	0.00	0.001	O	|	|	|	|	0.02
105.500	0.00	0.00	0.001	O	|	|	|	|	0.02
105.583	0.00	0.00	0.001	O	|	|	|	|	0.02
105.667	0.00	0.00	0.001	O	|	|	|	|	0.02
105.750	0.00	0.00	0.001	O	|	|	|	|	0.02
105.833	0.00	0.00	0.001	O	|	|	|	|	0.02
105.917	0.00	0.00	0.001	O	|	|	|	|	0.02
106.000	0.00	0.00	0.001	O	|	|	|	|	0.02

**********HYDROGRAPH DATA**********

Number of intervals = 1272
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.045 (CFS)
Total volume = 0.324 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2018
Study date: 08/07/22

Iris and Oliver
Post Development
100 yr
24 hr

Program License Serial Number 6481

********** HYDROGRAPH INFORMATION **********

From study/file name: iris24100.rte

**********HYDROGRAPH DATA**********

Number of intervals = 296
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.987 (CFS)
Total volume = 0.573 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++++++++++

Process from Point/Station 0.000 to Point/Station 0.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 296
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.024	0.045	0.024	0.024
4.500	0.164	0.045	0.164	0.164
8.500	0.326	0.045	0.326	0.326
9.000	0.339	0.045	0.339	0.339
9.250	0.348	0.550	0.346	0.350
9.500	0.349	1.440	0.344	0.354
10.000	0.350	1.440	0.345	0.355

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.2 0.49 0.74 0.99	Depth (Ft.)
0.083	0.01	0.00	0.000	O	0.00
0.167	0.04	0.00	0.000	OI	0.01
0.250	0.05	0.00	0.000	OI	0.02
0.333	0.05	0.00	0.001	OI	0.03
0.417	0.07	0.00	0.001	O I	0.05
0.500	0.08	0.00	0.002	O I	0.07
0.583	0.08	0.00	0.002	O I	0.09
0.667	0.08	0.01	0.003	O I	0.11
0.750	0.08	0.01	0.003	O I	0.13
0.833	0.09	0.01	0.004	O I	0.16
0.917	0.10	0.01	0.004	O I	0.18
1.000	0.10	0.01	0.005	O I	0.21
1.083	0.10	0.01	0.006	O I	0.24
1.167	0.09	0.01	0.006	O I	0.26
1.250	0.09	0.01	0.007	O I	0.28
1.333	0.08	0.01	0.007	O I	0.30
1.417	0.08	0.01	0.008	O I	0.32
1.500	0.08	0.02	0.008	O I	0.34
1.583	0.08	0.02	0.009	O I	0.36
1.667	0.08	0.02	0.009	O I	0.38
1.750	0.08	0.02	0.010	O I	0.40
1.833	0.09	0.02	0.010	O I	0.42
1.917	0.10	0.02	0.011	O I	0.44
2.000	0.10	0.02	0.011	O I	0.46
2.083	0.11	0.02	0.012	O I	0.49
2.167	0.11	0.02	0.012	O I	0.51
2.250	0.11	0.02	0.013	O I	0.54
2.333	0.11	0.03	0.013	O I	0.56

2.417	0.11	0.03	0.014	O I	|	|	|	0.58
2.500	0.11	0.03	0.015	O I	|	|	|	0.61
2.583	0.11	0.03	0.015	O I	|	|	|	0.63
2.667	0.13	0.03	0.016	O I	|	|	|	0.66
2.750	0.13	0.03	0.016	|O I	|	|	|	0.69
2.833	0.13	0.03	0.017	|O I	|	|	|	0.72
2.917	0.14	0.03	0.018	|O I	|	|	|	0.75
3.000	0.14	0.03	0.019	|O I	|	|	|	0.77
3.083	0.14	0.04	0.019	|O I	|	|	|	0.80
3.167	0.14	0.04	0.020	|O I	|	|	|	0.83
3.250	0.14	0.04	0.021	|O I	|	|	|	0.86
3.333	0.14	0.04	0.021	|O I	|	|	|	0.89
3.417	0.14	0.04	0.022	|O I	|	|	|	0.92
3.500	0.14	0.04	0.023	|O I	|	|	|	0.94
3.583	0.14	0.04	0.023	|O I	|	|	|	0.97
3.667	0.14	0.04	0.024	|O I	|	|	|	1.00
3.750	0.14	0.04	0.025	|O I	|	|	|	1.01
3.833	0.14	0.04	0.025	|O I	|	|	|	1.03
3.917	0.16	0.04	0.026	|O I	|	|	|	1.05
4.000	0.16	0.04	0.027	|O I	|	|	|	1.07
4.083	0.16	0.04	0.028	|O I	|	|	|	1.09
4.167	0.16	0.04	0.028	|O I	|	|	|	1.11
4.250	0.16	0.04	0.029	|O I	|	|	|	1.13
4.333	0.17	0.04	0.030	|O I	|	|	|	1.15
4.417	0.18	0.04	0.031	|O I	|	|	|	1.17
4.500	0.19	0.04	0.032	|O I	|	|	|	1.20
4.583	0.19	0.04	0.033	|O I	|	|	|	1.22
4.667	0.19	0.04	0.034	|O I	|	|	|	1.25
4.750	0.19	0.04	0.035	|O I	|	|	|	1.27
4.833	0.20	0.04	0.036	|O I	|	|	|	1.30
4.917	0.21	0.04	0.037	|O I	|	|	|	1.32
5.000	0.21	0.04	0.038	|O I	|	|	|	1.35
5.083	0.21	0.04	0.039	|O I	|	|	|	1.38
5.167	0.18	0.04	0.040	|O I	|	|	|	1.41
5.250	0.17	0.04	0.041	|O I	|	|	|	1.43
5.333	0.17	0.04	0.042	|O I	|	|	|	1.45
5.417	0.19	0.04	0.043	|O I	|	|	|	1.47
5.500	0.19	0.04	0.044	|O I	|	|	|	1.50
5.583	0.20	0.04	0.045	|O I	|	|	|	1.52
5.667	0.21	0.04	0.046	|O I	|	|	|	1.55
5.750	0.21	0.04	0.047	|O I	|	|	|	1.58
5.833	0.22	0.04	0.048	|O I|	|	|	|	1.61
5.917	0.22	0.04	0.050	|O I|	|	|	|	1.64
6.000	0.22	0.04	0.051	|O I|	|	|	|	1.67
6.083	0.22	0.04	0.052	|O I|	|	|	|	1.70
6.167	0.24	0.04	0.053	|O I|	|	|	|	1.73
6.250	0.24	0.04	0.055	|O I|	|	|	|	1.76
6.333	0.24	0.04	0.056	|O I|	|	|	|	1.80
6.417	0.25	0.04	0.057	|O I|	|	|	|	1.83
6.500	0.25	0.04	0.059	|O I|	|	|	|	1.87

6.583	0.25	0.04	0.060	O	I			1.90
6.667	0.26	0.04	0.062	O	I			1.94
6.750	0.27	0.04	0.063	O	I			1.98
6.833	0.27	0.04	0.065	O	I			2.02
6.917	0.27	0.04	0.066	O	I			2.06
7.000	0.27	0.04	0.068	O	I			2.09
7.083	0.27	0.04	0.069	O	I			2.13
7.167	0.27	0.04	0.071	O	I			2.17
7.250	0.27	0.04	0.073	O	I			2.21
7.333	0.28	0.04	0.074	O	I			2.25
7.417	0.29	0.04	0.076	O	I			2.29
7.500	0.30	0.04	0.077	O	I			2.34
7.583	0.30	0.04	0.079	O	I			2.38
7.667	0.32	0.04	0.081	O	I			2.43
7.750	0.32	0.04	0.083	O	I			2.47
7.833	0.33	0.04	0.085	O	I			2.52
7.917	0.35	0.04	0.087	O	I			2.57
8.000	0.35	0.04	0.089	O	I			2.63
8.083	0.36	0.04	0.091	O	I			2.68
8.167	0.39	0.04	0.093	O	I			2.74
8.250	0.40	0.04	0.096	O	I			2.80
8.333	0.41	0.04	0.098	O	I			2.86
8.417	0.41	0.04	0.101	O	I			2.92
8.500	0.41	0.04	0.103	O	I			2.98
8.583	0.42	0.04	0.106	O	I			3.05
8.667	0.43	0.04	0.108	O	I			3.11
8.750	0.43	0.04	0.111	O	I			3.18
8.833	0.44	0.04	0.114	O	I			3.25
8.917	0.46	0.04	0.117	O	I			3.32
9.000	0.46	0.04	0.119	O	I			3.39
9.083	0.47	0.04	0.122	O	I			3.46
9.167	0.50	0.04	0.125	O	I			3.54
9.250	0.51	0.04	0.129	O	I			3.61
9.333	0.52	0.04	0.132	O	I			3.70
9.417	0.54	0.04	0.135	O	I			3.78
9.500	0.54	0.04	0.139	O	I			3.86
9.583	0.55	0.04	0.142	O	I			3.95
9.667	0.56	0.04	0.146	O	I			4.04
9.750	0.57	0.04	0.149	O	I			4.13
9.833	0.58	0.04	0.153	O	I			4.22
9.917	0.59	0.04	0.156	O	I			4.31
10.000	0.60	0.04	0.160	O	I			4.41
10.083	0.57	0.04	0.164	O	I			4.50
10.167	0.47	0.04	0.167	O	I			4.58
10.250	0.44	0.04	0.170	O	I			4.65
10.333	0.43	0.04	0.173	O	I			4.72
10.417	0.42	0.04	0.175	O	I			4.78
10.500	0.42	0.04	0.178	O	I			4.85
10.583	0.44	0.04	0.181	O	I			4.91
10.667	0.50	0.04	0.184	O	I			4.98

```
10.750    0.52    0.04      0.187  |O      |       I       |       |     5.06
10.833    0.53    0.04      0.190  |O      |       |I      |       |     5.15
10.917    0.54    0.04      0.194  |O      |       |I      |       |     5.23
11.000    0.54    0.04      0.197  |O      |       |I      |       |     5.31
11.083    0.54    0.04      0.200  |O      |       |I      |       |     5.40
11.167    0.53    0.04      0.204  |O      |       |I      |       |     5.48
11.250    0.53    0.04      0.207  |O      |       |I      |       |     5.56
11.333    0.52    0.04      0.210  |O      |       I       |       |     5.65
11.417    0.52    0.04      0.214  |O      |       I       |       |     5.73
11.500    0.52    0.04      0.217  |O      |       I       |       |     5.81
11.583    0.51    0.04      0.220  |O      |       I       |       |     5.89
11.667    0.49    0.04      0.223  |O      |      I|       |       |     5.97
11.750    0.48    0.04      0.226  |O      |      I|       |       |     6.04
11.833    0.48    0.04      0.229  |O      |      I|       |       |     6.11
11.917    0.49    0.04      0.232  |O      |      I|       |       |     6.19
12.000    0.49    0.04      0.235  |O      |      I|       |       |     6.26
12.083    0.53    0.04      0.239  |O      |       |I      |       |     6.34
12.167    0.62    0.04      0.242  |O      |       |   I   |       |     6.43
12.250    0.65    0.04      0.246  |O      |       |    I  |       |     6.53
12.333    0.67    0.04      0.251  |O      |       |    I  |       |     6.64
12.417    0.69    0.04      0.255  |O      |       |     I |       |     6.75
12.500    0.70    0.04      0.259  |O      |       |     I |       |     6.86
12.583    0.72    0.04      0.264  |O      |       |      I|       |     6.97
12.667    0.76    0.04      0.269  |O      |       |       I       |     7.09
12.750    0.77    0.04      0.274  |O      |       |       |I      |     7.21
12.833    0.79    0.04      0.279  |O      |       |       |I      |     7.34
12.917    0.80    0.04      0.284  |O      |       |       | I     |     7.46
13.000    0.81    0.04      0.289  |O      |       |       | I     |     7.59
13.083    0.85    0.04      0.295  |O      |       |       |  I    |     7.73
13.167    0.93    0.04      0.301  |O      |       |       |     I |     7.87
13.250    0.96    0.04      0.307  |O      |       |       |      I|     8.02
13.333    0.97    0.04      0.313  |O      |       |       |      I|     8.18
13.417    0.98    0.04      0.319  |O      |       |       |      I|     8.34
13.500    0.99    0.04      0.326  |O      |       |       |       I     8.50
13.583    0.93    0.04      0.332  |O      |       |       |    I  |     8.74
13.667    0.75    0.04      0.338  |O      |       |       I       |     8.95
13.750    0.70    0.20      0.342  |     O |       |     I |       |     9.08
13.833    0.67    0.36      0.345  |       |  O    |    I  |       |     9.16
13.917    0.65    0.46      0.346  |       |    O  |    I  |       |     9.20
14.000    0.64    0.52      0.347  |       |      O|   I   |       |     9.23
14.083    0.66    0.61      0.348  |       |       |  O I  |       |     9.27
14.167    0.72    0.73      0.348  |       |       |     O|       |     9.30
14.250    0.74    0.73      0.348  |       |       |     OI       |     9.30
14.333    0.75    0.75      0.348  |       |       |      O       |     9.31
14.417    0.74    0.74      0.348  |       |       |     O|       |     9.30
14.500    0.74    0.74      0.348  |       |       |     O|       |     9.30
14.583    0.74    0.74      0.348  |       |       |     O|       |     9.30
14.667    0.74    0.74      0.348  |       |       |     O|       |     9.30
14.750    0.74    0.74      0.348  |       |       |     O|       |     9.30
14.833    0.73    0.73      0.348  |       |       |     O|       |     9.30
```

14.917	0.72	0.72	0.348	|	|	| O|	|	9.30
15.000	0.71	0.71	0.348	|	|	| O|	|	9.30
15.083	0.70	0.71	0.348	|	|	| O |	|	9.29
15.167	0.69	0.69	0.348	|	|	| O |	|	9.29
15.250	0.68	0.68	0.348	|	|	| O |	|	9.29
15.333	0.67	0.67	0.348	|	|	| O |	|	9.28
15.417	0.66	0.66	0.348	|	|	| O |	|	9.28
15.500	0.65	0.65	0.348	|	|	| O |	|	9.28
15.583	0.62	0.63	0.348	|	|	| O |	|	9.27
15.667	0.56	0.58	0.348	|	|	| O |	|	9.26
15.750	0.54	0.55	0.348	|	|	|O |	|	9.25
15.833	0.53	0.55	0.348	|	|	|O |	|	9.25
15.917	0.53	0.54	0.348	|	|	|O |	|	9.25
16.000	0.53	0.54	0.348	|	|	|O |	|	9.24
16.083	0.45	0.52	0.347	|	| I O |	|	9.24
16.167	0.25	0.47	0.346	|	I O|	|	|	9.21
16.250	0.18	0.39	0.345	| I | O |	|	|	9.17
16.333	0.15	0.31	0.344	| I | O |	|	|	9.13
16.417	0.14	0.26	0.343	| I O |	|	|	9.11
16.500	0.12	0.22	0.342	| I O|	|	|	9.09
16.583	0.11	0.19	0.342	| I O |	|	|	9.07
16.667	0.09	0.16	0.341	| I O |	|	|	9.06
16.750	0.09	0.14	0.341	| I O |	|	|	9.05
16.833	0.09	0.12	0.340	| IO |	|	|	9.04
16.917	0.08	0.11	0.340	| IO |	|	|	9.03
17.000	0.08	0.10	0.340	| IO |	|	|	9.03
17.083	0.09	0.10	0.340	| O |	|	|	9.03
17.167	0.12	0.10	0.340	| O |	|	|	9.03
17.250	0.13	0.11	0.340	| OI |	|	|	9.03
17.333	0.13	0.11	0.340	| OI |	|	|	9.03
17.417	0.13	0.12	0.340	| OI |	|	|	9.04
17.500	0.14	0.12	0.340	| O |	|	|	9.04
17.583	0.14	0.13	0.340	| O |	|	|	9.04
17.667	0.14	0.13	0.341	| O |	|	|	9.04
17.750	0.14	0.13	0.341	| O |	|	|	9.04
17.833	0.13	0.13	0.341	| O |	|	|	9.04
17.917	0.12	0.13	0.341	| IO |	|	|	9.04
18.000	0.11	0.13	0.340	| IO |	|	|	9.04
18.083	0.11	0.12	0.340	| O |	|	|	9.04
18.167	0.11	0.12	0.340	| O |	|	|	9.04
18.250	0.11	0.12	0.340	| O |	|	|	9.04
18.333	0.11	0.11	0.340	| O |	|	|	9.03
18.417	0.11	0.11	0.340	| O |	|	|	9.03
18.500	0.11	0.11	0.340	| O |	|	|	9.03
18.583	0.10	0.11	0.340	| O |	|	|	9.03
18.667	0.09	0.11	0.340	| IO |	|	|	9.03
18.750	0.09	0.10	0.340	| IO |	|	|	9.03
18.833	0.08	0.10	0.340	| IO |	|	|	9.02
18.917	0.07	0.09	0.340	| O |	|	|	9.02
19.000	0.06	0.08	0.340	|IO |	|	|	9.02

19.083	0.06	0.07	0.340	O				9.01
19.167	0.07	0.07	0.339	O				9.01
19.250	0.08	0.07	0.340	O				9.01
19.333	0.08	0.08	0.340	O				9.02
19.417	0.10	0.08	0.340	OI				9.02
19.500	0.10	0.09	0.340	OI				9.02
19.583	0.10	0.09	0.340	O				9.02
19.667	0.09	0.09	0.340	IO				9.02
19.750	0.09	0.09	0.340	O				9.02
19.833	0.08	0.09	0.340	O				9.02
19.917	0.07	0.08	0.340	O				9.02
20.000	0.06	0.08	0.340	IO				9.02
20.083	0.06	0.07	0.339	O				9.01
20.167	0.07	0.07	0.339	O				9.01
20.250	0.08	0.07	0.339	O				9.01
20.333	0.08	0.07	0.340	O				9.01
20.417	0.08	0.08	0.340	O				9.02
20.500	0.08	0.08	0.340	O				9.02
20.583	0.08	0.08	0.340	O				9.02
20.667	0.08	0.08	0.340	O				9.02
20.750	0.08	0.08	0.340	O				9.02
20.833	0.08	0.08	0.340	O				9.02
20.917	0.06	0.08	0.340	O				9.02
21.000	0.06	0.07	0.339	IO				9.01
21.083	0.06	0.07	0.339	O				9.01
21.167	0.07	0.07	0.339	O				9.01
21.250	0.08	0.07	0.339	O				9.01
21.333	0.08	0.07	0.339	O				9.01
21.417	0.06	0.07	0.339	O				9.01
21.500	0.06	0.07	0.339	IO				9.01
21.583	0.06	0.07	0.339	O				9.01
21.667	0.07	0.07	0.339	O				9.01
21.750	0.08	0.07	0.339	O				9.01
21.833	0.08	0.07	0.339	O				9.01
21.917	0.06	0.07	0.339	O				9.01
22.000	0.06	0.07	0.339	IO				9.01
22.083	0.06	0.07	0.339	O				9.01
22.167	0.07	0.07	0.339	O				9.01
22.250	0.08	0.07	0.339	O				9.01
22.333	0.08	0.07	0.339	O				9.01
22.417	0.06	0.07	0.339	O				9.01
22.500	0.06	0.07	0.339	IO				9.01
22.583	0.06	0.06	0.339	IO				9.01
22.667	0.06	0.06	0.339	IO				9.01
22.750	0.06	0.06	0.339	O				9.01
22.833	0.06	0.06	0.339	O				9.01
22.917	0.06	0.06	0.339	O				9.01
23.000	0.05	0.06	0.339	O				9.01
23.083	0.05	0.06	0.339	O				9.01
23.167	0.05	0.06	0.339	O				9.01

23.250	0.05	0.06	0.339	|O	|	|	|	9.01
23.333	0.05	0.06	0.339	|O	|	|	|	9.01
23.417	0.05	0.06	0.339	|O	|	|	|	9.01
23.500	0.05	0.06	0.339	|O	|	|	|	9.00
23.583	0.05	0.05	0.339	|O	|	|	|	9.00
23.667	0.05	0.05	0.339	|O	|	|	|	9.00
23.750	0.05	0.05	0.339	|O	|	|	|	9.00
23.833	0.05	0.05	0.339	|O	|	|	|	9.00
23.917	0.05	0.05	0.339	|O	|	|	|	9.00
24.000	0.05	0.05	0.339	|O	|	|	|	9.00
24.083	0.05	0.05	0.339	|O	|	|	|	9.00
24.167	0.02	0.05	0.339	IO	|	|	|	9.00
24.250	0.01	0.04	0.339	IO	|	|	|	8.99
24.333	0.01	0.04	0.339	IO	|	|	|	8.98
24.417	0.00	0.04	0.338	IO	|	|	|	8.97
24.500	0.00	0.04	0.338	IO	|	|	|	8.96
24.583	0.00	0.04	0.338	IO	|	|	|	8.95
24.667	0.00	0.04	0.337	IO	|	|	|	8.94
24.750	0.00	0.04	0.337	IO	|	|	|	8.93
24.833	0.00	0.04	0.337	IO	|	|	|	8.91
24.917	0.00	0.04	0.336	IO	|	|	|	8.90
25.000	0.00	0.04	0.336	IO	|	|	|	8.89
25.083	0.00	0.04	0.336	IO	|	|	|	8.88
25.167	0.00	0.04	0.336	IO	|	|	|	8.87
25.250	0.00	0.04	0.335	IO	|	|	|	8.85
25.333	0.00	0.04	0.335	IO	|	|	|	8.84
25.417	0.00	0.04	0.335	IO	|	|	|	8.83
25.500	0.00	0.04	0.334	IO	|	|	|	8.82
25.583	0.00	0.04	0.334	IO	|	|	|	8.81
25.667	0.00	0.04	0.334	IO	|	|	|	8.79
25.750	0.00	0.04	0.333	IO	|	|	|	8.78
25.833	0.00	0.04	0.333	IO	|	|	|	8.77
25.917	0.00	0.04	0.333	IO	|	|	|	8.76
26.000	0.00	0.04	0.332	IO	|	|	|	8.75
26.083	0.00	0.04	0.332	IO	|	|	|	8.73
26.167	0.00	0.04	0.332	IO	|	|	|	8.72
26.250	0.00	0.04	0.331	IO	|	|	|	8.71
26.333	0.00	0.04	0.331	IO	|	|	|	8.70
26.417	0.00	0.04	0.331	IO	|	|	|	8.69
26.500	0.00	0.04	0.331	IO	|	|	|	8.68
26.583	0.00	0.04	0.330	IO	|	|	|	8.66
26.667	0.00	0.04	0.330	IO	|	|	|	8.65
26.750	0.00	0.04	0.330	IO	|	|	|	8.64
26.833	0.00	0.04	0.329	IO	|	|	|	8.63
26.917	0.00	0.04	0.329	IO	|	|	|	8.62
27.000	0.00	0.04	0.329	IO	|	|	|	8.60
27.083	0.00	0.04	0.328	IO	|	|	|	8.59
27.167	0.00	0.04	0.328	IO	|	|	|	8.58
27.250	0.00	0.04	0.328	IO	|	|	|	8.57
27.333	0.00	0.04	0.327	IO	|	|	|	8.56

27.417	0.00	0.04	0.327	IO				8.54
27.500	0.00	0.04	0.327	IO				8.53
27.583	0.00	0.04	0.327	IO				8.52
27.667	0.00	0.04	0.326	IO				8.51
27.750	0.00	0.04	0.326	IO				8.50
27.833	0.00	0.04	0.326	IO				8.49
27.917	0.00	0.04	0.325	IO				8.48
28.000	0.00	0.04	0.325	IO				8.47
28.083	0.00	0.04	0.325	IO				8.47
28.167	0.00	0.04	0.324	IO				8.46
28.250	0.00	0.04	0.324	IO				8.45
28.333	0.00	0.04	0.324	IO				8.44
28.417	0.00	0.04	0.323	IO				8.44
28.500	0.00	0.04	0.323	IO				8.43
28.583	0.00	0.04	0.323	IO				8.42
28.667	0.00	0.04	0.323	IO				8.41
28.750	0.00	0.04	0.322	IO				8.41
28.833	0.00	0.04	0.322	IO				8.40
28.917	0.00	0.04	0.322	IO				8.39
29.000	0.00	0.04	0.321	IO				8.38
29.083	0.00	0.04	0.321	IO				8.38
29.167	0.00	0.04	0.321	IO				8.37
29.250	0.00	0.04	0.320	IO				8.36
29.333	0.00	0.04	0.320	IO				8.35
29.417	0.00	0.04	0.320	IO				8.34
29.500	0.00	0.04	0.319	IO				8.34
29.583	0.00	0.04	0.319	IO				8.33
29.667	0.00	0.04	0.319	IO				8.32
29.750	0.00	0.04	0.318	IO				8.31
29.833	0.00	0.04	0.318	IO				8.31
29.917	0.00	0.04	0.318	IO				8.30
30.000	0.00	0.04	0.318	IO				8.29
30.083	0.00	0.04	0.317	IO				8.28
30.167	0.00	0.04	0.317	IO				8.28
30.250	0.00	0.04	0.317	IO				8.27
30.333	0.00	0.04	0.316	IO				8.26
30.417	0.00	0.04	0.316	IO				8.25
30.500	0.00	0.04	0.316	IO				8.25
30.583	0.00	0.04	0.315	IO				8.24
30.667	0.00	0.04	0.315	IO				8.23
30.750	0.00	0.04	0.315	IO				8.22
30.833	0.00	0.04	0.314	IO				8.21
30.917	0.00	0.04	0.314	IO				8.21
31.000	0.00	0.04	0.314	IO				8.20
31.083	0.00	0.04	0.314	IO				8.19
31.167	0.00	0.04	0.313	IO				8.18
31.250	0.00	0.04	0.313	IO				8.18
31.333	0.00	0.04	0.313	IO				8.17
31.417	0.00	0.04	0.312	IO				8.16
31.500	0.00	0.04	0.312	IO				8.15

31.583	0.00	0.04	0.312	IO				8.15
31.667	0.00	0.04	0.311	IO				8.14
31.750	0.00	0.04	0.311	IO				8.13
31.833	0.00	0.04	0.311	IO				8.12
31.917	0.00	0.04	0.310	IO				8.12
32.000	0.00	0.04	0.310	IO				8.11
32.083	0.00	0.04	0.310	IO				8.10
32.167	0.00	0.04	0.309	IO				8.09
32.250	0.00	0.04	0.309	IO				8.08
32.333	0.00	0.04	0.309	IO				8.08
32.417	0.00	0.04	0.309	IO				8.07
32.500	0.00	0.04	0.308	IO				8.06
32.583	0.00	0.04	0.308	IO				8.05
32.667	0.00	0.04	0.308	IO				8.05
32.750	0.00	0.04	0.307	IO				8.04
32.833	0.00	0.04	0.307	IO				8.03
32.917	0.00	0.04	0.307	IO				8.02
33.000	0.00	0.04	0.306	IO				8.02
33.083	0.00	0.04	0.306	IO				8.01
33.167	0.00	0.04	0.306	IO				8.00
33.250	0.00	0.04	0.305	IO				7.99
33.333	0.00	0.04	0.305	IO				7.99
33.417	0.00	0.04	0.305	IO				7.98
33.500	0.00	0.04	0.305	IO				7.97
33.583	0.00	0.04	0.304	IO				7.96
33.667	0.00	0.04	0.304	IO				7.95
33.750	0.00	0.04	0.304	IO				7.95
33.833	0.00	0.04	0.303	IO				7.94
33.917	0.00	0.04	0.303	IO				7.93
34.000	0.00	0.04	0.303	IO				7.92
34.083	0.00	0.04	0.302	IO				7.92
34.167	0.00	0.04	0.302	IO				7.91
34.250	0.00	0.04	0.302	IO				7.90
34.333	0.00	0.04	0.301	IO				7.89
34.417	0.00	0.04	0.301	IO				7.89
34.500	0.00	0.04	0.301	IO				7.88
34.583	0.00	0.04	0.300	IO				7.87
34.667	0.00	0.04	0.300	IO				7.86
34.750	0.00	0.04	0.300	IO				7.86
34.833	0.00	0.04	0.300	IO				7.85
34.917	0.00	0.04	0.299	IO				7.84
35.000	0.00	0.04	0.299	IO				7.83
35.083	0.00	0.04	0.299	IO				7.82
35.167	0.00	0.04	0.298	IO				7.82
35.250	0.00	0.04	0.298	IO				7.81
35.333	0.00	0.04	0.298	IO				7.80
35.417	0.00	0.04	0.297	IO				7.79
35.500	0.00	0.04	0.297	IO				7.79
35.583	0.00	0.04	0.297	IO				7.78
35.667	0.00	0.04	0.296	IO				7.77

35.750	0.00	0.04	0.296	IO				7.76
35.833	0.00	0.04	0.296	IO				7.76
35.917	0.00	0.04	0.296	IO				7.75
36.000	0.00	0.04	0.295	IO				7.74
36.083	0.00	0.04	0.295	IO				7.73
36.167	0.00	0.04	0.295	IO				7.72
36.250	0.00	0.04	0.294	IO				7.72
36.333	0.00	0.04	0.294	IO				7.71
36.417	0.00	0.04	0.294	IO				7.70
36.500	0.00	0.04	0.293	IO				7.69
36.583	0.00	0.04	0.293	IO				7.69
36.667	0.00	0.04	0.293	IO				7.68
36.750	0.00	0.04	0.292	IO				7.67
36.833	0.00	0.04	0.292	IO				7.66
36.917	0.00	0.04	0.292	IO				7.66
37.000	0.00	0.04	0.292	IO				7.65
37.083	0.00	0.04	0.291	IO				7.64
37.167	0.00	0.04	0.291	IO				7.63
37.250	0.00	0.04	0.291	IO				7.63
37.333	0.00	0.04	0.290	IO				7.62
37.417	0.00	0.04	0.290	IO				7.61
37.500	0.00	0.04	0.290	IO				7.60
37.583	0.00	0.04	0.289	IO				7.59
37.667	0.00	0.04	0.289	IO				7.59
37.750	0.00	0.04	0.289	IO				7.58
37.833	0.00	0.04	0.288	IO				7.57
37.917	0.00	0.04	0.288	IO				7.56
38.000	0.00	0.04	0.288	IO				7.56
38.083	0.00	0.04	0.287	IO				7.55
38.167	0.00	0.04	0.287	IO				7.54
38.250	0.00	0.04	0.287	IO				7.53
38.333	0.00	0.04	0.287	IO				7.53
38.417	0.00	0.04	0.286	IO				7.52
38.500	0.00	0.04	0.286	IO				7.51
38.583	0.00	0.04	0.286	IO				7.50
38.667	0.00	0.04	0.285	IO				7.50
38.750	0.00	0.04	0.285	IO				7.49
38.833	0.00	0.04	0.285	IO				7.48
38.917	0.00	0.04	0.284	IO				7.47
39.000	0.00	0.04	0.284	IO				7.46
39.083	0.00	0.04	0.284	IO				7.46
39.167	0.00	0.04	0.283	IO				7.45
39.250	0.00	0.04	0.283	IO				7.44
39.333	0.00	0.04	0.283	IO				7.43
39.417	0.00	0.04	0.283	IO				7.43
39.500	0.00	0.04	0.282	IO				7.42
39.583	0.00	0.04	0.282	IO				7.41
39.667	0.00	0.04	0.282	IO				7.40
39.750	0.00	0.04	0.281	IO				7.40
39.833	0.00	0.04	0.281	IO				7.39

39.917	0.00	0.04	0.281	IO				7.38
40.000	0.00	0.04	0.280	IO				7.37
40.083	0.00	0.04	0.280	IO				7.37
40.167	0.00	0.04	0.280	IO				7.36
40.250	0.00	0.04	0.279	IO				7.35
40.333	0.00	0.04	0.279	IO				7.34
40.417	0.00	0.04	0.279	IO				7.33
40.500	0.00	0.04	0.278	IO				7.33
40.583	0.00	0.04	0.278	IO				7.32
40.667	0.00	0.04	0.278	IO				7.31
40.750	0.00	0.04	0.278	IO				7.30
40.833	0.00	0.04	0.277	IO				7.30
40.917	0.00	0.04	0.277	IO				7.29
41.000	0.00	0.04	0.277	IO				7.28
41.083	0.00	0.04	0.276	IO				7.27
41.167	0.00	0.04	0.276	IO				7.27
41.250	0.00	0.04	0.276	IO				7.26
41.333	0.00	0.04	0.275	IO				7.25
41.417	0.00	0.04	0.275	IO				7.24
41.500	0.00	0.04	0.275	IO				7.24
41.583	0.00	0.04	0.274	IO				7.23
41.667	0.00	0.04	0.274	IO				7.22
41.750	0.00	0.04	0.274	IO				7.21
41.833	0.00	0.04	0.274	IO				7.20
41.917	0.00	0.04	0.273	IO				7.20
42.000	0.00	0.04	0.273	IO				7.19
42.083	0.00	0.04	0.273	IO				7.18
42.167	0.00	0.04	0.272	IO				7.17
42.250	0.00	0.04	0.272	IO				7.17
42.333	0.00	0.04	0.272	IO				7.16
42.417	0.00	0.04	0.271	IO				7.15
42.500	0.00	0.04	0.271	IO				7.14
42.583	0.00	0.04	0.271	IO				7.14
42.667	0.00	0.04	0.270	IO				7.13
42.750	0.00	0.04	0.270	IO				7.12
42.833	0.00	0.04	0.270	IO				7.11
42.917	0.00	0.04	0.270	IO				7.11
43.000	0.00	0.04	0.269	IO				7.10
43.083	0.00	0.04	0.269	IO				7.09
43.167	0.00	0.04	0.269	IO				7.08
43.250	0.00	0.04	0.268	IO				7.07
43.333	0.00	0.04	0.268	IO				7.07
43.417	0.00	0.04	0.268	IO				7.06
43.500	0.00	0.04	0.267	IO				7.05
43.583	0.00	0.04	0.267	IO				7.04
43.667	0.00	0.04	0.267	IO				7.04
43.750	0.00	0.04	0.266	IO				7.03
43.833	0.00	0.04	0.266	IO				7.02
43.917	0.00	0.04	0.266	IO				7.01
44.000	0.00	0.04	0.265	IO				7.01

44.083	0.00	0.04	0.265	IO				7.00
44.167	0.00	0.04	0.265	IO				6.99
44.250	0.00	0.04	0.265	IO				6.98
44.333	0.00	0.04	0.264	IO				6.98
44.417	0.00	0.04	0.264	IO				6.97
44.500	0.00	0.04	0.264	IO				6.96
44.583	0.00	0.04	0.263	IO				6.95
44.667	0.00	0.04	0.263	IO				6.94
44.750	0.00	0.04	0.263	IO				6.94
44.833	0.00	0.04	0.262	IO				6.93
44.917	0.00	0.04	0.262	IO				6.92
45.000	0.00	0.04	0.262	IO				6.91
45.083	0.00	0.04	0.261	IO				6.91
45.167	0.00	0.04	0.261	IO				6.90
45.250	0.00	0.04	0.261	IO				6.89
45.333	0.00	0.04	0.261	IO				6.88
45.417	0.00	0.04	0.260	IO				6.88
45.500	0.00	0.04	0.260	IO				6.87
45.583	0.00	0.04	0.260	IO				6.86
45.667	0.00	0.04	0.259	IO				6.85
45.750	0.00	0.04	0.259	IO				6.84
45.833	0.00	0.04	0.259	IO				6.84
45.917	0.00	0.04	0.258	IO				6.83
46.000	0.00	0.04	0.258	IO				6.82
46.083	0.00	0.04	0.258	IO				6.81
46.167	0.00	0.04	0.257	IO				6.81
46.250	0.00	0.04	0.257	IO				6.80
46.333	0.00	0.04	0.257	IO				6.79
46.417	0.00	0.04	0.256	IO				6.78
46.500	0.00	0.04	0.256	IO				6.78
46.583	0.00	0.04	0.256	IO				6.77
46.667	0.00	0.04	0.256	IO				6.76
46.750	0.00	0.04	0.255	IO				6.75
46.833	0.00	0.04	0.255	IO				6.75
46.917	0.00	0.04	0.255	IO				6.74
47.000	0.00	0.04	0.254	IO				6.73
47.083	0.00	0.04	0.254	IO				6.72
47.167	0.00	0.04	0.254	IO				6.71
47.250	0.00	0.04	0.253	IO				6.71
47.333	0.00	0.04	0.253	IO				6.70
47.417	0.00	0.04	0.253	IO				6.69
47.500	0.00	0.04	0.252	IO				6.68
47.583	0.00	0.04	0.252	IO				6.68
47.667	0.00	0.04	0.252	IO				6.67
47.750	0.00	0.04	0.252	IO				6.66
47.833	0.00	0.04	0.251	IO				6.65
47.917	0.00	0.04	0.251	IO				6.65
48.000	0.00	0.04	0.251	IO				6.64
48.083	0.00	0.04	0.250	IO				6.63
48.167	0.00	0.04	0.250	IO				6.62

48.250	0.00	0.04	0.250	IO				6.62
48.333	0.00	0.04	0.249	IO				6.61
48.417	0.00	0.04	0.249	IO				6.60
48.500	0.00	0.04	0.249	IO				6.59
48.583	0.00	0.04	0.248	IO				6.58
48.667	0.00	0.04	0.248	IO				6.58
48.750	0.00	0.04	0.248	IO				6.57
48.833	0.00	0.04	0.248	IO				6.56
48.917	0.00	0.04	0.247	IO				6.55
49.000	0.00	0.04	0.247	IO				6.55
49.083	0.00	0.04	0.247	IO				6.54
49.167	0.00	0.04	0.246	IO				6.53
49.250	0.00	0.04	0.246	IO				6.52
49.333	0.00	0.04	0.246	IO				6.52
49.417	0.00	0.04	0.245	IO				6.51
49.500	0.00	0.04	0.245	IO				6.50
49.583	0.00	0.04	0.245	IO				6.49
49.667	0.00	0.04	0.244	IO				6.49
49.750	0.00	0.04	0.244	IO				6.48
49.833	0.00	0.04	0.244	IO				6.47
49.917	0.00	0.04	0.243	IO				6.46
50.000	0.00	0.04	0.243	IO				6.45
50.083	0.00	0.04	0.243	IO				6.45
50.167	0.00	0.04	0.243	IO				6.44
50.250	0.00	0.04	0.242	IO				6.43
50.333	0.00	0.04	0.242	IO				6.42
50.417	0.00	0.04	0.242	IO				6.42
50.500	0.00	0.04	0.241	IO				6.41
50.583	0.00	0.04	0.241	IO				6.40
50.667	0.00	0.04	0.241	IO				6.39
50.750	0.00	0.04	0.240	IO				6.39
50.833	0.00	0.04	0.240	IO				6.38
50.917	0.00	0.04	0.240	IO				6.37
51.000	0.00	0.04	0.239	IO				6.36
51.083	0.00	0.04	0.239	IO				6.36
51.167	0.00	0.04	0.239	IO				6.35
51.250	0.00	0.04	0.239	IO				6.34
51.333	0.00	0.04	0.238	IO				6.33
51.417	0.00	0.04	0.238	IO				6.32
51.500	0.00	0.04	0.238	IO				6.32
51.583	0.00	0.04	0.237	IO				6.31
51.667	0.00	0.04	0.237	IO				6.30
51.750	0.00	0.04	0.237	IO				6.29
51.833	0.00	0.04	0.236	IO				6.29
51.917	0.00	0.04	0.236	IO				6.28
52.000	0.00	0.04	0.236	IO				6.27
52.083	0.00	0.04	0.235	IO				6.26
52.167	0.00	0.04	0.235	IO				6.26
52.250	0.00	0.04	0.235	IO				6.25
52.333	0.00	0.04	0.234	IO				6.24

52.417	0.00	0.04	0.234	IO				6.23
52.500	0.00	0.04	0.234	IO				6.23
52.583	0.00	0.04	0.234	IO				6.22
52.667	0.00	0.04	0.233	IO				6.21
52.750	0.00	0.04	0.233	IO				6.20
52.833	0.00	0.04	0.233	IO				6.19
52.917	0.00	0.04	0.232	IO				6.19
53.000	0.00	0.04	0.232	IO				6.18
53.083	0.00	0.04	0.232	IO				6.17
53.167	0.00	0.04	0.231	IO				6.16
53.250	0.00	0.04	0.231	IO				6.16
53.333	0.00	0.04	0.231	IO				6.15
53.417	0.00	0.04	0.230	IO				6.14
53.500	0.00	0.04	0.230	IO				6.13
53.583	0.00	0.04	0.230	IO				6.13
53.667	0.00	0.04	0.230	IO				6.12
53.750	0.00	0.04	0.229	IO				6.11
53.833	0.00	0.04	0.229	IO				6.10
53.917	0.00	0.04	0.229	IO				6.10
54.000	0.00	0.04	0.228	IO				6.09
54.083	0.00	0.04	0.228	IO				6.08
54.167	0.00	0.04	0.228	IO				6.07
54.250	0.00	0.04	0.227	IO				6.06
54.333	0.00	0.04	0.227	IO				6.06
54.417	0.00	0.04	0.227	IO				6.05
54.500	0.00	0.04	0.226	IO				6.04
54.583	0.00	0.04	0.226	IO				6.03
54.667	0.00	0.04	0.226	IO				6.03
54.750	0.00	0.04	0.225	IO				6.02
54.833	0.00	0.04	0.225	IO				6.01
54.917	0.00	0.04	0.225	IO				6.00
55.000	0.00	0.04	0.225	IO				6.00
55.083	0.00	0.04	0.224	IO				5.99
55.167	0.00	0.04	0.224	IO				5.98
55.250	0.00	0.04	0.224	IO				5.97
55.333	0.00	0.04	0.223	IO				5.96
55.417	0.00	0.04	0.223	IO				5.96
55.500	0.00	0.04	0.223	IO				5.95
55.583	0.00	0.04	0.222	IO				5.94
55.667	0.00	0.04	0.222	IO				5.93
55.750	0.00	0.04	0.222	IO				5.93
55.833	0.00	0.04	0.221	IO				5.92
55.917	0.00	0.04	0.221	IO				5.91
56.000	0.00	0.04	0.221	IO				5.90
56.083	0.00	0.04	0.221	IO				5.90
56.167	0.00	0.04	0.220	IO				5.89
56.250	0.00	0.04	0.220	IO				5.88
56.333	0.00	0.04	0.220	IO				5.87
56.417	0.00	0.04	0.219	IO				5.87
56.500	0.00	0.04	0.219	IO				5.86

56.583	0.00	0.04	0.219	IO				5.85
56.667	0.00	0.04	0.218	IO				5.84
56.750	0.00	0.04	0.218	IO				5.83
56.833	0.00	0.04	0.218	IO				5.83
56.917	0.00	0.04	0.217	IO				5.82
57.000	0.00	0.04	0.217	IO				5.81
57.083	0.00	0.04	0.217	IO				5.80
57.167	0.00	0.04	0.217	IO				5.80
57.250	0.00	0.04	0.216	IO				5.79
57.333	0.00	0.04	0.216	IO				5.78
57.417	0.00	0.04	0.216	IO				5.77
57.500	0.00	0.04	0.215	IO				5.77
57.583	0.00	0.04	0.215	IO				5.76
57.667	0.00	0.04	0.215	IO				5.75
57.750	0.00	0.04	0.214	IO				5.74
57.833	0.00	0.04	0.214	IO				5.74
57.917	0.00	0.04	0.214	IO				5.73
58.000	0.00	0.04	0.213	IO				5.72
58.083	0.00	0.04	0.213	IO				5.71
58.167	0.00	0.04	0.213	IO				5.70
58.250	0.00	0.04	0.212	IO				5.70
58.333	0.00	0.04	0.212	IO				5.69
58.417	0.00	0.04	0.212	IO				5.68
58.500	0.00	0.04	0.212	IO				5.67
58.583	0.00	0.04	0.211	IO				5.67
58.667	0.00	0.04	0.211	IO				5.66
58.750	0.00	0.04	0.211	IO				5.65
58.833	0.00	0.04	0.210	IO				5.64
58.917	0.00	0.04	0.210	IO				5.64
59.000	0.00	0.04	0.210	IO				5.63
59.083	0.00	0.04	0.209	IO				5.62
59.167	0.00	0.04	0.209	IO				5.61
59.250	0.00	0.04	0.209	IO				5.61
59.333	0.00	0.04	0.208	IO				5.60
59.417	0.00	0.04	0.208	IO				5.59
59.500	0.00	0.04	0.208	IO				5.58
59.583	0.00	0.04	0.208	IO				5.57
59.667	0.00	0.04	0.207	IO				5.57
59.750	0.00	0.04	0.207	IO				5.56
59.833	0.00	0.04	0.207	IO				5.55
59.917	0.00	0.04	0.206	IO				5.54
60.000	0.00	0.04	0.206	IO				5.54
60.083	0.00	0.04	0.206	IO				5.53
60.167	0.00	0.04	0.205	IO				5.52
60.250	0.00	0.04	0.205	IO				5.51
60.333	0.00	0.04	0.205	IO				5.51
60.417	0.00	0.04	0.204	IO				5.50
60.500	0.00	0.04	0.204	IO				5.49
60.583	0.00	0.04	0.204	IO				5.48
60.667	0.00	0.04	0.203	IO				5.48

60.750	0.00	0.04	0.203	IO				5.47
60.833	0.00	0.04	0.203	IO				5.46
60.917	0.00	0.04	0.203	IO				5.45
61.000	0.00	0.04	0.202	IO				5.44
61.083	0.00	0.04	0.202	IO				5.44
61.167	0.00	0.04	0.202	IO				5.43
61.250	0.00	0.04	0.201	IO				5.42
61.333	0.00	0.04	0.201	IO				5.41
61.417	0.00	0.04	0.201	IO				5.41
61.500	0.00	0.04	0.200	IO				5.40
61.583	0.00	0.04	0.200	IO				5.39
61.667	0.00	0.04	0.200	IO				5.38
61.750	0.00	0.04	0.199	IO				5.38
61.833	0.00	0.04	0.199	IO				5.37
61.917	0.00	0.04	0.199	IO				5.36
62.000	0.00	0.04	0.199	IO				5.35
62.083	0.00	0.04	0.198	IO				5.35
62.167	0.00	0.04	0.198	IO				5.34
62.250	0.00	0.04	0.198	IO				5.33
62.333	0.00	0.04	0.197	IO				5.32
62.417	0.00	0.04	0.197	IO				5.31
62.500	0.00	0.04	0.197	IO				5.31
62.583	0.00	0.04	0.196	IO				5.30
62.667	0.00	0.04	0.196	IO				5.29
62.750	0.00	0.04	0.196	IO				5.28
62.833	0.00	0.04	0.195	IO				5.28
62.917	0.00	0.04	0.195	IO				5.27
63.000	0.00	0.04	0.195	IO				5.26
63.083	0.00	0.04	0.195	IO				5.25
63.167	0.00	0.04	0.194	IO				5.25
63.250	0.00	0.04	0.194	IO				5.24
63.333	0.00	0.04	0.194	IO				5.23
63.417	0.00	0.04	0.193	IO				5.22
63.500	0.00	0.04	0.193	IO				5.21
63.583	0.00	0.04	0.193	IO				5.21
63.667	0.00	0.04	0.192	IO				5.20
63.750	0.00	0.04	0.192	IO				5.19
63.833	0.00	0.04	0.192	IO				5.18
63.917	0.00	0.04	0.191	IO				5.18
64.000	0.00	0.04	0.191	IO				5.17
64.083	0.00	0.04	0.191	IO				5.16
64.167	0.00	0.04	0.190	IO				5.15
64.250	0.00	0.04	0.190	IO				5.15
64.333	0.00	0.04	0.190	IO				5.14
64.417	0.00	0.04	0.190	IO				5.13
64.500	0.00	0.04	0.189	IO				5.12
64.583	0.00	0.04	0.189	IO				5.12
64.667	0.00	0.04	0.189	IO				5.11
64.750	0.00	0.04	0.188	IO				5.10
64.833	0.00	0.04	0.188	IO				5.09

64.917	0.00	0.04	0.188	IO				5.08
65.000	0.00	0.04	0.187	IO				5.08
65.083	0.00	0.04	0.187	IO				5.07
65.167	0.00	0.04	0.187	IO				5.06
65.250	0.00	0.04	0.186	IO				5.05
65.333	0.00	0.04	0.186	IO				5.05
65.417	0.00	0.04	0.186	IO				5.04
65.500	0.00	0.04	0.186	IO				5.03
65.583	0.00	0.04	0.185	IO				5.02
65.667	0.00	0.04	0.185	IO				5.02
65.750	0.00	0.04	0.185	IO				5.01
65.833	0.00	0.04	0.184	IO				5.00
65.917	0.00	0.04	0.184	IO				4.99
66.000	0.00	0.04	0.184	IO				4.99
66.083	0.00	0.04	0.183	IO				4.98
66.167	0.00	0.04	0.183	IO				4.97
66.250	0.00	0.04	0.183	IO				4.96
66.333	0.00	0.04	0.182	IO				4.95
66.417	0.00	0.04	0.182	IO				4.95
66.500	0.00	0.04	0.182	IO				4.94
66.583	0.00	0.04	0.181	IO				4.93
66.667	0.00	0.04	0.181	IO				4.92
66.750	0.00	0.04	0.181	IO				4.92
66.833	0.00	0.04	0.181	IO				4.91
66.917	0.00	0.04	0.180	IO				4.90
67.000	0.00	0.04	0.180	IO				4.89
67.083	0.00	0.04	0.180	IO				4.89
67.167	0.00	0.04	0.179	IO				4.88
67.250	0.00	0.04	0.179	IO				4.87
67.333	0.00	0.04	0.179	IO				4.86
67.417	0.00	0.04	0.178	IO				4.86
67.500	0.00	0.04	0.178	IO				4.85
67.583	0.00	0.04	0.178	IO				4.84
67.667	0.00	0.04	0.177	IO				4.83
67.750	0.00	0.04	0.177	IO				4.82
67.833	0.00	0.04	0.177	IO				4.82
67.917	0.00	0.04	0.177	IO				4.81
68.000	0.00	0.04	0.176	IO				4.80
68.083	0.00	0.04	0.176	IO				4.79
68.167	0.00	0.04	0.176	IO				4.79
68.250	0.00	0.04	0.175	IO				4.78
68.333	0.00	0.04	0.175	IO				4.77
68.417	0.00	0.04	0.175	IO				4.76
68.500	0.00	0.04	0.174	IO				4.76
68.583	0.00	0.04	0.174	IO				4.75
68.667	0.00	0.04	0.174	IO				4.74
68.750	0.00	0.04	0.173	IO				4.73
68.833	0.00	0.04	0.173	IO				4.73
68.917	0.00	0.04	0.173	IO				4.72
69.000	0.00	0.04	0.173	IO				4.71

69.083	0.00	0.04	0.172	IO				4.70
69.167	0.00	0.04	0.172	IO				4.69
69.250	0.00	0.04	0.172	IO				4.69
69.333	0.00	0.04	0.171	IO				4.68
69.417	0.00	0.04	0.171	IO				4.67
69.500	0.00	0.04	0.171	IO				4.66
69.583	0.00	0.04	0.170	IO				4.66
69.667	0.00	0.04	0.170	IO				4.65
69.750	0.00	0.04	0.170	IO				4.64
69.833	0.00	0.04	0.169	IO				4.63
69.917	0.00	0.04	0.169	IO				4.63
70.000	0.00	0.04	0.169	IO				4.62
70.083	0.00	0.04	0.168	IO				4.61
70.167	0.00	0.04	0.168	IO				4.60
70.250	0.00	0.04	0.168	IO				4.60
70.333	0.00	0.04	0.168	IO				4.59
70.417	0.00	0.04	0.167	IO				4.58
70.500	0.00	0.04	0.167	IO				4.57
70.583	0.00	0.04	0.167	IO				4.56
70.667	0.00	0.04	0.166	IO				4.56
70.750	0.00	0.04	0.166	IO				4.55
70.833	0.00	0.04	0.166	IO				4.54
70.917	0.00	0.04	0.165	IO				4.53
71.000	0.00	0.04	0.165	IO				4.53
71.083	0.00	0.04	0.165	IO				4.52
71.167	0.00	0.04	0.164	IO				4.51
71.250	0.00	0.04	0.164	IO				4.50
71.333	0.00	0.04	0.164	IO				4.50
71.417	0.00	0.04	0.164	IO				4.49
71.500	0.00	0.04	0.163	IO				4.48
71.583	0.00	0.04	0.163	IO				4.47
71.667	0.00	0.04	0.163	IO				4.46
71.750	0.00	0.04	0.162	IO				4.46
71.833	0.00	0.04	0.162	IO				4.45
71.917	0.00	0.04	0.162	IO				4.44
72.000	0.00	0.04	0.161	IO				4.43
72.083	0.00	0.04	0.161	IO				4.43
72.167	0.00	0.04	0.161	IO				4.42
72.250	0.00	0.04	0.160	IO				4.41
72.333	0.00	0.04	0.160	IO				4.40
72.417	0.00	0.04	0.160	IO				4.39
72.500	0.00	0.04	0.159	IO				4.39
72.583	0.00	0.04	0.159	IO				4.38
72.667	0.00	0.04	0.159	IO				4.37
72.750	0.00	0.04	0.159	IO				4.36
72.833	0.00	0.04	0.158	IO				4.36
72.917	0.00	0.04	0.158	IO				4.35
73.000	0.00	0.04	0.158	IO				4.34
73.083	0.00	0.04	0.157	IO				4.33
73.167	0.00	0.04	0.157	IO				4.33

73.250	0.00	0.04	0.157	IO				4.32
73.333	0.00	0.04	0.156	IO				4.31
73.417	0.00	0.04	0.156	IO				4.30
73.500	0.00	0.04	0.156	IO				4.29
73.583	0.00	0.04	0.155	IO				4.29
73.667	0.00	0.04	0.155	IO				4.28
73.750	0.00	0.04	0.155	IO				4.27
73.833	0.00	0.04	0.155	IO				4.26
73.917	0.00	0.04	0.154	IO				4.26
74.000	0.00	0.04	0.154	IO				4.25
74.083	0.00	0.04	0.154	IO				4.24
74.167	0.00	0.04	0.153	IO				4.23
74.250	0.00	0.04	0.153	IO				4.22
74.333	0.00	0.04	0.153	IO				4.22
74.417	0.00	0.04	0.152	IO				4.21
74.500	0.00	0.04	0.152	IO				4.20
74.583	0.00	0.04	0.152	IO				4.19
74.667	0.00	0.04	0.151	IO				4.19
74.750	0.00	0.04	0.151	IO				4.18
74.833	0.00	0.04	0.151	IO				4.17
74.917	0.00	0.04	0.150	IO				4.16
75.000	0.00	0.04	0.150	IO				4.15
75.083	0.00	0.04	0.150	IO				4.15
75.167	0.00	0.04	0.150	IO				4.14
75.250	0.00	0.04	0.149	IO				4.13
75.333	0.00	0.04	0.149	IO				4.12
75.417	0.00	0.04	0.149	IO				4.12
75.500	0.00	0.04	0.148	IO				4.11
75.583	0.00	0.04	0.148	IO				4.10
75.667	0.00	0.04	0.148	IO				4.09
75.750	0.00	0.04	0.147	IO				4.08
75.833	0.00	0.04	0.147	IO				4.08
75.917	0.00	0.04	0.147	IO				4.07
76.000	0.00	0.04	0.146	IO				4.06
76.083	0.00	0.04	0.146	IO				4.05
76.167	0.00	0.04	0.146	IO				4.05
76.250	0.00	0.04	0.146	IO				4.04
76.333	0.00	0.04	0.145	IO				4.03
76.417	0.00	0.04	0.145	IO				4.02
76.500	0.00	0.04	0.145	IO				4.02
76.583	0.00	0.04	0.144	IO				4.01
76.667	0.00	0.04	0.144	IO				4.00
76.750	0.00	0.04	0.144	IO				3.99
76.833	0.00	0.04	0.143	IO				3.98
76.917	0.00	0.04	0.143	IO				3.98
77.000	0.00	0.04	0.143	IO				3.97
77.083	0.00	0.04	0.142	IO				3.96
77.167	0.00	0.04	0.142	IO				3.95
77.250	0.00	0.04	0.142	IO				3.95
77.333	0.00	0.04	0.142	IO				3.94

77.417	0.00	0.04	0.141	IO				3.93
77.500	0.00	0.04	0.141	IO				3.92
77.583	0.00	0.04	0.141	IO				3.91
77.667	0.00	0.04	0.140	IO				3.91
77.750	0.00	0.04	0.140	IO				3.90
77.833	0.00	0.04	0.140	IO				3.89
77.917	0.00	0.04	0.139	IO				3.88
78.000	0.00	0.04	0.139	IO				3.88
78.083	0.00	0.04	0.139	IO				3.87
78.167	0.00	0.04	0.138	IO				3.86
78.250	0.00	0.04	0.138	IO				3.85
78.333	0.00	0.04	0.138	IO				3.84
78.417	0.00	0.04	0.137	IO				3.84
78.500	0.00	0.04	0.137	IO				3.83
78.583	0.00	0.04	0.137	IO				3.82
78.667	0.00	0.04	0.137	IO				3.81
78.750	0.00	0.04	0.136	IO				3.81
78.833	0.00	0.04	0.136	IO				3.80
78.917	0.00	0.04	0.136	IO				3.79
79.000	0.00	0.04	0.135	IO				3.78
79.083	0.00	0.04	0.135	IO				3.78
79.167	0.00	0.04	0.135	IO				3.77
79.250	0.00	0.04	0.134	IO				3.76
79.333	0.00	0.04	0.134	IO				3.75
79.417	0.00	0.04	0.134	IO				3.74
79.500	0.00	0.04	0.133	IO				3.74
79.583	0.00	0.04	0.133	IO				3.73
79.667	0.00	0.04	0.133	IO				3.72
79.750	0.00	0.04	0.133	IO				3.71
79.833	0.00	0.04	0.132	IO				3.71
79.917	0.00	0.04	0.132	IO				3.70
80.000	0.00	0.04	0.132	IO				3.69
80.083	0.00	0.04	0.131	IO				3.68
80.167	0.00	0.04	0.131	IO				3.67
80.250	0.00	0.04	0.131	IO				3.67
80.333	0.00	0.04	0.130	IO				3.66
80.417	0.00	0.04	0.130	IO				3.65
80.500	0.00	0.04	0.130	IO				3.64
80.583	0.00	0.04	0.129	IO				3.64
80.667	0.00	0.04	0.129	IO				3.63
80.750	0.00	0.04	0.129	IO				3.62
80.833	0.00	0.04	0.128	IO				3.61
80.917	0.00	0.04	0.128	IO				3.60
81.000	0.00	0.04	0.128	IO				3.60
81.083	0.00	0.04	0.128	IO				3.59
81.167	0.00	0.04	0.127	IO				3.58
81.250	0.00	0.04	0.127	IO				3.57
81.333	0.00	0.04	0.127	IO				3.57
81.417	0.00	0.04	0.126	IO				3.56
81.500	0.00	0.04	0.126	IO				3.55

81.583	0.00	0.04	0.126	IO				3.54
81.667	0.00	0.04	0.125	IO				3.53
81.750	0.00	0.04	0.125	IO				3.53
81.833	0.00	0.04	0.125	IO				3.52
81.917	0.00	0.04	0.124	IO				3.51
82.000	0.00	0.04	0.124	IO				3.50
82.083	0.00	0.04	0.124	IO				3.50
82.167	0.00	0.04	0.124	IO				3.49
82.250	0.00	0.04	0.123	IO				3.48
82.333	0.00	0.04	0.123	IO				3.47
82.417	0.00	0.04	0.123	IO				3.47
82.500	0.00	0.04	0.122	IO				3.46
82.583	0.00	0.04	0.122	IO				3.45
82.667	0.00	0.04	0.122	IO				3.44
82.750	0.00	0.04	0.121	IO				3.43
82.833	0.00	0.04	0.121	IO				3.43
82.917	0.00	0.04	0.121	IO				3.42
83.000	0.00	0.04	0.120	IO				3.41
83.083	0.00	0.04	0.120	IO				3.40
83.167	0.00	0.04	0.120	IO				3.40
83.250	0.00	0.04	0.120	IO				3.39
83.333	0.00	0.04	0.119	IO				3.38
83.417	0.00	0.04	0.119	IO				3.37
83.500	0.00	0.04	0.119	IO				3.36
83.583	0.00	0.04	0.118	IO				3.36
83.667	0.00	0.04	0.118	IO				3.35
83.750	0.00	0.04	0.118	IO				3.34
83.833	0.00	0.04	0.117	IO				3.33
83.917	0.00	0.04	0.117	IO				3.33
84.000	0.00	0.04	0.117	IO				3.32
84.083	0.00	0.04	0.116	IO				3.31
84.167	0.00	0.04	0.116	IO				3.30
84.250	0.00	0.04	0.116	IO				3.29
84.333	0.00	0.04	0.115	IO				3.29
84.417	0.00	0.04	0.115	IO				3.28
84.500	0.00	0.04	0.115	IO				3.27
84.583	0.00	0.04	0.115	IO				3.26
84.667	0.00	0.04	0.114	IO				3.26
84.750	0.00	0.04	0.114	IO				3.25
84.833	0.00	0.04	0.114	IO				3.24
84.917	0.00	0.04	0.113	IO				3.23
85.000	0.00	0.04	0.113	IO				3.22
85.083	0.00	0.04	0.113	IO				3.22
85.167	0.00	0.04	0.112	IO				3.21
85.250	0.00	0.04	0.112	IO				3.20
85.333	0.00	0.04	0.112	IO				3.19
85.417	0.00	0.04	0.111	IO				3.19
85.500	0.00	0.04	0.111	IO				3.18
85.583	0.00	0.04	0.111	IO				3.17
85.667	0.00	0.04	0.111	IO				3.16

85.750	0.00	0.04	0.110	IO				3.16
85.833	0.00	0.04	0.110	IO				3.15
85.917	0.00	0.04	0.110	IO				3.14
86.000	0.00	0.04	0.109	IO				3.13
86.083	0.00	0.04	0.109	IO				3.12
86.167	0.00	0.04	0.109	IO				3.12
86.250	0.00	0.04	0.108	IO				3.11
86.333	0.00	0.04	0.108	IO				3.10
86.417	0.00	0.04	0.108	IO				3.09
86.500	0.00	0.04	0.107	IO				3.09
86.583	0.00	0.04	0.107	IO				3.08
86.667	0.00	0.04	0.107	IO				3.07
86.750	0.00	0.04	0.106	IO				3.06
86.833	0.00	0.04	0.106	IO				3.05
86.917	0.00	0.04	0.106	IO				3.05
87.000	0.00	0.04	0.106	IO				3.04
87.083	0.00	0.04	0.105	IO				3.03
87.167	0.00	0.04	0.105	IO				3.02
87.250	0.00	0.04	0.105	IO				3.02
87.333	0.00	0.04	0.104	IO				3.01
87.417	0.00	0.04	0.104	IO				3.00
87.500	0.00	0.04	0.104	IO				2.99
87.583	0.00	0.04	0.103	IO				2.98
87.667	0.00	0.04	0.103	IO				2.98
87.750	0.00	0.04	0.103	IO				2.97
87.833	0.00	0.04	0.102	IO				2.96
87.917	0.00	0.04	0.102	IO				2.95
88.000	0.00	0.04	0.102	IO				2.95
88.083	0.00	0.04	0.102	IO				2.94
88.167	0.00	0.04	0.101	IO				2.93
88.250	0.00	0.04	0.101	IO				2.92
88.333	0.00	0.04	0.101	IO				2.92
88.417	0.00	0.04	0.100	IO				2.91
88.500	0.00	0.04	0.100	IO				2.90
88.583	0.00	0.04	0.100	IO				2.89
88.667	0.00	0.04	0.099	IO				2.88
88.750	0.00	0.04	0.099	IO				2.88
88.833	0.00	0.04	0.099	IO				2.87
88.917	0.00	0.04	0.098	IO				2.86
89.000	0.00	0.04	0.098	IO				2.85
89.083	0.00	0.04	0.098	IO				2.85
89.167	0.00	0.04	0.098	IO				2.84
89.250	0.00	0.04	0.097	IO				2.83
89.333	0.00	0.04	0.097	IO				2.82
89.417	0.00	0.04	0.097	IO				2.81
89.500	0.00	0.04	0.096	IO				2.81
89.583	0.00	0.04	0.096	IO				2.80
89.667	0.00	0.04	0.096	IO				2.79
89.750	0.00	0.04	0.095	IO				2.78
89.833	0.00	0.04	0.095	IO				2.78

89.917	0.00	0.04	0.095	IO				2.77
90.000	0.00	0.04	0.094	IO				2.76
90.083	0.00	0.04	0.094	IO				2.75
90.167	0.00	0.04	0.094	IO				2.74
90.250	0.00	0.04	0.093	IO				2.74
90.333	0.00	0.04	0.093	IO				2.73
90.417	0.00	0.04	0.093	IO				2.72
90.500	0.00	0.04	0.093	IO				2.71
90.583	0.00	0.04	0.092	IO				2.71
90.667	0.00	0.04	0.092	IO				2.70
90.750	0.00	0.04	0.092	IO				2.69
90.833	0.00	0.04	0.091	IO				2.68
90.917	0.00	0.04	0.091	IO				2.67
91.000	0.00	0.04	0.091	IO				2.67
91.083	0.00	0.04	0.090	IO				2.66
91.167	0.00	0.04	0.090	IO				2.65
91.250	0.00	0.04	0.090	IO				2.64
91.333	0.00	0.04	0.089	IO				2.64
91.417	0.00	0.04	0.089	IO				2.63
91.500	0.00	0.04	0.089	IO				2.62
91.583	0.00	0.04	0.089	IO				2.61
91.667	0.00	0.04	0.088	IO				2.61
91.750	0.00	0.04	0.088	IO				2.60
91.833	0.00	0.04	0.088	IO				2.59
91.917	0.00	0.04	0.087	IO				2.58
92.000	0.00	0.04	0.087	IO				2.57
92.083	0.00	0.04	0.087	IO				2.57
92.167	0.00	0.04	0.086	IO				2.56
92.250	0.00	0.04	0.086	IO				2.55
92.333	0.00	0.04	0.086	IO				2.54
92.417	0.00	0.04	0.085	IO				2.54
92.500	0.00	0.04	0.085	IO				2.53
92.583	0.00	0.04	0.085	IO				2.52
92.667	0.00	0.04	0.084	IO				2.51
92.750	0.00	0.04	0.084	IO				2.50
92.833	0.00	0.04	0.084	IO				2.50
92.917	0.00	0.04	0.084	IO				2.49
93.000	0.00	0.04	0.083	IO				2.48
93.083	0.00	0.04	0.083	IO				2.47
93.167	0.00	0.04	0.083	IO				2.47
93.250	0.00	0.04	0.082	IO				2.46
93.333	0.00	0.04	0.082	IO				2.45
93.417	0.00	0.04	0.082	IO				2.44
93.500	0.00	0.04	0.081	IO				2.43
93.583	0.00	0.04	0.081	IO				2.43
93.667	0.00	0.04	0.081	IO				2.42
93.750	0.00	0.04	0.080	IO				2.41
93.833	0.00	0.04	0.080	IO				2.40
93.917	0.00	0.04	0.080	IO				2.40
94.000	0.00	0.04	0.080	IO				2.39

94.083	0.00	0.04	0.079	IO				2.38
94.167	0.00	0.04	0.079	IO				2.37
94.250	0.00	0.04	0.079	IO				2.36
94.333	0.00	0.04	0.078	IO				2.36
94.417	0.00	0.04	0.078	IO				2.35
94.500	0.00	0.04	0.078	IO				2.34
94.583	0.00	0.04	0.077	IO				2.33
94.667	0.00	0.04	0.077	IO				2.33
94.750	0.00	0.04	0.077	IO				2.32
94.833	0.00	0.04	0.076	IO				2.31
94.917	0.00	0.04	0.076	IO				2.30
95.000	0.00	0.04	0.076	IO				2.30
95.083	0.00	0.04	0.075	IO				2.29
95.167	0.00	0.04	0.075	IO				2.28
95.250	0.00	0.04	0.075	IO				2.27
95.333	0.00	0.04	0.075	IO				2.26
95.417	0.00	0.04	0.074	IO				2.26
95.500	0.00	0.04	0.074	IO				2.25
95.583	0.00	0.04	0.074	IO				2.24
95.667	0.00	0.04	0.073	IO				2.23
95.750	0.00	0.04	0.073	IO				2.23
95.833	0.00	0.04	0.073	IO				2.22
95.917	0.00	0.04	0.072	IO				2.21
96.000	0.00	0.04	0.072	IO				2.20
96.083	0.00	0.04	0.072	IO				2.19
96.167	0.00	0.04	0.071	IO				2.19
96.250	0.00	0.04	0.071	IO				2.18
96.333	0.00	0.04	0.071	IO				2.17
96.417	0.00	0.04	0.071	IO				2.16
96.500	0.00	0.04	0.070	IO				2.16
96.583	0.00	0.04	0.070	IO				2.15
96.667	0.00	0.04	0.070	IO				2.14
96.750	0.00	0.04	0.069	IO				2.13
96.833	0.00	0.04	0.069	IO				2.12
96.917	0.00	0.04	0.069	IO				2.12
97.000	0.00	0.04	0.068	IO				2.11
97.083	0.00	0.04	0.068	IO				2.10
97.167	0.00	0.04	0.068	IO				2.09
97.250	0.00	0.04	0.067	IO				2.09
97.333	0.00	0.04	0.067	IO				2.08
97.417	0.00	0.04	0.067	IO				2.07
97.500	0.00	0.04	0.067	IO				2.06
97.583	0.00	0.04	0.066	IO				2.06
97.667	0.00	0.04	0.066	IO				2.05
97.750	0.00	0.04	0.066	IO				2.04
97.833	0.00	0.04	0.065	IO				2.03
97.917	0.00	0.04	0.065	IO				2.02
98.000	0.00	0.04	0.065	IO				2.02
98.083	0.00	0.04	0.064	IO				2.01
98.167	0.00	0.04	0.064	IO				2.00

98.250	0.00	0.04	0.064	IO				1.99
98.333	0.00	0.04	0.063	IO				1.99
98.417	0.00	0.04	0.063	IO				1.98
98.500	0.00	0.04	0.063	IO				1.97
98.583	0.00	0.04	0.062	IO				1.96
98.667	0.00	0.04	0.062	IO				1.95
98.750	0.00	0.04	0.062	IO				1.95
98.833	0.00	0.04	0.062	IO				1.94
98.917	0.00	0.04	0.061	IO				1.93
99.000	0.00	0.04	0.061	IO				1.92
99.083	0.00	0.04	0.061	IO				1.92
99.167	0.00	0.04	0.060	IO				1.91
99.250	0.00	0.04	0.060	IO				1.90
99.333	0.00	0.04	0.060	IO				1.89
99.417	0.00	0.04	0.059	IO				1.88
99.500	0.00	0.04	0.059	IO				1.88
99.583	0.00	0.04	0.059	IO				1.87
99.667	0.00	0.04	0.058	IO				1.86
99.750	0.00	0.04	0.058	IO				1.85
99.833	0.00	0.04	0.058	IO				1.85
99.917	0.00	0.04	0.058	IO				1.84
100.000	0.00	0.04	0.057	IO				1.83
100.083	0.00	0.04	0.057	IO				1.82
100.167	0.00	0.04	0.057	IO				1.81
100.250	0.00	0.04	0.056	IO				1.81
100.333	0.00	0.04	0.056	IO				1.80
100.417	0.00	0.04	0.056	IO				1.79
100.500	0.00	0.04	0.055	IO				1.78
100.583	0.00	0.04	0.055	IO				1.78
100.667	0.00	0.04	0.055	IO				1.77
100.750	0.00	0.04	0.054	IO				1.76
100.833	0.00	0.04	0.054	IO				1.75
100.917	0.00	0.04	0.054	IO				1.75
101.000	0.00	0.04	0.053	IO				1.74
101.083	0.00	0.04	0.053	IO				1.73
101.167	0.00	0.04	0.053	IO				1.72
101.250	0.00	0.04	0.053	IO				1.71
101.333	0.00	0.04	0.052	IO				1.71
101.417	0.00	0.04	0.052	IO				1.70
101.500	0.00	0.04	0.052	IO				1.69
101.583	0.00	0.04	0.051	IO				1.68
101.667	0.00	0.04	0.051	IO				1.68
101.750	0.00	0.04	0.051	IO				1.67
101.833	0.00	0.04	0.050	IO				1.66
101.917	0.00	0.04	0.050	IO				1.65
102.000	0.00	0.04	0.050	IO				1.64
102.083	0.00	0.04	0.049	IO				1.64
102.167	0.00	0.04	0.049	IO				1.63
102.250	0.00	0.04	0.049	IO				1.62
102.333	0.00	0.04	0.049	IO				1.61

102.417	0.00	0.04	0.048	IO				1.61
102.500	0.00	0.04	0.048	IO				1.60
102.583	0.00	0.04	0.048	IO				1.59
102.667	0.00	0.04	0.047	IO				1.58
102.750	0.00	0.04	0.047	IO				1.57
102.833	0.00	0.04	0.047	IO				1.57
102.917	0.00	0.04	0.046	IO				1.56
103.000	0.00	0.04	0.046	IO				1.55
103.083	0.00	0.04	0.046	IO				1.54
103.167	0.00	0.04	0.045	IO				1.54
103.250	0.00	0.04	0.045	IO				1.53
103.333	0.00	0.04	0.045	IO				1.52
103.417	0.00	0.04	0.045	IO				1.51
103.500	0.00	0.04	0.044	IO				1.50
103.583	0.00	0.04	0.044	IO				1.50
103.667	0.00	0.04	0.044	IO				1.49
103.750	0.00	0.04	0.043	IO				1.48
103.833	0.00	0.04	0.043	IO				1.47
103.917	0.00	0.04	0.043	IO				1.47
104.000	0.00	0.04	0.042	IO				1.46
104.083	0.00	0.04	0.042	IO				1.45
104.167	0.00	0.04	0.042	IO				1.44
104.250	0.00	0.04	0.041	IO				1.44
104.333	0.00	0.04	0.041	IO				1.43
104.417	0.00	0.04	0.041	IO				1.42
104.500	0.00	0.04	0.040	IO				1.41
104.583	0.00	0.04	0.040	IO				1.40
104.667	0.00	0.04	0.040	IO				1.40
104.750	0.00	0.04	0.040	IO				1.39
104.833	0.00	0.04	0.039	IO				1.38
104.917	0.00	0.04	0.039	IO				1.37
105.000	0.00	0.04	0.039	IO				1.37
105.083	0.00	0.04	0.038	IO				1.36
105.167	0.00	0.04	0.038	IO				1.35
105.250	0.00	0.04	0.038	IO				1.34
105.333	0.00	0.04	0.037	IO				1.33
105.417	0.00	0.04	0.037	IO				1.33
105.500	0.00	0.04	0.037	IO				1.32
105.583	0.00	0.04	0.036	IO				1.31
105.667	0.00	0.04	0.036	IO				1.30
105.750	0.00	0.04	0.036	IO				1.30
105.833	0.00	0.04	0.036	IO				1.29
105.917	0.00	0.04	0.035	IO				1.28
106.000	0.00	0.04	0.035	IO				1.27
106.083	0.00	0.04	0.035	IO				1.26
106.167	0.00	0.04	0.034	IO				1.26
106.250	0.00	0.04	0.034	IO				1.25
106.333	0.00	0.04	0.034	IO				1.24
106.417	0.00	0.04	0.033	IO				1.23
106.500	0.00	0.04	0.033	IO				1.23

106.583	0.00	0.04	0.033	IO				1.22
106.667	0.00	0.04	0.032	IO				1.21
106.750	0.00	0.04	0.032	IO				1.20
106.833	0.00	0.04	0.032	IO				1.20
106.917	0.00	0.04	0.031	IO				1.19
107.000	0.00	0.04	0.031	IO				1.18
107.083	0.00	0.04	0.031	IO				1.17
107.167	0.00	0.04	0.031	IO				1.16
107.250	0.00	0.04	0.030	IO				1.16
107.333	0.00	0.04	0.030	IO				1.15
107.417	0.00	0.04	0.030	IO				1.14
107.500	0.00	0.04	0.029	IO				1.13
107.583	0.00	0.04	0.029	IO				1.13
107.667	0.00	0.04	0.029	IO				1.12
107.750	0.00	0.04	0.028	IO				1.11
107.833	0.00	0.04	0.028	IO				1.10
107.917	0.00	0.04	0.028	IO				1.09
108.000	0.00	0.04	0.027	IO				1.09
108.083	0.00	0.04	0.027	IO				1.08
108.167	0.00	0.04	0.027	IO				1.07
108.250	0.00	0.04	0.027	IO				1.06
108.333	0.00	0.04	0.026	IO				1.06
108.417	0.00	0.04	0.026	IO				1.05
108.500	0.00	0.04	0.026	IO				1.04
108.583	0.00	0.04	0.025	IO				1.03
108.667	0.00	0.04	0.025	IO				1.02
108.750	0.00	0.04	0.025	IO				1.02
108.833	0.00	0.04	0.024	IO				1.01
108.917	0.00	0.04	0.024	IO				1.00
109.000	0.00	0.04	0.024	IO				0.99
109.083	0.00	0.04	0.023	IO				0.98
109.167	0.00	0.04	0.023	IO				0.96
109.250	0.00	0.04	0.023	IO				0.95
109.333	0.00	0.04	0.023	IO				0.94
109.417	0.00	0.04	0.022	IO				0.93
109.500	0.00	0.04	0.022	IO				0.92
109.583	0.00	0.04	0.022	IO				0.90
109.667	0.00	0.04	0.021	IO				0.89
109.750	0.00	0.04	0.021	IO				0.88
109.833	0.00	0.04	0.021	IO				0.87
109.917	0.00	0.04	0.021	IO				0.86
110.000	0.00	0.04	0.020	IO				0.85
110.083	0.00	0.04	0.020	IO				0.84
110.167	0.00	0.04	0.020	IO				0.83
110.250	0.00	0.04	0.020	IO				0.82
110.333	0.00	0.04	0.019	IO				0.80
110.417	0.00	0.04	0.019	IO				0.79
110.500	0.00	0.04	0.019	IO				0.78
110.583	0.00	0.03	0.019	IO				0.77
110.667	0.00	0.03	0.018	IO				0.76

110.750	0.00	0.03	0.018	IO				0.75
110.833	0.00	0.03	0.018	IO				0.74
110.917	0.00	0.03	0.018	IO				0.74
111.000	0.00	0.03	0.017	IO				0.73
111.083	0.00	0.03	0.017	IO				0.72
111.167	0.00	0.03	0.017	IO				0.71
111.250	0.00	0.03	0.017	IO				0.70
111.333	0.00	0.03	0.017	IO				0.69
111.417	0.00	0.03	0.016	O				0.68
111.500	0.00	0.03	0.016	O				0.67
111.583	0.00	0.03	0.016	O				0.66
111.667	0.00	0.03	0.016	O				0.65
111.750	0.00	0.03	0.016	O				0.65
111.833	0.00	0.03	0.015	O				0.64
111.917	0.00	0.03	0.015	O				0.63
112.000	0.00	0.03	0.015	O				0.62
112.083	0.00	0.03	0.015	O				0.61
112.167	0.00	0.03	0.015	O				0.61
112.250	0.00	0.03	0.014	O				0.60
112.333	0.00	0.03	0.014	O				0.59
112.417	0.00	0.03	0.014	O				0.58
112.500	0.00	0.03	0.014	O				0.58
112.583	0.00	0.03	0.014	O				0.57
112.667	0.00	0.03	0.013	O				0.56
112.750	0.00	0.02	0.013	O				0.55
112.833	0.00	0.02	0.013	O				0.55
112.917	0.00	0.02	0.013	O				0.54
113.000	0.00	0.02	0.013	O				0.53
113.083	0.00	0.02	0.013	O				0.53
113.167	0.00	0.02	0.012	O				0.52
113.250	0.00	0.02	0.012	O				0.51
113.333	0.00	0.02	0.012	O				0.51
113.417	0.00	0.02	0.012	O				0.50
113.500	0.00	0.02	0.012	O				0.49
113.583	0.00	0.02	0.012	O				0.49
113.667	0.00	0.02	0.012	O				0.48
113.750	0.00	0.02	0.011	O				0.47
113.833	0.00	0.02	0.011	O				0.47
113.917	0.00	0.02	0.011	O				0.46
114.000	0.00	0.02	0.011	O				0.46
114.083	0.00	0.02	0.011	O				0.45
114.167	0.00	0.02	0.011	O				0.44
114.250	0.00	0.02	0.011	O				0.44
114.333	0.00	0.02	0.010	O				0.43
114.417	0.00	0.02	0.010	O				0.43
114.500	0.00	0.02	0.010	O				0.42
114.583	0.00	0.02	0.010	O				0.42
114.667	0.00	0.02	0.010	O				0.41
114.750	0.00	0.02	0.010	O				0.41
114.833	0.00	0.02	0.010	O				0.40

114.917	0.00	0.02	0.009	O	|	|	|	0.40
115.000	0.00	0.02	0.009	O	|	|	|	0.39
115.083	0.00	0.02	0.009	O	|	|	|	0.39
115.167	0.00	0.02	0.009	O	|	|	|	0.38
115.250	0.00	0.02	0.009	O	|	|	|	0.38
115.333	0.00	0.02	0.009	O	|	|	|	0.37
115.417	0.00	0.02	0.009	O	|	|	|	0.37
115.500	0.00	0.02	0.009	O	|	|	|	0.36
115.583	0.00	0.02	0.009	O	|	|	|	0.36
115.667	0.00	0.02	0.008	O	|	|	|	0.35
115.750	0.00	0.02	0.008	O	|	|	|	0.35
115.833	0.00	0.02	0.008	O	|	|	|	0.34
115.917	0.00	0.02	0.008	O	|	|	|	0.34
116.000	0.00	0.02	0.008	O	|	|	|	0.33
116.083	0.00	0.01	0.008	O	|	|	|	0.33
116.167	0.00	0.01	0.008	O	|	|	|	0.33
116.250	0.00	0.01	0.008	O	|	|	|	0.32
116.333	0.00	0.01	0.008	O	|	|	|	0.32
116.417	0.00	0.01	0.008	O	|	|	|	0.31
116.500	0.00	0.01	0.007	O	|	|	|	0.31
116.583	0.00	0.01	0.007	O	|	|	|	0.31
116.667	0.00	0.01	0.007	O	|	|	|	0.30
116.750	0.00	0.01	0.007	O	|	|	|	0.30
116.833	0.00	0.01	0.007	O	|	|	|	0.29
116.917	0.00	0.01	0.007	O	|	|	|	0.29
117.000	0.00	0.01	0.007	O	|	|	|	0.29
117.083	0.00	0.01	0.007	O	|	|	|	0.28
117.167	0.00	0.01	0.007	O	|	|	|	0.28
117.250	0.00	0.01	0.007	O	|	|	|	0.28
117.333	0.00	0.01	0.007	O	|	|	|	0.27
117.417	0.00	0.01	0.006	O	|	|	|	0.27
117.500	0.00	0.01	0.006	O	|	|	|	0.27
117.583	0.00	0.01	0.006	O	|	|	|	0.26
117.667	0.00	0.01	0.006	O	|	|	|	0.26
117.750	0.00	0.01	0.006	O	|	|	|	0.25
117.833	0.00	0.01	0.006	O	|	|	|	0.25
117.917	0.00	0.01	0.006	O	|	|	|	0.25
118.000	0.00	0.01	0.006	O	|	|	|	0.25
118.083	0.00	0.01	0.006	O	|	|	|	0.24
118.167	0.00	0.01	0.006	O	|	|	|	0.24
118.250	0.00	0.01	0.006	O	|	|	|	0.24
118.333	0.00	0.01	0.006	O	|	|	|	0.23
118.417	0.00	0.01	0.006	O	|	|	|	0.23
118.500	0.00	0.01	0.005	O	|	|	|	0.23
118.583	0.00	0.01	0.005	O	|	|	|	0.22
118.667	0.00	0.01	0.005	O	|	|	|	0.22
118.750	0.00	0.01	0.005	O	|	|	|	0.22
118.833	0.00	0.01	0.005	O	|	|	|	0.22
118.917	0.00	0.01	0.005	O	|	|	|	0.21
119.000	0.00	0.01	0.005	O	|	|	|	0.21

119.083	0.00	0.01	0.005	O				0.21
119.167	0.00	0.01	0.005	O				0.20
119.250	0.00	0.01	0.005	O				0.20
119.333	0.00	0.01	0.005	O				0.20
119.417	0.00	0.01	0.005	O				0.20
119.500	0.00	0.01	0.005	O				0.19
119.583	0.00	0.01	0.005	O				0.19
119.667	0.00	0.01	0.005	O				0.19
119.750	0.00	0.01	0.004	O				0.19
119.833	0.00	0.01	0.004	O				0.18
119.917	0.00	0.01	0.004	O				0.18
120.000	0.00	0.01	0.004	O				0.18
120.083	0.00	0.01	0.004	O				0.18
120.167	0.00	0.01	0.004	O				0.18
120.250	0.00	0.01	0.004	O				0.17
120.333	0.00	0.01	0.004	O				0.17
120.417	0.00	0.01	0.004	O				0.17
120.500	0.00	0.01	0.004	O				0.17
120.583	0.00	0.01	0.004	O				0.16
120.667	0.00	0.01	0.004	O				0.16
120.750	0.00	0.01	0.004	O				0.16
120.833	0.00	0.01	0.004	O				0.16
120.917	0.00	0.01	0.004	O				0.16
121.000	0.00	0.01	0.004	O				0.15
121.083	0.00	0.01	0.004	O				0.15
121.167	0.00	0.01	0.004	O				0.15
121.250	0.00	0.01	0.004	O				0.15
121.333	0.00	0.01	0.004	O				0.15
121.417	0.00	0.01	0.003	O				0.14
121.500	0.00	0.01	0.003	O				0.14
121.583	0.00	0.01	0.003	O				0.14
121.667	0.00	0.01	0.003	O				0.14
121.750	0.00	0.01	0.003	O				0.14
121.833	0.00	0.01	0.003	O				0.14
121.917	0.00	0.01	0.003	O				0.13
122.000	0.00	0.01	0.003	O				0.13
122.083	0.00	0.01	0.003	O				0.13
122.167	0.00	0.01	0.003	O				0.13
122.250	0.00	0.01	0.003	O				0.13
122.333	0.00	0.01	0.003	O				0.13
122.417	0.00	0.01	0.003	O				0.12
122.500	0.00	0.01	0.003	O				0.12
122.583	0.00	0.01	0.003	O				0.12
122.667	0.00	0.01	0.003	O				0.12
122.750	0.00	0.01	0.003	O				0.12
122.833	0.00	0.01	0.003	O				0.12
122.917	0.00	0.01	0.003	O				0.11
123.000	0.00	0.01	0.003	O				0.11
123.083	0.00	0.01	0.003	O				0.11
123.167	0.00	0.00	0.003	O				0.11

123.250	0.00	0.00	0.003	O	|	|	|	0.11
123.333	0.00	0.00	0.003	O	|	|	|	0.11
123.417	0.00	0.00	0.003	O	|	|	|	0.11
123.500	0.00	0.00	0.003	O	|	|	|	0.10
123.583	0.00	0.00	0.002	O	|	|	|	0.10
123.667	0.00	0.00	0.002	O	|	|	|	0.10
123.750	0.00	0.00	0.002	O	|	|	|	0.10
123.833	0.00	0.00	0.002	O	|	|	|	0.10
123.917	0.00	0.00	0.002	O	|	|	|	0.10
124.000	0.00	0.00	0.002	O	|	|	|	0.10
124.083	0.00	0.00	0.002	O	|	|	|	0.10
124.167	0.00	0.00	0.002	O	|	|	|	0.09
124.250	0.00	0.00	0.002	O	|	|	|	0.09
124.333	0.00	0.00	0.002	O	|	|	|	0.09
124.417	0.00	0.00	0.002	O	|	|	|	0.09
124.500	0.00	0.00	0.002	O	|	|	|	0.09
124.583	0.00	0.00	0.002	O	|	|	|	0.09
124.667	0.00	0.00	0.002	O	|	|	|	0.09
124.750	0.00	0.00	0.002	O	|	|	|	0.09
124.833	0.00	0.00	0.002	O	|	|	|	0.09
124.917	0.00	0.00	0.002	O	|	|	|	0.08
125.000	0.00	0.00	0.002	O	|	|	|	0.08
125.083	0.00	0.00	0.002	O	|	|	|	0.08
125.167	0.00	0.00	0.002	O	|	|	|	0.08
125.250	0.00	0.00	0.002	O	|	|	|	0.08
125.333	0.00	0.00	0.002	O	|	|	|	0.08
125.417	0.00	0.00	0.002	O	|	|	|	0.08
125.500	0.00	0.00	0.002	O	|	|	|	0.08
125.583	0.00	0.00	0.002	O	|	|	|	0.08
125.667	0.00	0.00	0.002	O	|	|	|	0.07
125.750	0.00	0.00	0.002	O	|	|	|	0.07
125.833	0.00	0.00	0.002	O	|	|	|	0.07
125.917	0.00	0.00	0.002	O	|	|	|	0.07
126.000	0.00	0.00	0.002	O	|	|	|	0.07
126.083	0.00	0.00	0.002	O	|	|	|	0.07
126.167	0.00	0.00	0.002	O	|	|	|	0.07
126.250	0.00	0.00	0.002	O	|	|	|	0.07
126.333	0.00	0.00	0.002	O	|	|	|	0.07
126.417	0.00	0.00	0.002	O	|	|	|	0.07
126.500	0.00	0.00	0.002	O	|	|	|	0.07
126.583	0.00	0.00	0.002	O	|	|	|	0.06
126.667	0.00	0.00	0.002	O	|	|	|	0.06
126.750	0.00	0.00	0.002	O	|	|	|	0.06
126.833	0.00	0.00	0.001	O	|	|	|	0.06
126.917	0.00	0.00	0.001	O	|	|	|	0.06
127.000	0.00	0.00	0.001	O	|	|	|	0.06
127.083	0.00	0.00	0.001	O	|	|	|	0.06
127.167	0.00	0.00	0.001	O	|	|	|	0.06
127.250	0.00	0.00	0.001	O	|	|	|	0.06
127.333	0.00	0.00	0.001	O	|	|	|	0.06

127.417	0.00	0.00	0.001	O	|	|	|	0.06
127.500	0.00	0.00	0.001	O	|	|	|	0.06
127.583	0.00	0.00	0.001	O	|	|	|	0.06
127.667	0.00	0.00	0.001	O	|	|	|	0.05
127.750	0.00	0.00	0.001	O	|	|	|	0.05
127.833	0.00	0.00	0.001	O	|	|	|	0.05
127.917	0.00	0.00	0.001	O	|	|	|	0.05
128.000	0.00	0.00	0.001	O	|	|	|	0.05
128.083	0.00	0.00	0.001	O	|	|	|	0.05
128.167	0.00	0.00	0.001	O	|	|	|	0.05
128.250	0.00	0.00	0.001	O	|	|	|	0.05
128.333	0.00	0.00	0.001	O	|	|	|	0.05
128.417	0.00	0.00	0.001	O	|	|	|	0.05
128.500	0.00	0.00	0.001	O	|	|	|	0.05
128.583	0.00	0.00	0.001	O	|	|	|	0.05
128.667	0.00	0.00	0.001	O	|	|	|	0.05
128.750	0.00	0.00	0.001	O	|	|	|	0.05
128.833	0.00	0.00	0.001	O	|	|	|	0.05
128.917	0.00	0.00	0.001	O	|	|	|	0.05
129.000	0.00	0.00	0.001	O	|	|	|	0.04
129.083	0.00	0.00	0.001	O	|	|	|	0.04
129.167	0.00	0.00	0.001	O	|	|	|	0.04
129.250	0.00	0.00	0.001	O	|	|	|	0.04
129.333	0.00	0.00	0.001	O	|	|	|	0.04
129.417	0.00	0.00	0.001	O	|	|	|	0.04
129.500	0.00	0.00	0.001	O	|	|	|	0.04
129.583	0.00	0.00	0.001	O	|	|	|	0.04
129.667	0.00	0.00	0.001	O	|	|	|	0.04
129.750	0.00	0.00	0.001	O	|	|	|	0.04
129.833	0.00	0.00	0.001	O	|	|	|	0.04
129.917	0.00	0.00	0.001	O	|	|	|	0.04
130.000	0.00	0.00	0.001	O	|	|	|	0.04
130.083	0.00	0.00	0.001	O	|	|	|	0.04
130.167	0.00	0.00	0.001	O	|	|	|	0.04
130.250	0.00	0.00	0.001	O	|	|	|	0.04
130.333	0.00	0.00	0.001	O	|	|	|	0.04
130.417	0.00	0.00	0.001	O	|	|	|	0.04
130.500	0.00	0.00	0.001	O	|	|	|	0.04
130.583	0.00	0.00	0.001	O	|	|	|	0.03
130.667	0.00	0.00	0.001	O	|	|	|	0.03
130.750	0.00	0.00	0.001	O	|	|	|	0.03
130.833	0.00	0.00	0.001	O	|	|	|	0.03
130.917	0.00	0.00	0.001	O	|	|	|	0.03
131.000	0.00	0.00	0.001	O	|	|	|	0.03
131.083	0.00	0.00	0.001	O	|	|	|	0.03
131.167	0.00	0.00	0.001	O	|	|	|	0.03
131.250	0.00	0.00	0.001	O	|	|	|	0.03
131.333	0.00	0.00	0.001	O	|	|	|	0.03
131.417	0.00	0.00	0.001	O	|	|	|	0.03
131.500	0.00	0.00	0.001	O	|	|	|	0.03

131.583	0.00	0.00	0.001	O	|	|	|	|	0.03
131.667	0.00	0.00	0.001	O	|	|	|	|	0.03
131.750	0.00	0.00	0.001	O	|	|	|	|	0.03
131.833	0.00	0.00	0.001	O	|	|	|	|	0.03
131.917	0.00	0.00	0.001	O	|	|	|	|	0.03
132.000	0.00	0.00	0.001	O	|	|	|	|	0.03
132.083	0.00	0.00	0.001	O	|	|	|	|	0.03
132.167	0.00	0.00	0.001	O	|	|	|	|	0.03
132.250	0.00	0.00	0.001	O	|	|	|	|	0.03
132.333	0.00	0.00	0.001	O	|	|	|	|	0.03
132.417	0.00	0.00	0.001	O	|	|	|	|	0.03
132.500	0.00	0.00	0.001	O	|	|	|	|	0.03
132.583	0.00	0.00	0.001	O	|	|	|	|	0.03
132.667	0.00	0.00	0.001	O	|	|	|	|	0.03
132.750	0.00	0.00	0.001	O	|	|	|	|	0.02
132.833	0.00	0.00	0.001	O	|	|	|	|	0.02
132.917	0.00	0.00	0.001	O	|	|	|	|	0.02
133.000	0.00	0.00	0.001	O	|	|	|	|	0.02
133.083	0.00	0.00	0.001	O	|	|	|	|	0.02
133.167	0.00	0.00	0.001	O	|	|	|	|	0.02
133.250	0.00	0.00	0.001	O	|	|	|	|	0.02
133.333	0.00	0.00	0.001	O	|	|	|	|	0.02
133.417	0.00	0.00	0.001	O	|	|	|	|	0.02
133.500	0.00	0.00	0.001	O	|	|	|	|	0.02

**********HYDROGRAPH DATA**********

Number of intervals = 1602
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.751 (CFS)
Total volume = 0.572 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****